Airborne Sound Insulation in Multi-Family Buildings

By J.D. Quirt and T.R.T. Nightingale

This Update explains how an emphasis on system performance can achieve good sound insulation in multi-family buildings in a cost-effective manner. It reviews the concepts and terminology used to describe sound insulation for the complete building system, and presents research results that illustrate how typical wood-frame construction details can determine the sound insulation actually achieved.1

The traditional approach to designing for noise control (sound insulation) in North American multi-family wood-frame buildings usually fails to address important aspects of how sound is transmitted. Canadian and U.S. building codes2 have long considered only the Sound Transmission Class (STC) rating of the assembly separating adjacent dwellings—that is, the separating wall assembly when the units are side by side, or the floor/ceiling assembly when units are one above the other.

This approach does not ensure satisfactory sound insulation between units because it fails to consider flanking transmission, which is structure-borne sound transmission that bypasses the separating wall and travels through other building elements such as the floor, ceiling, or walls abutting the separating wall (also known as sidewalls).

Occupant satisfaction with the sound insulation between one's own unit and other adjacent units is determined by the combined performance of the separating wall or floor assemblies and all the elements coupled to those assemblies. Controlling flanking transmission requires the proper selection and design of the complete building system—i.e., all the structural elements, the fire blocks, the finishes, and the connections at the junctions of partition walls, floors and ceilings. In other words, it is the performance of the whole system and not just that of the separating assembly that will determine the sound insulation experienced by occupants.

Flanking transmission can result from both airborne and impact sources; however, this Update discusses only the transmission of airborne sound. A companion Update will address impact sound.
Flanking and Apparent Sound Transmission Class

When sound is produced, it causes all surfaces of the space to vibrate. Some of that vibration is transmitted across the floor, ceiling, and adjacent walls, and then through the floor/wall and wall/wall junctions to the corresponding surfaces of the adjacent room, where it is radiated as flanking sound (see Figure 2).

What is heard in the adjacent room is the combination of sound transmitted directly through the separating assembly plus the flanking sound transmitted via all other paths. The rating for this sound transmission via all paths, as experienced by the occupant, is called the Apparent Sound Transmission Class (ASTC). Like STC and FSTC (Field Sound Transmission Class), which are measures of the sound attenuation of the separating assembly only, ASTC is a single number rating defined in ASTM Standard E336.

The ASTC is usually lower than the STC or FSTC of the separating assembly, and for some combinations of assemblies it is much lower.

Controlling sound (vibrational acoustic energy) starts with choosing a good separating assembly, but ultimately depends on dealing with the sound energy transmitted by all paths.

The prevention of flanking transmission becomes even more important when higher levels of sound insulation are required.

Retrofitting to reduce flanking is a much more expensive option than addressing the issue in the original design.

Typical Wood-Frame Construction and Its Effects on Sound Transmission

The following section illustrates the effects of typical construction details on sound transmission. The discussion concentrates mainly on one set of base assemblies, but other more complex systems show comparable trends.

Side-by-Side Units

Floor joists parallel to separating walls

Figure 3 shows the wall with gypsum board screwed directly on to one side of the studs and mounted on resilient metal channels on the other side. Laboratory testing gives this wall assembly an STC of 52. The floor assembly has a bare oriented strandboard (OSB) floor surface, with the gypsum board ceiling mounted on resilient channels (STC 55 in laboratory testing).
In repeated tests with minor variations of the materials and in the floor/wall junction details, the overall sound insulation observed between the side-by-side rooms was ASTC 44 or 45. Measurements of the wall itself showed that its sound transmission in the complete building system is very similar to that of the laboratory results (STC 52) for a wall of the same construction. The difference between the wall performance and the system performance is due to flanking transmission via the floor assembly, which transmits far more sound than the separating wall assembly.

**Floor joists perpendicular to separating walls**

For the case shown in Figure 4, the measured ASTC was even lower than the ASTC observed when the joists were parallel to the separating wall (as illustrated in Figure 3). The problem here is not that the separating wall assembly is transmitting more sound than expected—it is performing as designed and built—but that most of the sound energy is able to circumvent the separating wall as structure-borne flanking transmission. Once again, the system ASTC is much lower than the STC of the separating assembly because flanking has not been properly considered in the design.

