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## **TERRA NOVA SEDIMENT DATA COMPILATION**

# **PETRO-CANADA 1997 GEOTECHNICAL INVESTIGATIONS**

**GSC OPEN FILE # 3680**

**Report submitted to the Geological Survey of Canada (Atlantic)  
Bedford Institute of Oceanography.**

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by

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## **INTRODUCTION**

Jacques/McClelland Geosciences Inc (JMGI) was retained by the Terra Nova Alliance to investigate and report on the geotechnical conditions at the proposed sites of subsea completions (Glory Holes, Anchor Piles and Flow Lines) at the Terra Nova Development site, located on the Grand Banks offshore Newfoundland (Jacques/McClelland Geosciences Inc., 1997).

The study comprised a total of:

- three boreholes and piezocone penetration tests (PCPTs) to 13 m, five boreholes and PCPTs to 42 m at five glory hole sites;
- six boreholes and PCPTs to 40 or 45 m at three anchor pile sites
- 20 boreholes and PCPTs to 3 m depth along \* flow line routes.

The field work was completed between 6 July to 21 July, 1997 onboard the drillship *MV Norskald*. In-situ testing comprised PCPTs and sediment samples taken with the Fugro Engineers Wip sampler. Onboard laboratory testing of samples was performed to determine physical properties to aid in classification. The onboard sample descriptions and laboratory results are presented in the Terra Nova Development Preliminary Field Report on 1997 TNA Offshore Geotechnical Investigation (Jacques/McClelland Geosciences Inc., 1997).

The onshore laboratory investigation comprised additional classification tests, physical property tests and strength testing including unconsolidated-undrained tests, triaxial compression tests and direct shear tests performed on undisturbed and reconstituted samples. The in-situ testing results, final stratigraphic profiles, classification and geotechnical testing results are presented in the Terra Nova Development Report on 1997 TNA Offshore Geotechnical Investigation (Jacques/McClelland Geosciences Inc., 1997).

GSC-Atlantic (GSCA) contracted Petro-Canada to extend Glory Hole site GS1\_97 from a depth of 42.00 m to 52.63 m with almost continuous sediment sampling. GSCA chose to extend one hole to ensure that the major shallow seismostratigraphic units (Sonnichsen and Cumming, 1996 \*) were penetrated and sampled. GS1\_97 was selected for extension because it was the longest borehole close to GSCA's existing seismic coverage. The GS1\_97 extension core samples were split, described, photographed and subsampled onboard by and brought back to the GSC-Atlantic Core Repository. Meghan MacCarthy of GSC-Atlantic was aboard M/V *Norskald* in order to digitally photograph, describe and subsample all recovered borehole sediment cores.

K & K Geoscience was contracted by G.Sonnichsen of GSC-Atlantic to:

- 1) compile the GSC-Atlantic digital photography, sediment descriptions and PCPT data for Terra Nova boreholes GS1\_97 and A3\_97;
- 2) describe and subsample the extended portion of GS1\_97;
- 3) to locate any hardpan layers in the Flow Line route boreholes and compile the GSC-Atlantic digital photography, sediment descriptions and PCPT data for those boreholes.

## DATA PROCESSING

### Digital Photography

GSCA provided 430 Adobe PhotoDeluxe jpeg files of the digital photography taken using an Olympus 300L digital camera. The jpeg images for eight Glory Hole boreholes (EFN1A\_97, EFN1B\_97, EFN2\_97, EFS1\_97, FEI\_97, GN1\_97, GS1\_97 and GS2\_97), one Anchor Pile site borehole (A3\_97) and nine Flow Line Route boreholes (FPSOB, FR1\_1B, FR1\_2B, FR1\_3B, FR1\_6B, FR1\_7, FR4\_1B, FR4\_3C and FR4\_4B) were processed using Adobe Photoshop 2.5.1. The images were rotated to a vertical position (top of the core up), auto adjusted, cropped (to reduce the file size) and saved as PC LZW compressed TIFF files. The sample number, sample depth, tiff filename, quality of image and other appropriate comments were recorded (Appendix 1).

### Cone Penetrometer Testing (CPT)

The raw CPT data of the individual pushes for each borehole were provided as compiled PC ASCII data files by JMGI. The CPT datafiles consisted of record number, depth (metres from the start of each push), time (seconds from the start of each push), cone tip resistance ( $q_c$  : Mpa), sleeve friction ( $f_s$  : MPa), friction ratio ( $R_f$ ) and pore pressure ( $u_2$  : Mpa).

The sleeve friction measurement ( $f_s$ ) is offset from the cone tip resistance measurement ( $q_c$ ) by 11 cm. This offset could not be corrected by simply shifting the sleeve friction datapoints. The depth correction for the sleeve friction was made using the MacCombine (version 1.0) program written by David Mosher. The MacCombine program combined the original depth and  $q_c$  values with the corrected depth (actual depth) and sleeve friction values by finding the closest corresponding depth for each value and combining the data.

The measured  $q_c$  and  $f_s$  values may not represent true total stress resistance of the sediment as a result of water pressures acting on the exposed surfaces behind the cone tip and on the ends of the friction sleeve (Robertson and Campanella, 1988). The  $q_c$  value was corrected for unequal pore pressure effects using:

$$q_t = q_c + u_2 (1-a)$$

where

$q_t$  = corrected total cone tip resistance

$q_c$  = measured cone tip resistance

$u_2$  = pore pressure generated immediately behind the cone tip

$a$  = net area ratio (equal to 0.75)

Robertson (1989) outlines a procedure to normalize total cone tip resistance using vertical effective stress. The CPT data in this study was not normalized on the advise of GSC-Atlantic.

Measured pore pressure was corrected for hydrostatic pressure. Hydrostatic pore pressure  $u_0$  was set to zero at the start of each push and kept at zero for the entire push. The hydrostatic pressure for each measurement was calculated as follows:

$$u_0 = z * 9.81 * \rho_{sw}$$

where

$z$  = distance from the start of each push

$\rho_{sw}$  = density of salt water assumed as 1.024 g/cm<sup>3</sup>

The measured pore pressure ( $u_2$ ) was corrected for the effect of hydrostatic pressure using:

$$u = u_2 - u_0$$

The sleeve friction ratio ( $R_f$ ) was recalculated using the depth adjusted  $f_s$  and the following:

$$R_f = (f_s/q_t) * 100\%$$

where

$R_f$  = friction ratio

$f_s$  = measured sleeve friction

$q_t$  = corrected cone tip resistance

The raw CPT data for each of the Glory Hole, Anchor Pile and Flow Line route boreholes was compiled into 3 excel 5.0 datafiles. The corrected CPT data for GS1\_97, A3\_97, FPSO, FR1\_1B, FR1\_3B and FR4\_1B was compiled into one excel 5.0 datafile for each site. Each corrected datafile comprises the original raw data and the MacCombine corrected depth (m), measured cone tip resistance ( $q_c$  : MPa), measured sleeve friction ( $f_s$  : Mpa), measured pore pressure ( $u_2$  : Mpa), corrected pore pressure ( $u$  : Mpa), total cone tip resistance ( $q_t$ ) using both measured pore pressure ( $u_2$ ) and corrected pore pressure ( $u$ ), friction ratio ( $R_f$ ) using both values of  $q_t$  and the cpt soil classification (see “Soil Classification and Core Description” section of this report). The data was then saved in excel 4.0 format and imported into Kaleidagraph 3.0.

### Grain Size Analysis

Sieve and hydrometer grain size analyses were conducted by JMGI according to ASTM Method D422. The results were presented as percent passing (Glory Hole and Anchor Hole Preliminary Field Reports) and percent grain size distribution curves and in table format (Flow Line Preliminary Field Report).

Cumulative relative frequency percentage curves and data tables were provided by the GSC-Atlantic Sedimentological Laboratory (Appendix 2) for the additional GS1\_97 borehole grain size subsamples taken at the GSC-Atlantic Core Laboratory.

The percent grain size was calculated for GS1\_97 and A3\_97 from the percent passing grain size data supplied by JMGI. Cumulative grain size percent was calculated for GS1\_97, A3\_97, FPSOB, FR1\_1B, FR1\_3B and FR4\_1B in individual Excel 5.0 datafiles.

## Soil Classification and Core Descriptions

### *Unified Soil Classification*

The Unified Soil Classification System (USCS) is commonly used in civil engineering practice. The basis for the USCS is that coarse-grained soils are classified according to their grain size distributions, whereas the engineering behaviour of fine grained soils is primarily related to their plasticity. Therefore only a sieve analysis and the Atterberg limits are required to completely classify a soil in this system. A summary of the USCS Soil Classification is shown in Table 1.

Table 1  
Unified Soil Classification

### **Coarse grained**

#### *Gravels*

- GW - Well graded gravels, gravel-sand mixtures, little or no fines
- GP - Poorly graded gravels, gravel-sand-silt mixtures
- GM - Silty gravels, gravel-sand-silt mixtures
- GC - Clayey gravels, gravel-sand-clay mixtures

#### *Sands*

- SW - Well graded sands, gravelly sands little or no fines
- SP - Poorly graded sands, gravelly sands little or no fines
- SM - Silty sands-sand silt mixtures
- SC - Clayey sands, sand-clay mixtures

### **Fine grained**

#### *Silts and Clays - liquid limit less than 50*

- ML - Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity
- CL - Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays ??
- OL - Organic silts and organic silty clays of low plasticity

#### *Silts and Clays - liquid greater than 50*

- MH - Inorganic silts, micaceous or diatomaceous fine sandy or silty soils elastic silts
- CH - Inorganic clays of high plasticity, fat clays
- OH - Organic clays of medium to high plasticity, organic silts

### *CPT Soil Classification*

The CPT data for the boreholes GS1\_97, A3\_97, FPSOB, FR1\_1B, FR1\_3B and FR4\_1B was classified using the Simplified Soil Classification Chart for Standard Electronic Friction Cone (Robertson et al.1986). This classification uses friction ratio ( $R_f$ ) versus log total cone tip resistance ( $q_t$ ) to define 12 soil behaviour type zones (Table 2).

Table 2  
Simplified Soil Behaviour Type Classification for Standard Electric Friction Cone

<b>Zone</b>	<b>Soil Behaviour Type</b>
1	- sensitive fine grained
2	- organic material
3	- clay
4	- silty clay to clay
5	- clayey silt to silty clay
6	- sandy silt to clayey silt
7	- silty sand to sandy silt
8	- sand to silty sand
9	- sand
10	- gravelly sand to sand
11	- very stiff fine grained
12	- sand to clayey sand

### *Core Description*

The core description was based upon the initial visual grain size description and then modified by grain size analysis data where available. Sediment containing gravel was classified after Folk (1968) and sand-silt-clay mixtures were classified after Shepard (1954).

## **DATA COMPILATION**

### Digital Photography

K & K Geoscience was contracted to integrate the core photography with the core descriptions and CPT data. In order to provide the best quality photography the images were compiled and printed in letter size page format. To reduce processing time and maintain photographic integrity the only modification to the images was an auto adjustment made in Adobe Photoshop 2.5.1. The images were scaled in the final format but file size was unchanged in order to maintain image quality. The downhole images are shown from left to right and where applicable a metre tape was used as the scale for images to the right of the metre tape.

The following borehole images are presented at the end of the written section of this report :

1. Glory Holes - EFN1A\_97, EFN1B\_97, EFN2\_97, EFS1\_97, FEI\_97, GN1\_97, GS1\_97 and GS2\_97;
2. Anchor Pile site borehole - A3\_97;
3. Flow Line Route boreholes - FPSO, FR1\_1B, FR1\_2B,FR1\_3B, FR1\_6B, FR1\_7, Fr4\_1B, FR4\_3C and FR4\_4B

#### Soil Classification, Core Descriptions, Grain Size and CPT Data

The Unified Soil Classification, Core Description and CPT Soil Classification were digitally compiled as separate logs utilizing the software package AppleCORE v0.7.5g. The AppleCORE digital logs incorporated the sediment classification, core description and sediment subsampling.

The AppleCORE Unified Soil Classification is based upon data obtained from the JMGI Terra Nova Draft and Preliminary Field Reports. The JMGI Terra Nova Draft Report contains summary tables consisting of samples recovered and the Unified Soil Classification of the samples tested. The JMGI Preliminary Field Reports contains the visual core description and incorporates core condition, core consistency, reaction to HCL, core colour, visual texture and grain size, lithologic contacts, bioturbation intensity, presence of shells, presence of organics and other visible features.

The AppleCORE CPT Soil Classification is based upon the Simplified Soil Classification Chart for Standard Electronic Friction Cone (Robertson et al.1986). For each depth interval where both  $q_t$  and  $R_f$  values were calculated the soil behaviour type zone was identified.

The AppleCORE Core Description is based upon the visual descriptions provided by: 1) JMGI (Preliminary Field Reports); 2) Meghan MacCarthy of GSC-Atlantic (field notes); and 3) K & K Geoscience (for the extended section of GS1\_97). The visual core descriptions incorporate core condition, core consistency, reaction to HCL, core colour, visual texture and grain size, lithologic contacts, bioturbation intensity, presence of shells, presence of organics and any other visible features. The AppleCORE Core Description was modified by the grain size analysis data provided by JMGI and the GSC-Atlantic Sedimentological Laboratory.

The AppleCORE Unified Soil Classification (Appendix 3), Core Description (Appendix 4) and CPT Soil Classification (Appendix 5) for GS1\_97, A3\_97, FPSOB, FR1\_1B, FR1\_3B and FR4\_1B were printed at 5 m downcore intervals.

Each of the three AppleCORE graphic lithology logs were exported as pict files (at scales of 1:250 and 1:25) and imported into Aldus Freehand 5.0. The entire length of the borehole was exported at a scale of 1:250. Ten metre length intervals were exported at a scale of 1:25 and further scaled to 1:12.5 in Aldus Freehand 5.0.

A Combined Core Description was made by superimposing the Core Description on the CPT Soil Classification in Aldus Freehand 5.0. In instances where there were intervals of both CPT data and sediment sample the Core Description was used.

The cumulative percent gravel, sand, silt and clay were plotted using Kaleidagraph 3.0 for GS1\_97 and A3\_97. No clay percentages were given for the Flow Lone Route boreholes and silt percent was defined as silt/clay percent. The cumulative percent gravel, sand, silt /clay were plotted using Kaleidagraph 3.0 for FPSOB, FR1\_1B, FR1\_3B and FR4\_1B. The cumulative percent plots were plotted at the same scales (1:250 and 1:12.5) as the AppleCORE lithology logs using Kaleidagraph 3.0. The plots were imported into Freehand 5.0 and coloured.

The four lithology logs and cumulative grain size plots for each borehole were compiled into a tabloid size format file and a letter size format file using Freehand 5.0 (Appendix 6 ). The tabloid size format comprises the entire length of each borehole and the letter size comprises 10 metre downcore intervals of each borehole.

The final Aldus Freehand files comprise the Combined Core Description, Core Sample Identifier, Cumulative Grain Size, Sleeve Friction ( $f_s$ ), Sleeve Friction Ratio ( $R_f$ ), Total Cone Tip Resistance ( $q_t$ ) and Corrected Pore Pressure ( $u$ ) as both tabloid (1:250) and letter size (1:12.5) plots. These plots are presented at the end of the written section of this report.



## **REFERENCES**

Folk, R.L. 1968. Petrology of Sedimentary Rocks. Hemphills

Jacques/McClelland Geoscience Inc., Terra Nova Development Preliminary field report on 1997 TNA Offshore Geotechnical Investigation. Volume 3- anchor pile sample data Contract report prepared for Petro-Canada Resources.

Jacques/McClelland Geoscience Inc., Terra Nova Development Preliminary field report on 1997 TNA Offshore Geotechnical Investigation. Volume 4- flow line route sample data Contract report prepared for Petro-Canada Resources.

Jacques/McClelland Geoscience Inc., Terra Nova Development draft report on anchor pile sites; 1997 TNA offshore geotechnical investigation. Contract report prepared for Petro-Canada Resources. 12 pages plus appendices

Jacques/McClelland Geoscience Inc., Terra Nova Development draft report on flow line routes; 1997 TNA offshore geotechnical investigation. Contract report prepared for Petro-Canada Resources. 33 pages plus appendices

Jacques/McClelland Geoscience Inc., Terra Nova Development draft report on seafloor structure (glory hole) sites; 1997 TNA offshore geotechnical investigation. Contract report prepared for Petro-Canada Resources. 25 pages plus appendices

Robertson P.K., and Campanella R.G. 1988: Guidelines for geotechnical design using CPT and CPTU. Soil Mechanics Series No. 120. Department of Civil Engineering, The University of British Columbia, Vancouver, B.C., 193p.

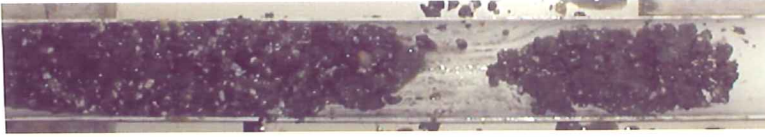
Robertson P.K. 1989: Soil classification using the cone penetration test. Canadian Geotechnical Journal, v.27, p.151-158.

Sonnichsen, G.V., and Cumming, E., 1996 Shallow stratigraphy, sediment properties and foundation stability in the Jeanne D'arc basin discovery areas. 49th Canadian Geotechnical Conference of the Canadian Geotechnical Society, 23-25 September 1996. St John's, Newfoundland.

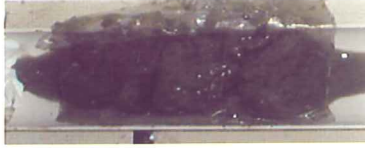
Shepard, F.P., 1954, Nomenclature based on sand-silt-clay ratios. Journal Sedimentary Petrology, v.24 pp 151-158.

Glory Hole  
Borehole Photography

H12



H10



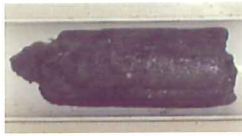
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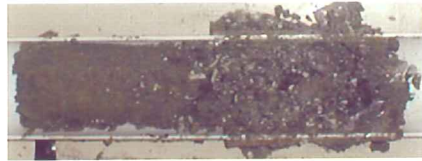
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H4



H3



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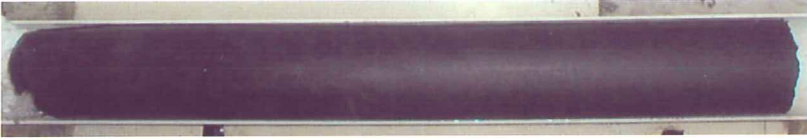
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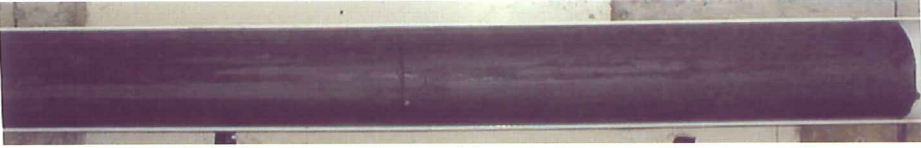
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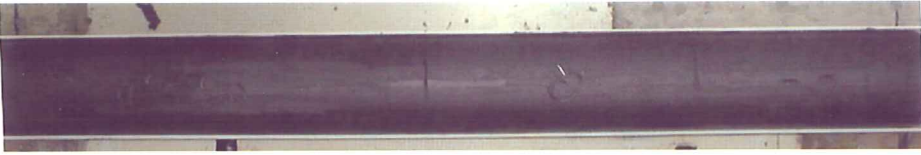
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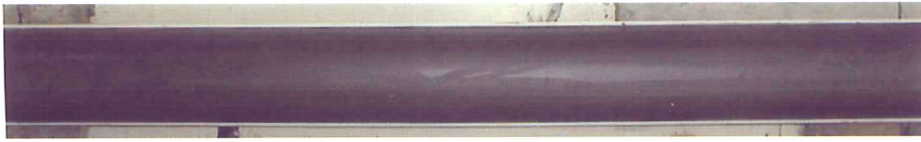
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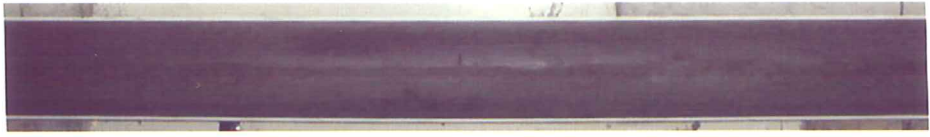
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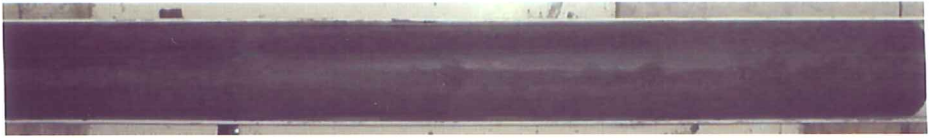
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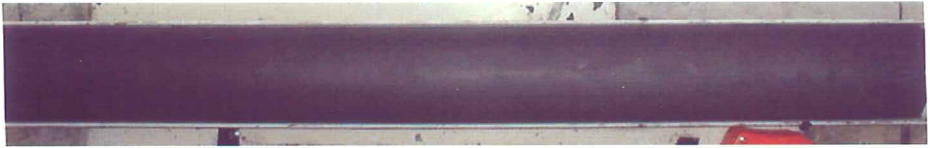
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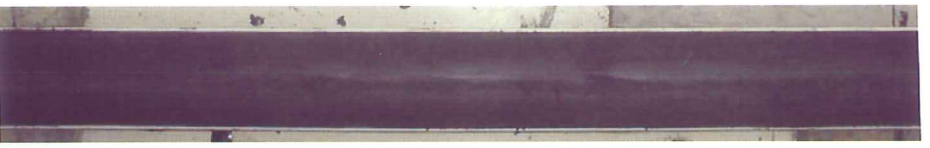
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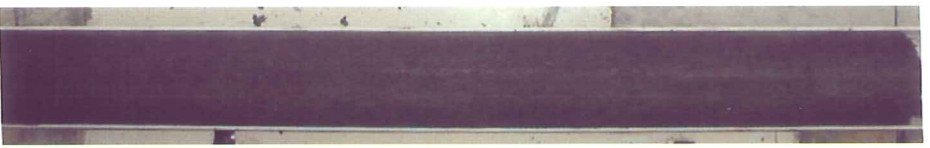
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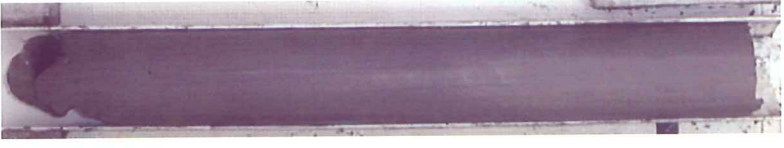
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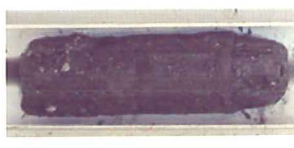
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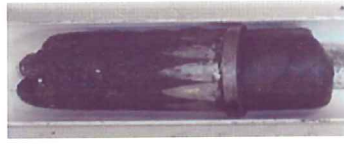
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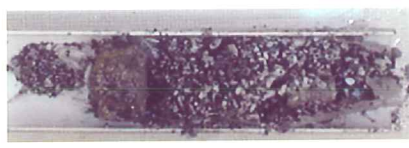
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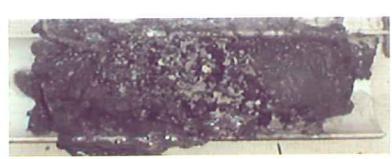
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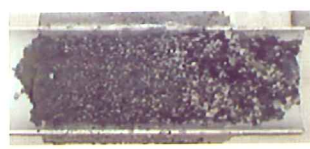
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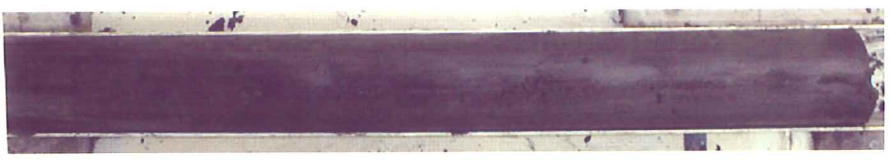
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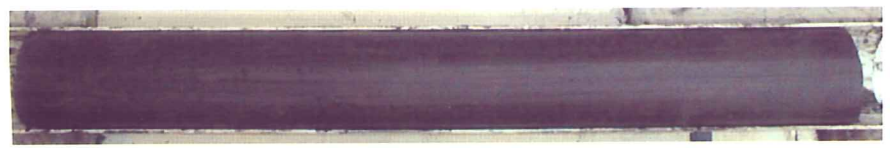
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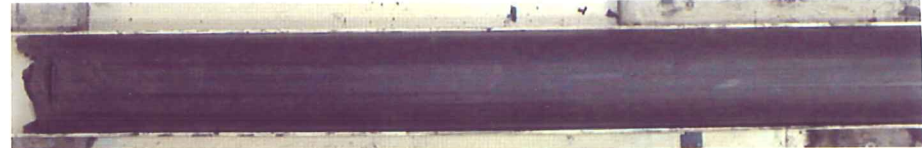
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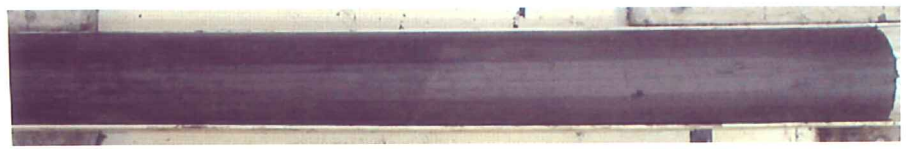
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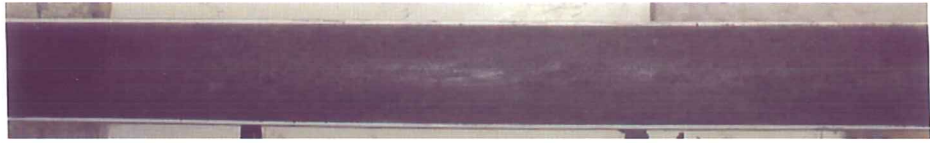
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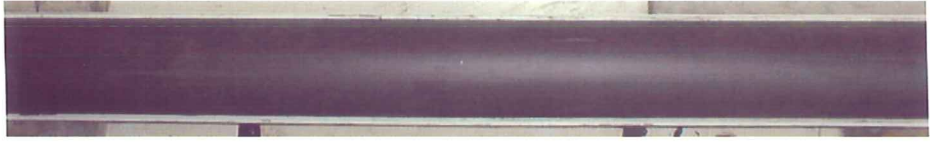
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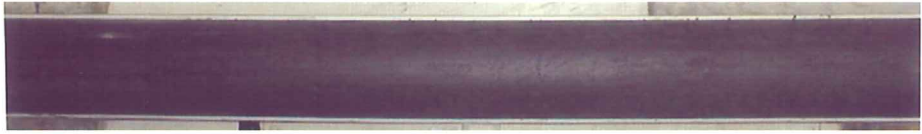
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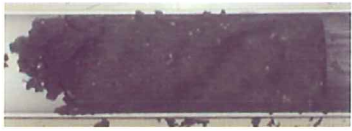
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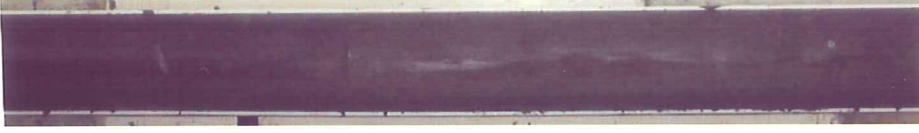


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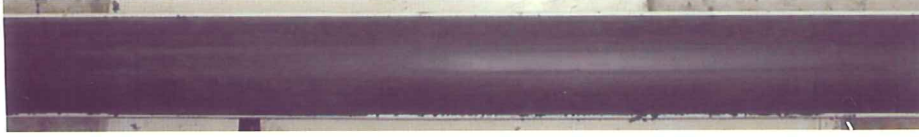




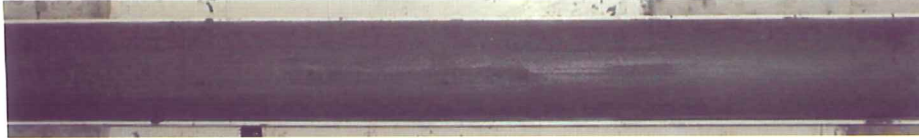
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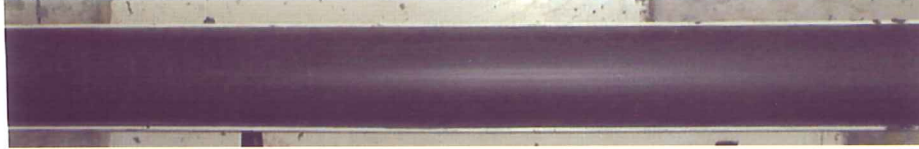
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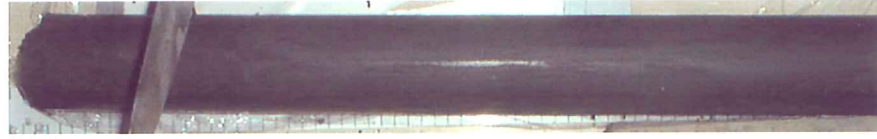
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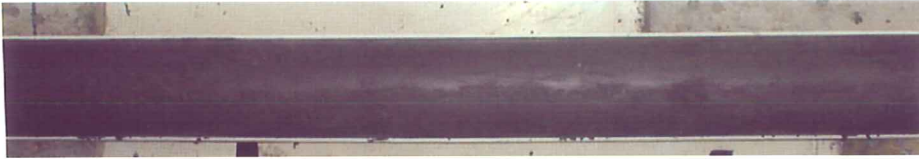
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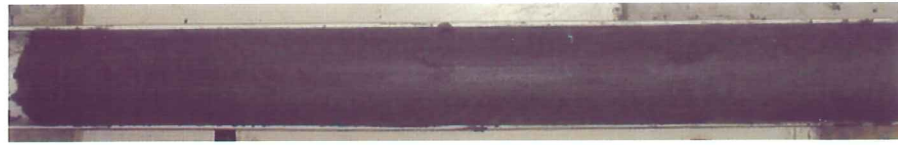
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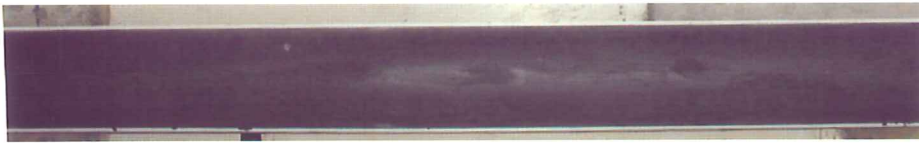
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P15



P13



fe1\_97 photo 1 page

H3



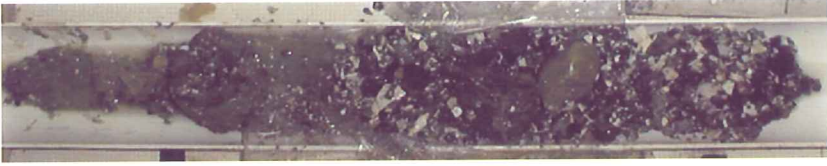
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H3



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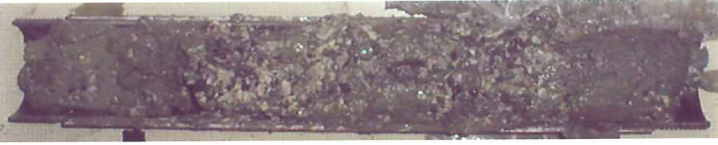
H7



H8



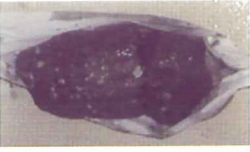
H9



H10



H11



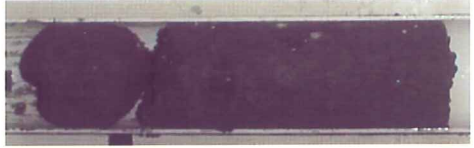
H3



H3



P21



P20



H19



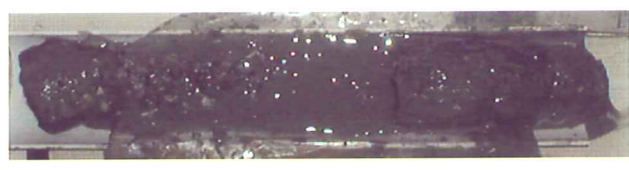
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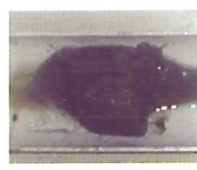
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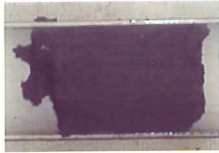
H15



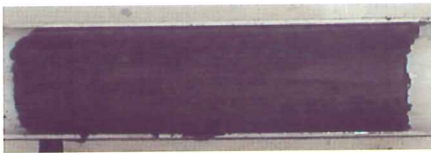
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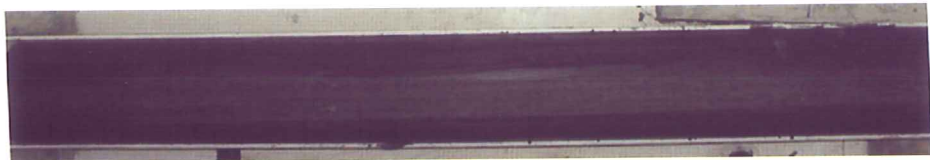
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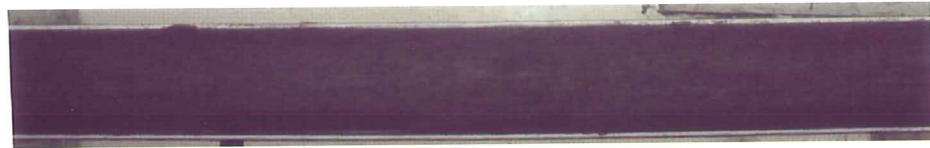
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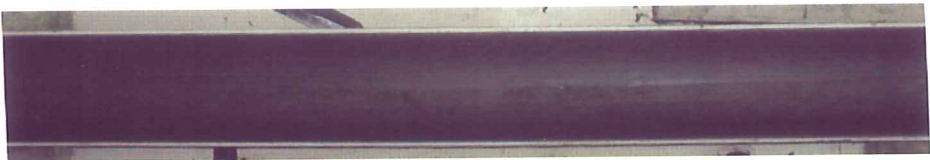
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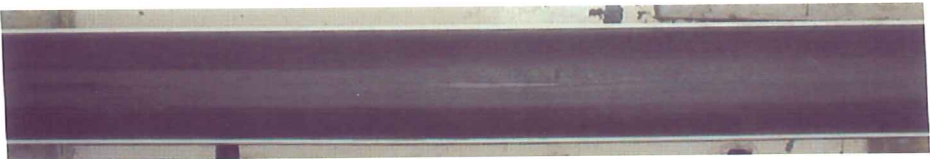
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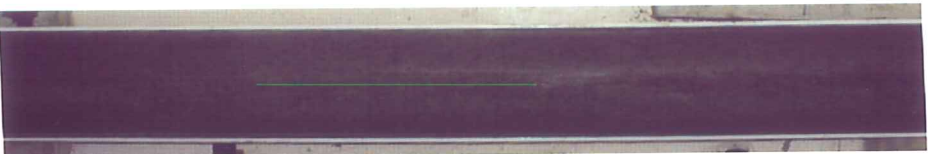
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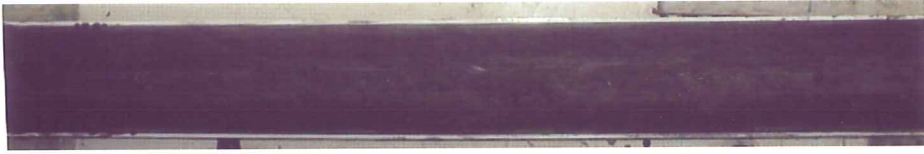
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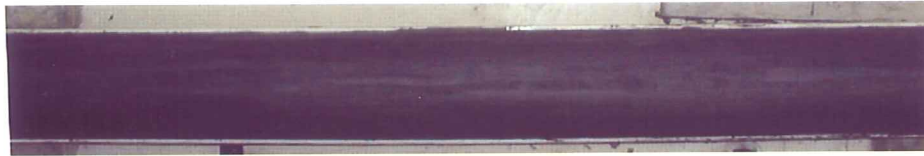
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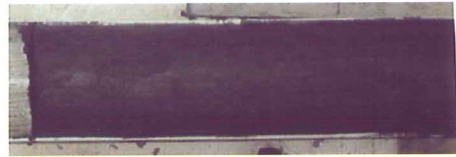
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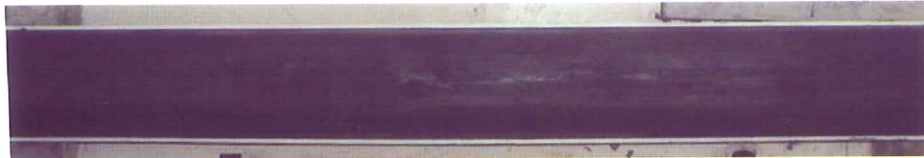
P40



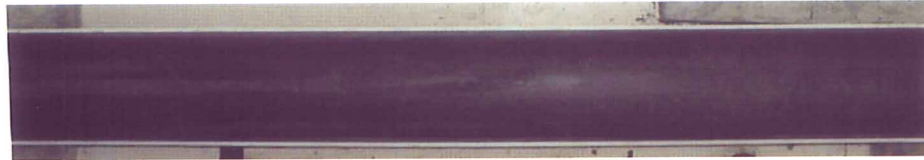
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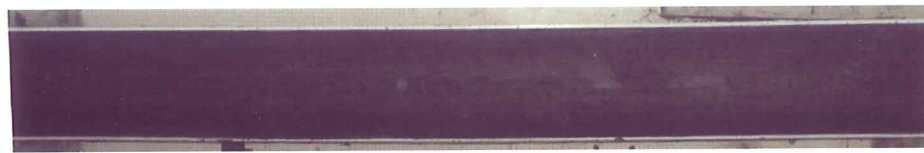
P37



P35



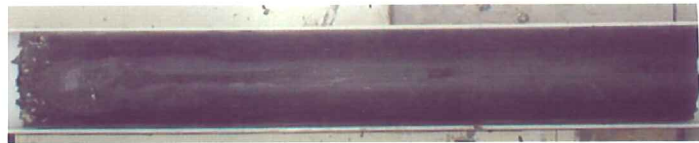
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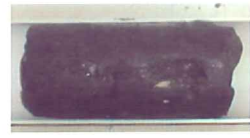
R2



R3



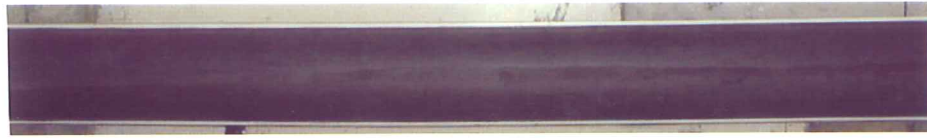
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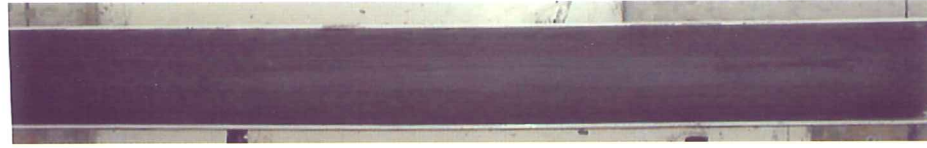
P4A



P6



P8



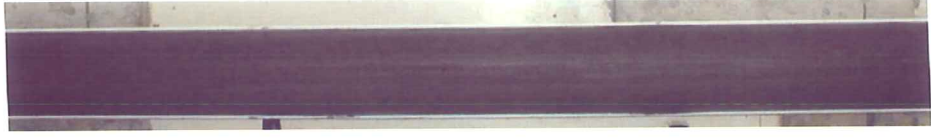
P10



P11



P27



P26



P24



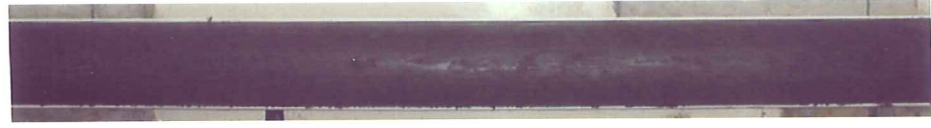
P23



P21



P20



P14

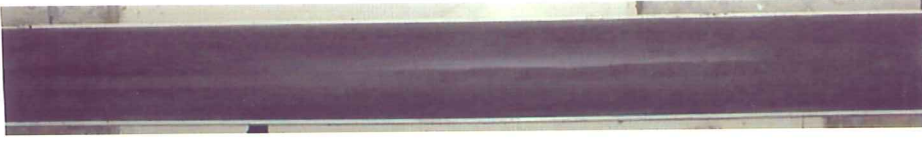


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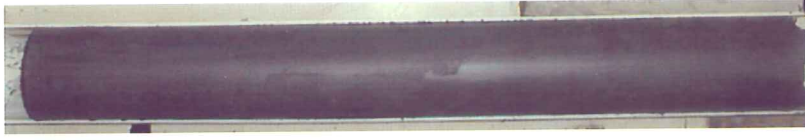




P12



P11A



P9



P8



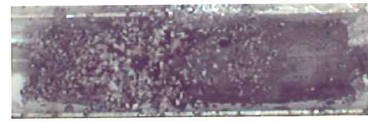
P6



P5



H4



P3



R2



P26



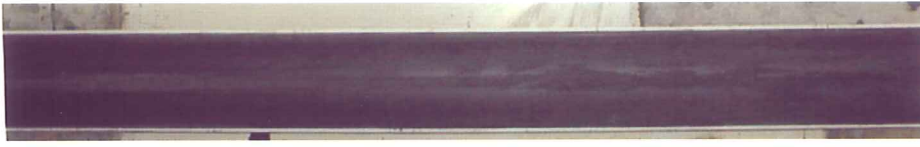
P24



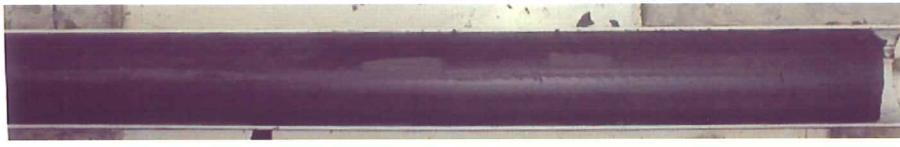
P23



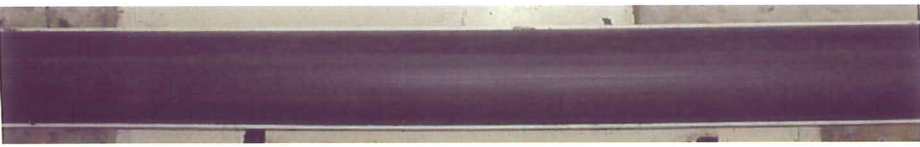
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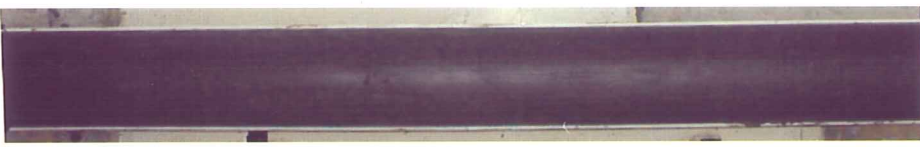
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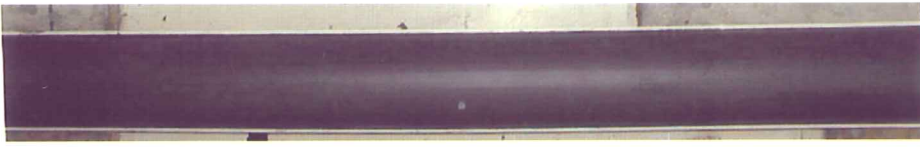
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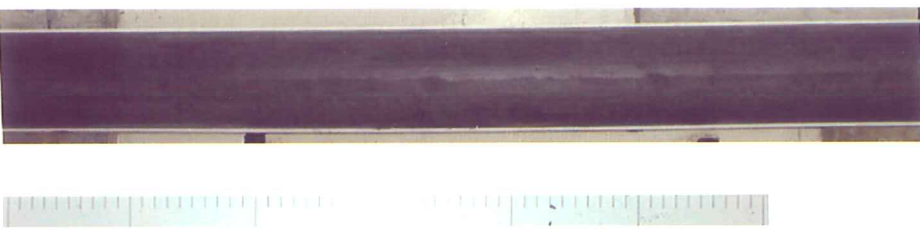
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P15



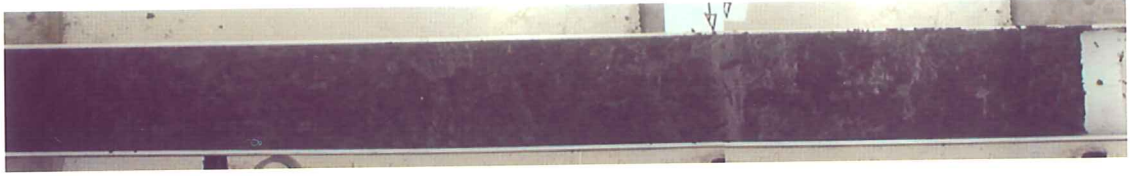
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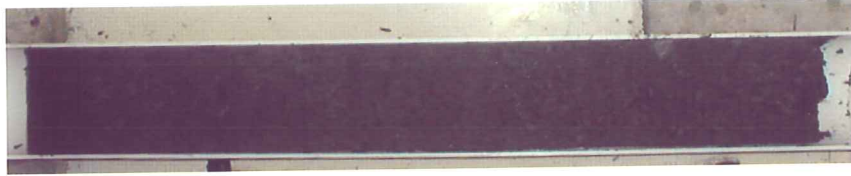
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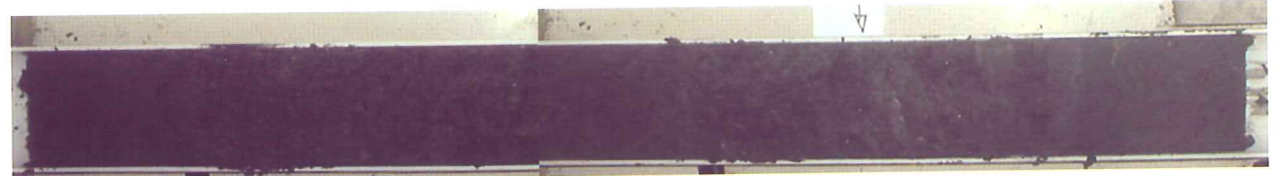
R32



R31



R30



R29



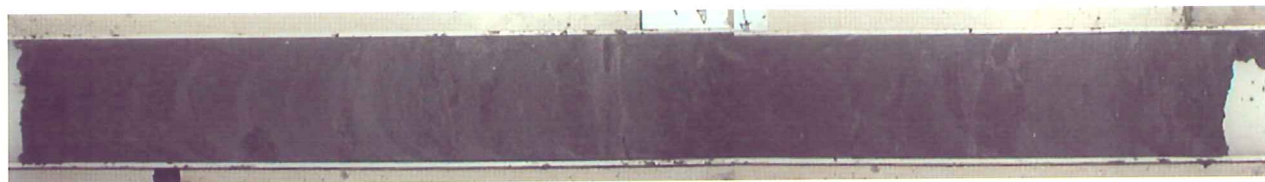
H28A



R40



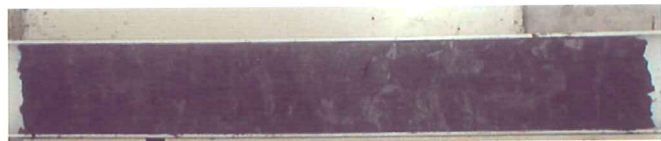
R39



R38



R37



R36



R34



P1



H3



H4



H5



H7



H8



H10

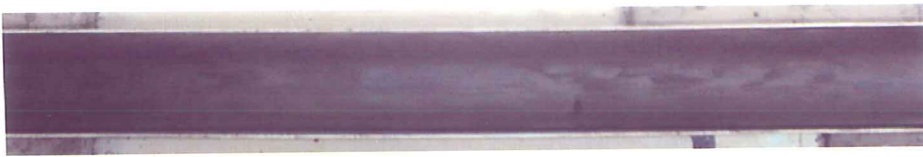


H11

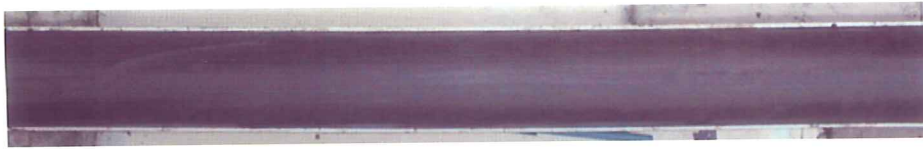


Anchor Pile  
Borehole Photography

P20



P19



H6



H5



H4



H3



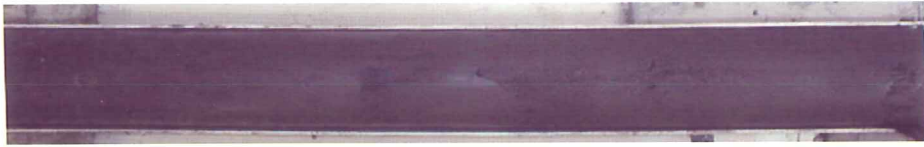
H2



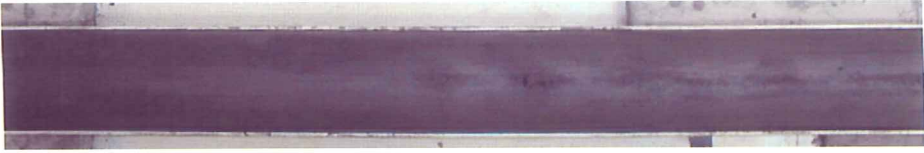
H1



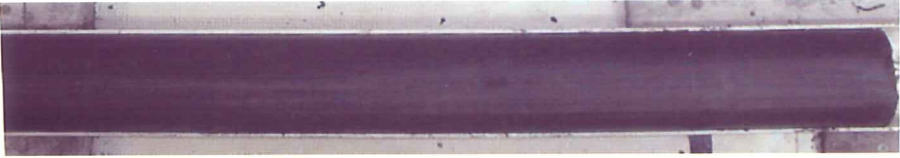
P22



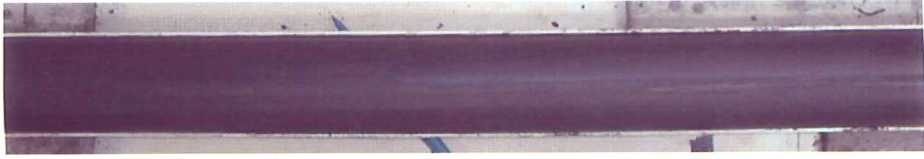
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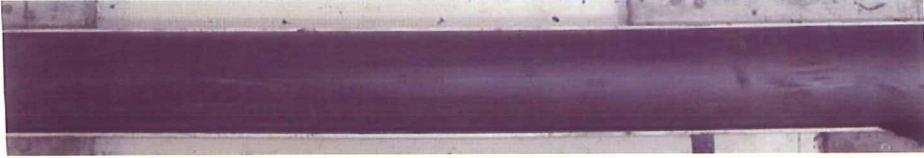
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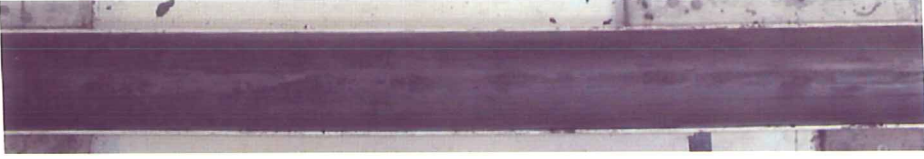
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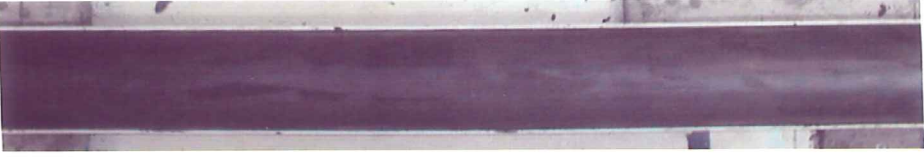
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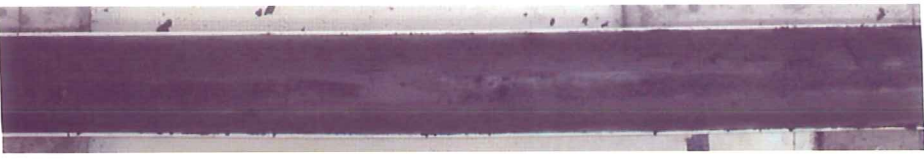
P29



P31



P32



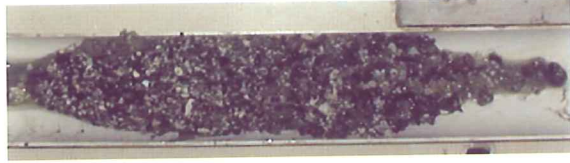
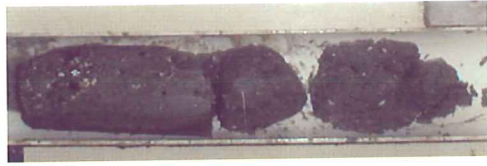


Flow Line Route  
Borehole Photography

H6



H5



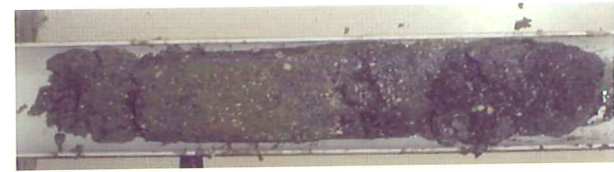
H4



H3



H2



R1



H1



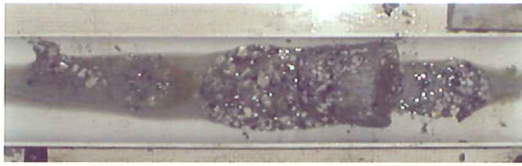
H2



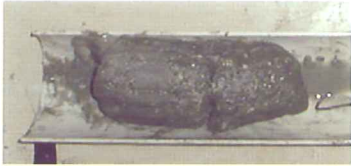
H3



H4



H5



H6



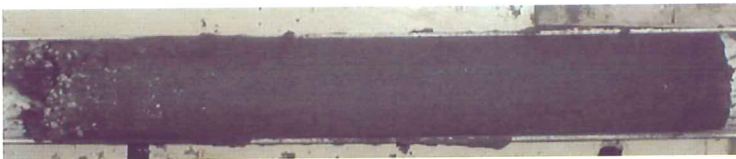
R1



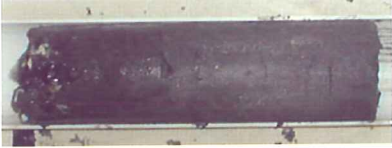
R2



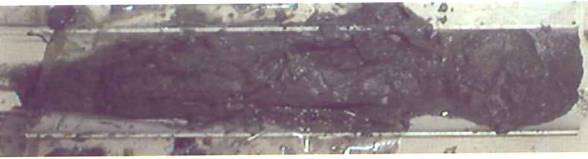
R3



R4



H5



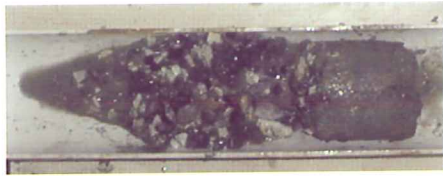
H6



H5



H4



H3



H2



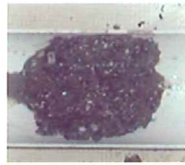
H1



R2



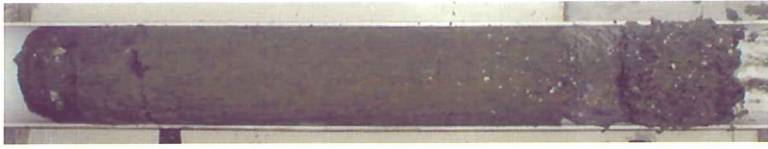
H3



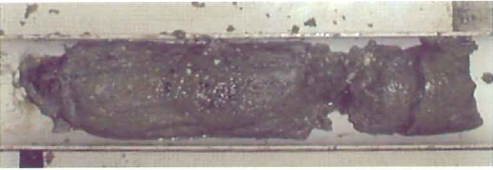
H4



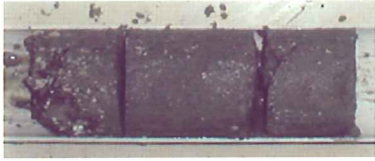
R1



H2



R3



H4



R5

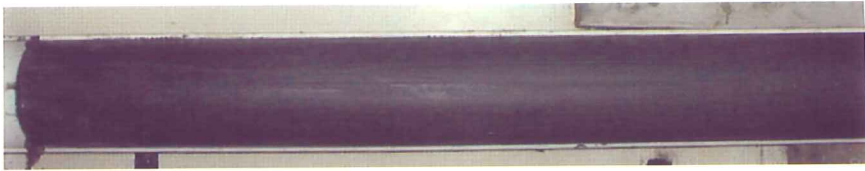




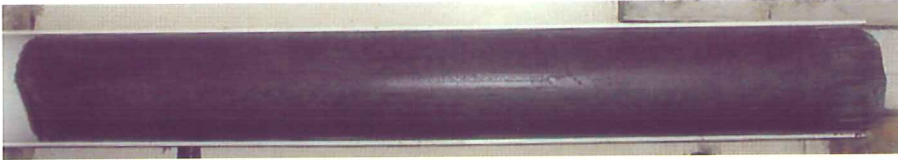
R1



R2

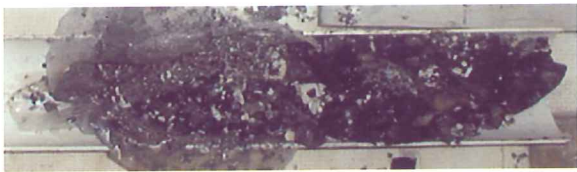


R3

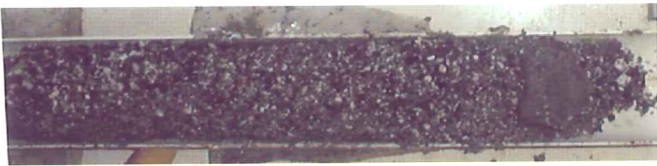




H1



H2



H3



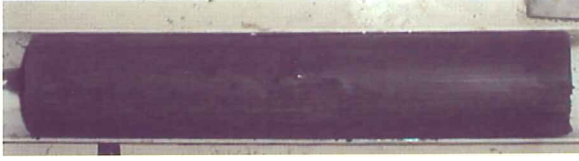
H4



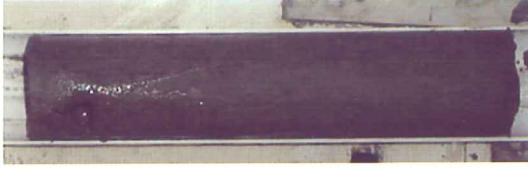
H5



P7



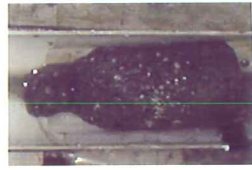
P6



H5



H4



H3










H2















# Legend

## Unified Soil Classification

	GW - well graded gravels, gravel sand mixtures, little or no fines		SC - clayey sands, sand clay mixtures
	SW - poorly graded gravels, gravel sand mixtures, little or no fines		CL - inorganic clays of low to medium plasticity, gravelly clays, sandy clays and silty clay
	SP - poorly graded sands, gravelly sand, little or no fines		CH - inorganic clays of high plasticity, fat clays
	SM - silty sands, sand silt mixtures		

## CPT Soil Classification

	Gravelly sand to sand		Clayey sand		Clayey silt to silty clay
	Sand		Silty sand to sandy silt		Silty clay to clay
	Sand to silty sand		Sandy silt to clayey silt		Clay
	Sand to clayey sand		Silt		Very stiff fine grained

## Grain Size Analysis

	Gravel		Sand		Silt/Clay		Silt		Clay
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# Legend

## Contacts

———— Sharp                      ////////////// Gradational                      \*\*\*\*\* Bioturbated

## Physical Structures

▬ - Graded Bedding                      ▬ - Reverse Graded Bedding

## Lithologic Accessories

◆	Cobble	∴ ∴ ∴	Sand Lenses	∅∅∅	Shell Fragments
•	Pebble	- - - - -	Silty/Clay Lenses	w	Wood Fragments
*****	Gravel			+++	Organic Black Flecks
◇◇◇◇	Pebbles/Granules			Py	Pyritized Worm Burrow

## Core Disturbance

| Slightly Disturbed                      } Very Disturbed

## Bioturbation

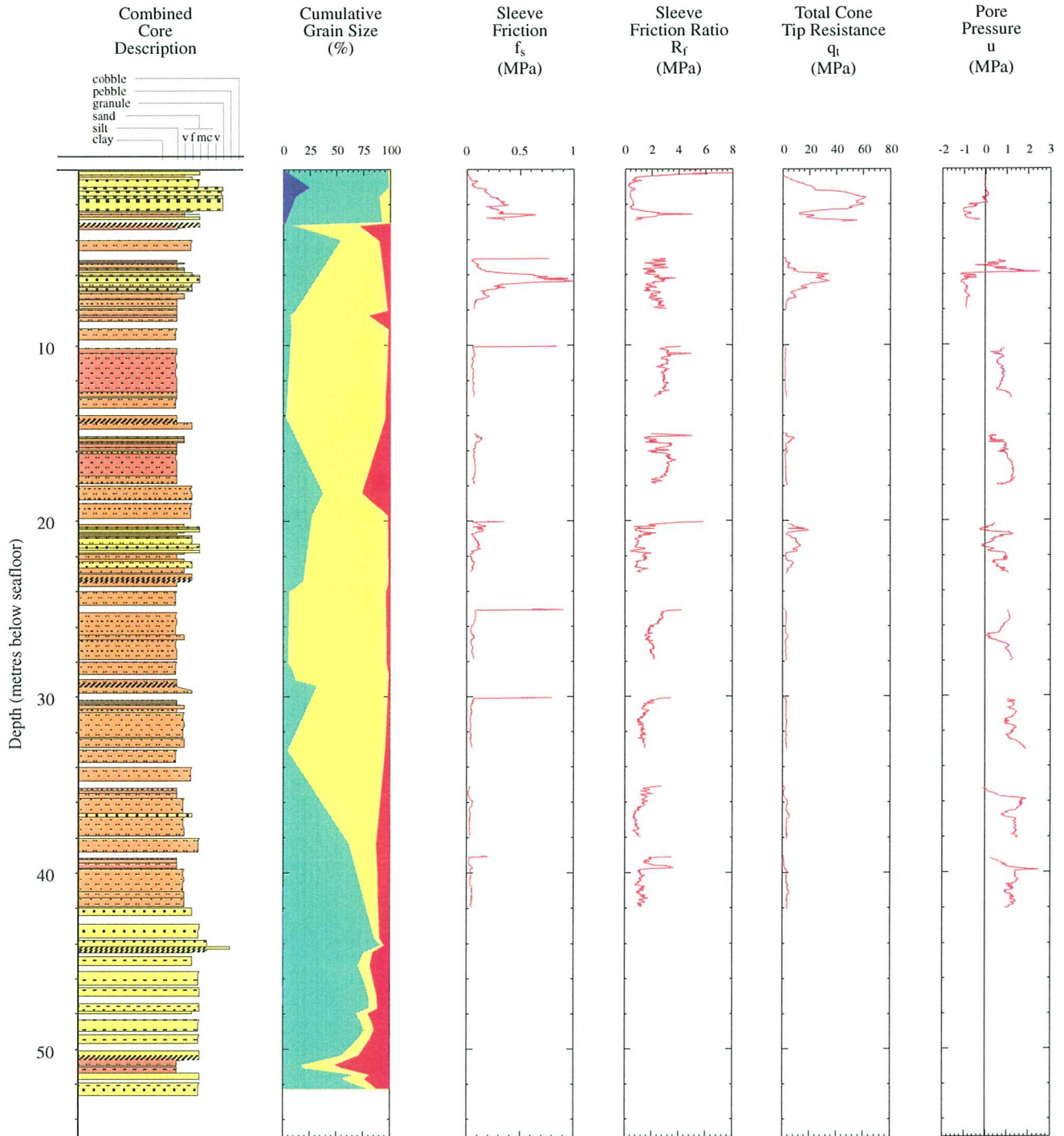
■ Abundant                      ▨ Common                      ▩ Moderate                      ▫ Rare                      □ Barren

# *Legend*

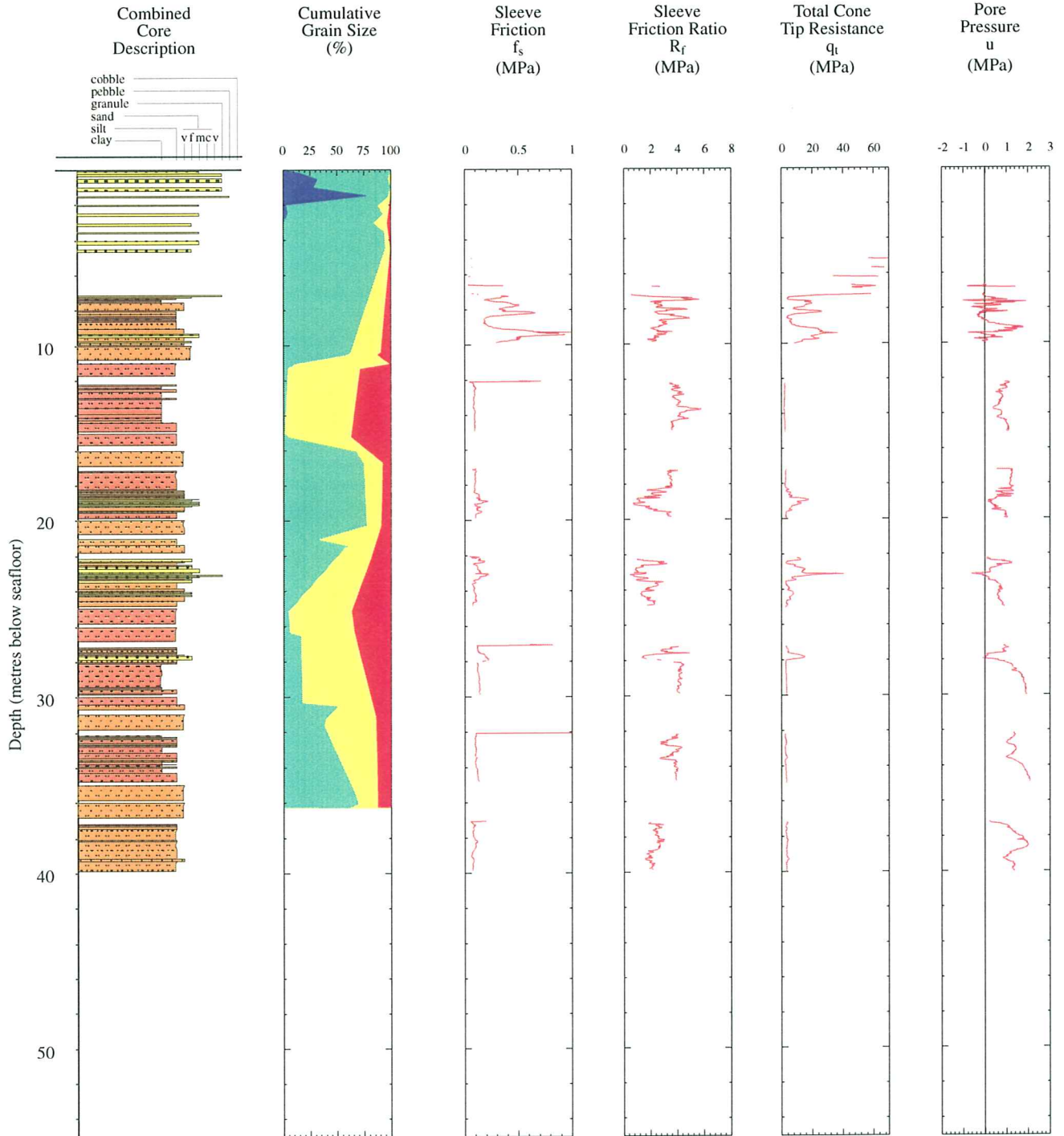
## **Subsamples**

d	JMGI density
w	JMGI water content
gs	JMGI grain size
pp	JMGI pocket penetrometer
t	JMGI torvane
Gb	GSC-Atlantic bulk
Gf	GSC-Atlantic foram
Ggs	GSC-Atlantic grain size