**Floor joists perpendicular to separating walls with added layer of gypsum board**

The systems illustrated in Figures 3 and 4 are likely to result in noise that most neighbouring occupants would find annoying. To remedy this, a builder’s first impulse would likely be to ‘fix’ the separating wall assembly by, for example, adding a second layer of gypsum board on the side with resilient channels (see Figure 5). Tables of acoustical ratings for wall assemblies (see Construction Technology Update No. 1) indicate that the added gypsum board should increase the STC for the wall assembly by about 5. In fact, detailed testing showed that the sound transmission directly through the wall was reduced (i.e., the STC increased) as expected, but the system performance was barely affected and only increased to ASTC 43 because the dominant sound transmission path (i.e., structure-borne flanking via the floor) was not dealt with. To address the problem, one must identify all the sound transmission paths and take appropriate measures to eliminate them.

**Floor joists perpendicular to separating walls with floor topping added**

Since the main problem with the constructions shown in Figures 3 to 5 is structure-borne flanking transmission via the floor surface, changing this surface is key to improving the system performance.
Adding a floor topping, such as a layer of concrete or simply a second layer of OSB, can significantly reduce flanking via the floor. Adding floor finishes, such as hardwood or laminate flooring over a resilient pad, can also reduce flanking transmission (see Figure 6). However, the improvement in the system ASTC rating depends not only on the materials added but also on the floor and junction details of the system to which they are added.

Flanking via the floor surface often dominates the sound transmission, especially when the floor surface is a single layer of OSB or plywood. When the paths involve the floor, there are several possible approaches:

- **Changing the orientation of the floor joists.** In general, floor framing that runs perpendicular to the separating wall transmits more flanking sound than framing that runs parallel, for both floor surfaces (as shown previously in Figures 3 and 4) and ceilings attached to the bottom of the framing (as discussed below).

- **Dealing with the flanking transmission via the floor/wall junction.** Reducing structural connections across the floor/wall junction reduces flanking; for example, there is more sound attenuation across the junction for a wall with a double row of studs (because of the gap between the two rows) than for a wall with a single row of studs (see Construction Technology Update No. 16).

- **Changing the materials installed on top of the subfloor.** This changes the transmission via the floor surfaces. A heavy floor topping, such as 38-mm concrete, provides much improved sound insulation. The addition of other toppings and flooring, including a combination of several different topping layers, can also help achieve reduced flanking.

Unfortunately, making improvements to the floor/floor path is not a complete solution, as other paths may also be significant. For example, once a better floor system has been put in place, sound transmission via other paths will become more obvious. At this point, there is greater benefit from improving other assemblies such as the separating wall, ceilings and sidewalls, which need to be considered as possible paths of sound transmission. The acoustical benefit of specific changes can be weighed and balanced against their cost to optimize the cost/benefit for the complete system.

**Designing for System Performance**

This section outlines the key issues that must be addressed in order to achieve design objectives based on system performance.

**Side-by-Side Units**

A systems design approach must take into account the transmitted sound energy due to direct transmission through the separating assembly along with that due to significant flanking paths.
For the gypsum board surfaces of walls and ceilings, typical approaches involve:

- **Attaching gypsum board on resilient channels.** This is an effective way to control flanking via these surfaces—the sound attenuation for the path increases by at least 10 dB. For the sidewall and ceiling paths illustrated in Figures 7 and 8, such an improvement can mean that flanking via these paths becomes insignificant. However, to achieve the full benefit of this approach, other flanking paths have to be dealt with as well.

- **Adding a second layer of directly attached gypsum board.** This improves flanking control only slightly—the sound attenuation of the path increases by only 1 or 2 dB.

Flanking via a sidewall transmits less sound than the other paths previously discussed. However, flanking via this path can also limit system performance especially when the separating wall and floor have been improved, as illustrated in Tables 1 and 2 (see page 6).

In applications where sound transmission between storeys within a dwelling unit is not a concern (e.g., row housing), the ceiling is typically screwed directly to the bottom of the joists, as shown in Figure 8. In such cases, the ceiling/ceiling flanking path also becomes significant.