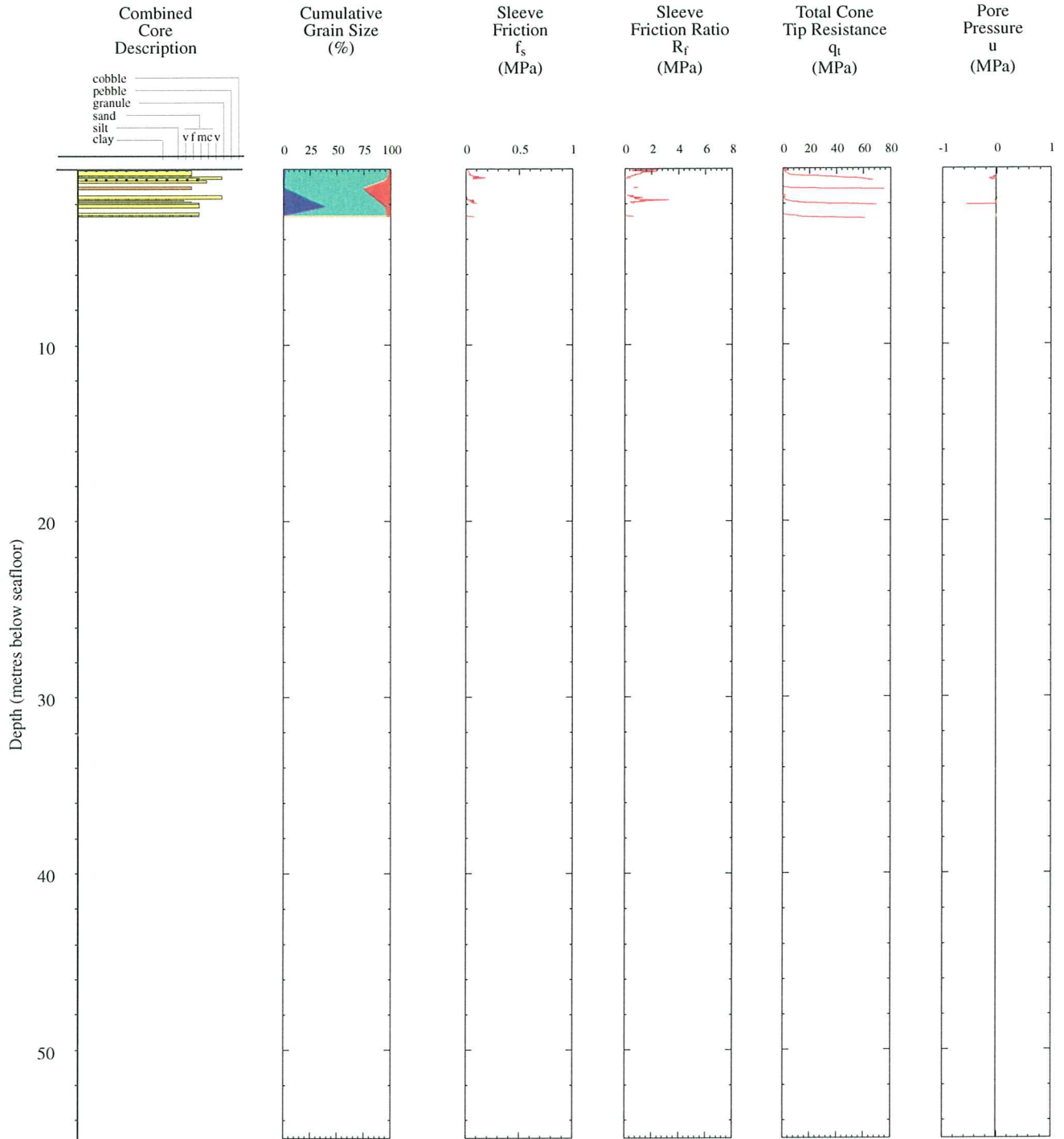
# GSI\_97



# A3\_97

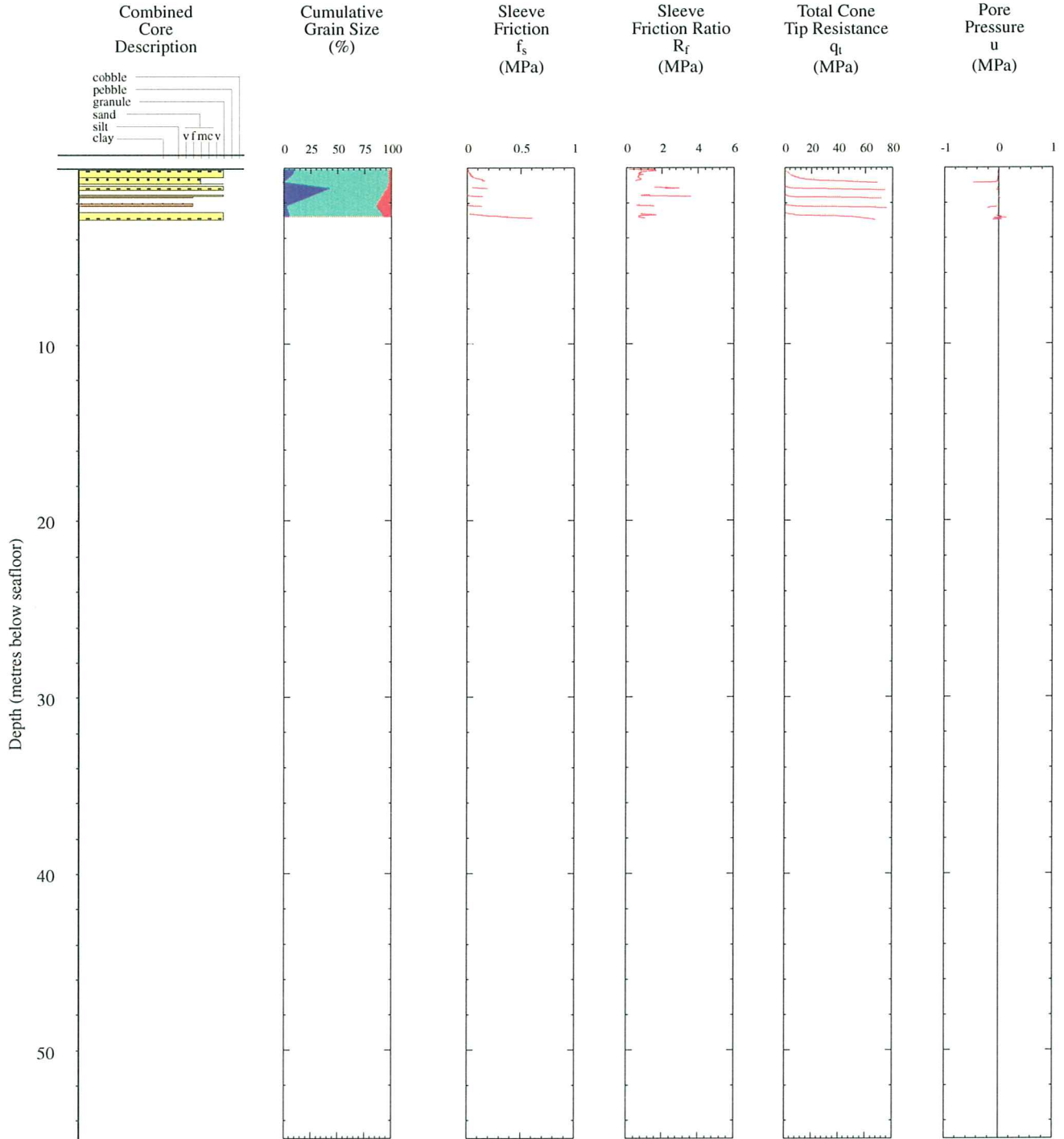


# FPSO\_B

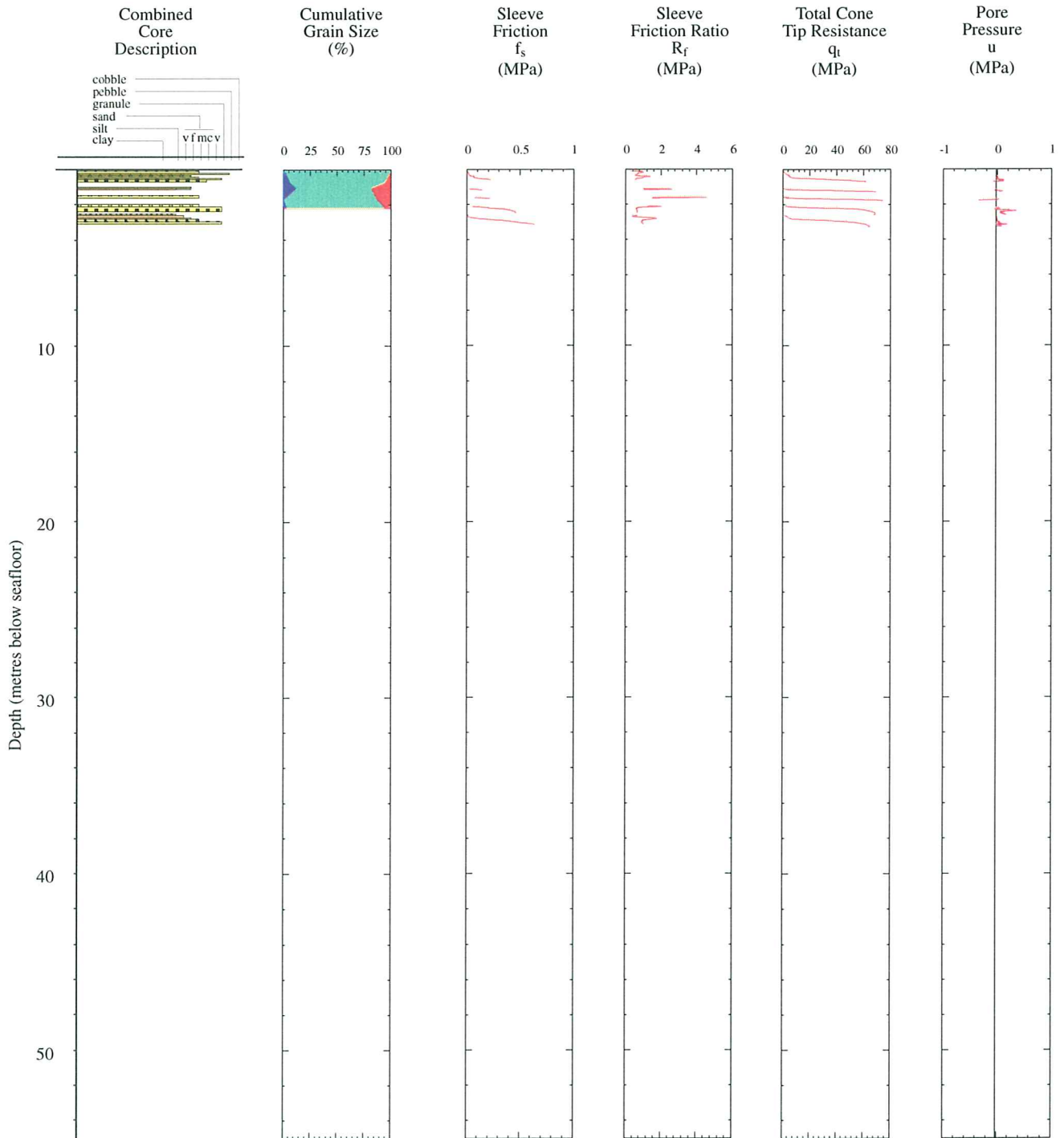




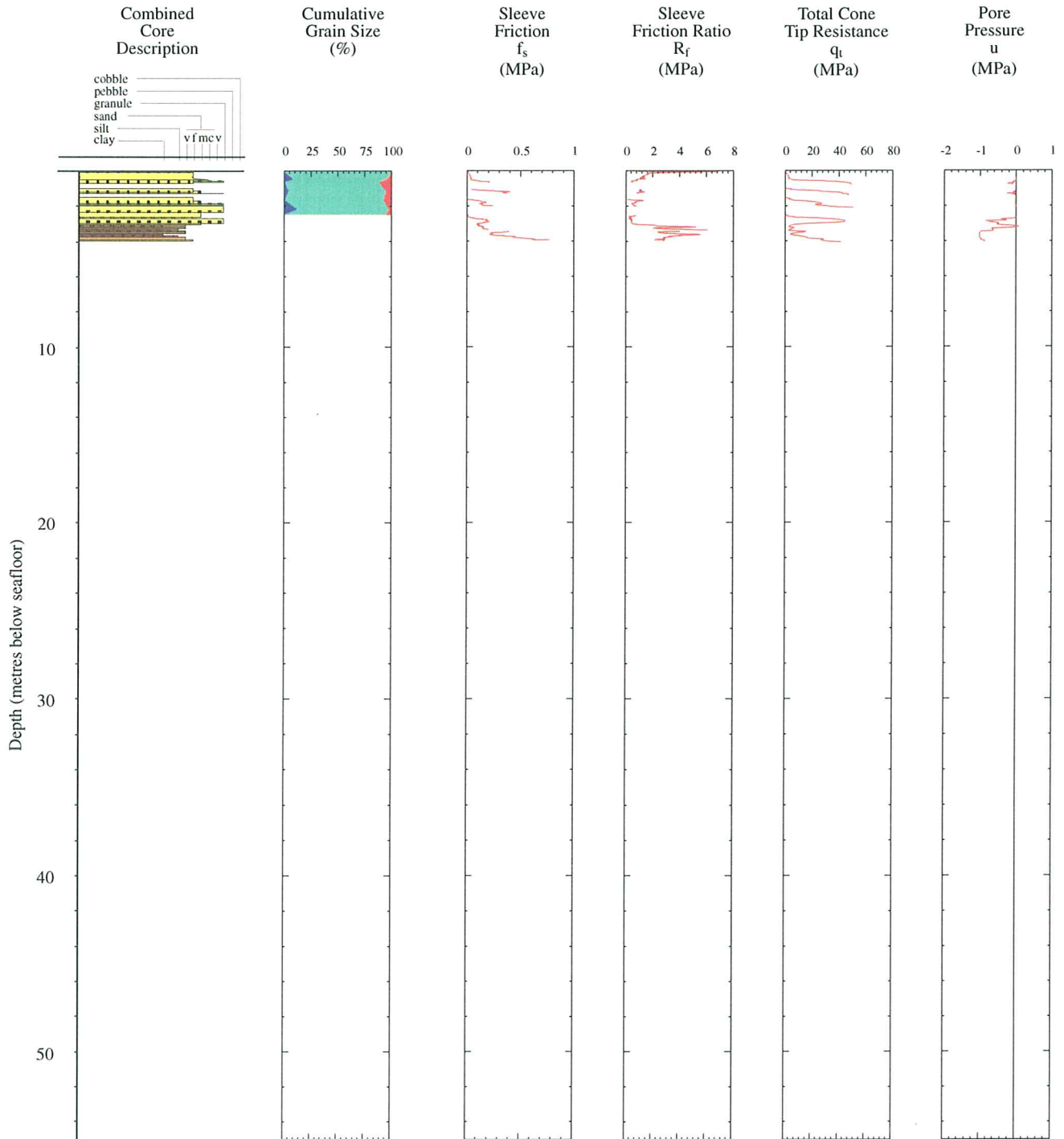
# FRI\_1B



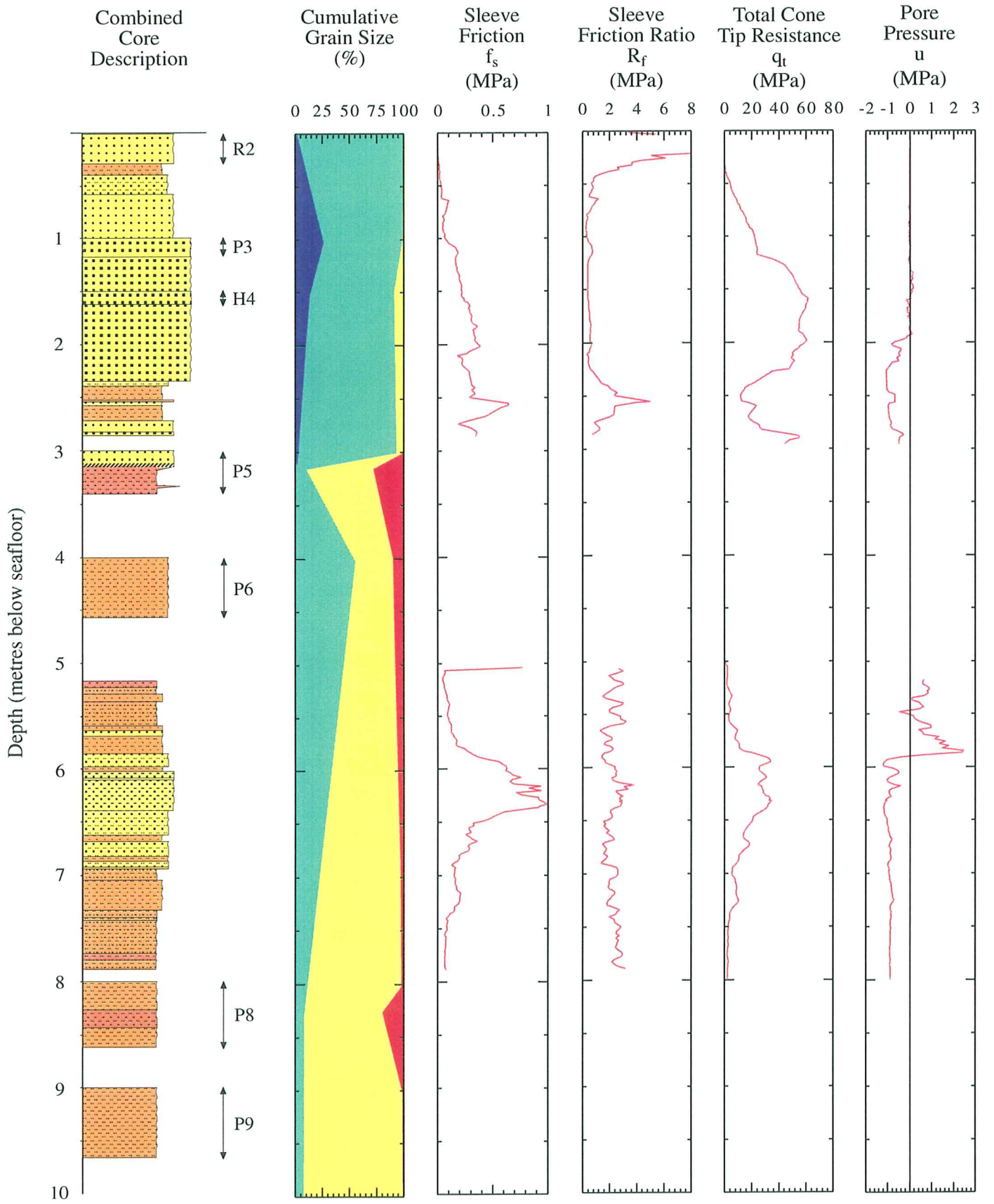
# FR1\_3B



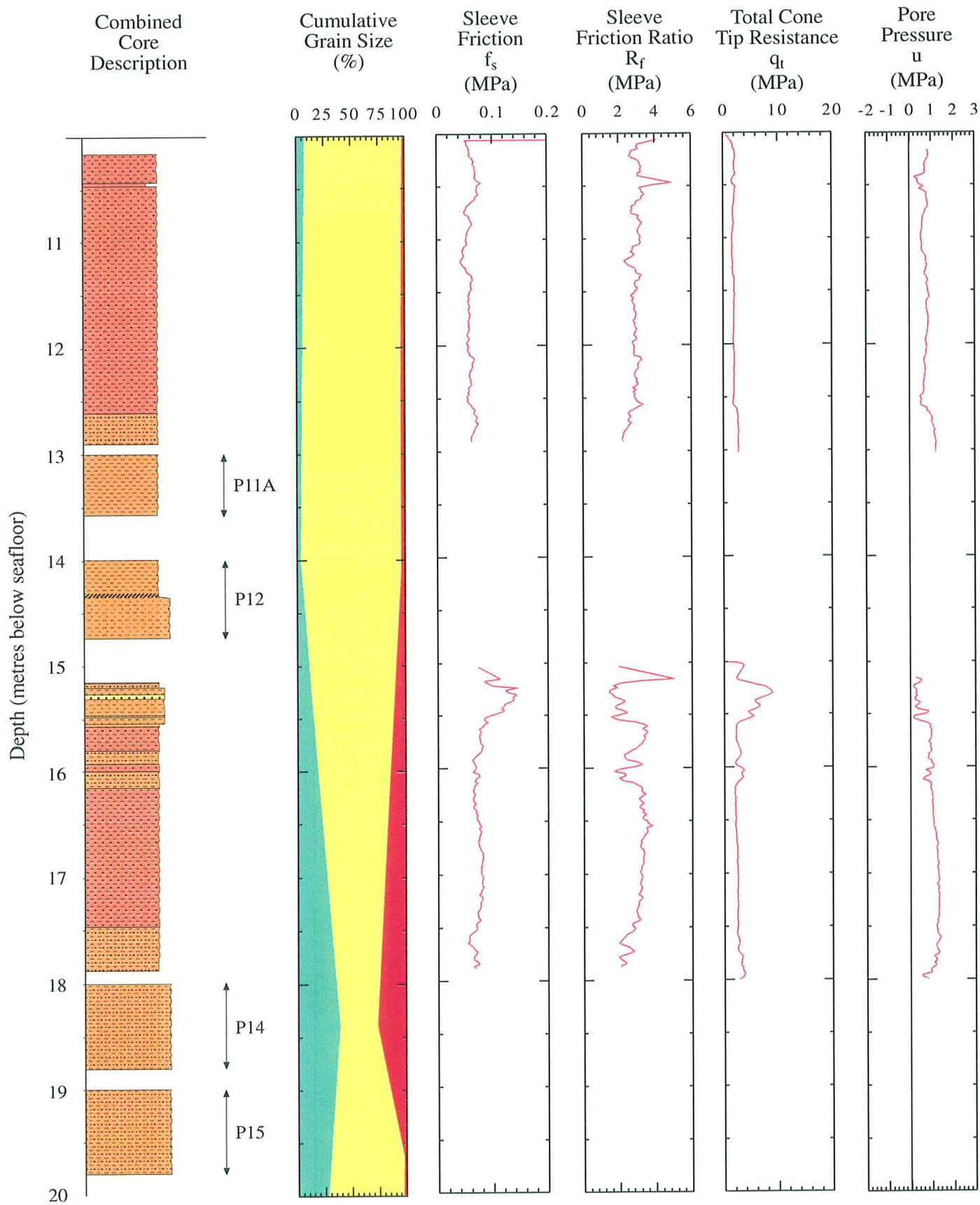
# FR4\_1B



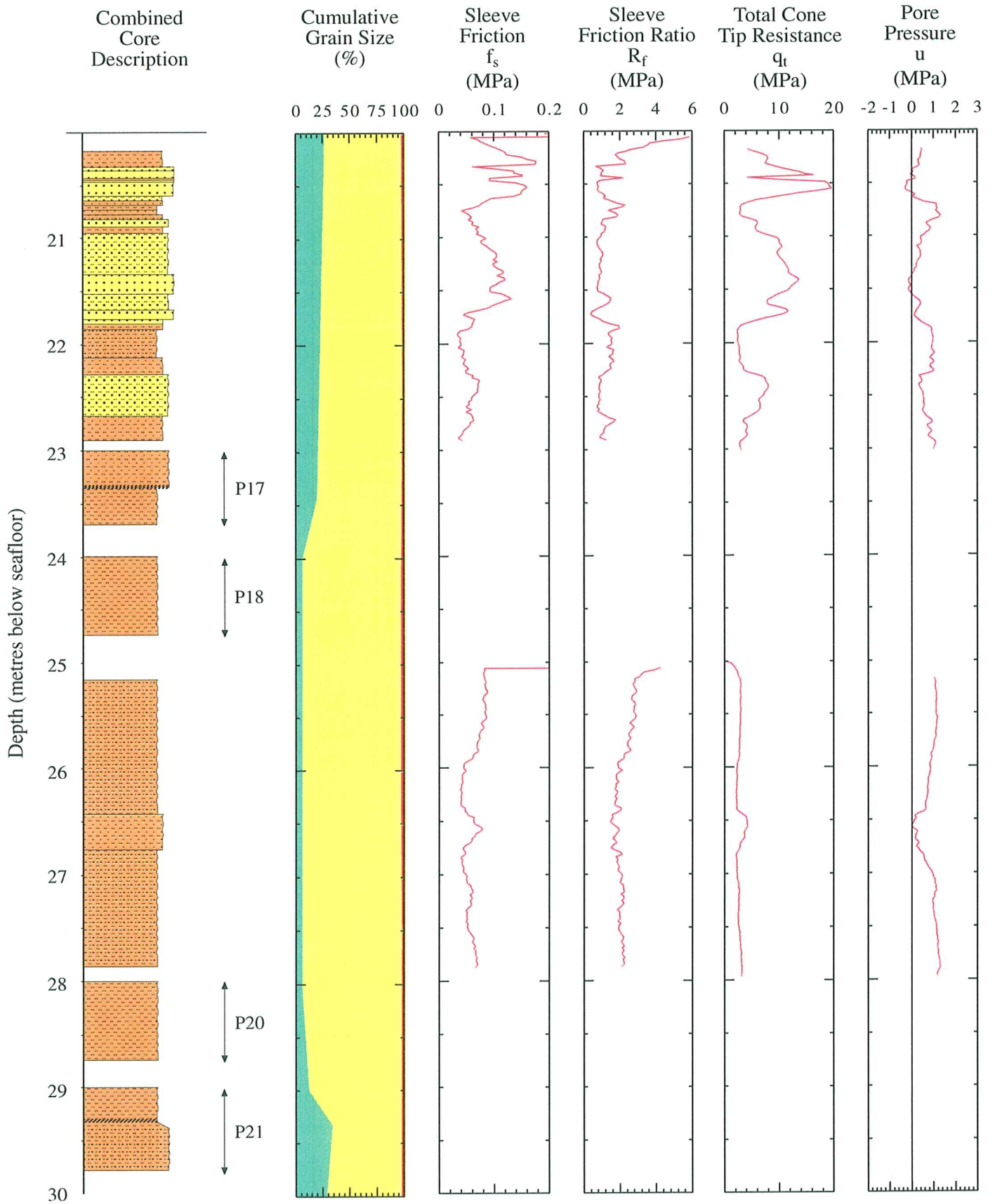
# GS1\_97



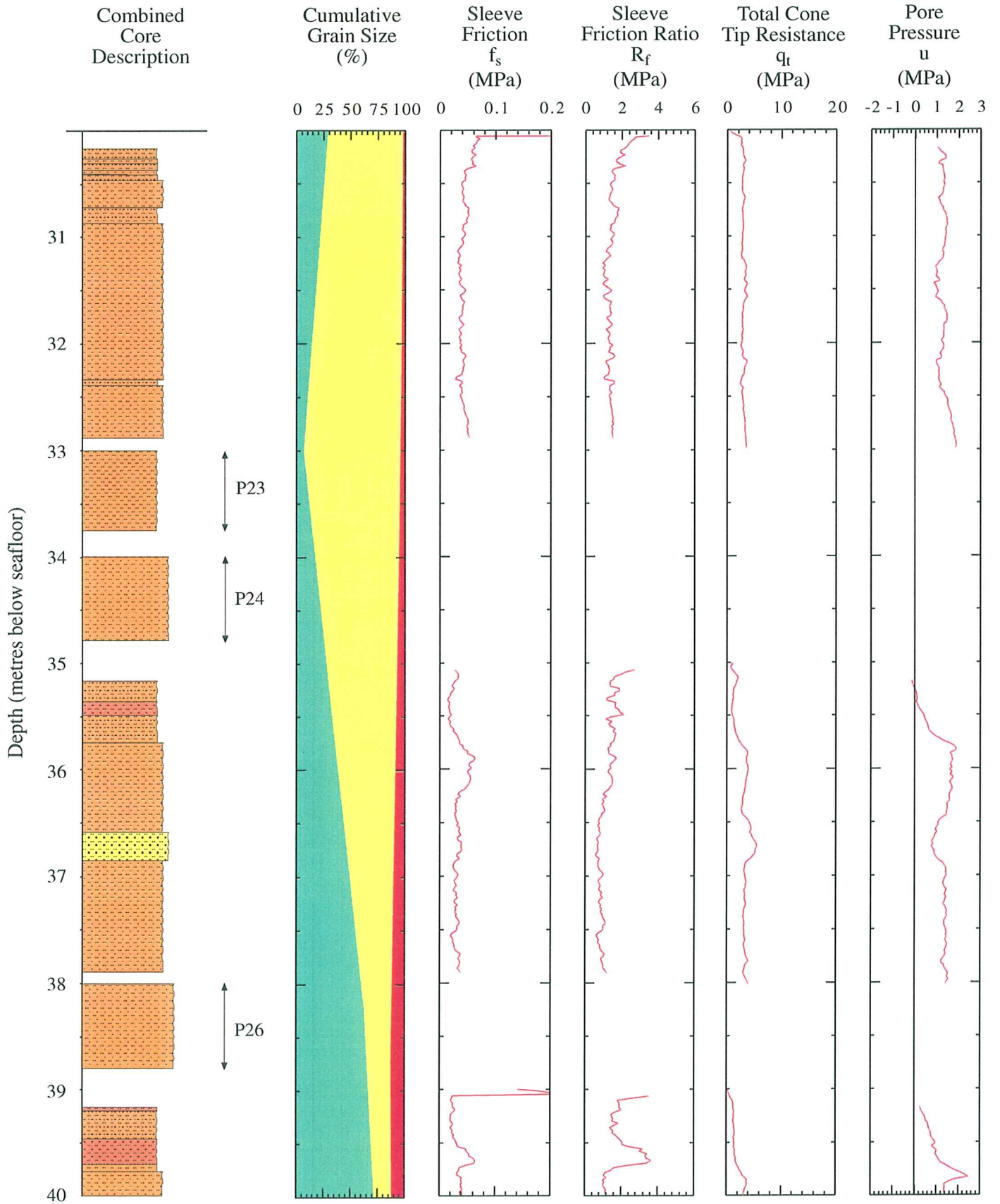
# GS1\_97



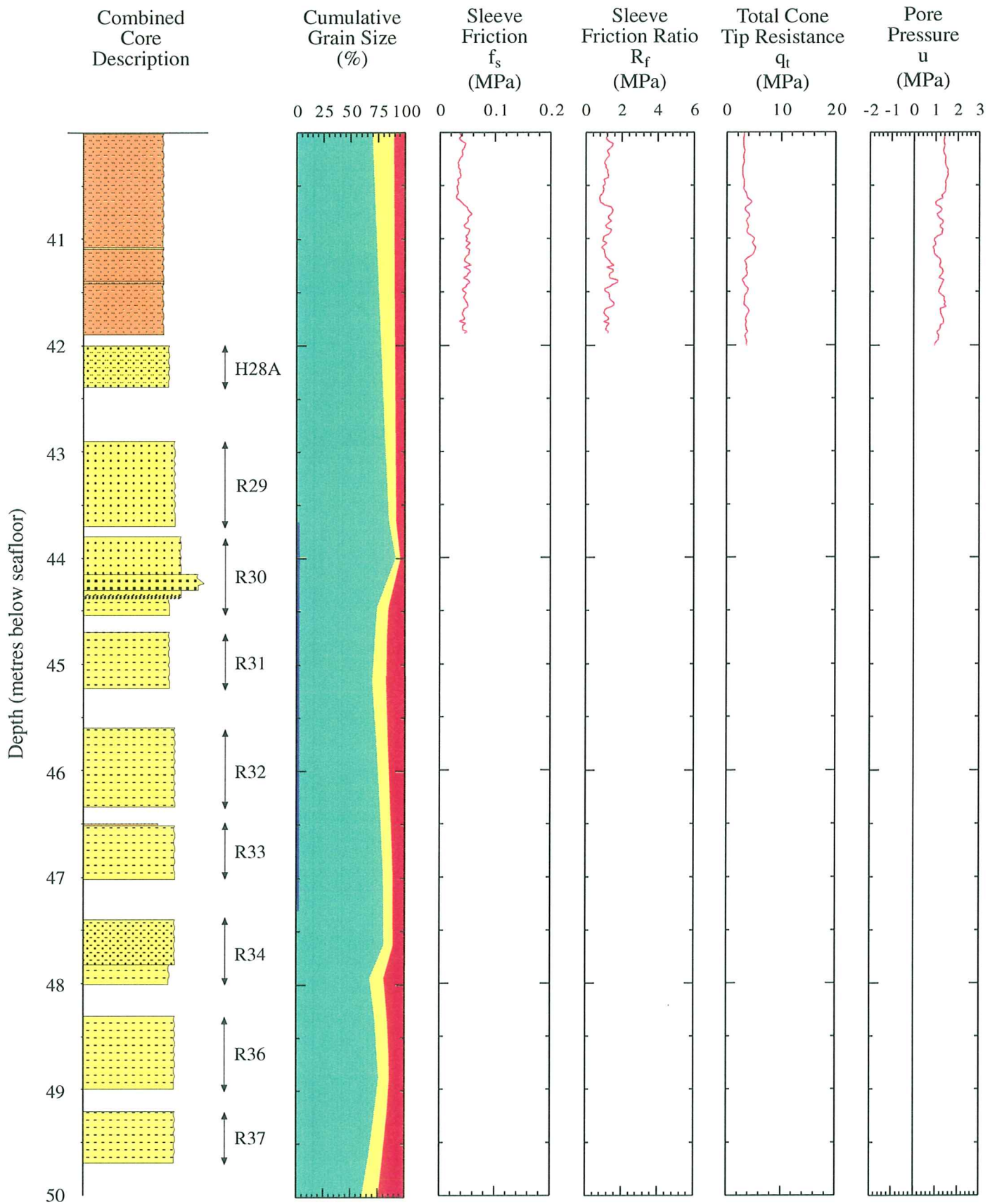
# GS1\_97



# GS1\_97

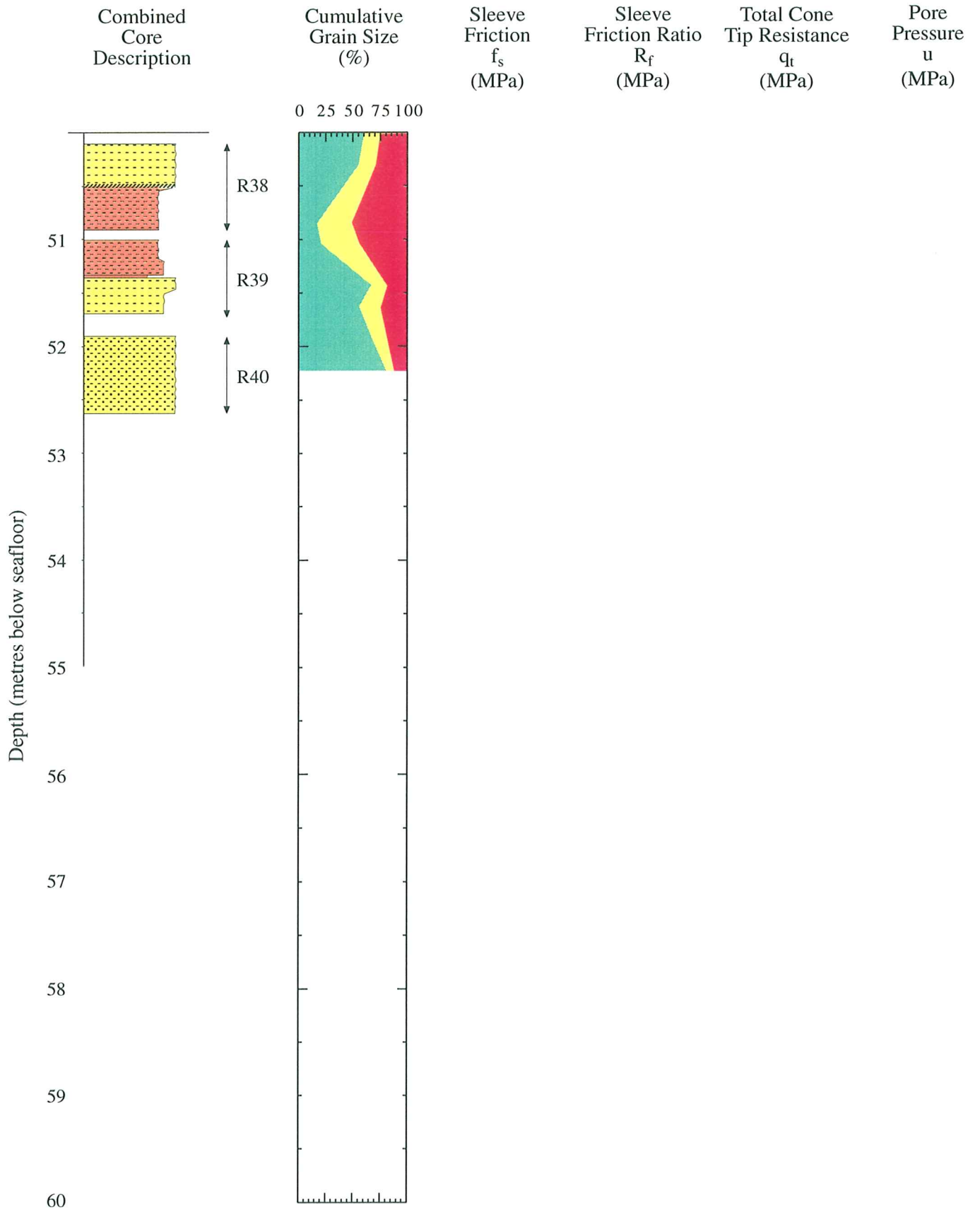


# GS1\_97

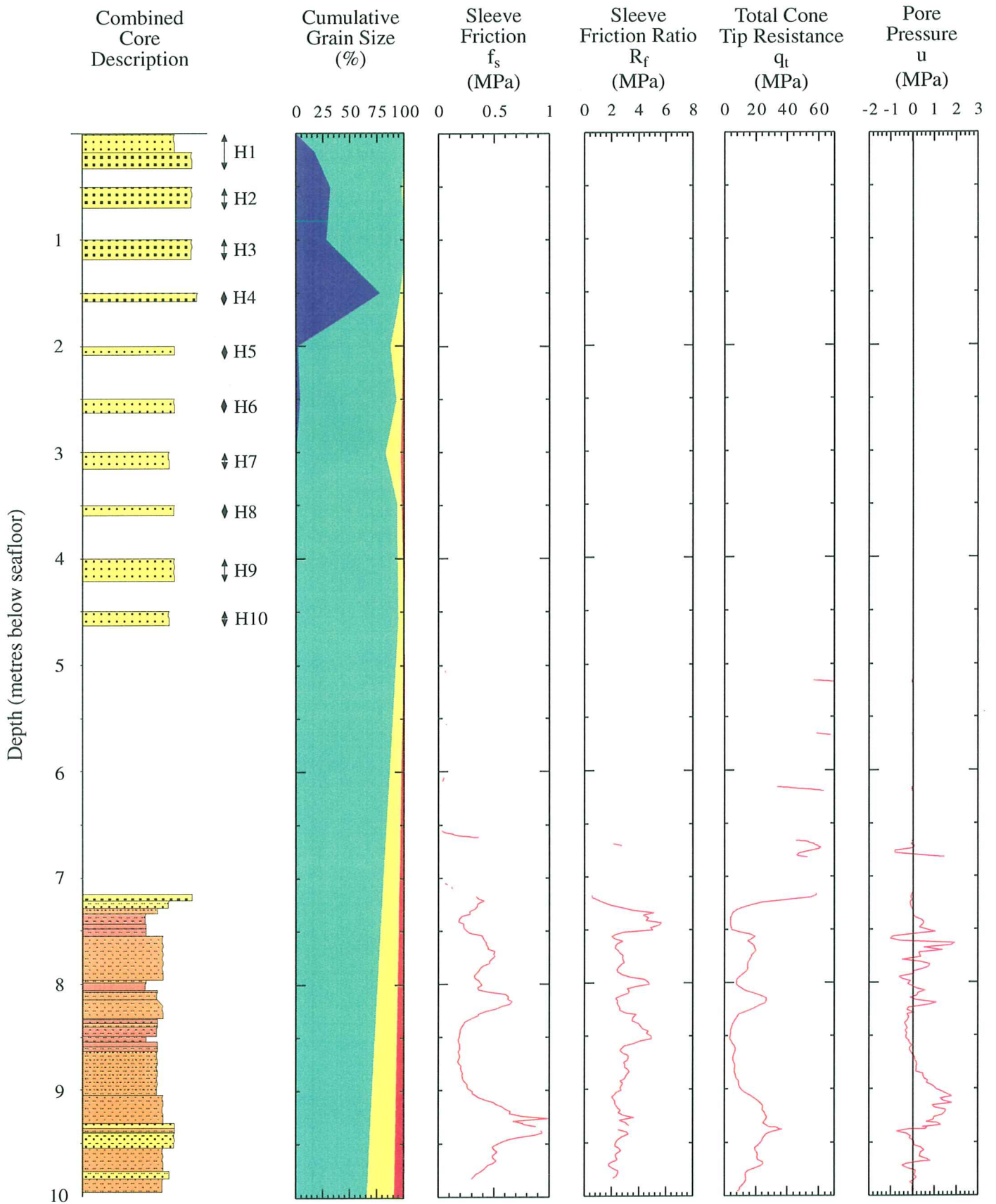




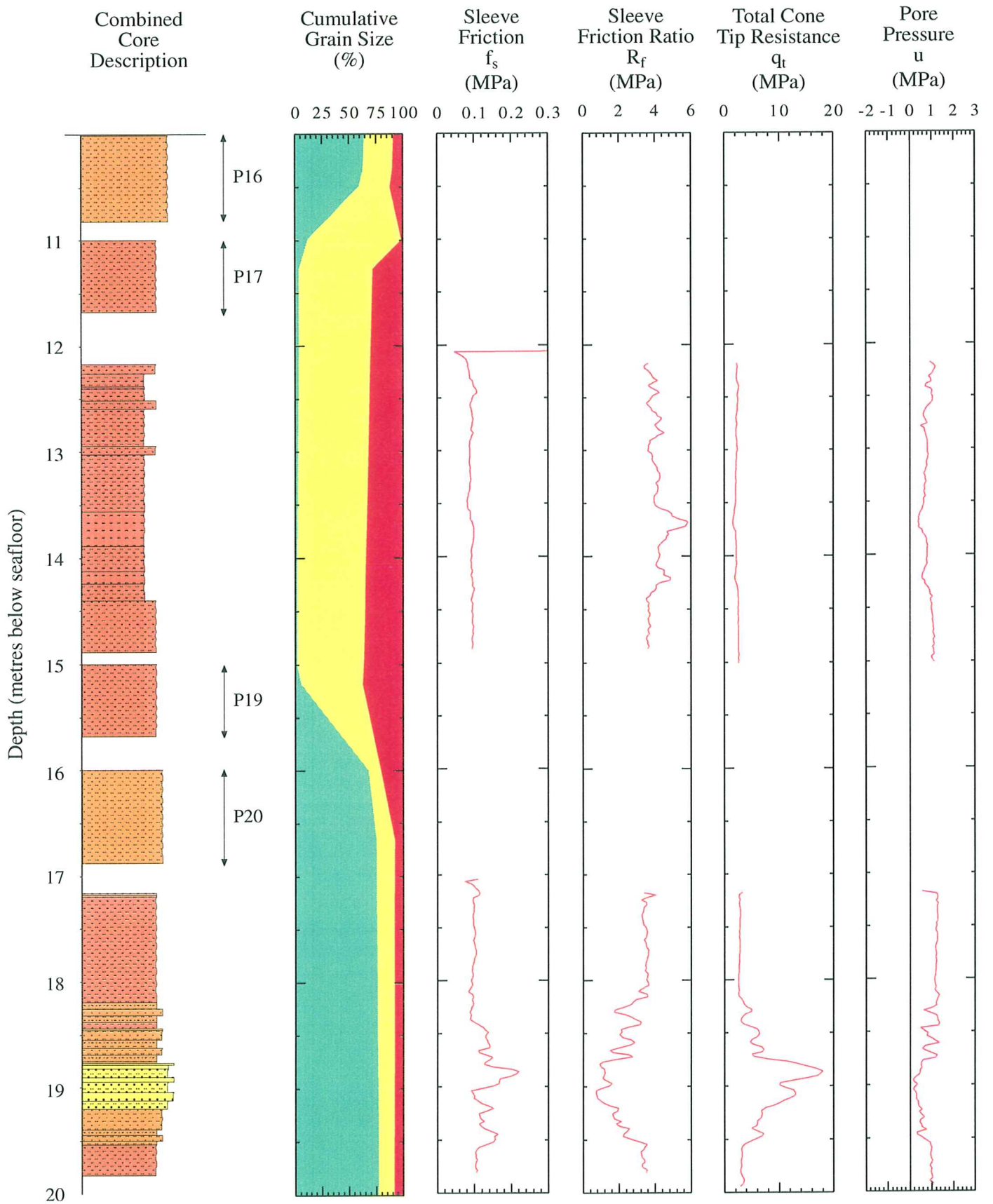
# GS1\_97



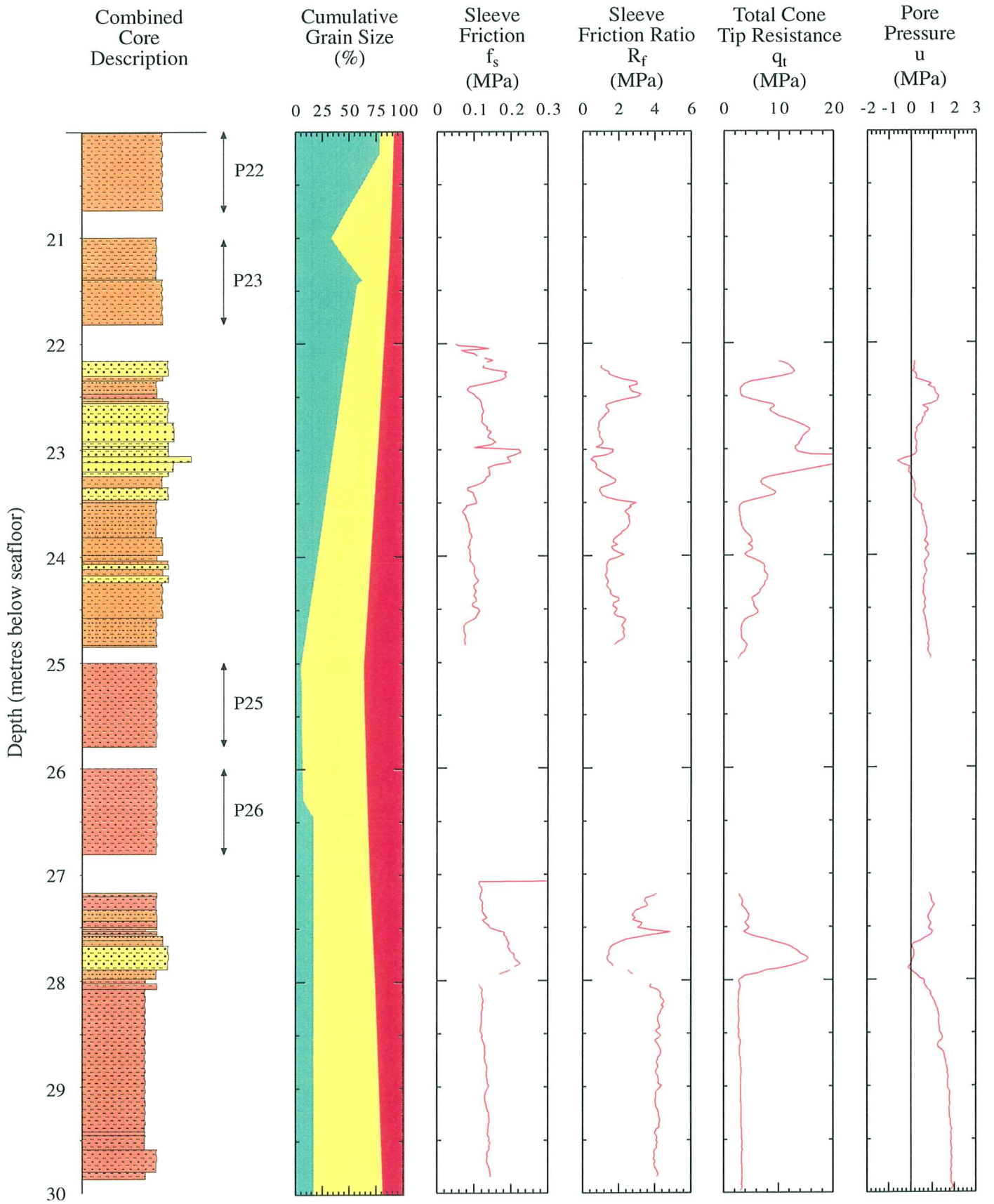
# A3\_97



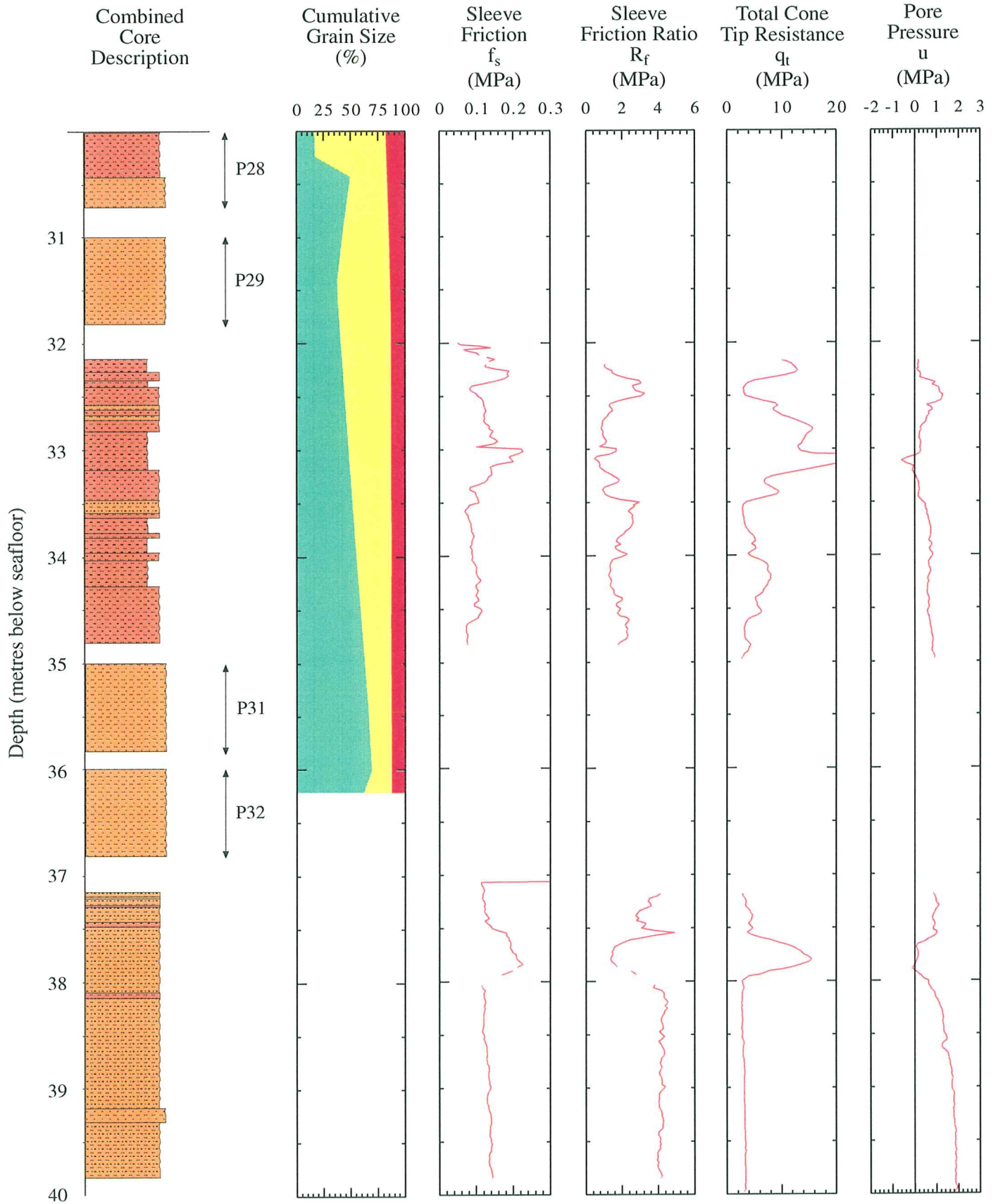
# A3\_97



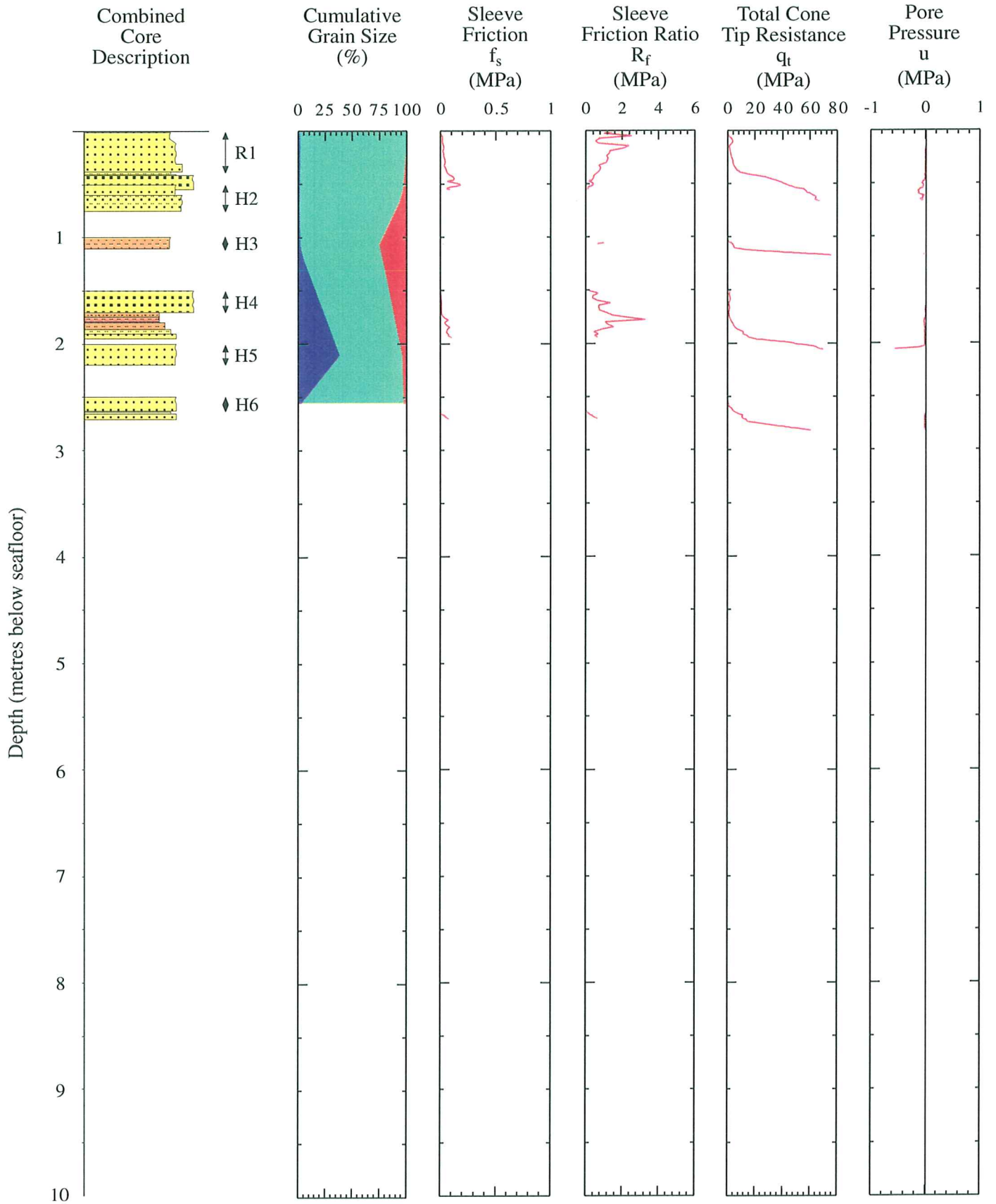
# A3\_97



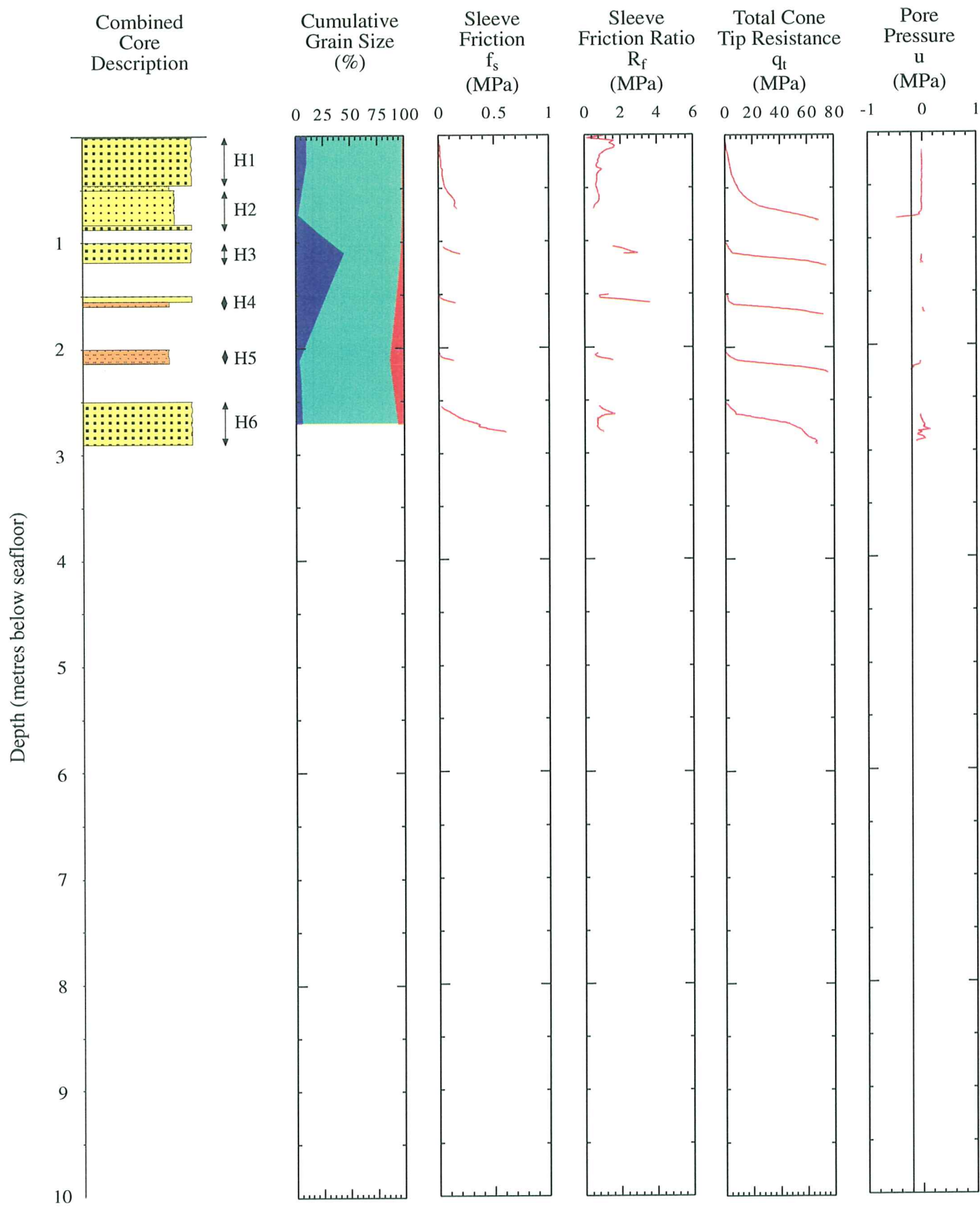
# A3\_97



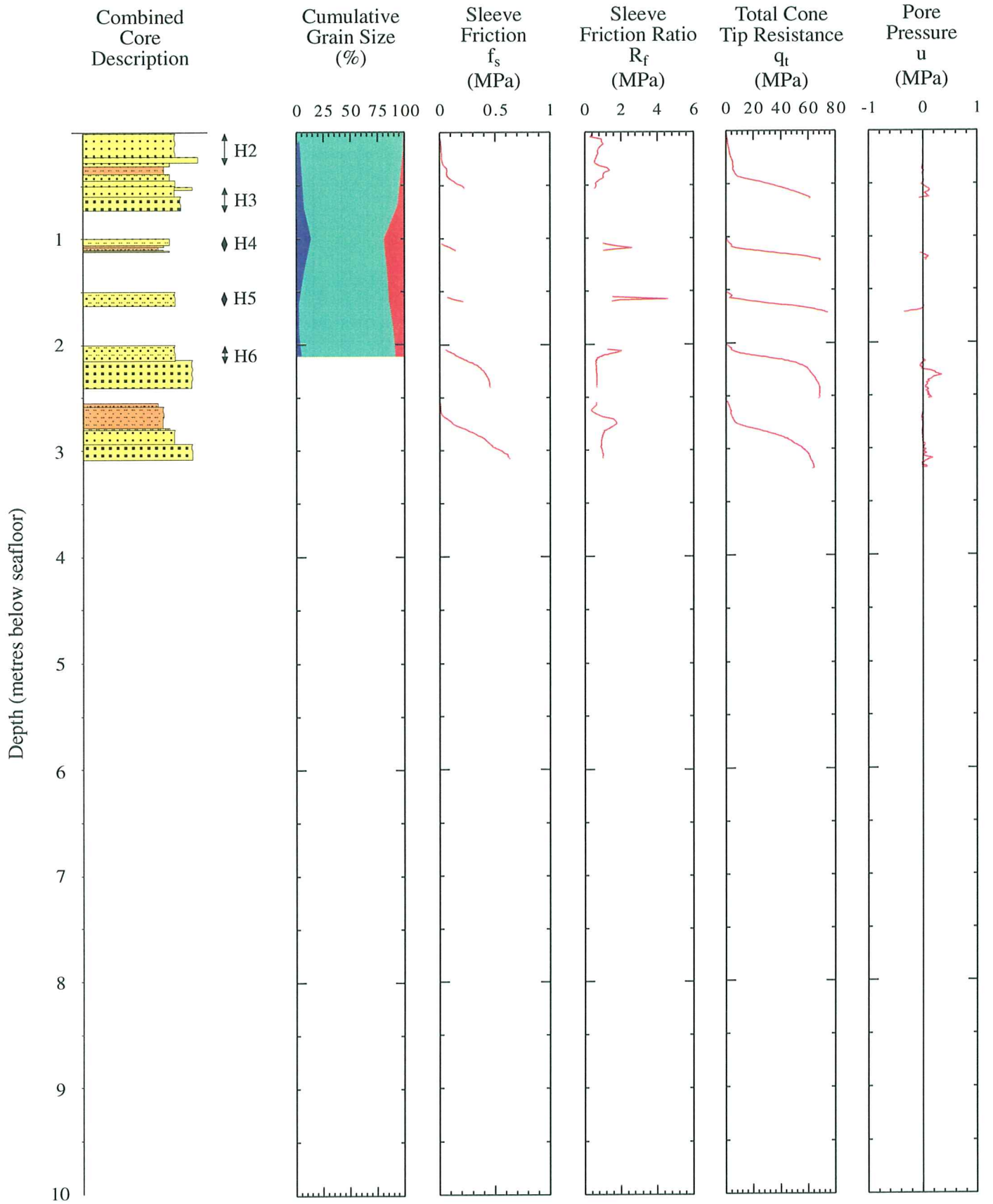
# FPSO\_B



# FR1\_1B

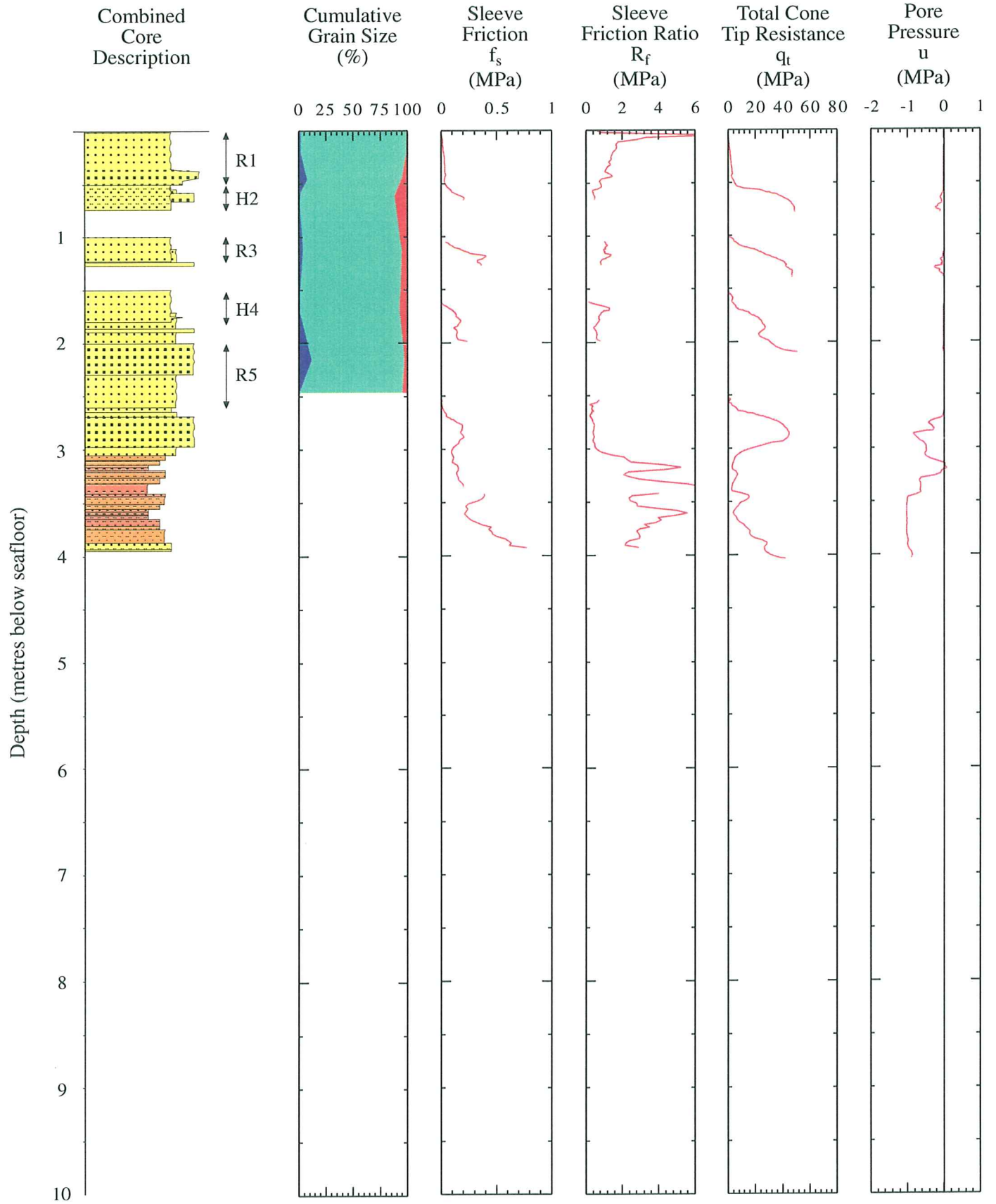


# FR1\_3B





# FR4\_1B



## Appendix 1

































97 Norskald :Terra Nova

Borehole: FE1-97 Glory Hole

Sample No.	Depth (m)	Book Length (m)	Photo Length (m)	Tiff filename	Comments
h2	-	-	-	-	no image
h3	1.0	0.08	0.08	fel-97h3	
	1.0			" h3a	" hard pan "
	1.0			" h3b	" " "
h5	-	-	-	-	no image
h6	1.5	?	-0.03	fel-97h6	piece of "hardpan" at top
h7	2.0	~0.10	?	" h7	" " " "
h8	2.5	~0.10	?	" h8	very disturbed - Jacques says softened "hardpan"
h9	3.0	0.30	~0.10	" h9	cuttings ?
h10	3.5	0.25		" h10	"
h11	4.0	0.10	~0.11	" h11	
h12	-	-	-	-	no image
h14	5.5	0.05	0.05	fel-97h14	
h15	6.0	0.15	0.15	" h15	cuttings on top ?
p16	-	-	-	-	no recovery
h17	6.5	0.40	0.43	fel-97h17	labelled as h18(b) but depth says 6.5 - relabelled as 17
h18	7.0	0.10	0.40?	" h18	cuttings ?
h19	7.5	0.24	0.25	" h19	labelled in book as h18 but h19 on image
p20	8.0	0.10	0.20	" p20	
p21	8.5	0.13	0.20-0.3	" p21	labelled "hardpan" in image
p22	8.5 ?	0.09	0.12	" p22	" " "
p24	10.0	0.24	0.25	" p24	
p26	14.0	0.62	0.60	" p26	missing top & bottom of image
p27	15.0	0.80	0.60	" p27	" " " "
p29	19.0	0.72	0.60	" p29	" " " "
p30	20.0	0.73	0.60	" p30	" " " "
p32	24.0	0.80	0.60	" p32	" " " "
p33	25.0	0.67	0.60	" p33	" " " "
p35	27.0	0.73	0.60	" p35	labelled p34 by mistake
p37	31.0	0.79	0.60	" p37	
p38	32.0	0.27	0.25	" p38	missing bottom of image
p40	36.0	0.68	0.6-0.65	" p40	missing top & bottom of image
p41	37.0	0.65	"	" p41	" " " "



97 Norskald :Terra Nova

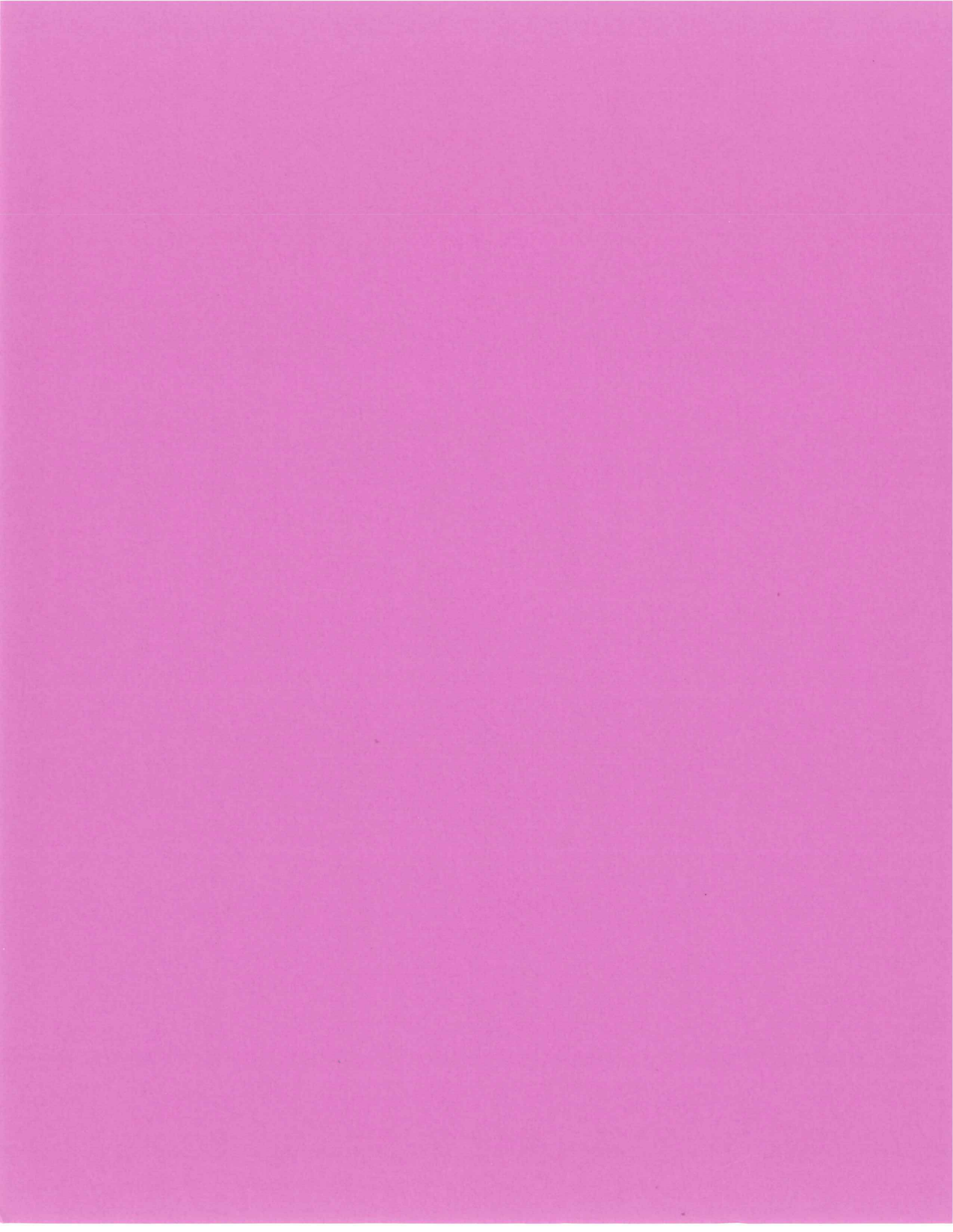
Borehole: GSI-97 Glory Hole upsplit and split cores.

Sample No.	Depth (m)	Book Length (m)	Photo Length (m)	Tiff filename	Comments
r2	0.0	0.29	0.37	gsi-97r2	
p3	1.0	0.4-0.5	0.5-0.6	" p3	missing top of image - disturbed
h4	1.5	0.12	0.20	" h4	labelled as 1.5 redo.
p5	3.0	0.40	0.60	" p5	missing bottom of image
p6	4.0	0.57	0.60	" p6	" " " " - cuttings?
p8	8.0	0.62	0.65	" p8	" " " "
p9	9.0	0.66	0.70	" p9	missing bottom of image
p11a	13.0	0.57	0.60	" p11a	disturbed sample
p12	14.0	0.74	0.75	" p12	missing top & bottom of image
p14	18.0	0.80	0.75	" p14	" " " " "
p15	19.0	"	"	" p15	" " " " "
p17	23.0	0.70	0.75	" p17	" " " " "
p18	24.0	0.74	"	" p18	" " " " "
p20	28.0	0.74	0.70	" p20	missing top of image
p21	29.0	0.78	0.70	" p21	missing top & bottom of image
p23	33.0	0.75	0.75	" p23	" " " " "
p24	34.0	0.78	0.82-0.90	" p24	" " " " "
p28	-	-	-	-	no recovery
Splitcore begins			GSC-	Atlantic	
h28a	42.0	0.40	0.46	gsi-97h28a	disturbed core
r29	42.9	0.80	0.55	" r29(1)	
			0.80	" r29(2)	
r30	43.8	0.74	0.55	" r30(1)	
			0.74	" r30(2)	
r31	44.7	0.53	0.56	" r31	
r32	45.6	0.74	0.50	" r32(1)	missing top of image.
			0.73	" r32(2)	
r33	46.5	0.51	0.54	" r33	
r34	47.4	0.60	0.64	" r34	missing top of image
r36	48.3	0.68	0.64	" r36	" " " "
r37	49.2	0.49	0.50	" r37	
r38	50.10	0.80	0.40	" r38(1)	
			0.51	" r38(2)	









# Legend

## Unified Soil Classification



GW - well graded gravels, gravel sand mixtures, little or no fines



SW - poorly graded gravels, gravel sand mixtures, little or no fines



SP - poorly graded sands, gravelly sand, little or no fines



SM - silty sands, sand silt mixtures



SC - clayey sands, sand clay mixtures



CL - inorganic clays of low to medium plasticity, gravelly clays, sandy clays and silty clay



CH - inorganic clays of high plasticity, fat clays

## CPT Soil Classification



Gravelly sand to sand



Sand



Sand to silty sand



Sand to clayey sand



Clayey sand



Silty sand to sandy silt



Sandy silt to clayey silt



Silt



Clayey silt to silty clay



Silty clay to clay



Clay



Very stiff fine grained

## Grain Size Analysis



Gravel



Sand



Silt/Clay



Silt



Clay



# Legend

## Contacts

———— Sharp                      ////////////// Gradational                      \*\*\*\*\* Bioturbated

## Physical Structures

▬ - Graded Bedding                      ▬ - Reverse Graded Bedding

## Lithologic Accessories

◆	Cobble	⋯	Sand Lenses	☉☉☉	Shell Fragments
•	Pebble	- - - - -	Silty/Clay Lenses	☞☞	Wood Fragments
◆◆◆◆	Gravel			◆◆◆◆	Organic Black Flecks
○ ○ ○ ○	Pebbles/Granules			Py	Pyritized Worm Burrow

## Core Disturbance

| Slightly Disturbed                      } Very Disturbed

## Bioturbation

■ Abundant                      ▨ Common                      ▩ Moderate                      ▫ Rare                      □ Barren

## *Legend*

### **Subsamples**

d	JMGI density
w	JMGI water content
gs	JMGI grain size
pp	JMGI pocket penetrometer
t	JMGI torvane
Gb	GSC-Atlantic bulk
Gf	GSC-Atlantic foram
Ggs	GSC-Atlantic grain size

## Appendix 3



# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
6          7          8          9          10	<div style="font-size: small;">                     cobble                      pebble                      granule                      sand                      silt                      clay                 </div>					<div style="font-size: x-small;">                     w                      m                      v                      p                      s                 </div>			<div style="font-size: small;">                     Sand seams up to 5 mm.                               Sand seams up to 5 mm.                 </div>
							<div style="font-size: x-small;">                     gs                      w                 </div>	<div style="font-size: small;">                     dk gn GY                         dk gn GY                 </div>	

# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="font-size: small;">                     cobble                      pebble                      granule                      sand                      silt                      clay                 </div>						<div style="font-size: x-small;">                     w                      m                      v                      p                      bi                 </div>			
-11           -12           -13 -14 -15								<div style="font-size: small;">                     gs                      Gf                      gn GY                      pp                      pp                      Gf                      dk gn GY                      w                      gs                 </div>	

# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS																																																																																																																			
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 5px;">w</div> <div style="margin-bottom: 5px;">m</div> <div style="margin-bottom: 5px;">f</div> <div style="margin-bottom: 5px;">c</div> <div style="margin-bottom: 5px;">v</div> <div style="margin-bottom: 5px;">b</div> </div>			<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;">dk gn GY</div> <div style="margin-bottom: 20px;">dk gn GY</div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div 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20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div> <div style="margin-bottom: 20px;"> </div>	<div style="margin-bottom: 20px;"> </div>

# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS		
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v fmc v</p> </div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <p>w</p> <p>cl</p> <p>sp</p> <p>sb</p> </div>			<div style="display: flex; flex-direction: column;"> <div style="margin-bottom: 10px;"> <p>gs w</p> </div> <div style="margin-bottom: 10px;"> <p>Gf</p> </div> <div style="margin-bottom: 10px;"> <p>gs w</p> </div> <div style="margin-bottom: 10px;"> <p>pp t w</p> </div> <div style="margin-bottom: 10px;"> <p>Gf</p> </div> </div>	<div style="display: flex; flex-direction: column;"> <div style="margin-bottom: 10px;"> <p>dk gn GY</p> </div> <div style="margin-bottom: 10px;"> <p>dk gn GY</p> </div> </div>	<div style="display: flex; flex-direction: column;"> <div style="margin-bottom: 10px;"> <p>Distinct pockets and lenses (up to 25 mm wide) of fine to medium sand throughout.</p> </div> <div style="margin-bottom: 10px;"> <p>Dark greenish grey clay with sand.</p> </div> </div>
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;">-21</div> <div style="margin-bottom: 10px;">-22</div> <div style="margin-bottom: 10px;">-23</div> <div style="margin-bottom: 10px;">-24</div> <div style="margin-bottom: 10px;">-25</div> </div>											



# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v fmc v</p> </div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <p>w</p> <p>gs</p> <p>fb</p> </div>			<div style="display: flex; flex-direction: column;"> <div style="margin-bottom: 10px;"> <p>Dark greenish grey clay with minor sand.</p> </div> <div style="margin-bottom: 10px;"> <p>Dark grey clay with minor sand.</p> <p>29.13 - 29.30 sandy clay (CH) to clay (CH).</p> <p>29.32 -29.78 sandy clay (CH).</p> <p>Trace of coarse sand.</p> </div> </div>
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;">-26-</div> <div style="margin-bottom: 10px;">-27-</div> <div style="margin-bottom: 10px;">-28-</div> <div style="margin-bottom: 10px;">-29-</div> <div style="margin-bottom: 10px;">-30-</div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>w</p> <p>Gf</p> <p>gs</p> </div> <div style="margin-bottom: 10px;"> <p>Gf</p> <p>d</p> <p>gs</p> <p>w</p> </div> </div>	<div style="display: flex; flex-direction: column;"> <div style="margin-bottom: 10px;"> <p>dk gn GY</p> </div> <div style="margin-bottom: 10px;"> <p>dk GY</p> </div> </div>		

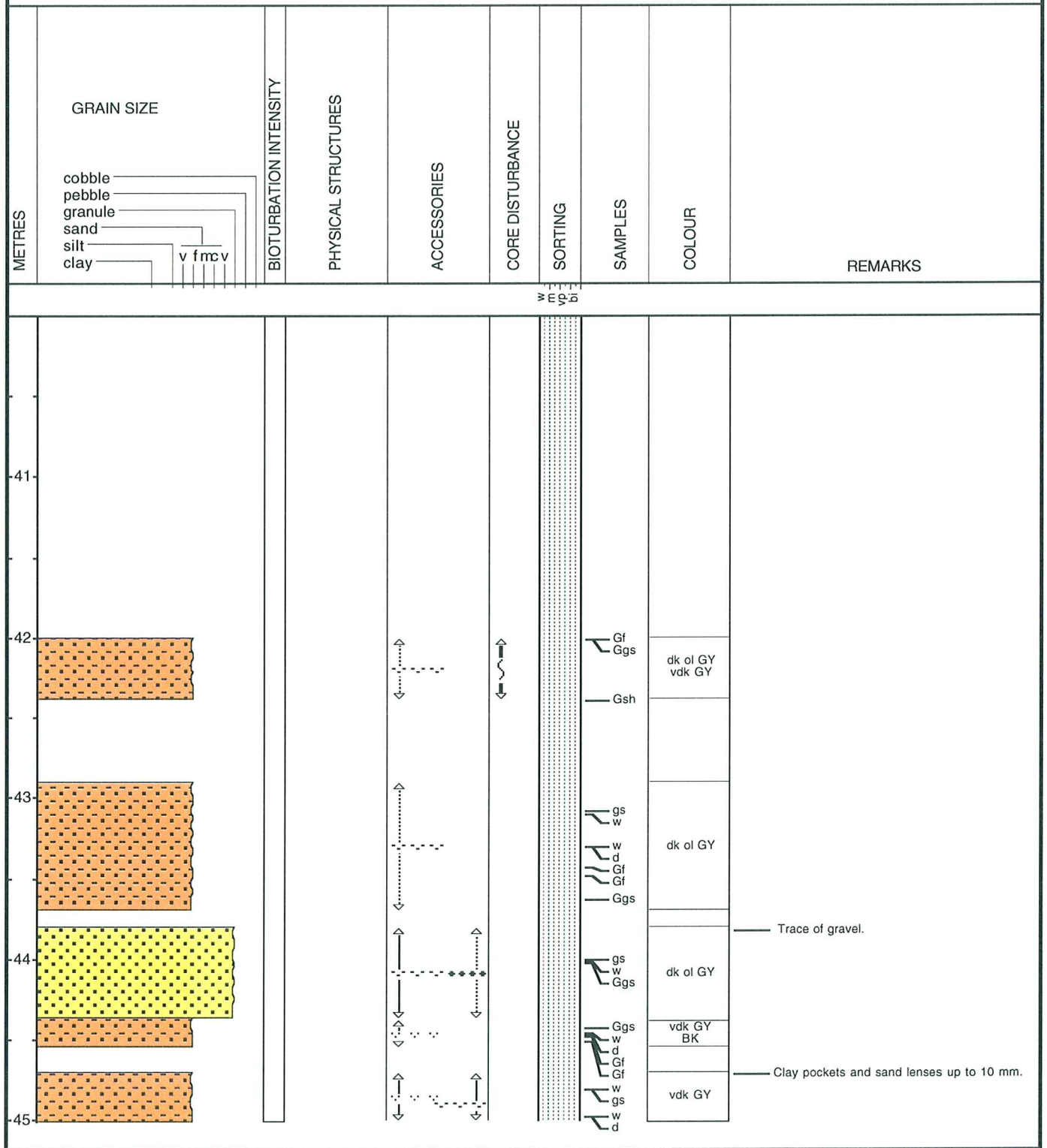
# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v fmc v</p> </div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <p>w</p> <p>m</p> <p>vp</p> <p>b</p> </div>			
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;">-31-</div> <div style="margin-bottom: 10px;">-32-</div> <div style="margin-bottom: 10px;">-33-</div> <div style="margin-bottom: 10px;">-34-</div> <div style="margin-bottom: 10px;">-35-</div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>w</p> <p>Gf</p> </div> <div style="margin-bottom: 10px;"> <p>dk gn GY</p> </div> <div style="margin-bottom: 10px;"> <p>dk GY</p> </div> <div style="margin-bottom: 10px;"> <p>w</p> <p>Gf</p> </div> </div>		<p>Dark greenish grey clay with minor sand.</p>	

# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> </div>									
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;">-36</div> <div style="margin-bottom: 10px;">-37</div> <div style="margin-bottom: 10px;">-38</div> <div style="margin-bottom: 10px;">-39</div> <div style="margin-bottom: 10px;">-40</div> </div>								<div style="border: 1px solid black; padding: 5px; text-align: center;">dk GY</div>	

# GS1\_97 Unified Soil Classification



# GS1\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
	cobble pebble granule sand silt clay v fmc v								
-46-				↑ ↓		w m v p b	Gf Gf Ggs	vdk GY	
-46-				↑ ↓			w gs w d Ggs Gf Gf	dk ol GY vdk GY	
-47-				↑ ↓			w d Gf Gf gs Ggs	dk ol GY dk GY	
-48-							w d Ggs Gf Gf w gs Ggs	dk ol GY vdk GY	
-49-							Ggs w d Gf Gf Ggs w gs	vdk GY	
-50-							w d Ggs Gf Gf w gs	vdk GY	



# A3\_97 Unified Soil Classification

	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
METRES									
5				↑ ↓		w f p b	d w gs Gb	ol GY	Gravel at the seafloor. Fine shell fragments.
4				∅∅∅			w Gb	dk GY	Sand with gravel and silt. Numerous shell fragments up to 5 mm.
3				∅∅∅			w Gb	dk GY	> 50 mm gravel-probably broken from a cobble.
2				∅∅∅			w Gb	dk GY	Sand with silt and gravel, numerous shell fragments.
1				∅∅∅			w Gs d	dk GY	Shell fragments up to 5 x 10 mm.
0				∅∅∅			Gb	dk GY	
-1				∅∅∅			w Gs d	dk GY	
-2				∅∅∅			Gb	dk GY	
-3				∅∅∅			w Gs d	dk GY	
-4				∅∅∅			Gb	dk GY	Frequent fine shell fragments.
-5				∅∅∅			Gs d w	dk GY	

## A3\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <span style="font-size: small;">cobble</span> _____</div> <div style="margin-bottom: 5px;"> <span style="font-size: small;">pebble</span> _____</div> <div style="margin-bottom: 5px;"> <span style="font-size: small;">granule</span> _____</div> <div style="margin-bottom: 5px;"> <span style="font-size: small;">sand</span> _____</div> <div style="margin-bottom: 5px;"> <span style="font-size: small;">silt</span> _____</div> <div style="margin-bottom: 5px;"> <span style="font-size: small;">clay</span> _____</div> </div> <div style="margin-top: 10px;"> <span style="font-size: x-small;">v f m c v</span> </div>									







# A3\_97 Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> </div>									<p>Clay seams up to 20 mm wide.</p> <p>Vertical sand seam up to 15 mm.</p> <p>Clay partings.</p> <p>Occasional sand seams up to 10 mm wide.</p>
<p>21</p> <p>22</p> <p>23</p> <p>24</p> <p>25</p>									<p>vdk GY</p> <p>vdk GY</p>









# FR1\_1B Unified Soil Classification

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
1				∅∅∅	∅∅∅	∅∅∅	w a gs	ol GY	Infrequent fine shell fragments. NB Grain size may not show gravel but it is present - approx 10% and up to 50 mm.
2				∅∅∅	∅∅∅	∅∅∅	w a gs Gf gs	GY	Abundant shell fragments up to 10 mm. Not sure of foram subsample location.
3				∅∅∅	∅∅∅	∅∅∅	Gf	∅∅∅	"Hardpan" - weak to moderately cemented silty sand with shell fragments. Calcareous. Not sure of foram subsample location.
4				∅∅∅	∅∅∅	∅∅∅	gs a w	dk gn GY	"Hardpan" - disturbed. Strong reaction to HCL.
5				∅∅∅	∅∅∅	∅∅∅	gs a	dk GY	Dark grey sand with silt? Occasional gravel and frequent fine shell fragments.





# FR4\_1B Unified Soil Classification

	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
METRES									
0								ol GY	0 - 0.35 m fine olive grey sand coarsening to coarse sand at 0.35 m. Organic odour.
1								GY dk gn GY ol GY	0.35 - 0.46 m gradational colour change from olive grey to grey. 0.35 - 0.50 m grey calcareous silty sand with a trace of gravel ( up to 15 mm) from 0.37 to 0.46 m. Frequent fine shell fragments.
2								dk GY	0.50 - 0.74 m dark greenish grey to olive grey calcareous silty sand with numerous shell fragments ( up to 5 mm). Trace of gravel. 4x4x3 cm cobble at 0.50 m. Same general appearance as "hardpan" but not cemented.
3								dk GY	1.0 - 1.23 m Dark grey calcareous silty sand with gravel and numerous shell fragments ( up to 10 mm).
4								dk GY	1.50 - 1.55 m Dark grey calcareous silty sand with small (up to 5 mm) gravels and shell fragments. 1.55 - 1.80 m Dark grey calcareous fine to medium grained silty sand with shell fragments. 1.75 m layer of medium to coarse sand
5								dk GY	2.0 - 2.30 m Dark grey with silt and gravel. 2.3 - 2.6 m Alternating layers of dark grey fine sand with few shell fragments and dark grey fine to medium sand with a high concentration of shell fragments.