For ceilings, the joists can be parallel or perpendicular to the separating wall. The ceiling path attenuation illustrated in Figure 8 shows the worst-case scenario, with supporting joists of the floor above running perpendicular to the separating wall. Less flanking via the ceiling/ceiling path can be expected when the joists are parallel to the wall. Tables 1 and 2 present the combined effect of all paths for typical variants in construction, capturing the two ceiling attachment cases (Figures 7 and 8) and the effect of specific floor toppings. (See the design guide for a series of similar tables.)
The ASTC in a given building may not match the tabulated values exactly, but the trends apply. In all cases, the system ASTC is lower than the STC rating for the separating wall—in some cases much lower.

**Units One Above the Other**

The preceding section shows that for side-by-side units, the ASTC for the whole building system may be far below the STC of the separating wall. The corresponding effects are less dramatic when one unit is above the other, but still warrant design consideration.

<table>
<thead>
<tr>
<th>Separating wall</th>
<th>Basic wall (STC 52)</th>
<th>“Better” wall (STC 57)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Attachment of gypsum board on sidewall</td>
<td>Direct or resilient</td>
<td>Direct</td>
</tr>
<tr>
<td>Floor surface</td>
<td>Apparent STC (ASTC)</td>
<td></td>
</tr>
<tr>
<td>• No topping (basic)</td>
<td>42</td>
<td>43</td>
</tr>
<tr>
<td>• 19-mm OSB stapled to subfloor</td>
<td>47</td>
<td>48</td>
</tr>
<tr>
<td>• 25-mm gypsum concrete bonded to subfloor</td>
<td>48</td>
<td>49</td>
</tr>
<tr>
<td>• 38-mm gypsum concrete + resilient mat on subfloor</td>
<td>49</td>
<td>51</td>
</tr>
</tbody>
</table>

The ASTC in a given building may not match the tabulated values exactly, but the trends apply. In all cases, the system ASTC is lower than the STC rating for the separating wall—in some cases much lower.
Flanking via the gypsum board surfaces of the walls can also be suppressed as shown in Table 3, which provides an example of sound insulation for a complete building system. The table shows the combined effect of changes to the floor surface, the ceiling and the walls, and allows one to perform a cost/benefit analysis for different design options. This approach follows the same pattern as that used for side-by-side units and is especially helpful when used with lightweight floor surfaces.

The balancing of the sound attenuation for all paths becomes increasingly important as the desired (design) ASTC increases. In the absence of such balancing, other efforts to achieve high levels of sound insulation can be compromised.

**Summary**

The experimental characterization of direct and flanking sound transmission paths in wood-frame construction has yielded a set of data that represents the effects of specific design choices. By combining the sound energy transmitted via all paths, it was possible to obtain estimates of the overall system performance—that is, the ASTC—for different combinations of construction details. These details have been combined in a design guide that allows designers to select cost-effective constructions with the desired ASTC.

**Table 3.** ASTC between units (one unit above the other) for selected variations of the floor/ceiling assembly and the wall surfaces in the room below

<table>
<thead>
<tr>
<th>Walls in room below</th>
<th>Floor surface</th>
<th>“Worse” ceiling</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>“Worse” ceiling</td>
</tr>
<tr>
<td></td>
<td></td>
<td>1 layer gypsum board on resilient metal channels spaced 400 mm o.c. (STC 51 if no topping)</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Apparent STC (ASTC)</td>
</tr>
<tr>
<td><strong>Basic walls</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>All walls with 1 layer of gypsum board fastened directly to the studs</td>
<td><em>No topping (OSB subfloor)</em></td>
<td>49</td>
</tr>
<tr>
<td></td>
<td><em>19-mm OSB stapled to subfloor</em></td>
<td>54</td>
</tr>
<tr>
<td></td>
<td><em>25-mm gypsum concrete bonded to subfloor</em></td>
<td>59</td>
</tr>
<tr>
<td></td>
<td><em>38-mm gypsum concrete + resilient mat on subfloor</em></td>
<td>63</td>
</tr>
<tr>
<td><strong>Flanking suppressed</strong></td>
<td></td>
<td></td>
</tr>
<tr>
<td>All walls with 1 layer of gypsum board supported on resilient channels</td>
<td><em>No topping (OSB subfloor)</em></td>
<td>51</td>
</tr>
<tr>
<td></td>
<td><em>19-mm OSB stapled to subfloor</em></td>
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</tbody>
</table>
Notes


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