## Appendix 4



# GS1\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v f m c v</p> </div> </div>									
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>w</p> <p>m</p> <p>ps</p> <p>b</p> </div> </div>									
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>6</p> </div> <div style="margin-bottom: 10px;"> <p>7</p> </div> <div style="margin-bottom: 10px;"> <p>8</p> </div> <div style="margin-bottom: 10px;"> <p>9</p> </div> <div style="margin-bottom: 10px;"> <p>10</p> </div> </div>									<div style="margin-bottom: 10px;"> <p>gs</p> <p>w</p> </div> <p>dk gn GY</p> <p>Sand seams up to 5 mm.</p> <div style="margin-bottom: 10px;"> <p>w</p> </div> <p>dk gn GY</p> <p>Sand seams up to 5 mm.</p>



# GS1\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <p>w</p> <p>m</p> <p>vp</p> <p>b</p> </div>			<div style="display: flex; flex-direction: column;"> <div style="margin-bottom: 10px;"> <p>18.00 - 18.80 Clayey silty sand.</p> </div> <div> <p>Distinct pockets and lenses of fine to medium grained sand (up to 25 mm).</p> </div> </div>
<p>-16</p> <p>-17</p> <p>-18</p> <p>-19</p> <p>-20</p>							<p>dk gn GY</p> <p>dk gn GY</p>		

# GS1\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
	<div style="font-size: small;">                     cobble                      pebble                      granule                      sand                      silt                      clay                 </div>								
-21-									
-22-									
-23-									Distinct pockets and lenses of fine to medium sand throughout (up to 25 mm).
-24-									
-25-									Dark greenish grey clay with minor sand.

w  
m  
yp  
bi

gs  
w  
Gf  
gs  
w  
pp  
t  
w  
Gf

dk gn GY  
dk gn GY

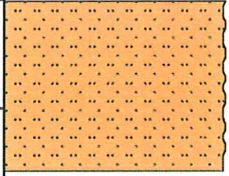
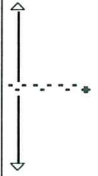
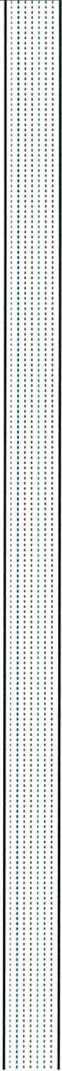



# GS1\_97 Core Description

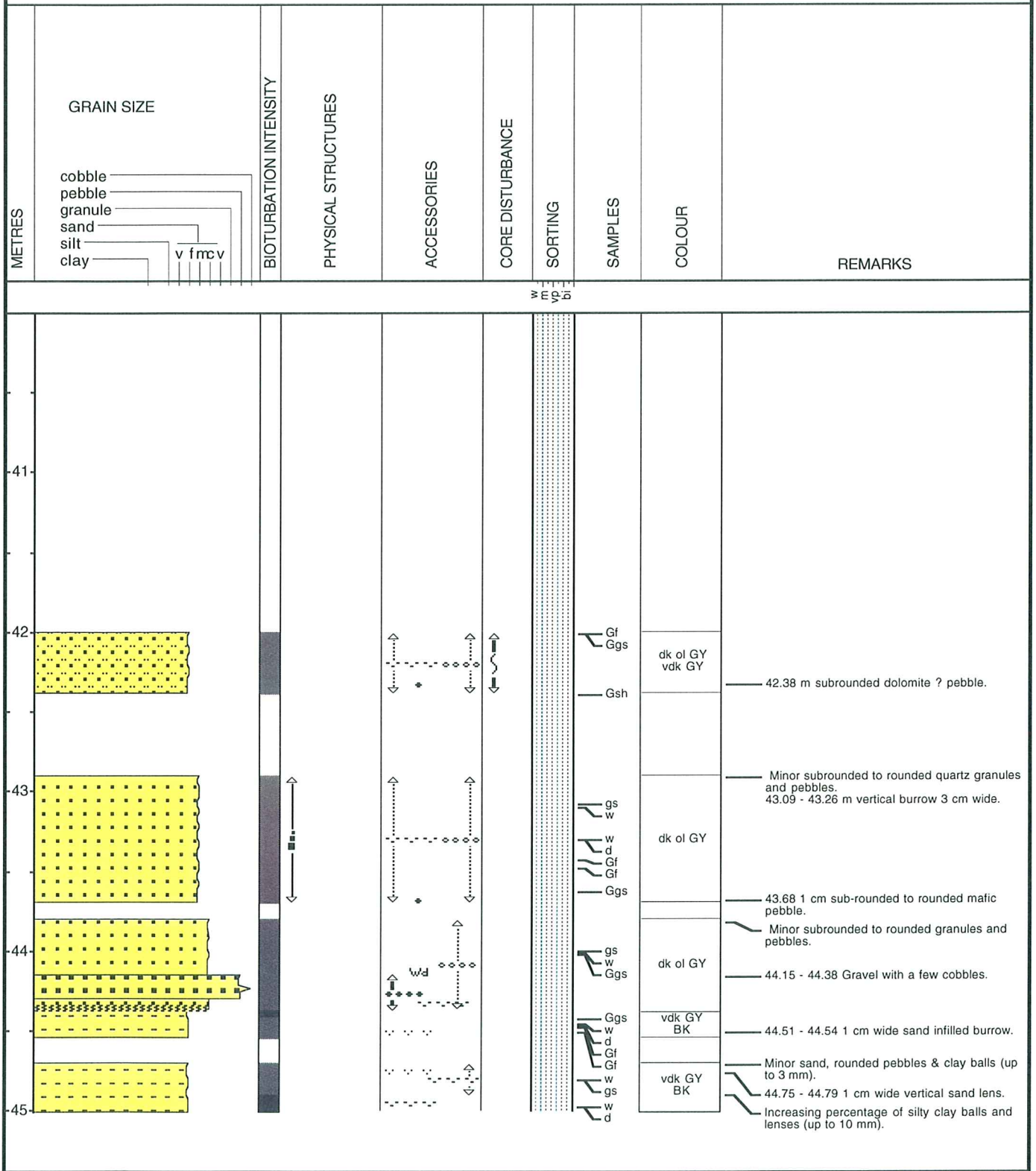
METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
	<div style="font-size: small;">                     cobble                      pebble                      granule                      sand                      silt                      clay                 </div>					w m c v bi			
-26-									
-27-									
-28-								dk gn GY	Dark greenish grey clay with minor sand.
-29-								dk GY	Dark grey clay with minor sand.
-30-									29.32 - 29.78 sandy silt. Trace of coarse sand.



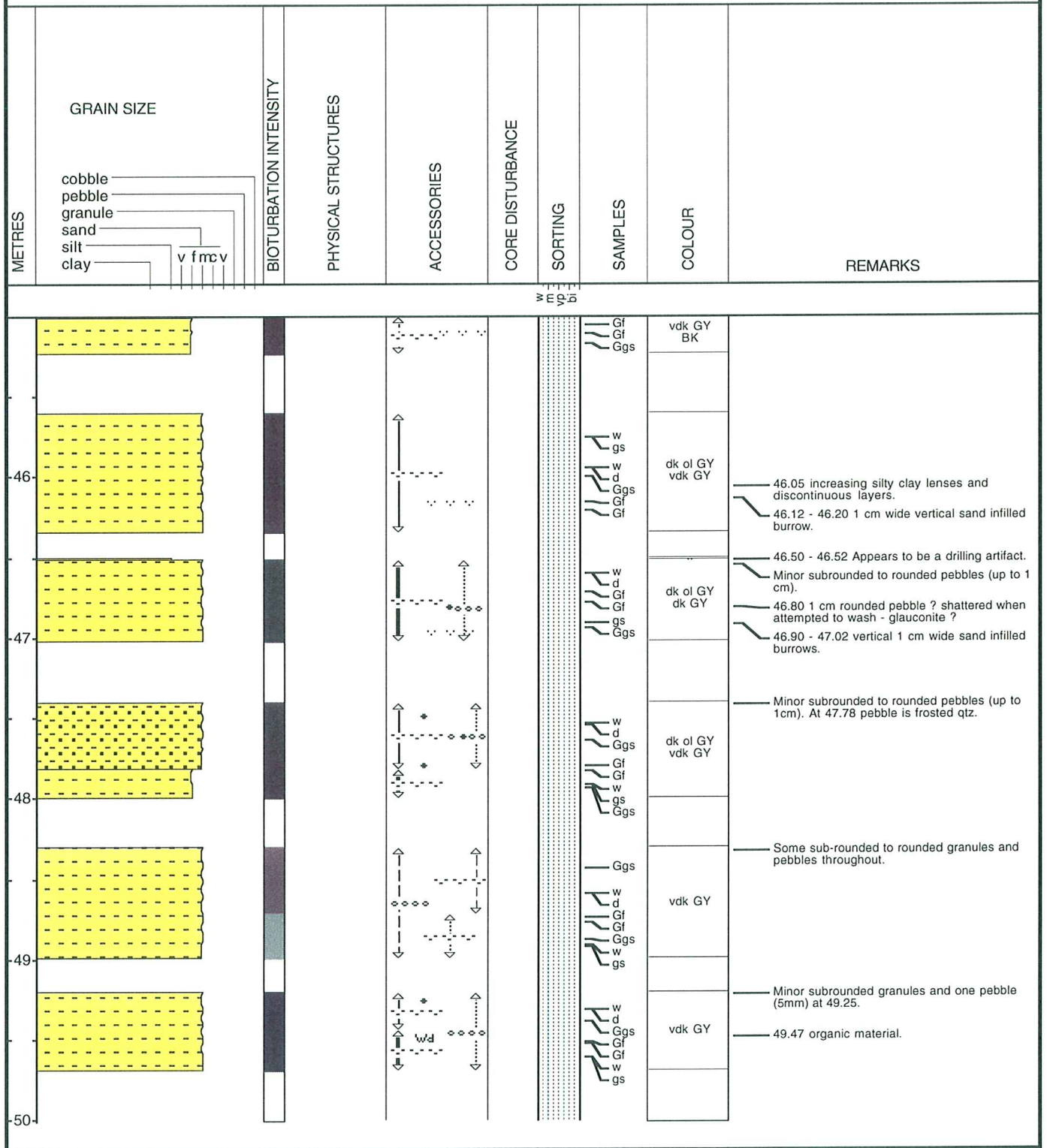
# GS1\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v fmc v</p> </div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <p>w</p> <p>m</p> <p>p</p> <p>b</p> </div>			
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;">-36</div> <div style="margin-bottom: 10px;">-37</div> <div style="margin-bottom: 10px;">-38</div> <div style="margin-bottom: 10px;">-39</div> <div style="margin-bottom: 10px;">-40</div> </div>								<p>dk GY</p>	

# GS1\_97 Core Description



# GS1\_97 Core Description





# A3\_97 Core Description

	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
METRES	cobble pebble granule sand silt clay v f m c v								
1							d w gs Gb	ol GY dk GY	Gravel at the seafloor. Fine shell fragments. Sand with gravel and silt. Numerous shell fragments up to 5 mm.
2							w Gb	dk GY	> 50 mm gravel-probably broken from a cobble.
3							w Gb	dk GY	Sand with silt and gravel, numerous shell fragments.
4							w Gb	dk GY	Shell fragments up to 5 x 10 mm.
5							w Gb	dk GY	Frequent fine shell fragments.
6							w Gb	dk GY	
7							w Gb	dk GY	
8							w Gb	dk GY	
9							w Gb	dk GY	
10							w Gb	dk GY	
11							w Gb	dk GY	
12							w Gb	dk GY	
13							w Gb	dk GY	
14							w Gb	dk GY	
15							w Gb	dk GY	

## A3\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <span style="font-size: small;">cobble</span>  <span style="font-size: small;">pebble</span>  <span style="font-size: small;">granule</span>  <span style="font-size: small;">sand</span>  <span style="font-size: small;">silt</span>  <span style="font-size: small;">clay</span> </div> <div style="margin-bottom: 10px;"> <span style="font-size: small;">v</span> <span style="font-size: small;">fmc</span> <span style="font-size: small;">v</span> </div> </div>						w m sp b			
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;">6</div> <div style="margin-bottom: 10px;">7</div> <div style="margin-bottom: 10px;">8</div> <div style="margin-bottom: 10px;">9</div> <div style="margin-bottom: 10px;">10</div> </div>									



# A3\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v fmc v</p> </div> </div>									<p style="text-align: center;">Bioturbated and dessicated.</p>
<p>11</p> <p>12</p> <p>13</p> <p>14</p> <p>15</p>						<p>w gs</p> <p>pp</p> <p>t w t pp</p> <p>pp t</p>	<p>vdk GY</p> <p>vdk GY</p>		

# A3\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v f m c v</p> </div> </div>						<div style="display: flex; flex-direction: column; align-items: center;"> <p>w</p> <p>u</p> <p>f</p> <p>sp</p> <p>b</p> </div>			<p>Trace of sand.</p>
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 20px;"> <p>16</p> </div> <div style="margin-bottom: 20px;"> <p>17</p> </div> <div style="margin-bottom: 20px;"> <p>18</p> </div> <div style="margin-bottom: 20px;"> <p>19</p> </div> <div> <p>20</p> </div> </div>							<p>pp</p> <p>w</p> <p>vdk GY</p> <p>vdk GY</p>		<p>Trace of sand.</p>

# A3\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
	cobble pebble granule sand silt clay								
-21									Clay seams up to 20 mm wide.
-22									21.0 - 21.40 sandy silt. Vertical sand seam up to 15 mm.
-23									Clay partings.
-24									
-25									Occasional sand seams up to 10 mm wide.





# A3\_97 Core Description

METRES	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
<div style="display: flex; flex-direction: column; align-items: center;"> <div style="margin-bottom: 10px;"> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> </div> <div style="margin-bottom: 10px;"> <p>v f m c v</p> </div> </div>									<p>REMARKS</p>
<p style="text-align: center;">w n p v b</p>							<p>vdK GY</p> <p>vdK GY</p>	<p>vdK GY</p>	

# FPSO\_B Core Description

	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
METRES	cobble pebble granule sand silt clay v f m c v								
1				∅∅∅		w gs d	ol GY		0.0 - 0.38 m Olive grey fine sand grading to coarse and fine at the base. Fine shell fragments increasing in percentage with depth.
2				∅∅∅		w gs d	ol GY dk GY		0.50 - 0.60 m Olive grey fine to medium sand with frequent fine shell fragments ( up to 2 mm). 0.60 - 0.75 m Dark grey calcareous fine to coarse sand with silt. Frequent shell fragments (up to 6 mm).
3				∅∅∅		w	GY		1.00 - 1.10 m Grey calcareous sand with silt and layer (1.04 - 1.055 m) of cemented dark grey silty sand (similar to FR1_3b) which can be broken apart with some force. Numerous shell fragments ( up to 10 mm). 1.04 - 1.10 m gravels (up to 2x1.5x1.2 cm) and shell fragments with some sand with silt.
4				∅∅∅		w gs	GY		1.50 - 1.70 Classified as well graded sand with gravel but 2nd attempt at this depth and highly disturbed. Numerous shell fragments.
5				∅∅∅		d w gs	dk GY		2.00 - 2.20 m Dark grey fine to medium sand with silt and gravel. Frequent fine shell fragments. Broken cobble (6.5x5.0x3.5 cm) at top of sample. Grain size analysis gives 39% gravel. 2.50 - 2.63 m Dark grey fine to medium sand with some gravel and some fine shell fragments. A piece of gravel (2.5x3x1.5 cm) that looks similar to the piece of gravel in the previous sample - could have been broken off the same cobble?







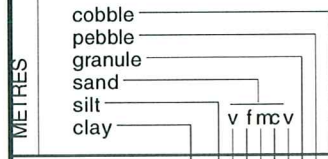
# FR4\_1B Core Description

	GRAIN SIZE	BIOTURBATION INTENSITY	PHYSICAL STRUCTURES	ACCESSORIES	CORE DISTURBANCE	SORTING	SAMPLES	COLOUR	REMARKS
METRES									
0								ol GY	0 - 0.35 m fine olive grey sand coarsening to coarse sand at 0.35 m. Organic odour.
1								GY	0.35 - 0.46 m gradational colour change from olive grey to grey.
2								dk gn GY ol GY	0.35 - 0.50 m grey calcareous silty sand with a trace of gravel (up to 15 mm) from 0.37 to 0.46 m. Frequent fine shell fragments.
3								dk GY	0.50 - 0.74 m dark greenish grey to olive grey calcareous silty sand with numerous shell fragments (up to 5 mm). Trace of gravel. 4x4x3 cm cobble at 0.50 m. Same general appearance as "hardpan" but not cemented.
4								dk GY	1.0 - 1.23 m Dark grey calcareous silty sand with gravel and numerous shell fragments (up to 10 mm).
5								dk GY	1.50 - 1.55 m Dark grey calcareous silty sand with small (up to 5 mm) gravels and shell fragments.
								dk GY	1.55 - 1.80 m Dark grey calcareous fine to medium grained silty sand with shell fragments.
								dk GY	1.75 m layer of medium to coarse sand
								dk GY	2.0 - 2.30 m Dark grey with silt and gravel.
								dk GY	2.3 - 2.6 m Alternating layers of dark grey fine sand with few shell fragments and dark grey fine to medium sand with a high concentration of shell fragments.

## Appendix 5

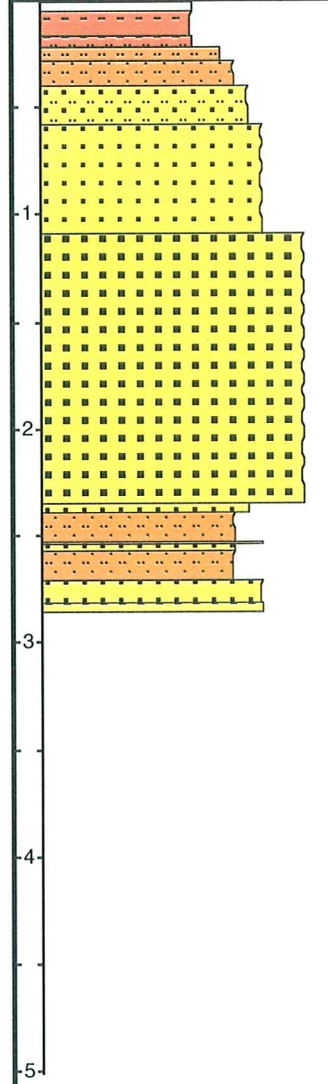
# GS1\_97 CPT Soil Classification

GRAIN SIZE



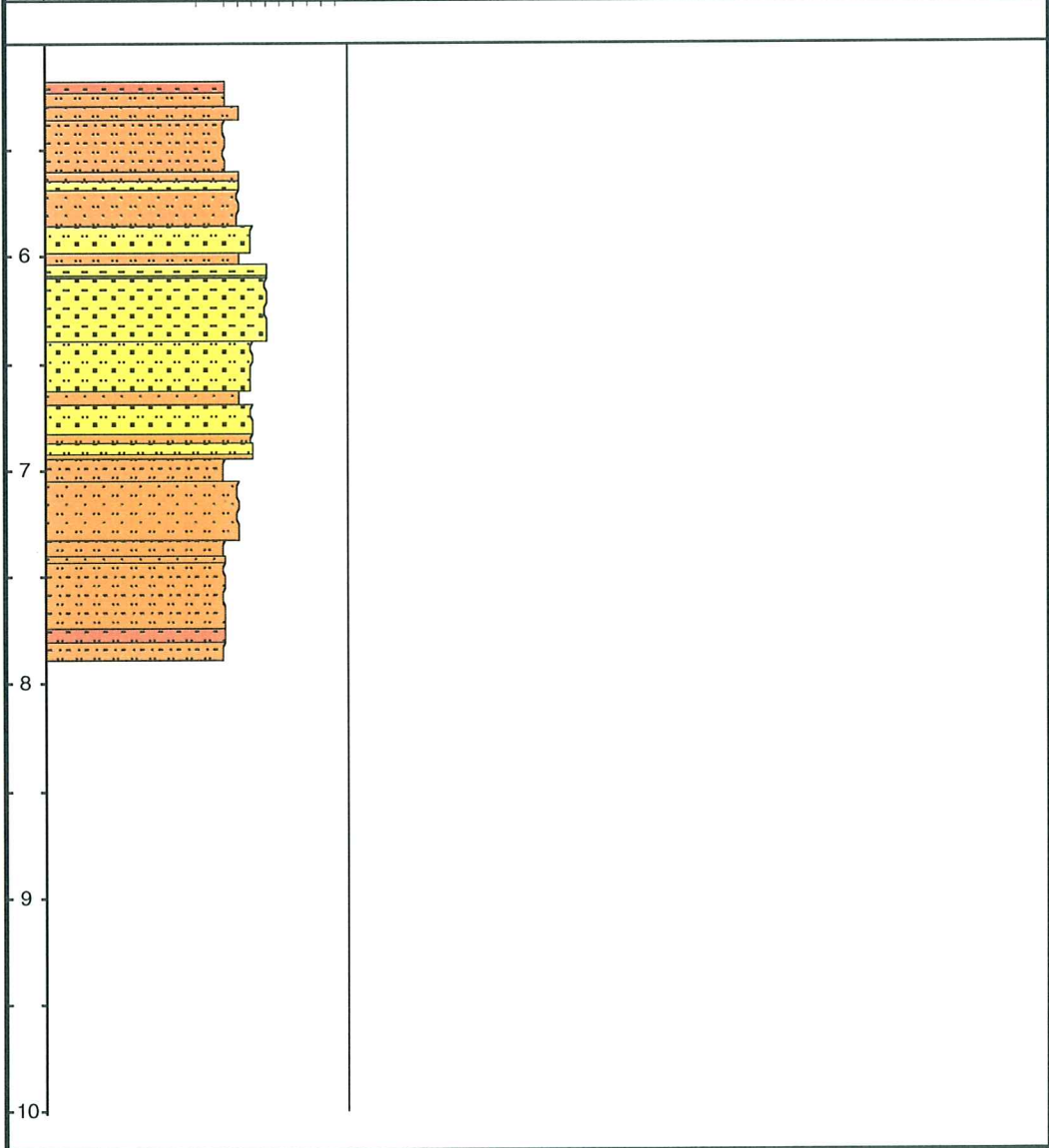
REMARKS

METRES



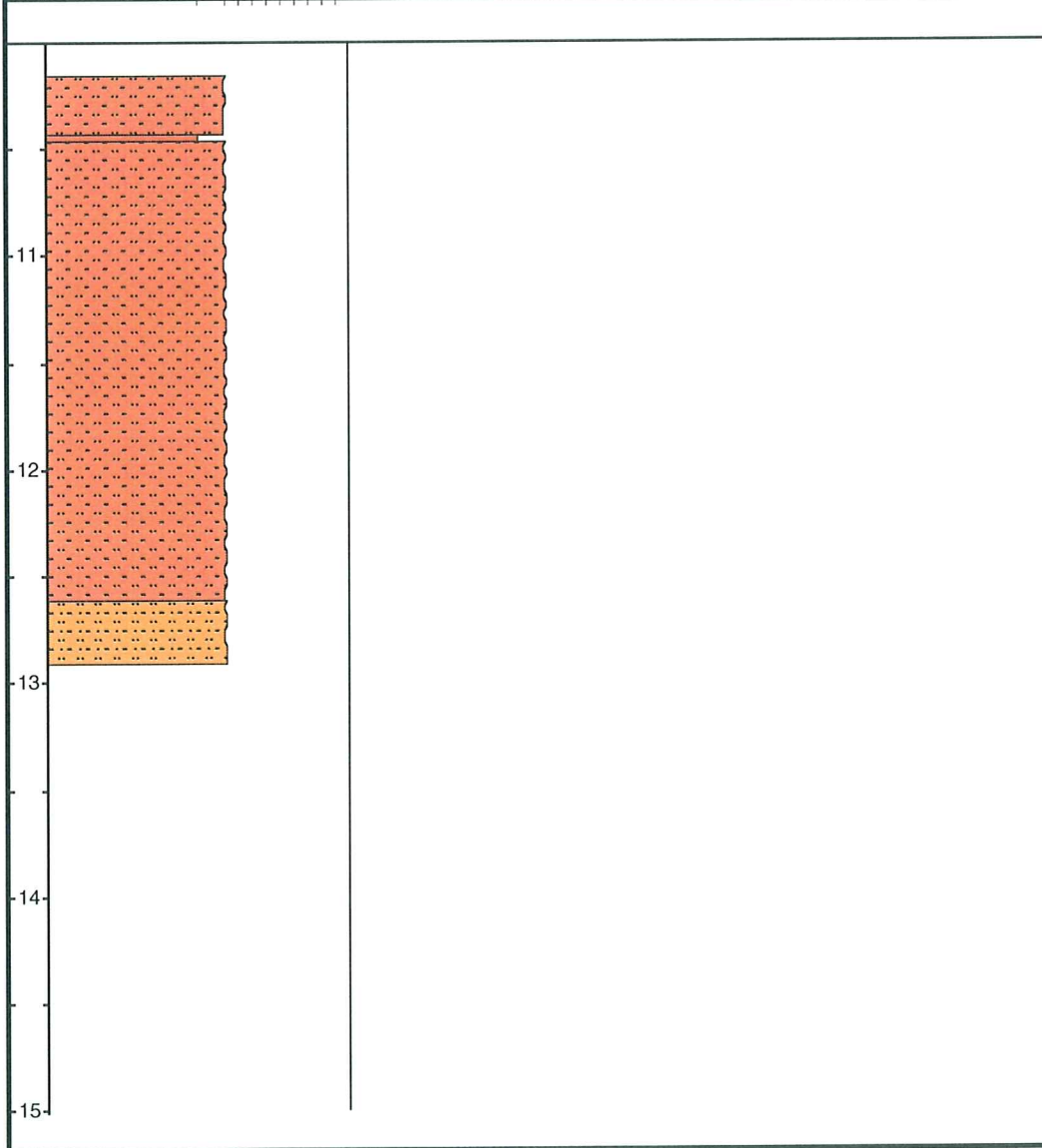
# GS1\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
	cobble pebble granule sand silt clay	



# GS1\_97 CPT Soil Classification

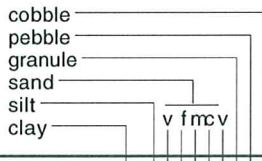
METRES	GRAIN SIZE	REMARKS
	cobble pebble granule sand silt clay v f m c v	



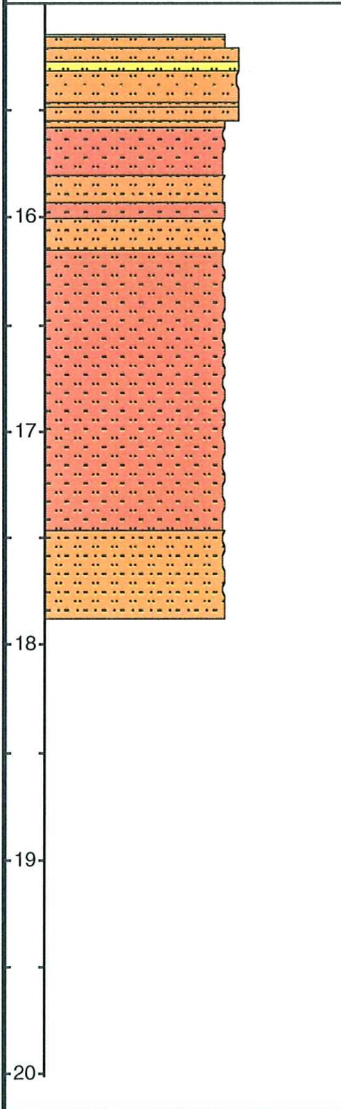
# GS1\_97 CPT Soil Classification

GRAIN SIZE

METRES



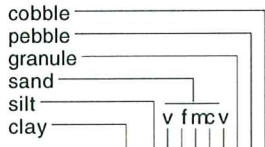
REMARKS



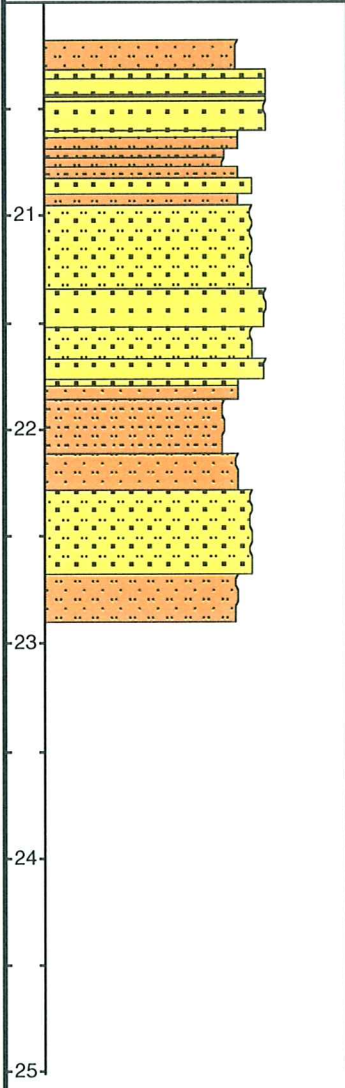
# GS1\_97 CPT Soil Classification

METRES

GRAIN SIZE



REMARKS

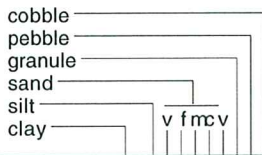




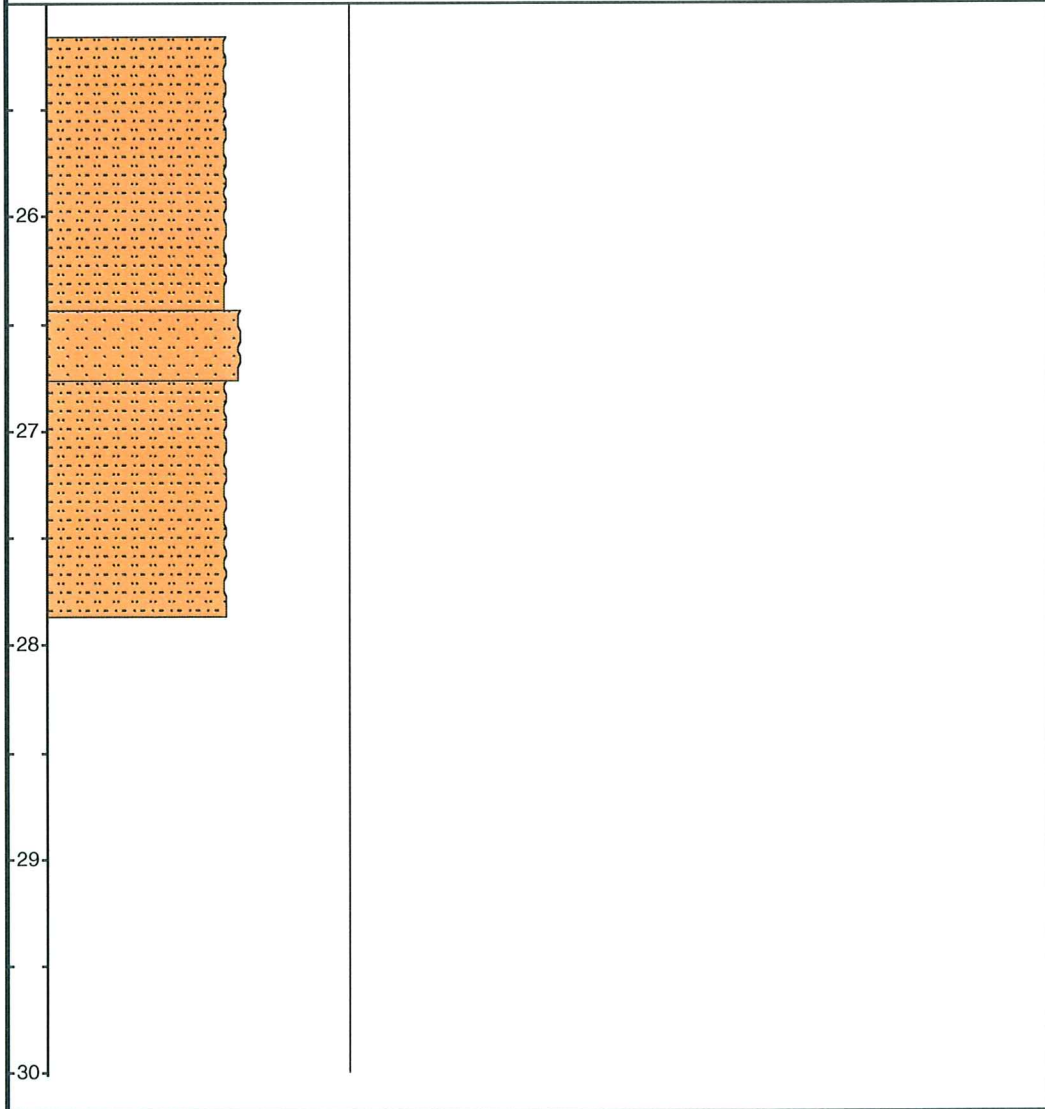
# GS1\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
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GRAIN SIZE

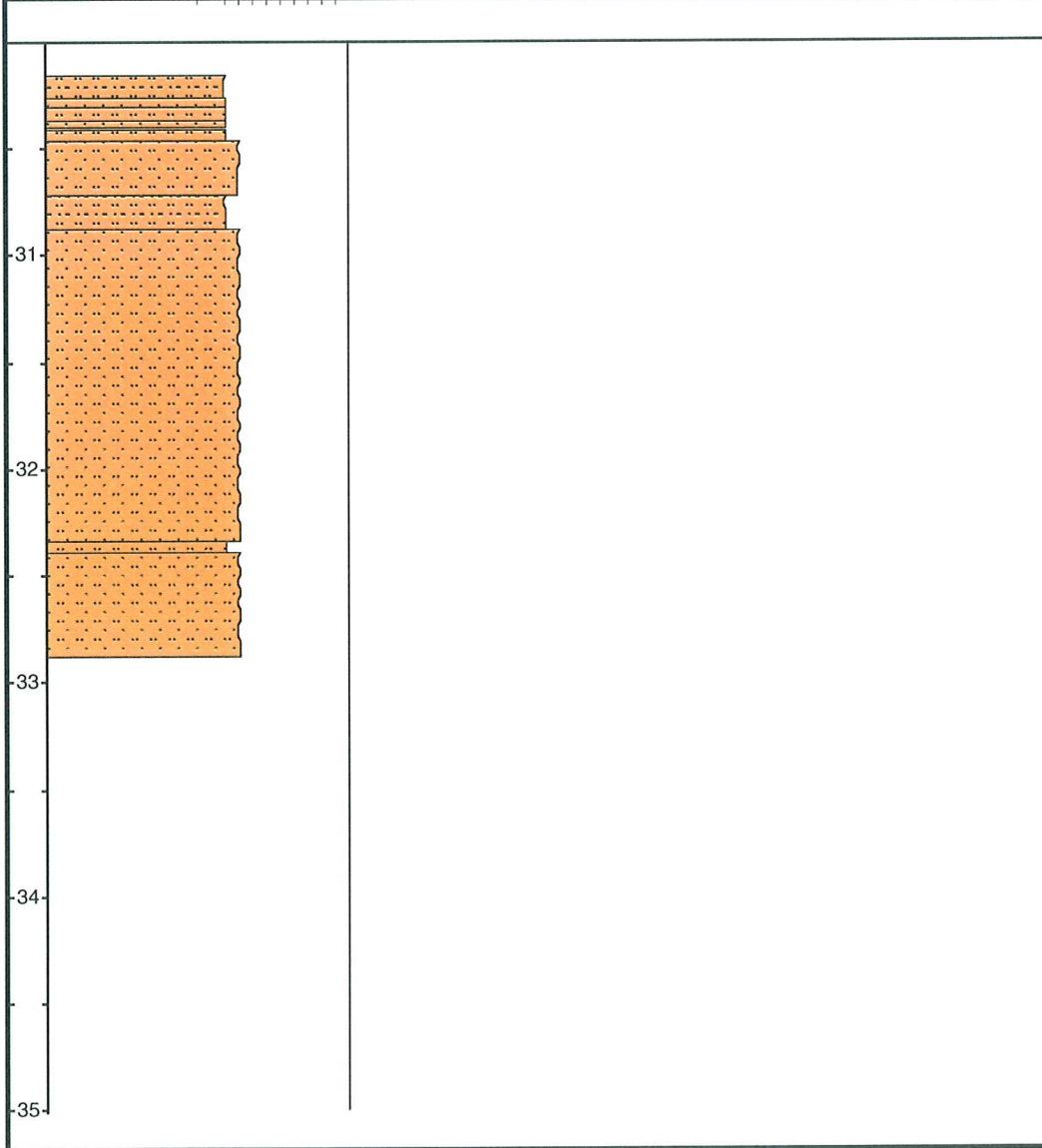
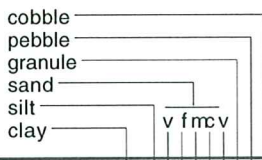


REMARKS



# GS1\_97 CPT Soil Classification

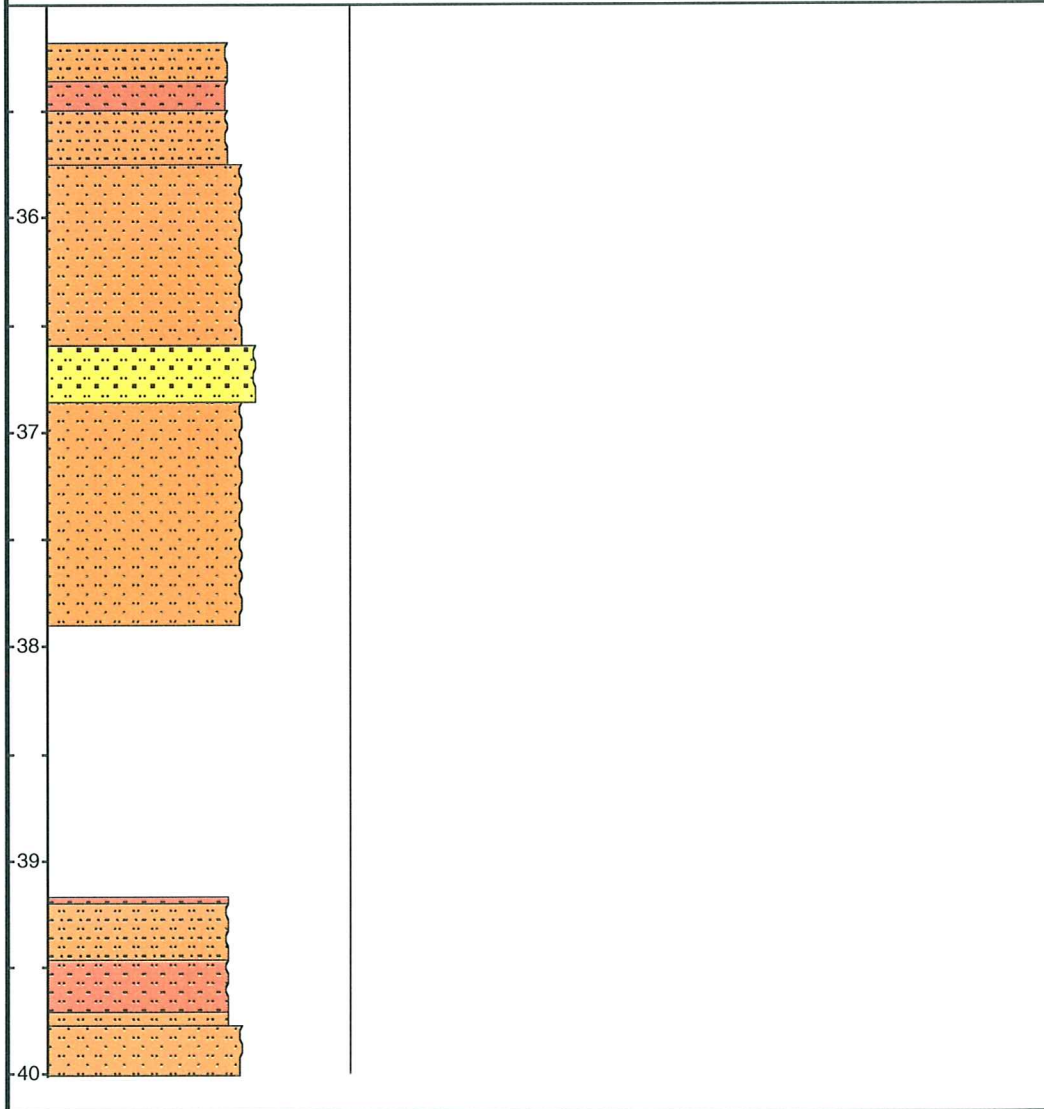
METRES	GRAIN SIZE	REMARKS
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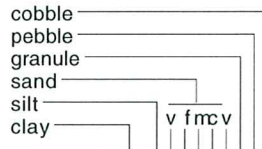
# GS1\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
	cobble pebble granule sand silt clay	

v f m v

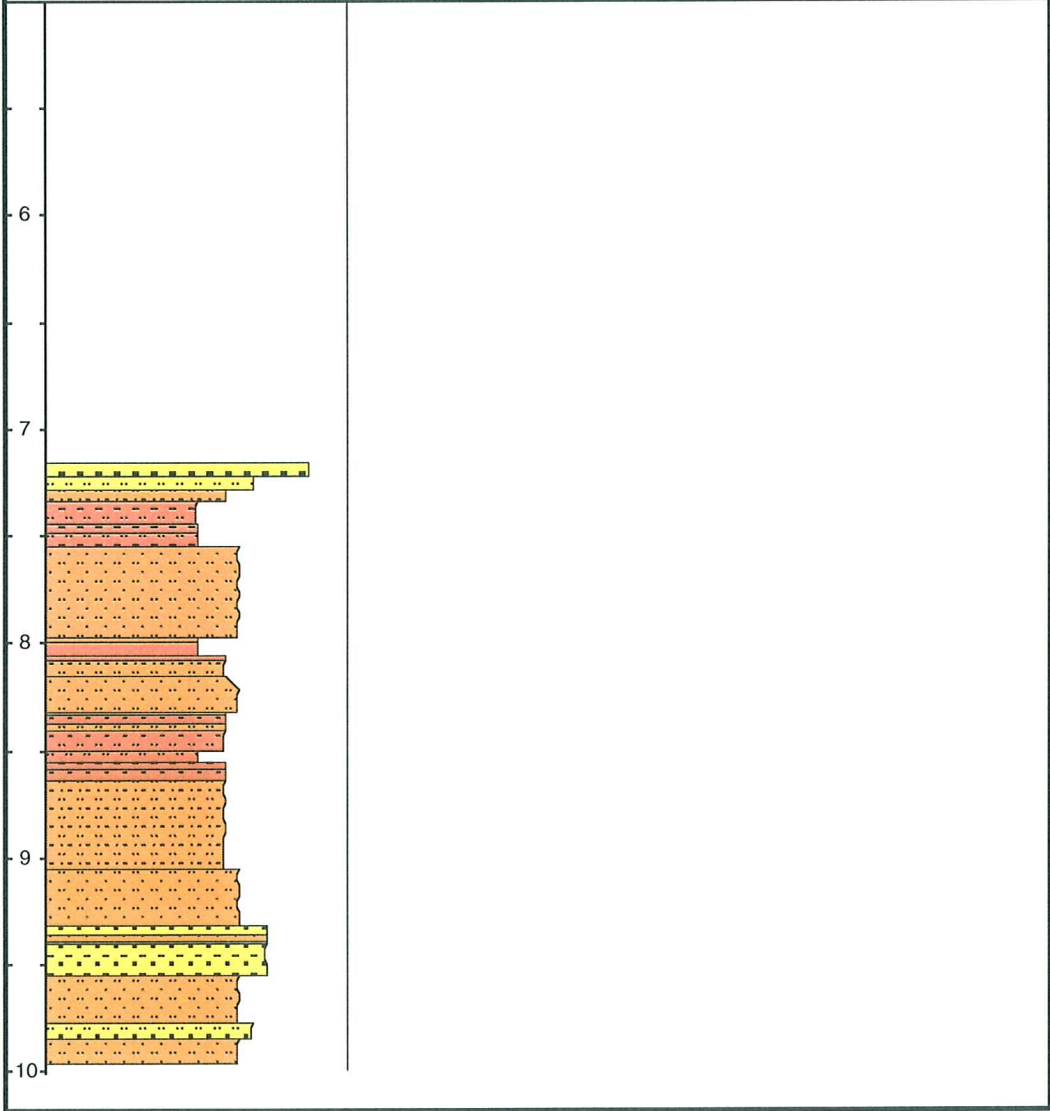


# A3\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
-1 -2 -3 -4 -5	 <p>Legend for Grain Size:</p> <ul style="list-style-type: none"><li>cobble</li><li>pebble</li><li>granule</li><li>sand</li><li>silt</li><li>clay</li></ul> <p>Sub-labels: v, fm, cv</p>	

# A3\_97 CPT Soil Classification

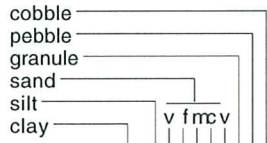
GRAIN SIZE	REMARKS
<p>METRES</p> <p>cobble</p> <p>pebble</p> <p>granule</p> <p>sand</p> <p>silt</p> <p>clay</p> <p>v fnc v</p>	



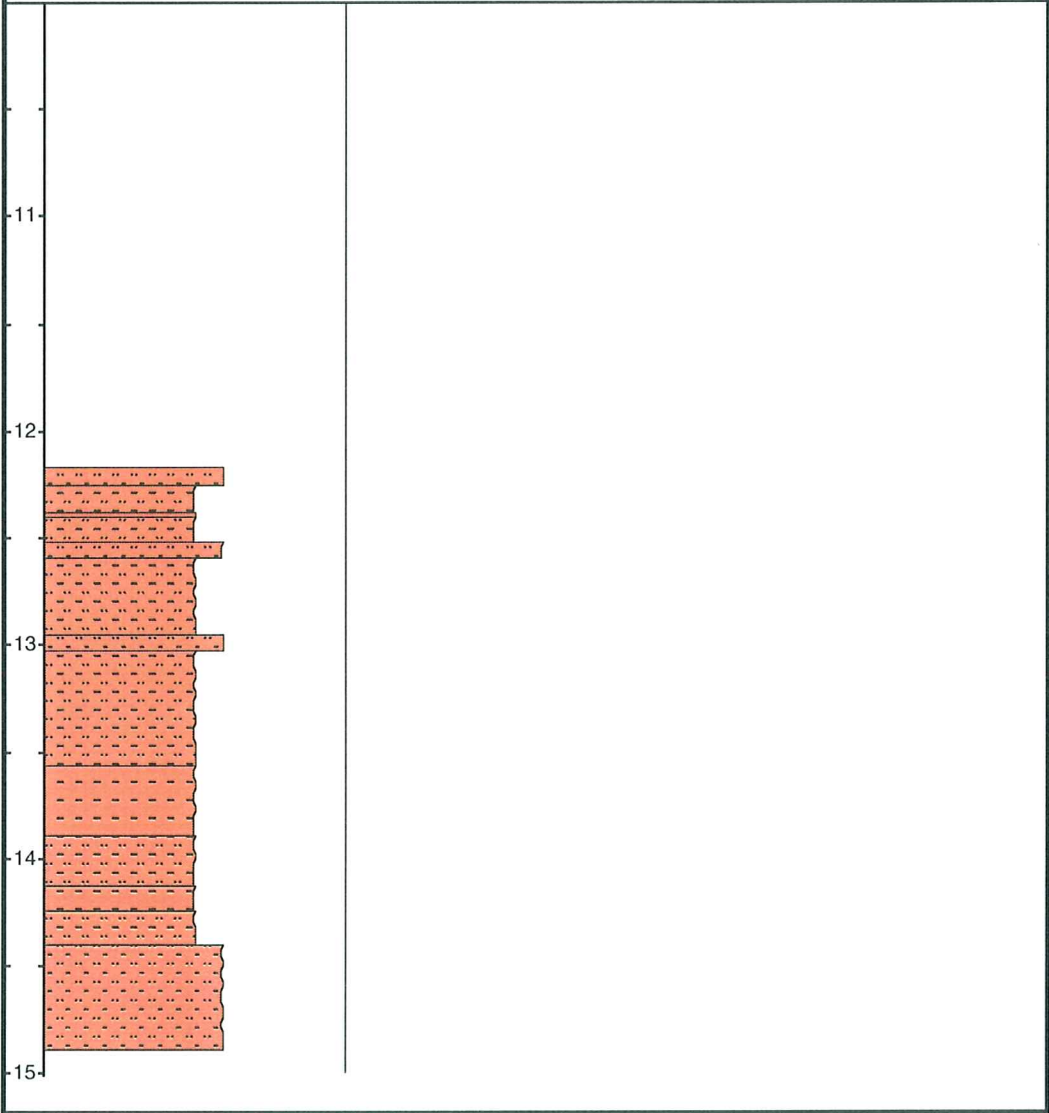
# A3\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
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GRAIN SIZE



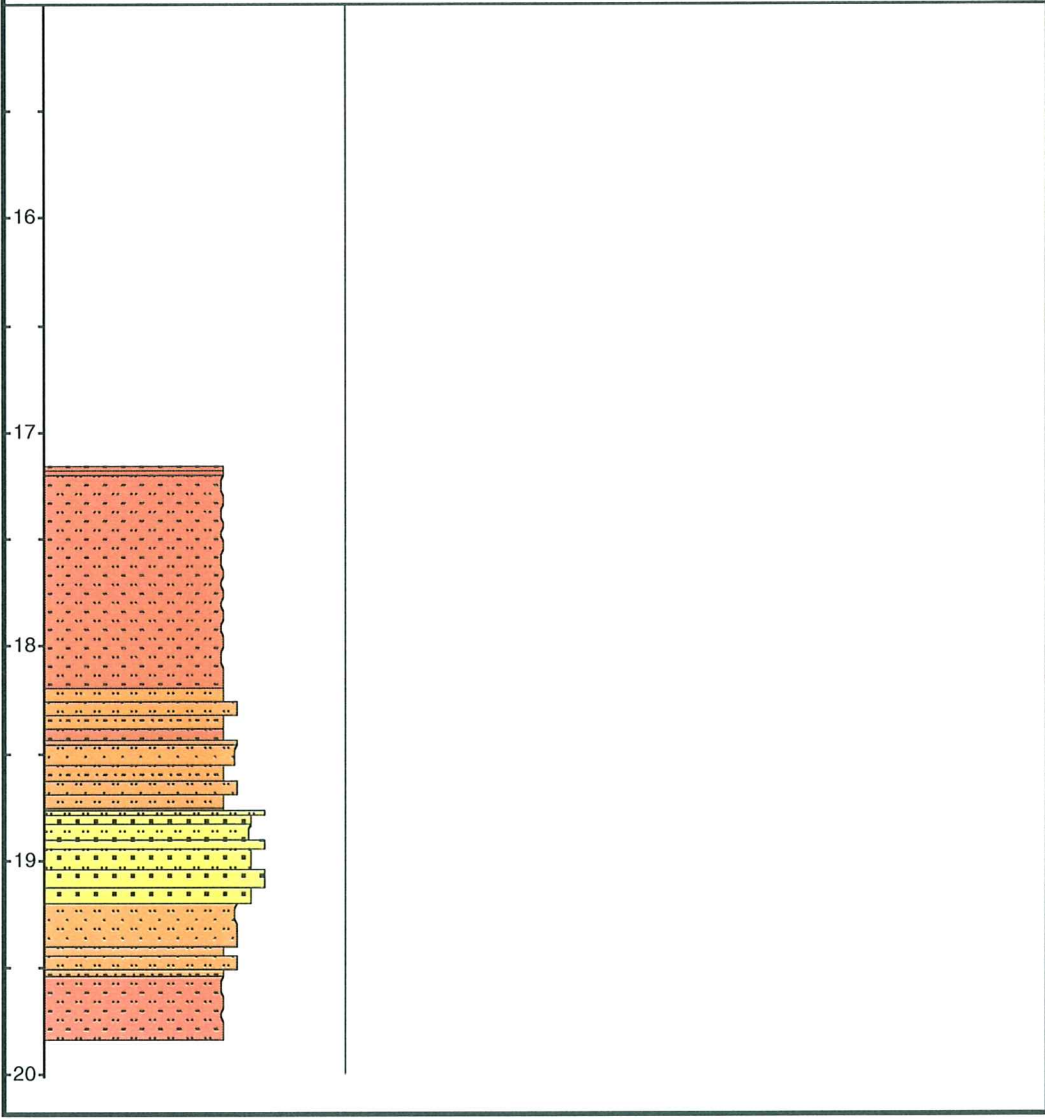
REMARKS



# A3\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
	cobble pebble granule sand silt clay	

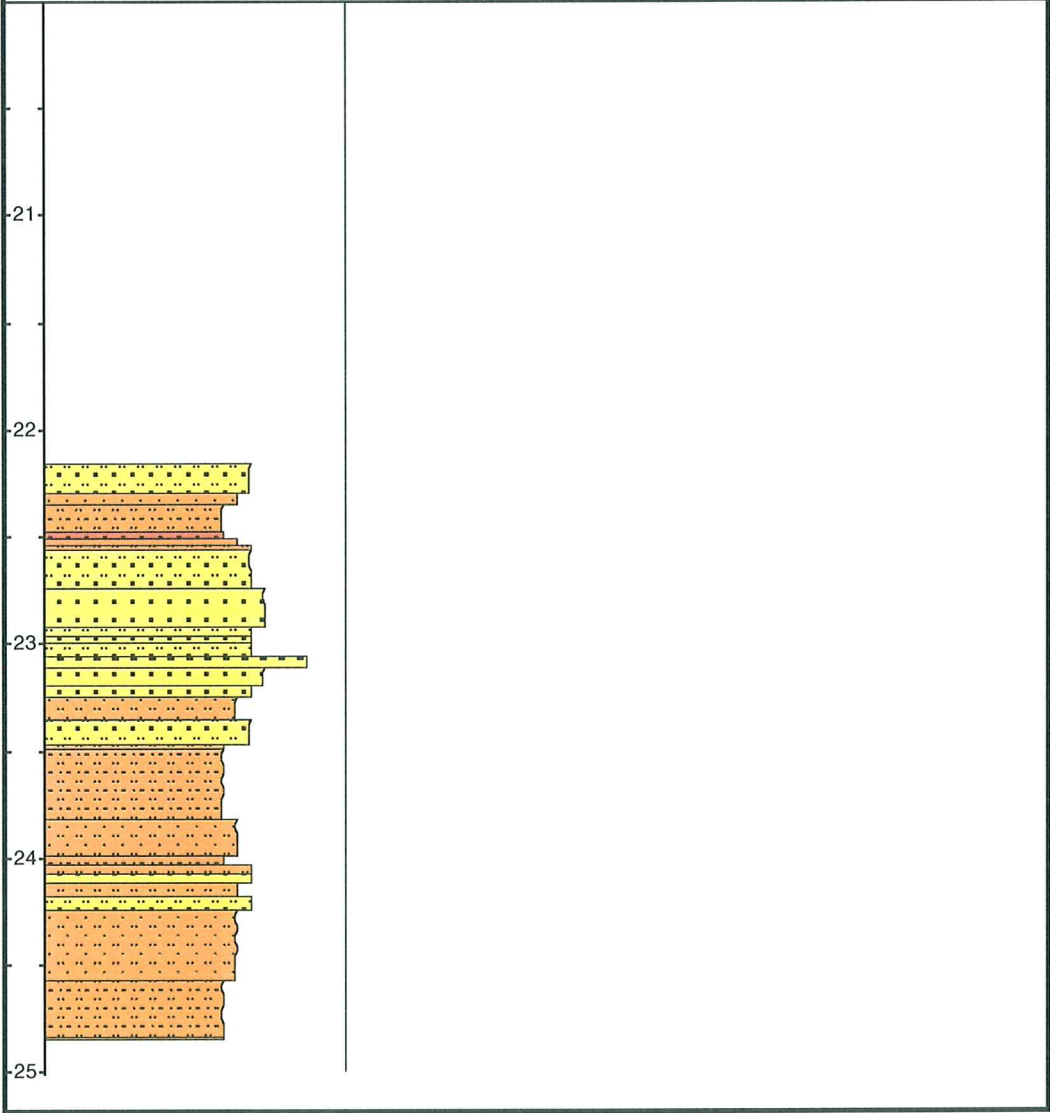
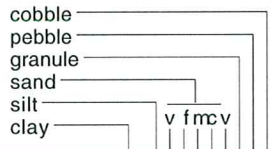
v f m c v



# A3\_97 CPT Soil Classification

METRES	REMARKS
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GRAIN SIZE

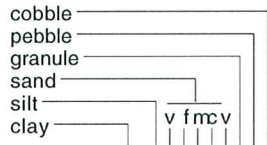




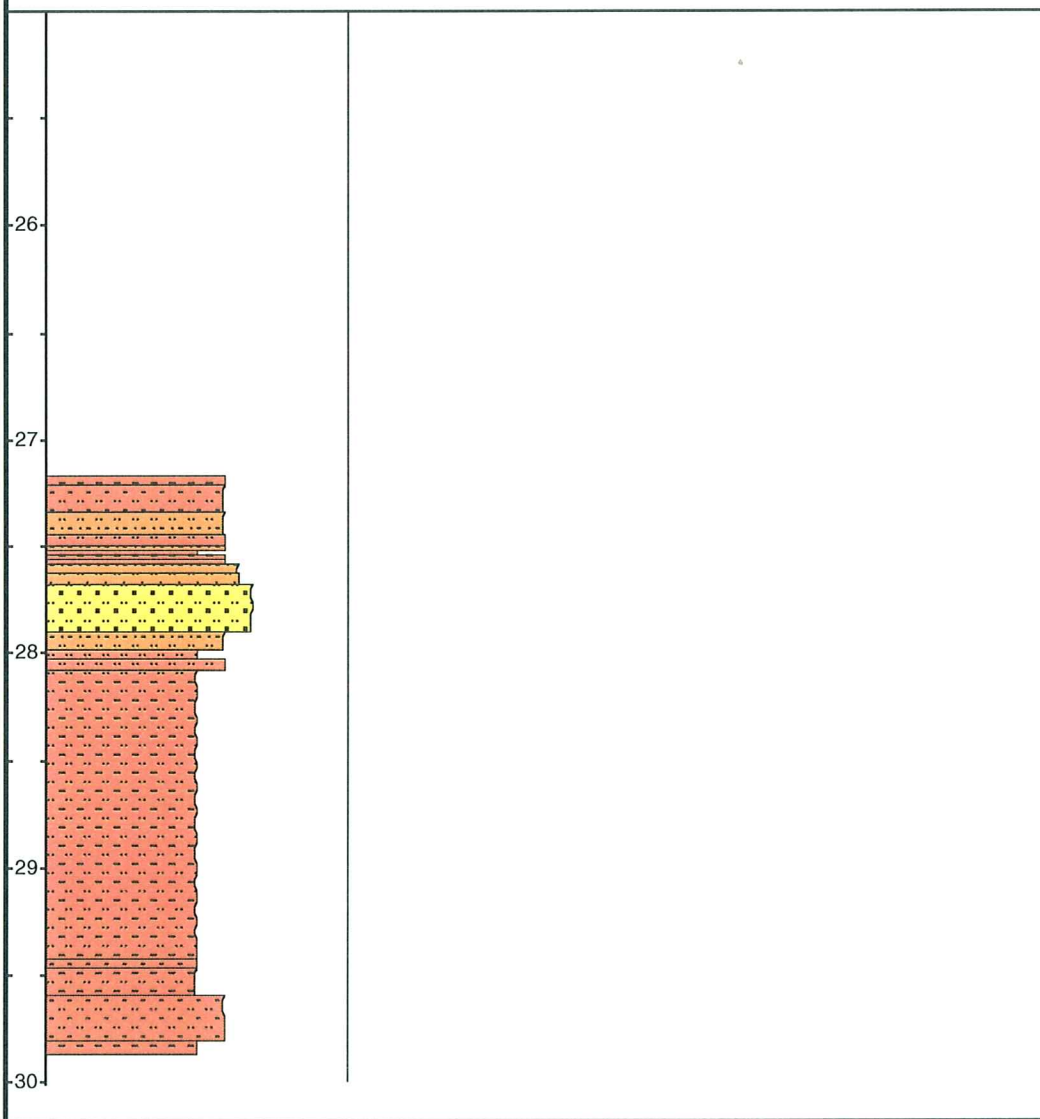
# A3\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
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GRAIN SIZE



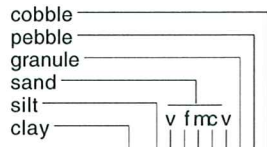
REMARKS



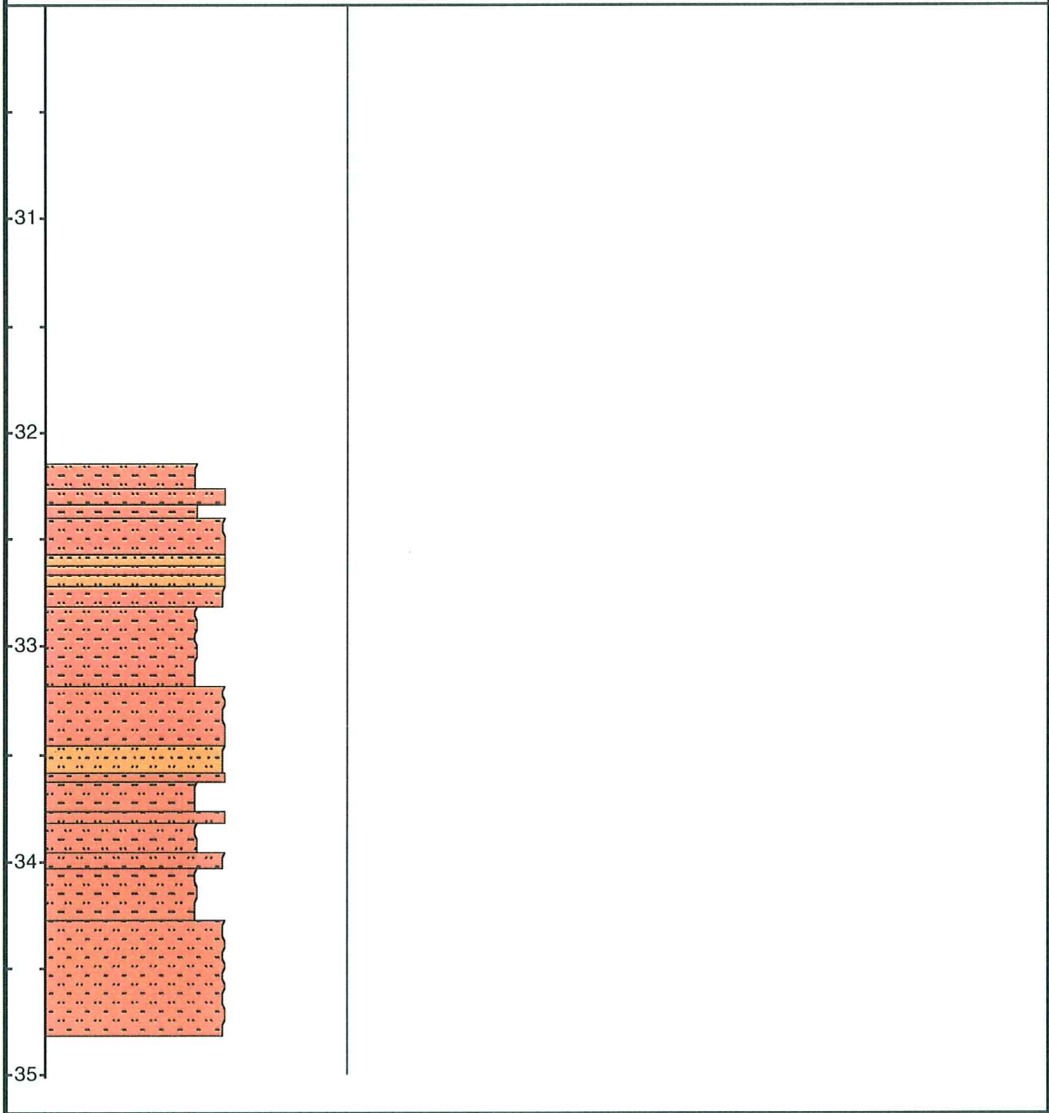
# A3\_97 CPT Soil Classification

METRES	GRAIN SIZE	REMARKS
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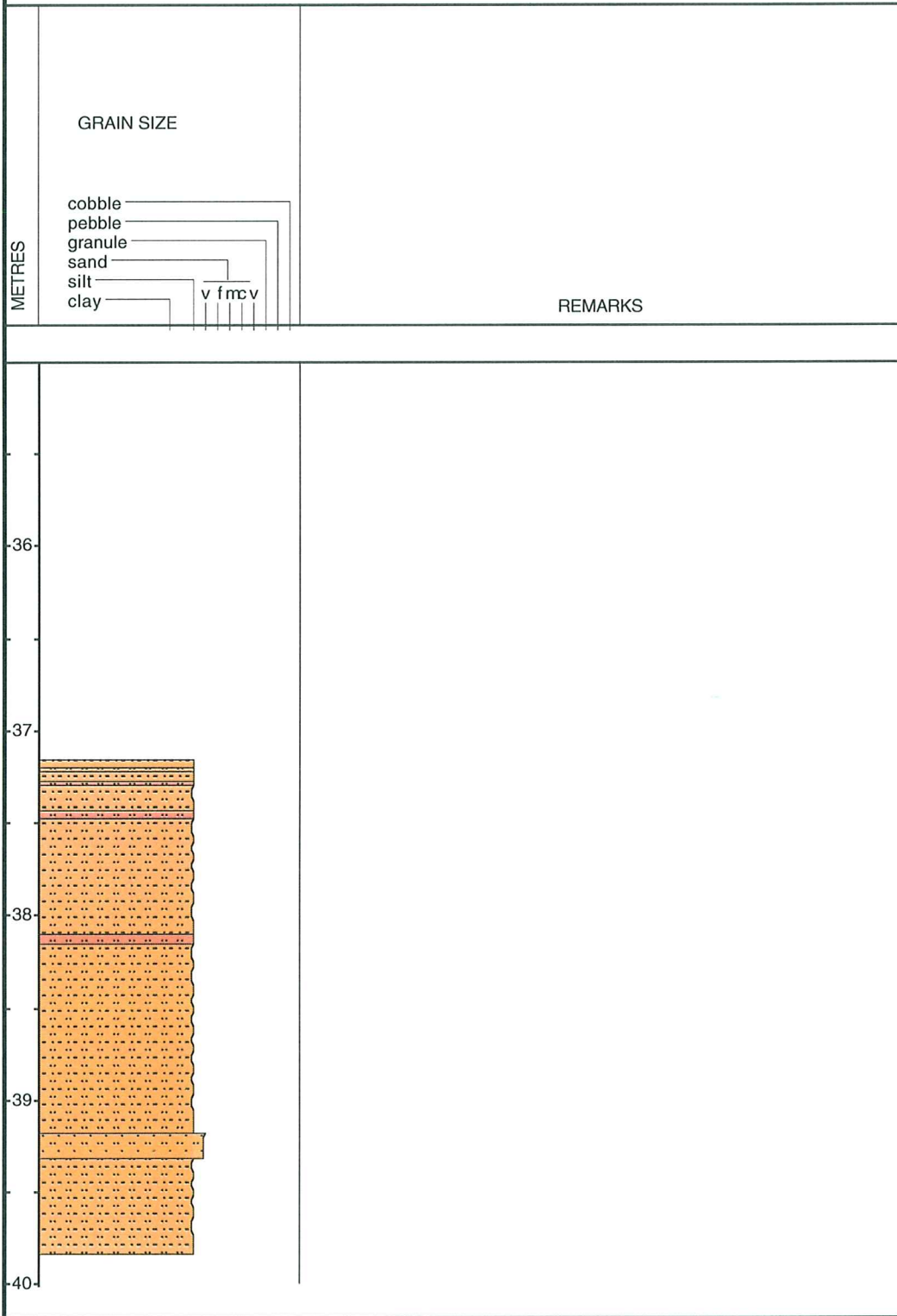
GRAIN SIZE



REMARKS

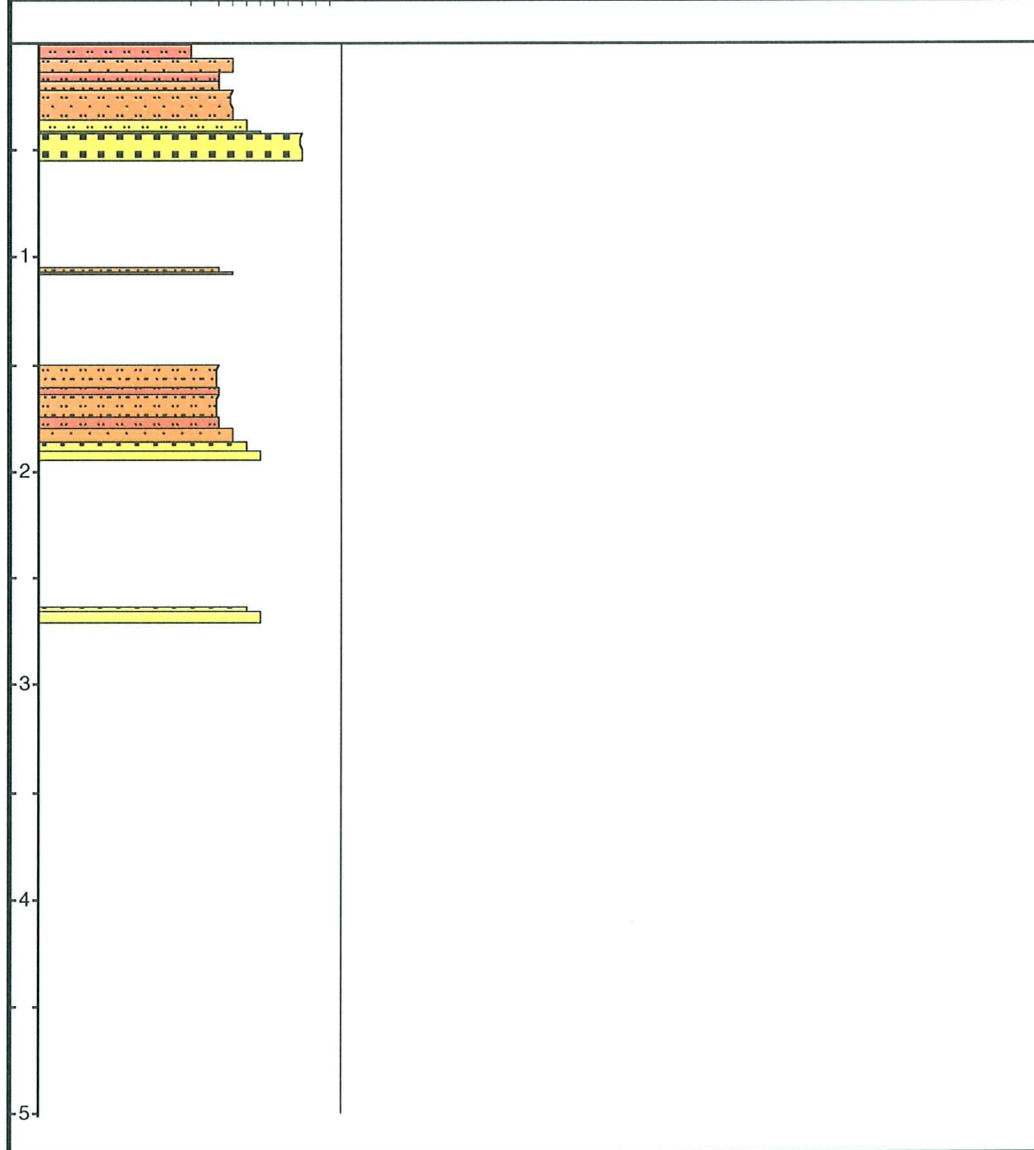


# A3\_97 CPT Soil Classification



# FPSO\_B Cpt Soil Classification

	GRAIN SIZE	
METRES	cobble pebble granule sand silt clay	REMARKS



# FR1\_1B Cpt Soil Classification

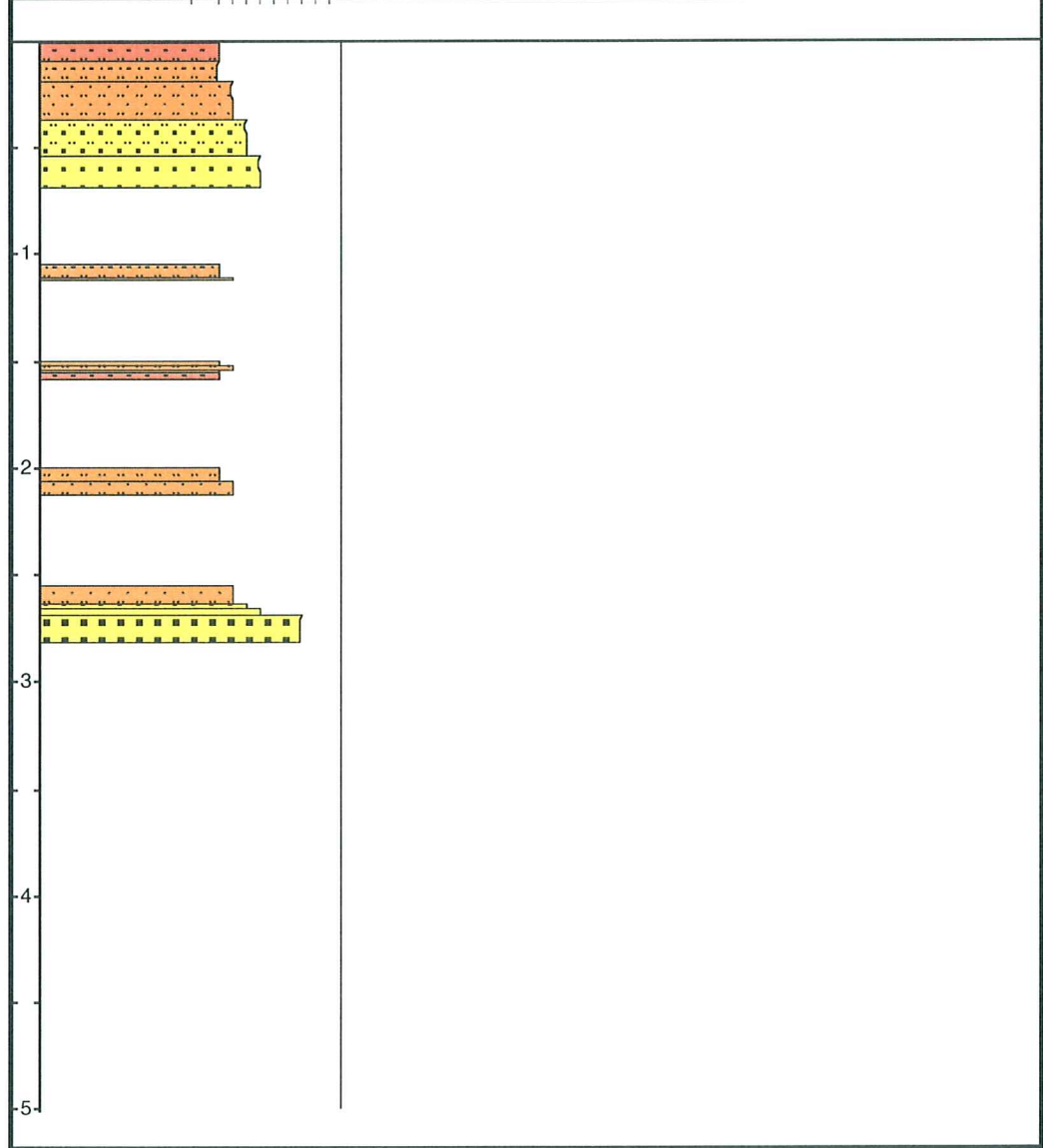
GRAIN SIZE

cobble  
pebble  
granule  
sand  
silt  
clay

v fmc v

METRES

REMARKS



# FR1\_3B Cpt Soil Classification

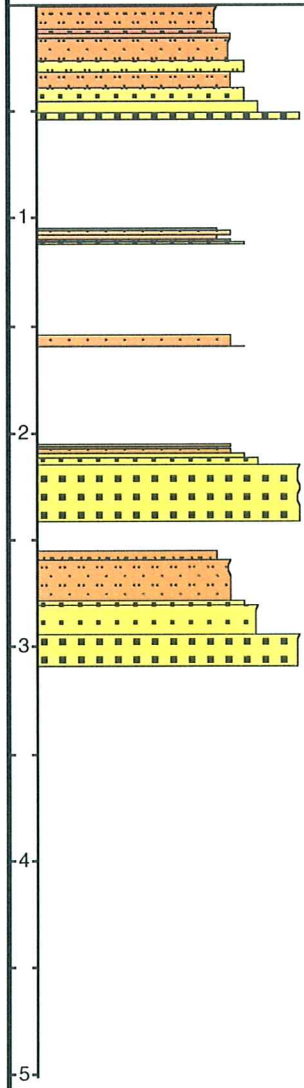
GRAIN SIZE

cobble  
pebble  
granule  
sand  
silt  
clay

v fmc v

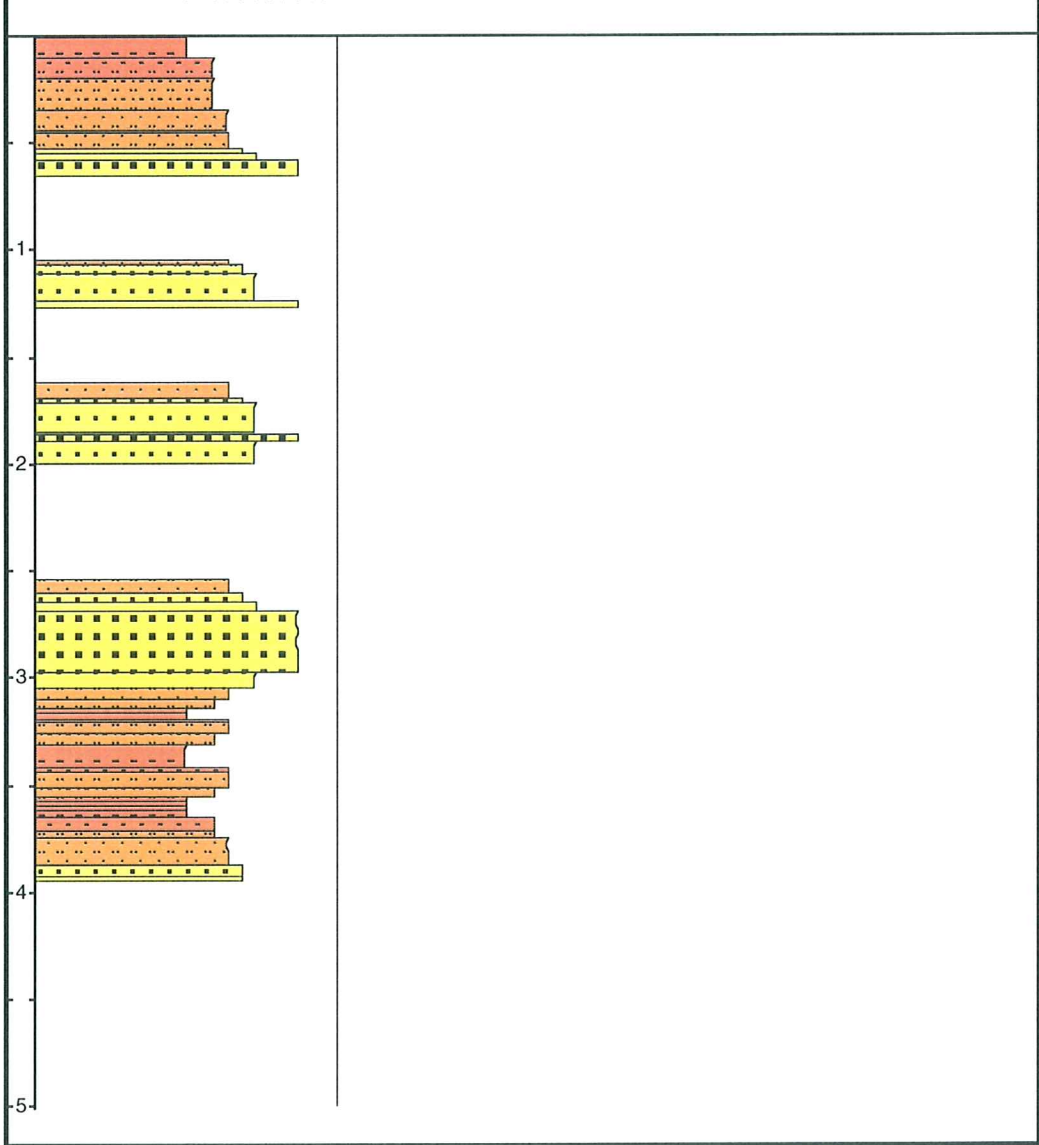
METRES

REMARKS



# FR4\_1B Cpt Soil Classification

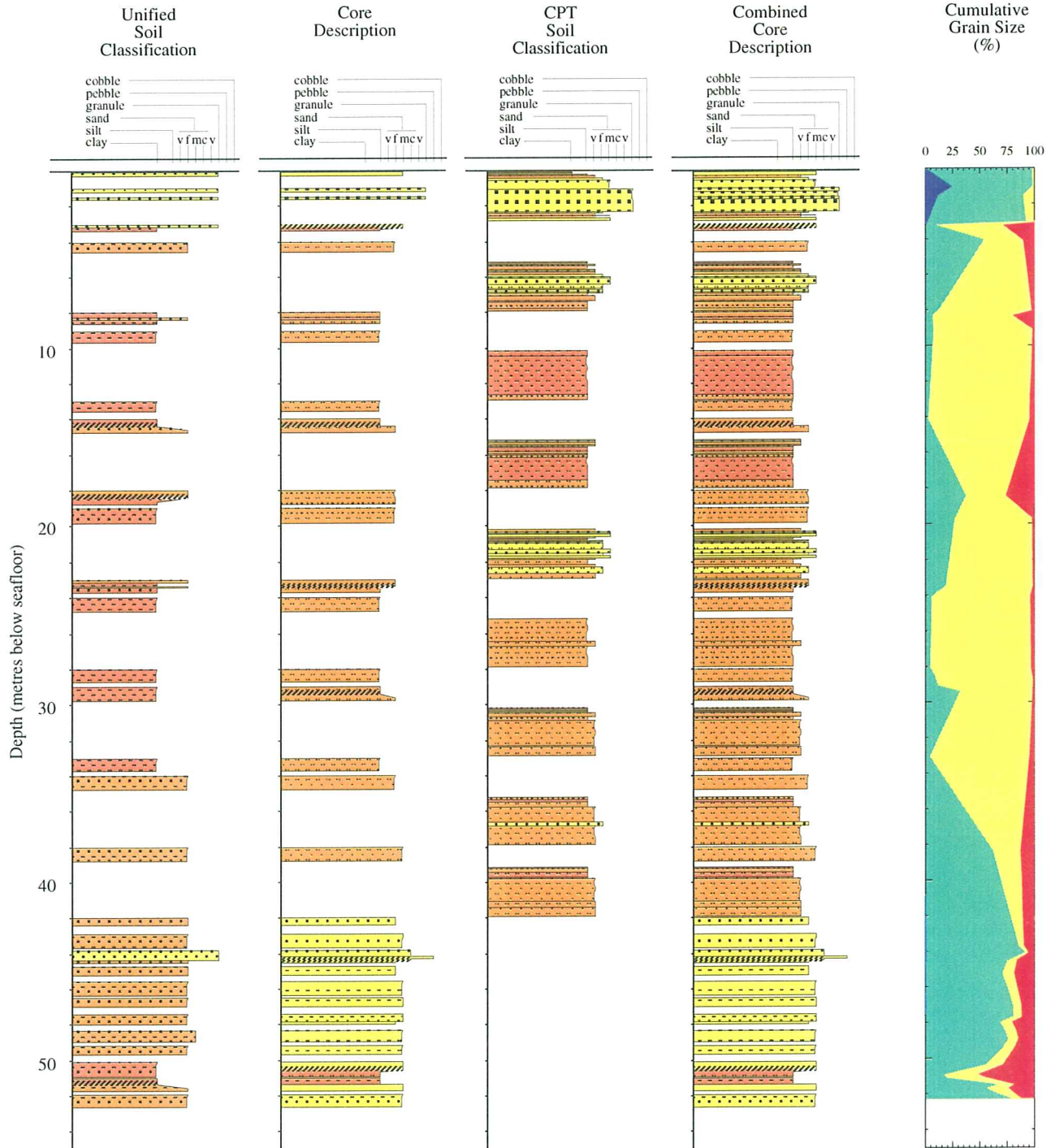
<p style="text-align: center;">GRAIN SIZE</p> <p style="text-align: center;">             cobble              pebble              granule              sand              silt              clay         </p>		<p style="text-align: center;">REMARKS</p>
--	--	--



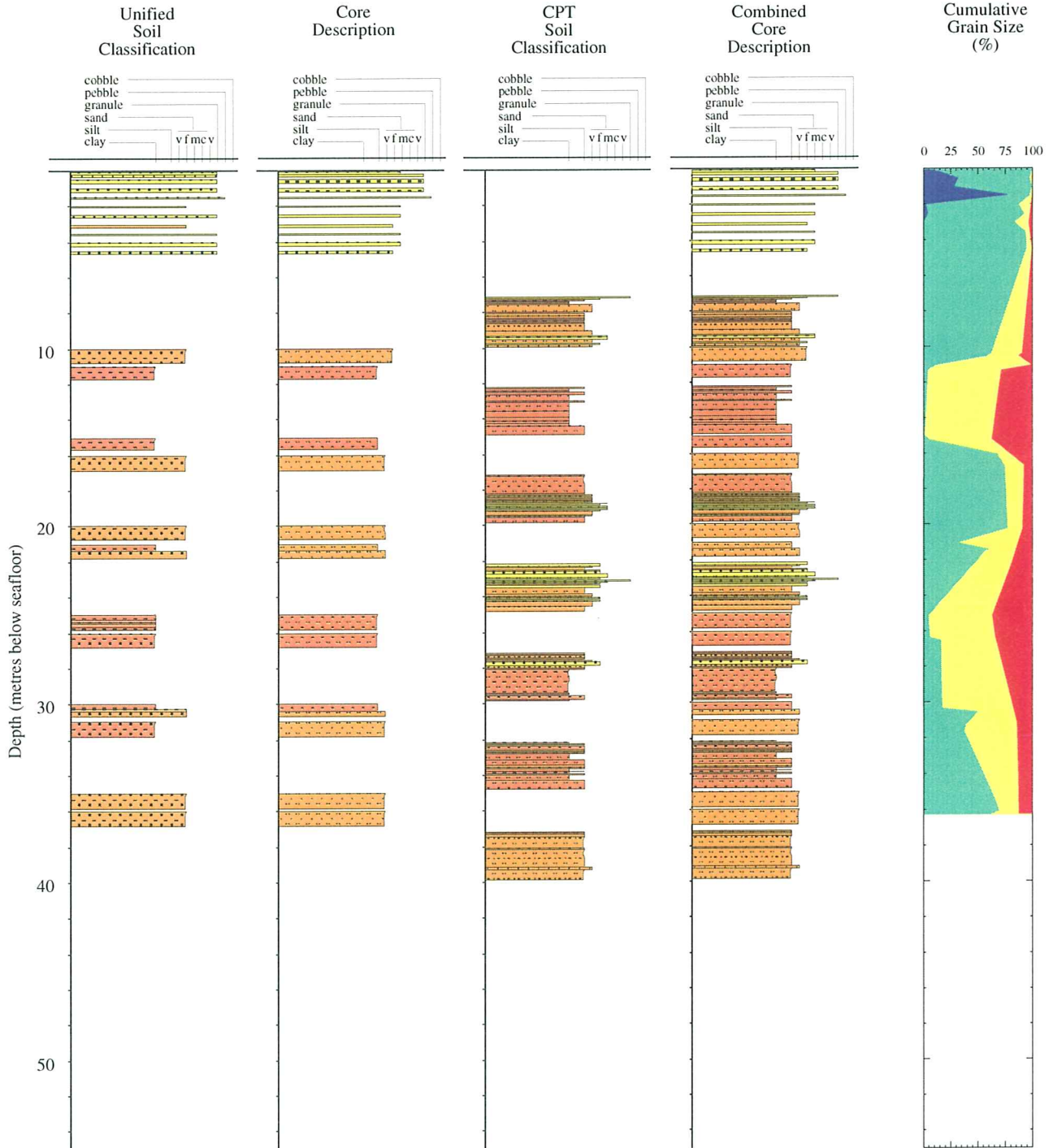
## Appendix 6



# GSI\_97



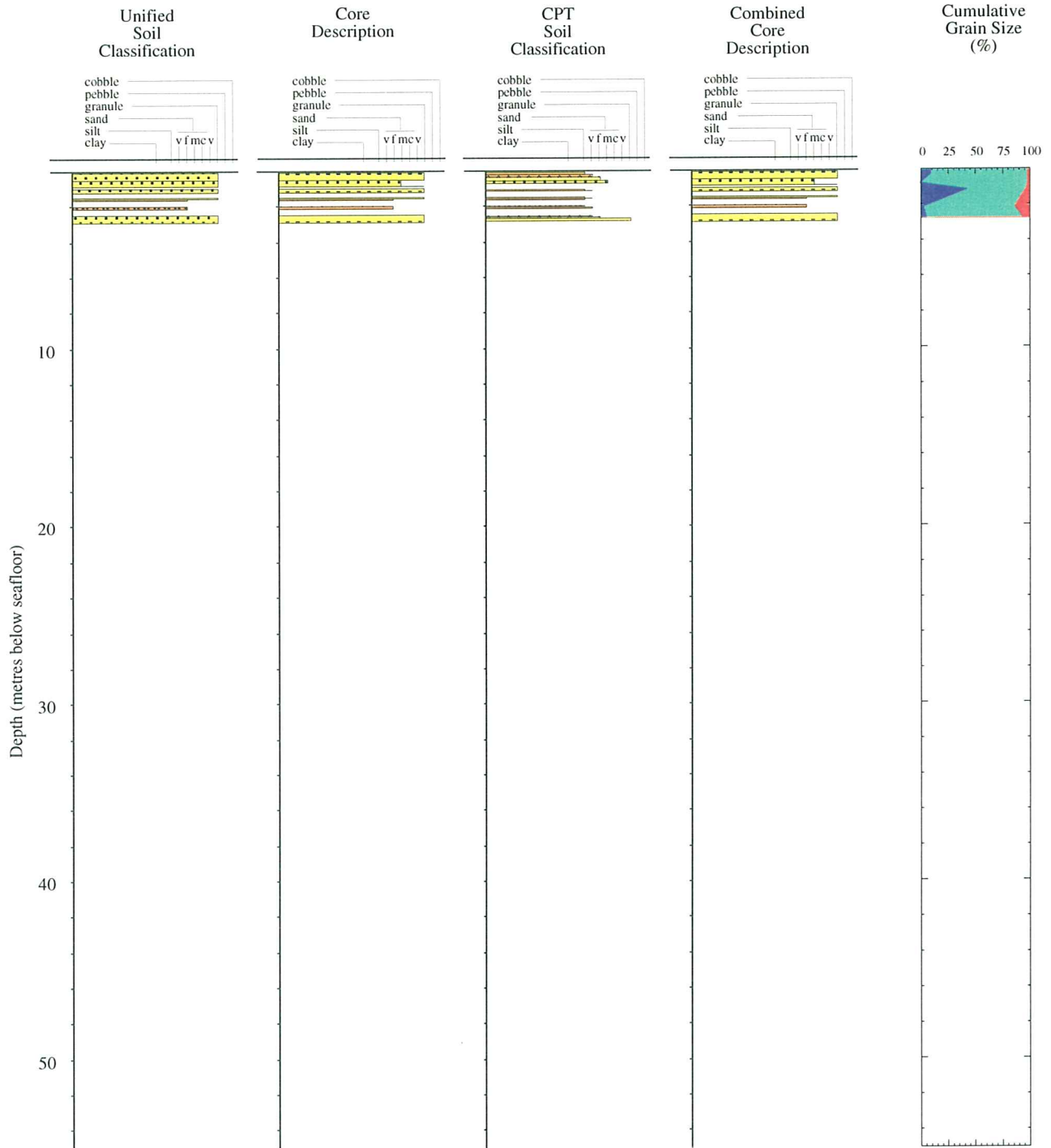
# A3\_97



# FPSO\_B



# FR1\_1B



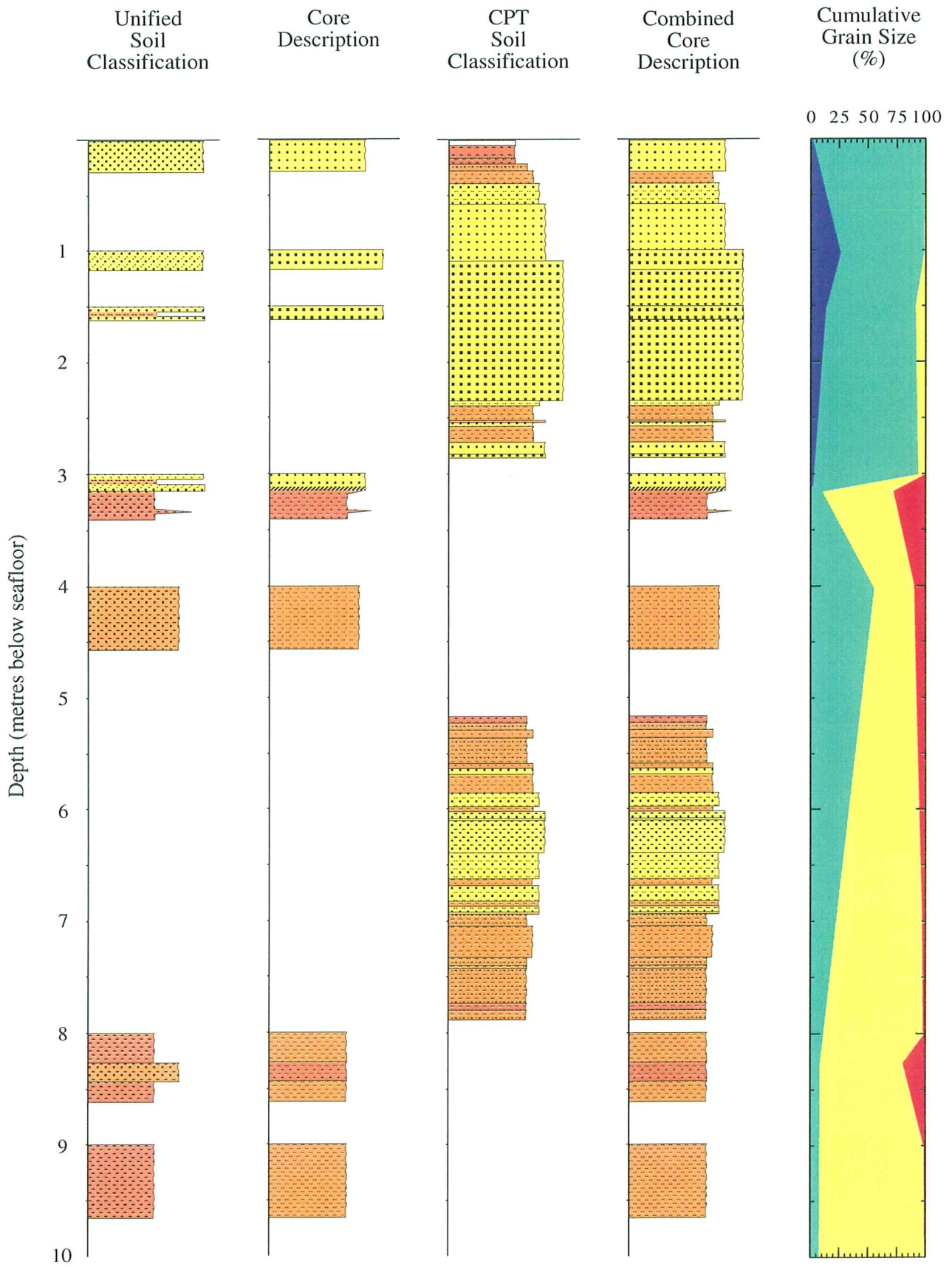
# FRI\_3B



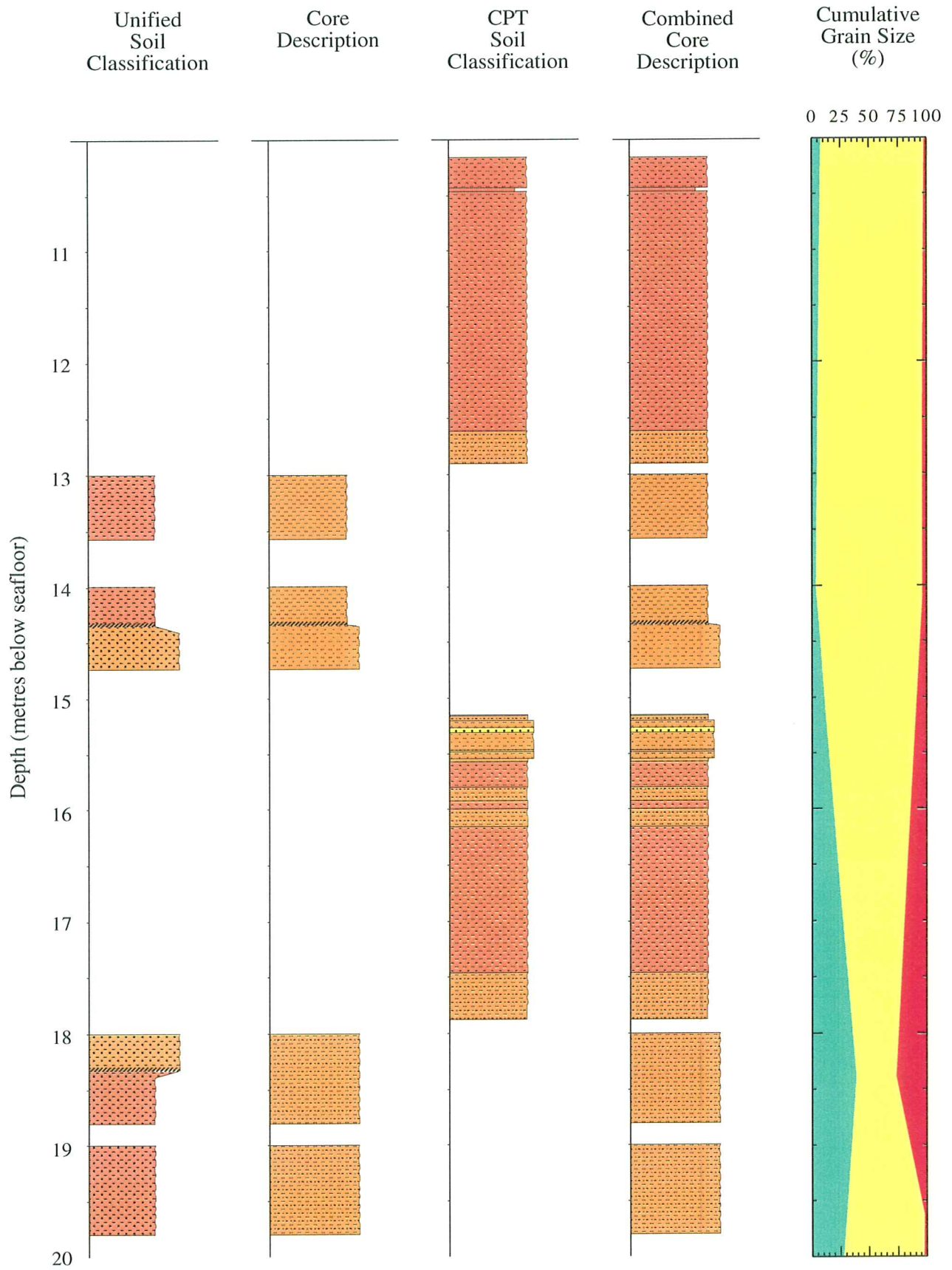
# FR4\_1B



# GSI\_97

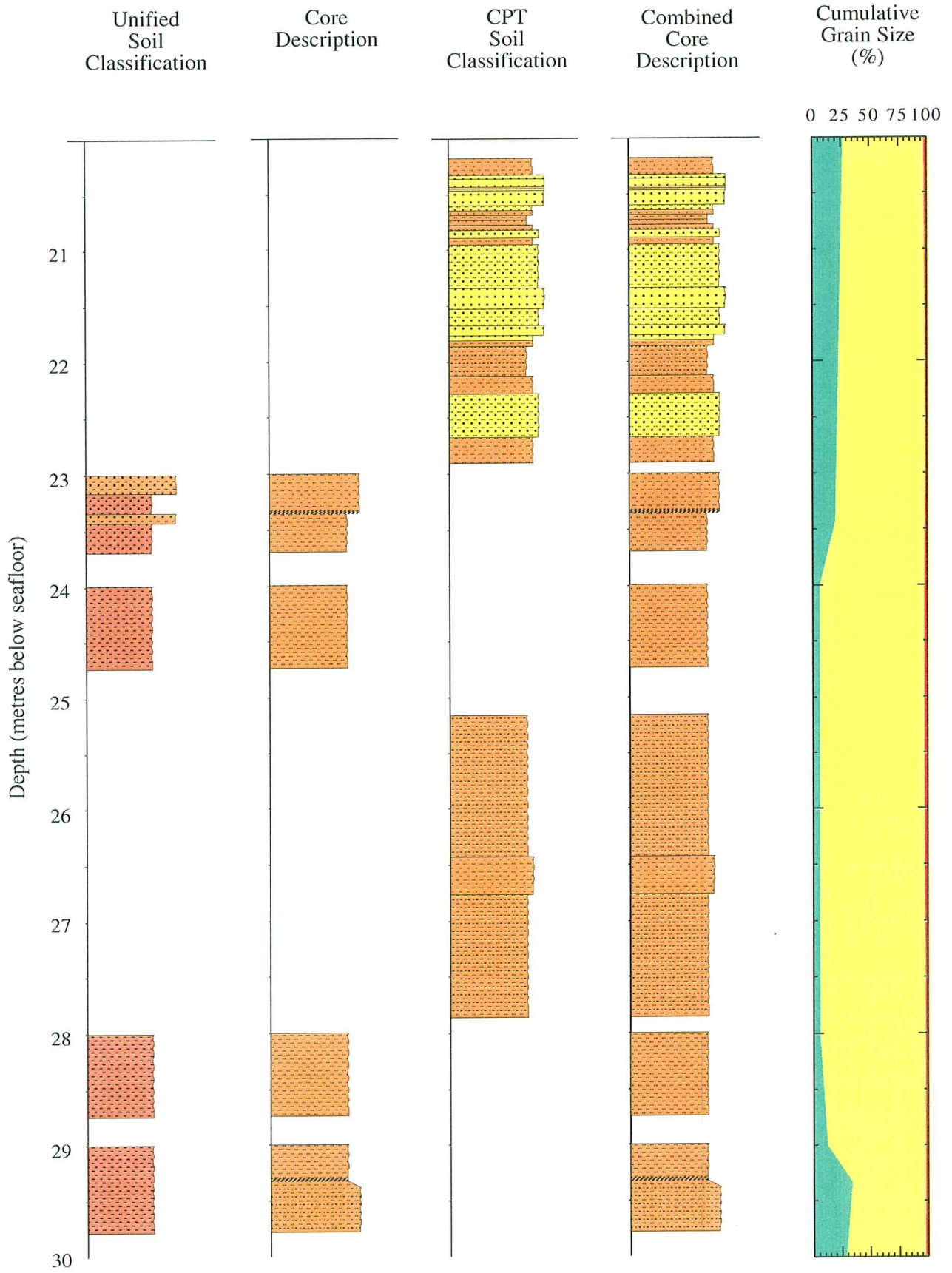


# GSI\_97

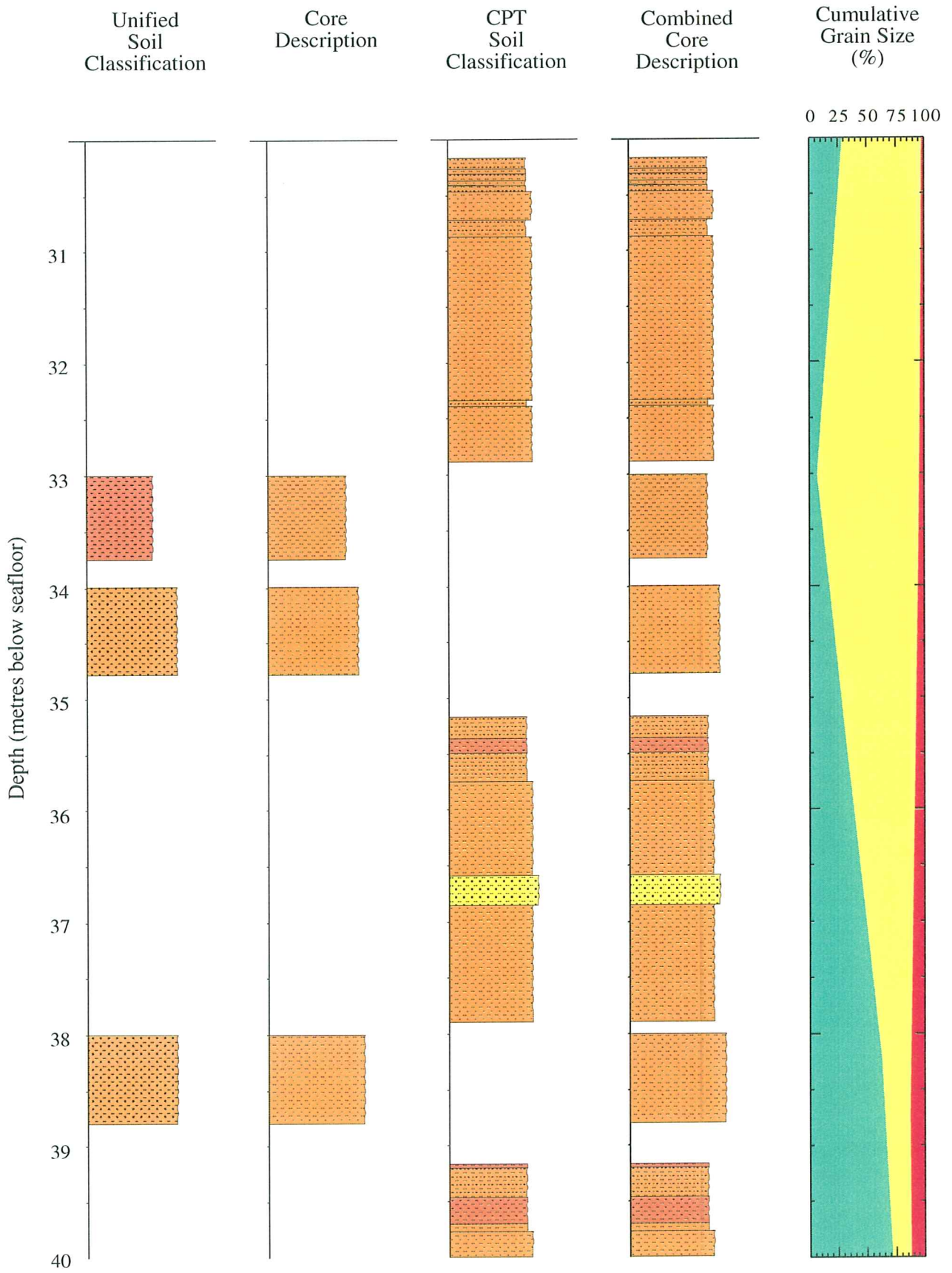




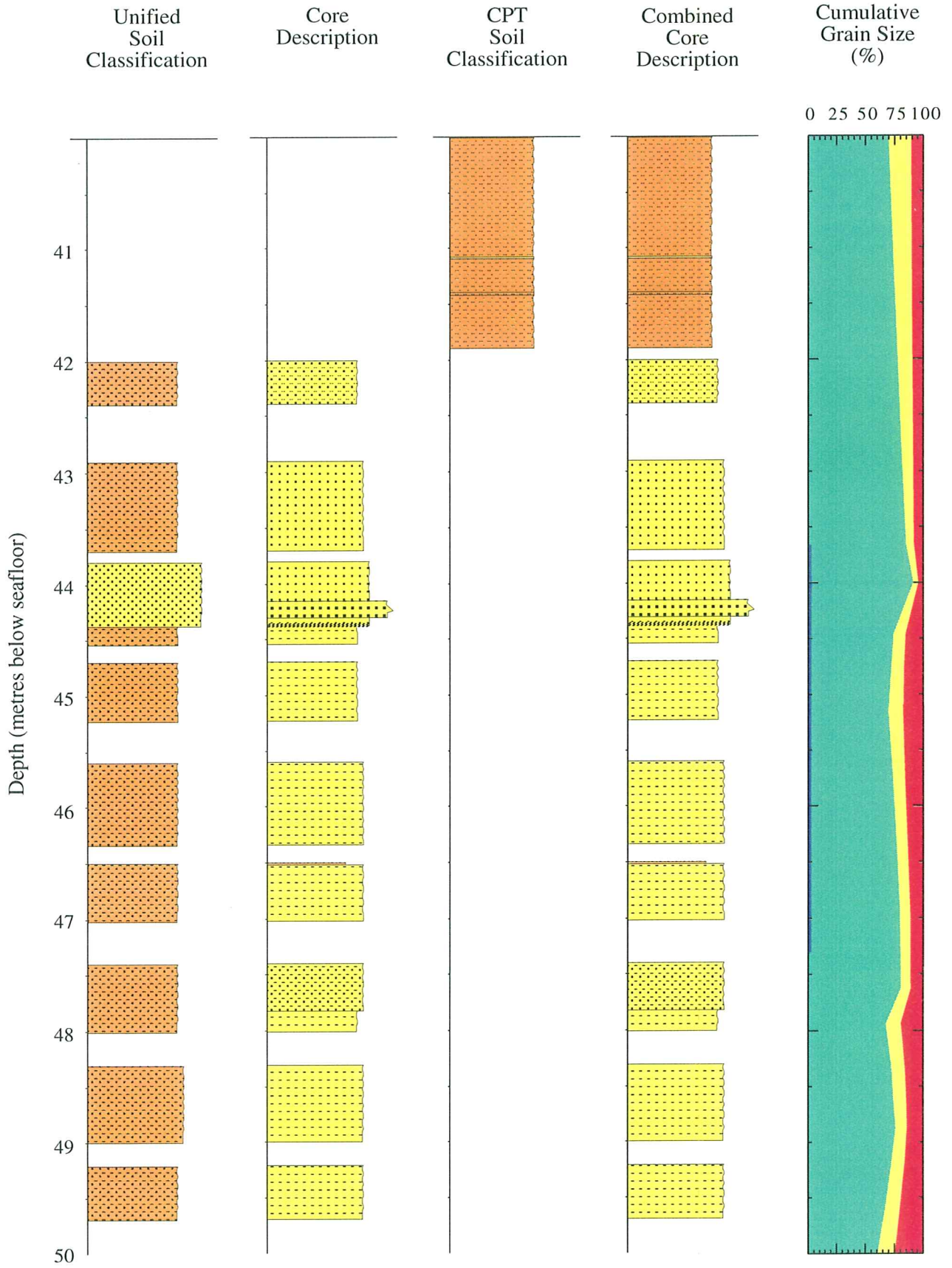
# GS1\_97



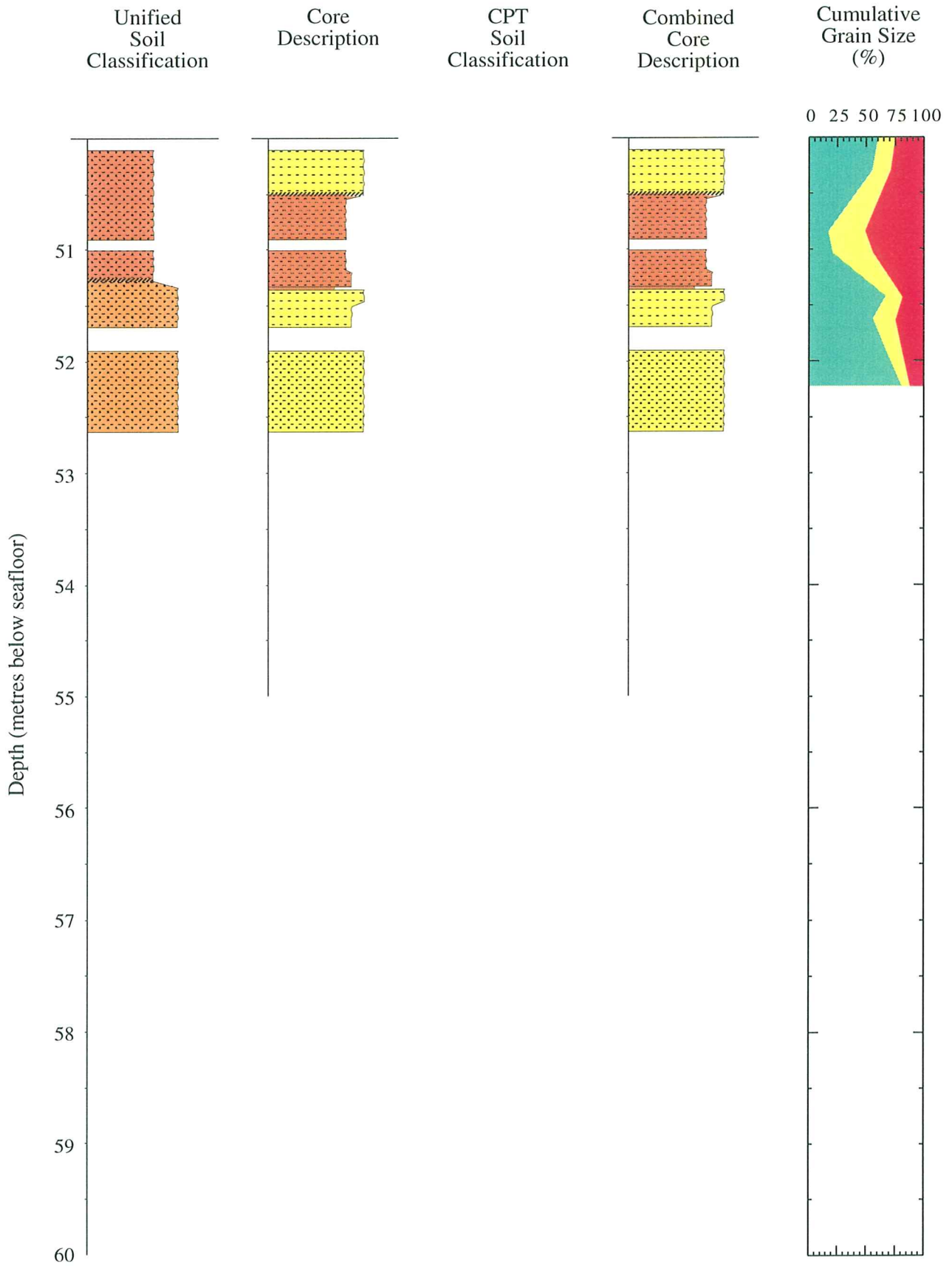
# GS1\_97



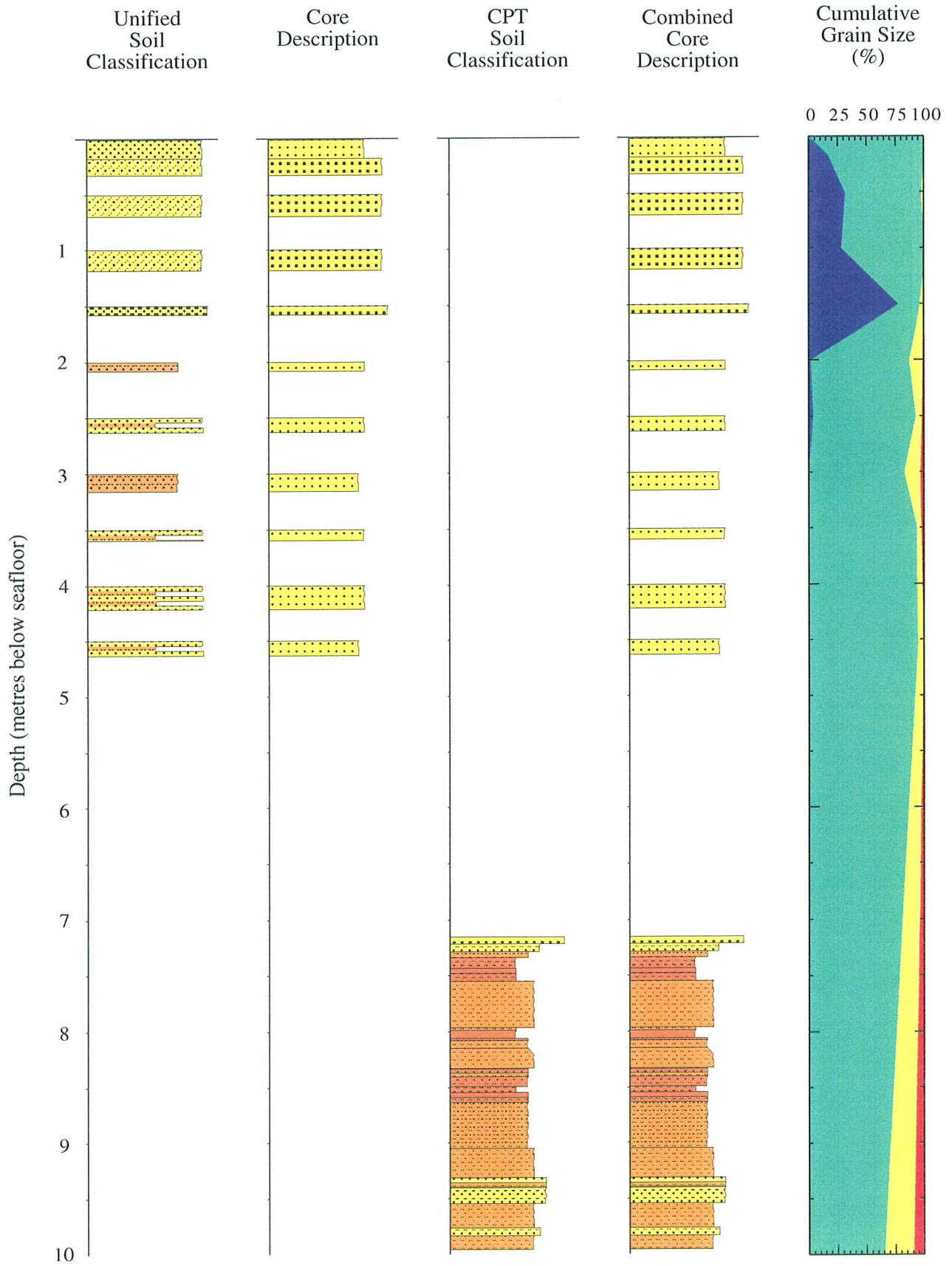
# GS1\_97

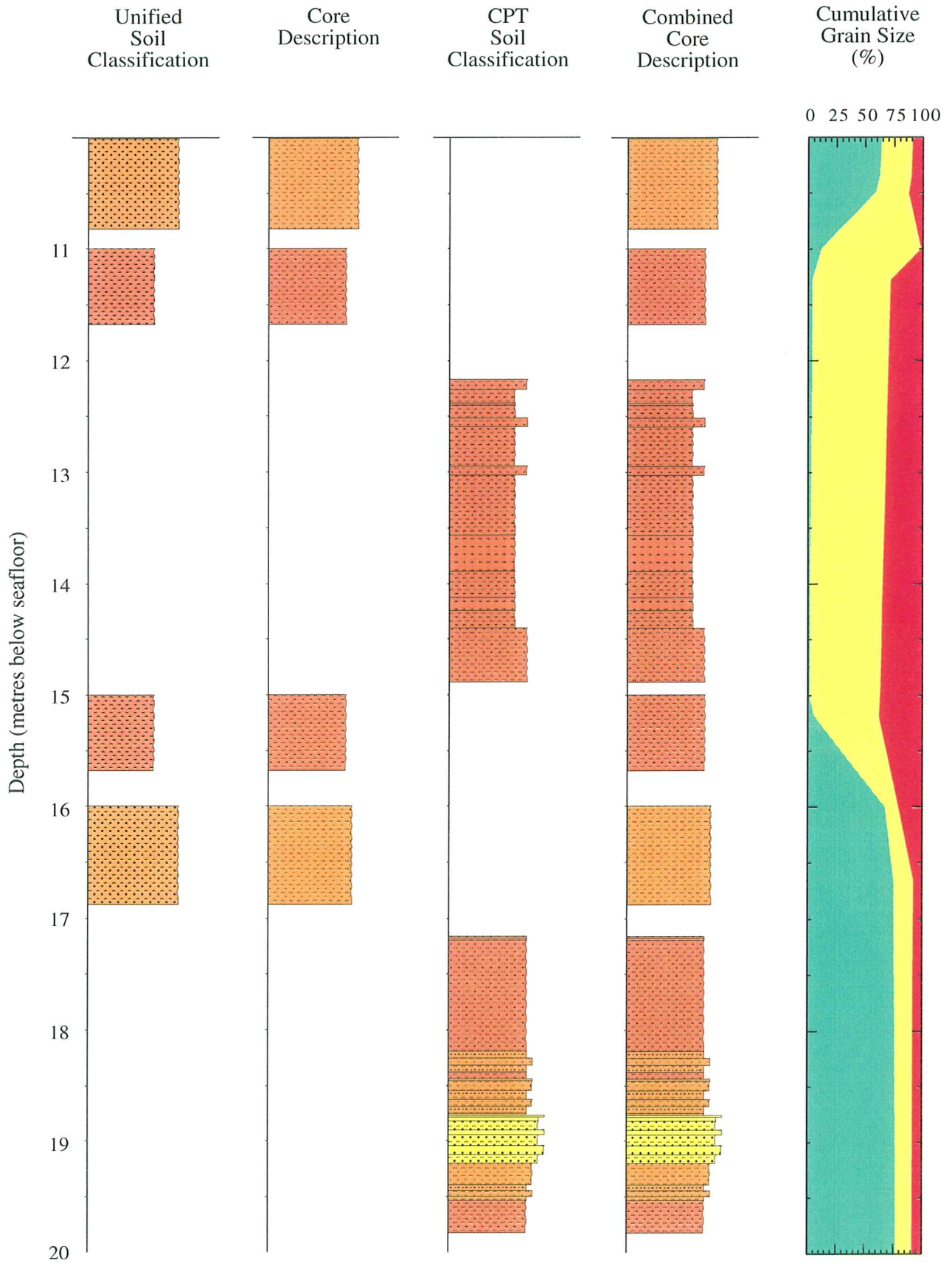


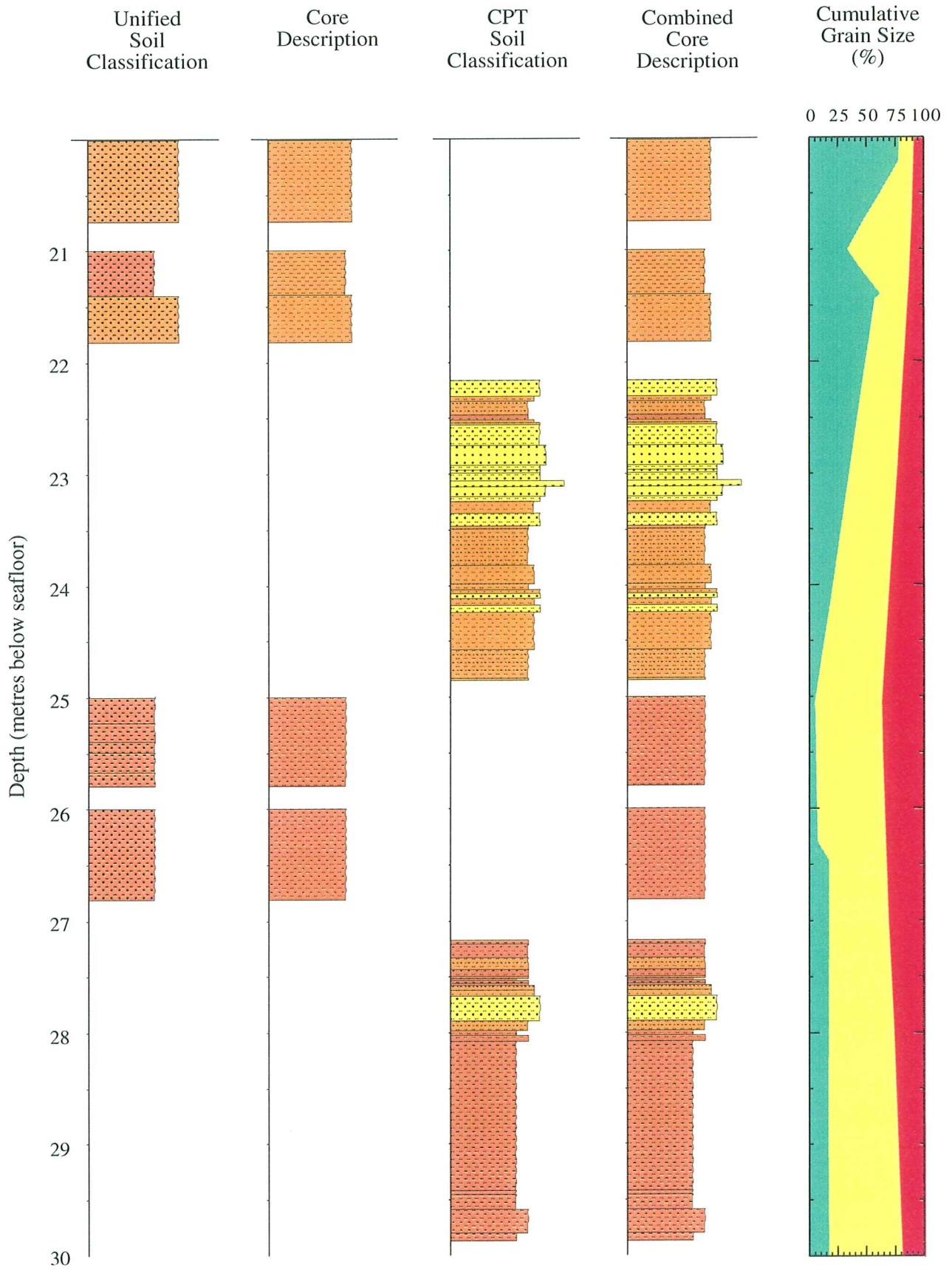
# GSI\_97

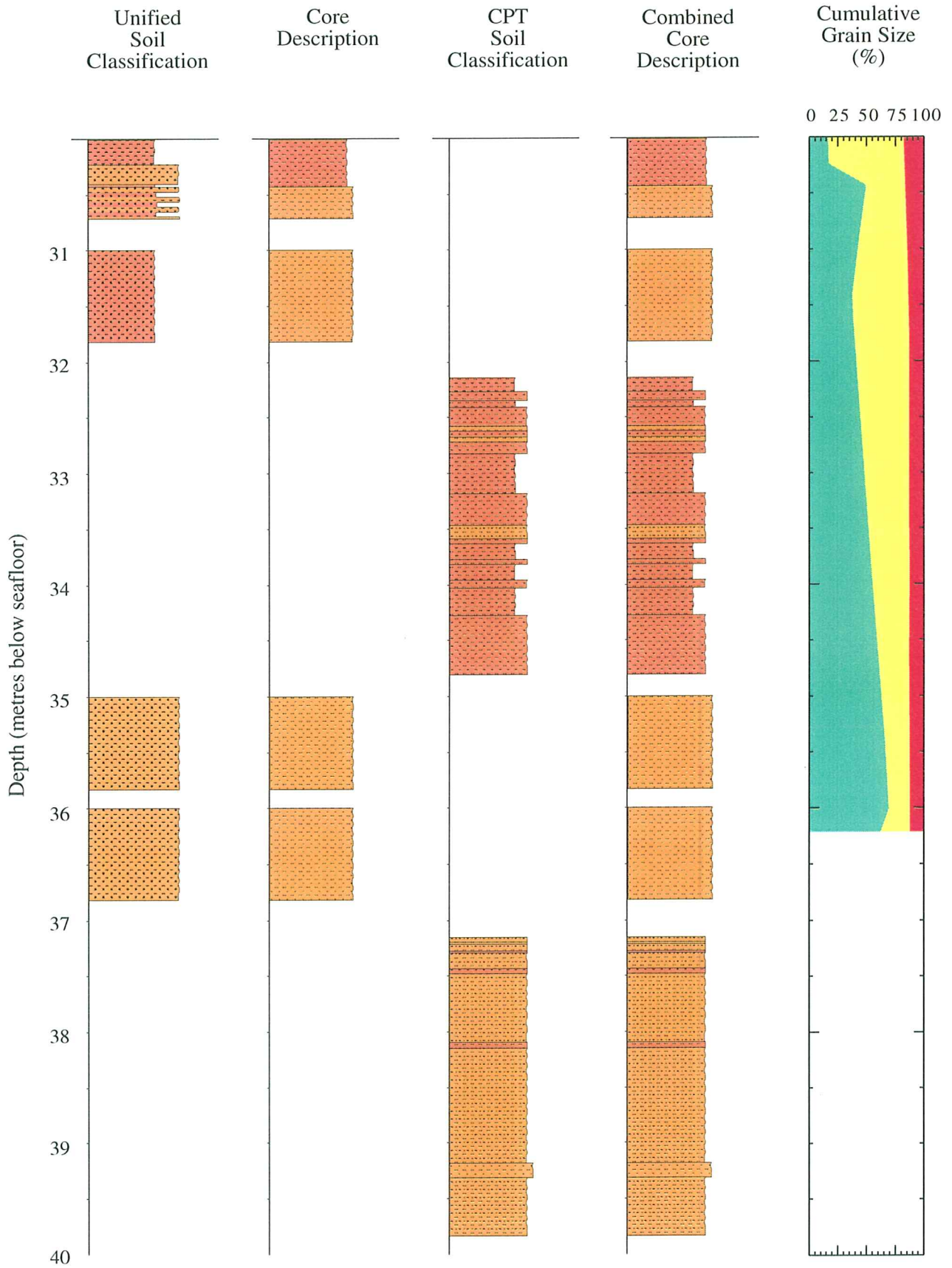


# A3\_97



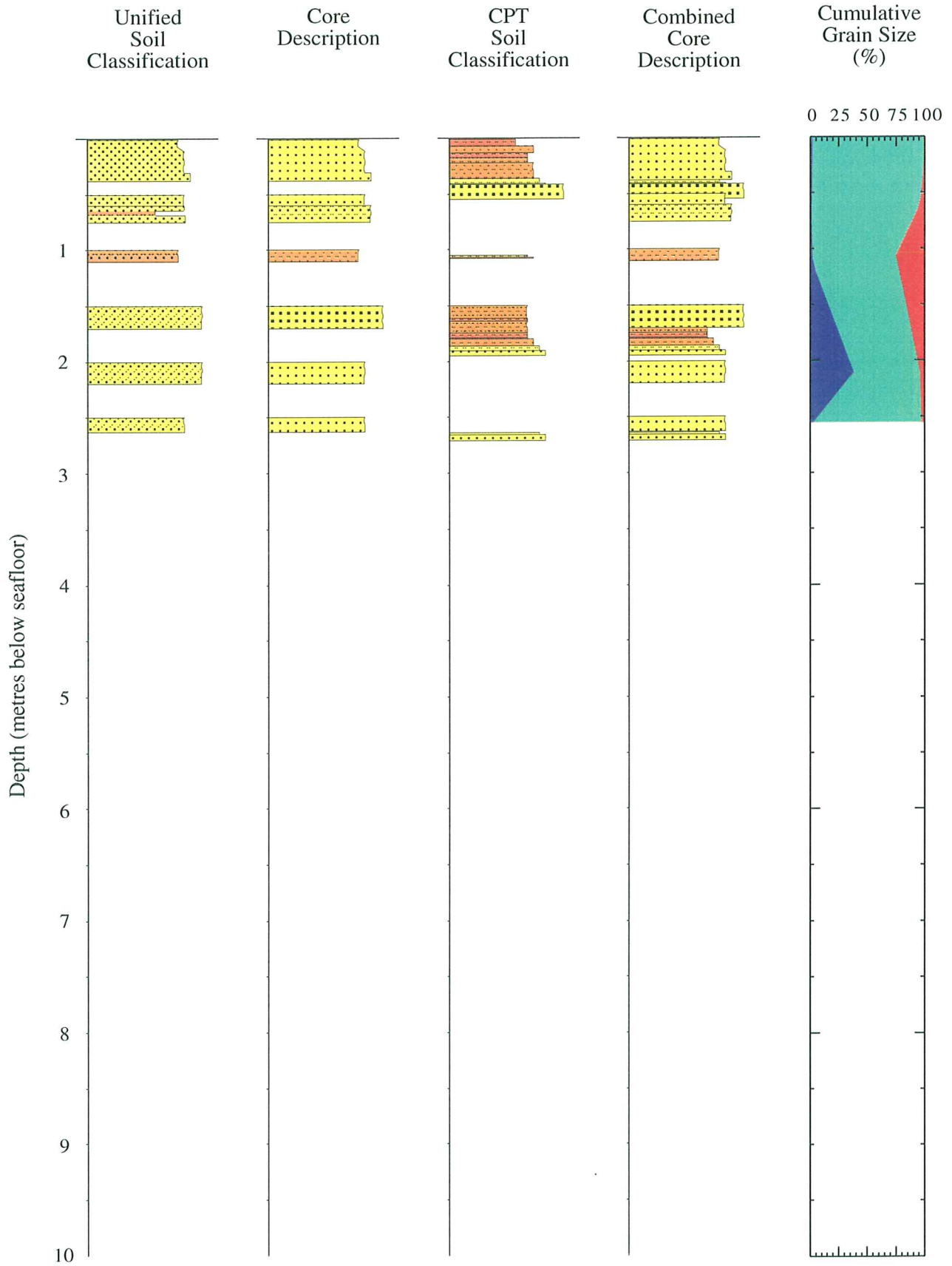




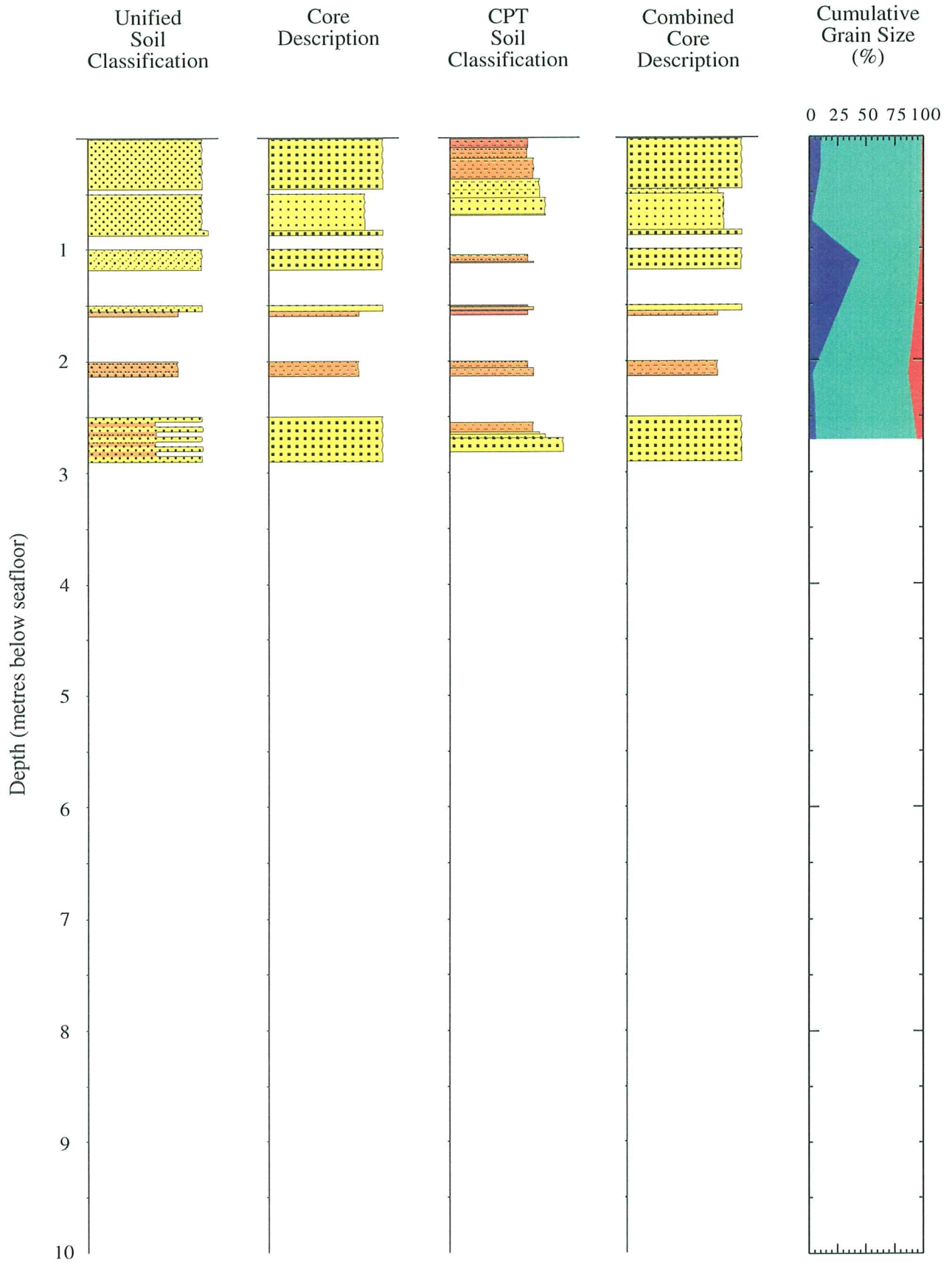




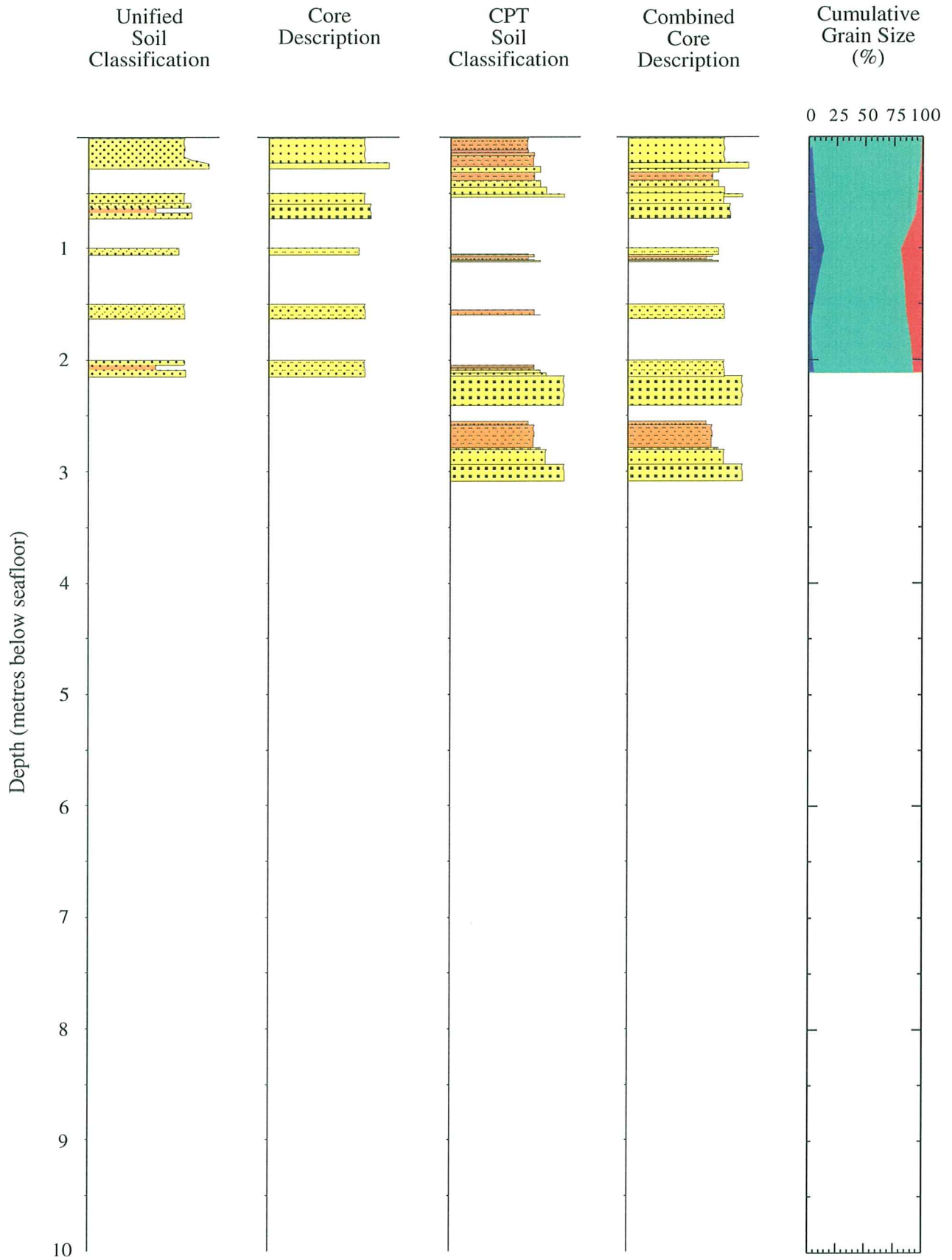
# FPSO\_B



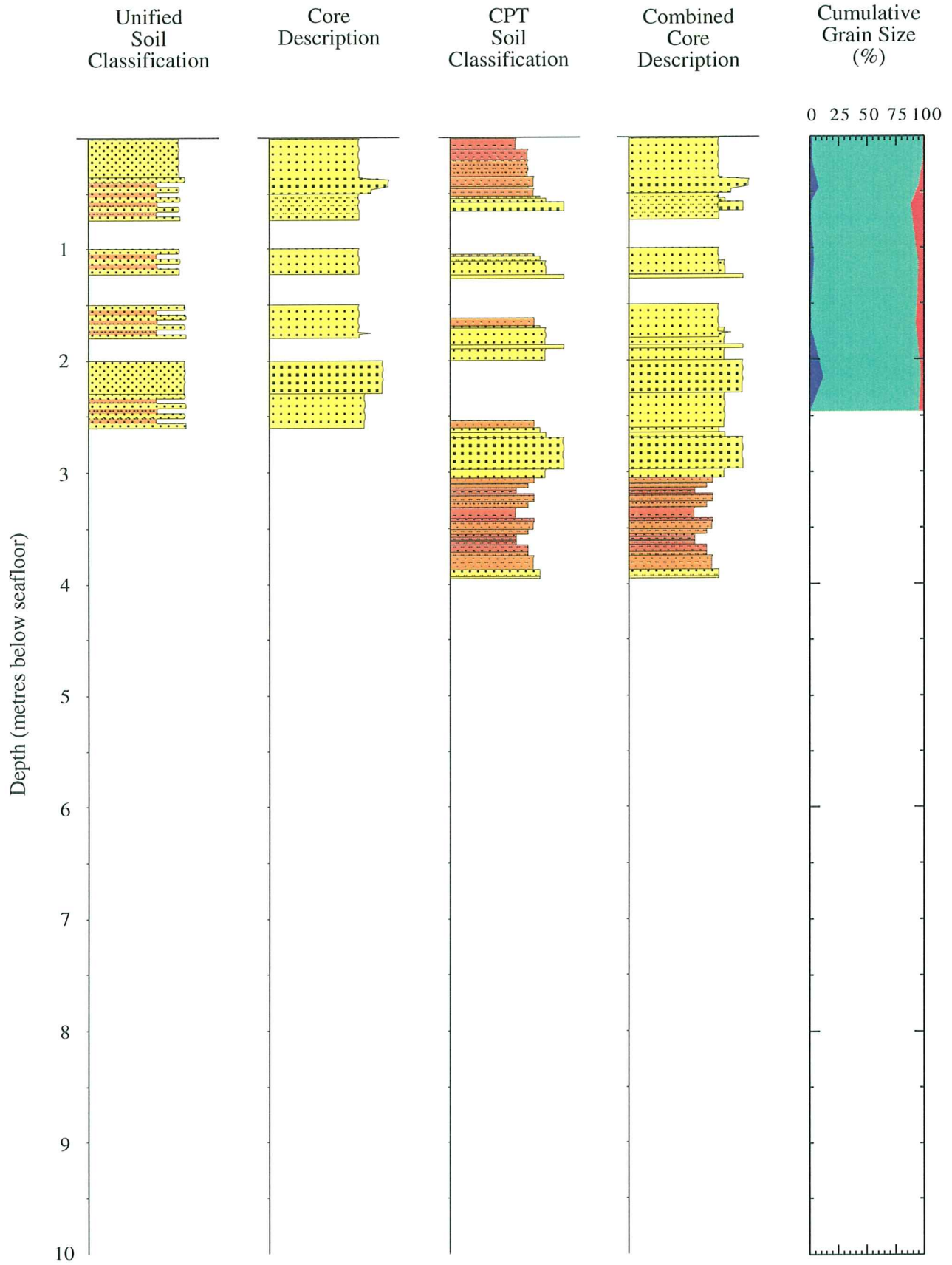
# FR1\_1B



# FR1\_3B



# FR4\_1B



## Appendix 2

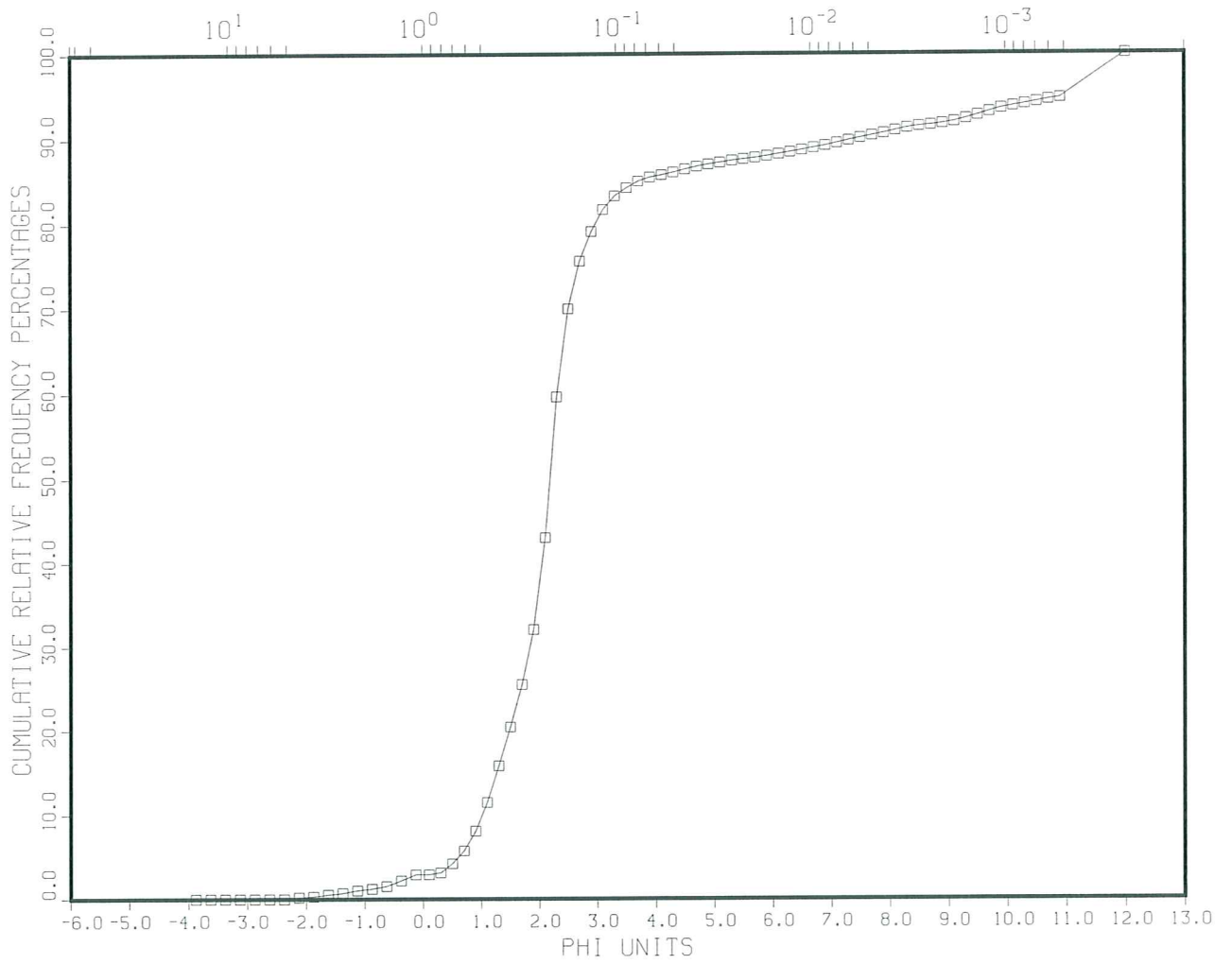
Calculation Results for  
The Sample with the Identifier:

V4.0  
5: 2:1998  
11421  
72  
GS1-97-4360-4364  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011421  
SWF00425  
4.360000000000000E+0003  
4.364000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

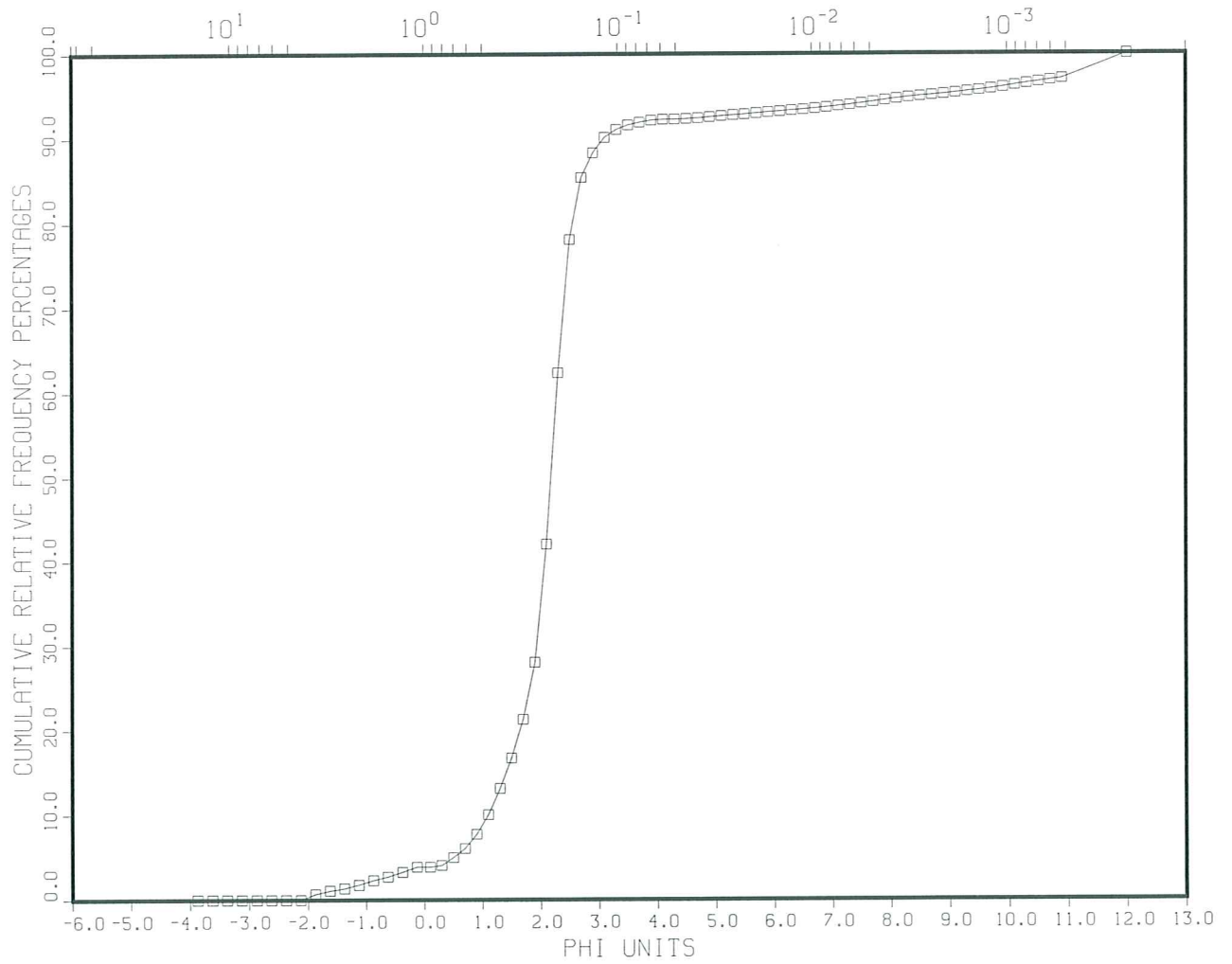
Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
		Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00
8.72e+00	-3.12	0.00

GS1-97-4360-4364, R0011421, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



GS1-97-4400-4404, RD011422, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS





7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.20	0.20
3.67e+00	-1.88	0.09	0.30
3.08e+00	-1.62	0.22	0.52
2.59e+00	-1.38	0.17	0.69
2.18e+00	-1.12	0.32	1.01
1.83e+00	-0.88	0.19	1.20
1.54e+00	-0.62	0.31	1.51
1.30e+00	-0.38	0.66	2.17
1.09e+00	-0.12	0.72	2.89
9.33e-01	0.10	0.01	2.90
8.12e-01	0.30	0.22	3.12
7.07e-01	0.50	1.09	4.21
6.16e-01	0.70	1.54	5.75
5.36e-01	0.90	2.35	8.10
4.67e-01	1.10	3.39	11.49
4.06e-01	1.30	4.36	15.86
3.54e-01	1.50	4.58	20.44
3.08e-01	1.70	5.14	25.58
2.68e-01	1.90	6.54	32.12
2.33e-01	2.10	10.95	43.07
2.03e-01	2.30	16.57	59.64
1.77e-01	2.50	10.35	69.99
1.54e-01	2.70	5.66	75.66
1.34e-01	2.90	3.48	79.13
1.17e-01	3.10	2.59	81.72
1.02e-01	3.30	1.62	83.35
8.84e-02	3.50	0.95	84.30
7.69e-02	3.70	0.78	85.08
6.70e-02	3.90	0.47	85.55
5.83e-02	4.10	0.27	85.82
5.08e-02	4.30	0.31	86.13
4.42e-02	4.50	0.35	86.48
3.85e-02	4.70	0.33	86.81
3.35e-02	4.90	0.25	87.06
2.92e-02	5.10	0.21	87.27
2.54e-02	5.30	0.23	87.50
2.21e-02	5.50	0.17	87.67
1.92e-02	5.70	0.15	87.82
1.67e-02	5.90	0.21	88.03
1.46e-02	6.10	0.23	88.26
1.27e-02	6.30	0.22	88.48
1.10e-02	6.50	0.24	88.73

9.62e-03	6.70	0.26	88.99
8.37e-03	6.90	0.25	89.23
7.29e-03	7.10	0.30	89.54
6.35e-03	7.30	0.32	89.85
5.52e-03	7.50	0.30	90.15
4.81e-03	7.70	0.26	90.41
4.19e-03	7.90	0.28	90.69
3.64e-03	8.10	0.31	91.01
3.17e-03	8.30	0.30	91.31
2.76e-03	8.50	0.20	91.51
2.40e-03	8.70	0.14	91.64
2.09e-03	8.90	0.16	91.80
1.82e-03	9.10	0.23	92.03
1.59e-03	9.30	0.33	92.36
1.38e-03	9.50	0.39	92.76
1.20e-03	9.70	0.42	93.17
1.05e-03	9.90	0.39	93.56
9.11e-04	10.10	0.25	93.81
7.93e-04	10.30	0.23	94.04
6.91e-04	10.50	0.25	94.29
6.01e-04	10.70	0.27	94.56
5.23e-04	10.90	0.19	94.75
2.44e-04	12.00	5.25	100.00

#### Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
1.01	84.54	5.14	9.31	14.45

#### Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
3.05	2.82	6.82	2.12

Calculation Results for  
The Sample with the Identifier:

V4.0  
5: 2:1998  
11422  
72  
GS1-97-4400-4404  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011422  
SWF00425  
4.400000000000000E+0003  
4.404000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.67	0.67
3.08e+00	-1.62	0.38	1.05
2.59e+00	-1.38	0.27	1.32
2.18e+00	-1.12	0.41	1.73
1.83e+00	-0.88	0.53	2.26
1.54e+00	-0.62	0.41	2.67
1.30e+00	-0.38	0.55	3.22
1.09e+00	-0.12	0.61	3.83
9.33e-01	0.10	0.00	3.83
8.12e-01	0.30	0.19	4.02
7.07e-01	0.50	0.93	4.95
6.16e-01	0.70	1.10	6.05
5.36e-01	0.90	1.69	7.74
4.67e-01	1.10	2.32	10.06
4.06e-01	1.30	3.08	13.14
3.54e-01	1.50	3.60	16.74
3.08e-01	1.70	4.57	21.30
2.68e-01	1.90	6.79	28.09
2.33e-01	2.10	13.98	42.07
2.03e-01	2.30	20.32	62.39
1.77e-01	2.50	15.69	78.08
1.54e-01	2.70	7.38	85.45
1.34e-01	2.90	2.90	88.35
1.17e-01	3.10	1.80	90.15
1.02e-01	3.30	0.91	91.07
8.84e-02	3.50	0.53	91.60
7.69e-02	3.70	0.32	91.91
6.70e-02	3.90	0.24	92.15
5.83e-02	4.10	0.11	92.26
5.08e-02	4.30	0.02	92.28
4.42e-02	4.50	0.04	92.32
3.85e-02	4.70	0.10	92.42
3.35e-02	4.90	0.12	92.53
2.92e-02	5.10	0.12	92.66
2.54e-02	5.30	0.10	92.75
2.21e-02	5.50	0.10	92.85
1.92e-02	5.70	0.13	92.98
1.67e-02	5.90	0.11	93.09
1.46e-02	6.10	0.10	93.19
1.27e-02	6.30	0.12	93.31

1.10e-02	6.50	0.10	93.41
9.62e-03	6.70	0.12	93.53
8.37e-03	6.90	0.13	93.66
7.29e-03	7.10	0.16	93.81
6.35e-03	7.30	0.15	93.96
5.52e-03	7.50	0.17	94.14
4.81e-03	7.70	0.18	94.31
4.19e-03	7.90	0.20	94.51
3.64e-03	8.10	0.18	94.69
3.17e-03	8.30	0.16	94.85
2.76e-03	8.50	0.13	94.98
2.40e-03	8.70	0.12	95.10
2.09e-03	8.90	0.12	95.22
1.82e-03	9.10	0.15	95.38
1.59e-03	9.30	0.16	95.54
1.38e-03	9.50	0.15	95.68
1.20e-03	9.70	0.17	95.85
1.05e-03	9.90	0.20	96.05
9.11e-04	10.10	0.23	96.27
7.93e-04	10.30	0.20	96.48
6.91e-04	10.50	0.19	96.67
6.01e-04	10.70	0.20	96.87
5.23e-04	10.90	0.18	97.05
2.44e-04	12.00	2.95	100.00

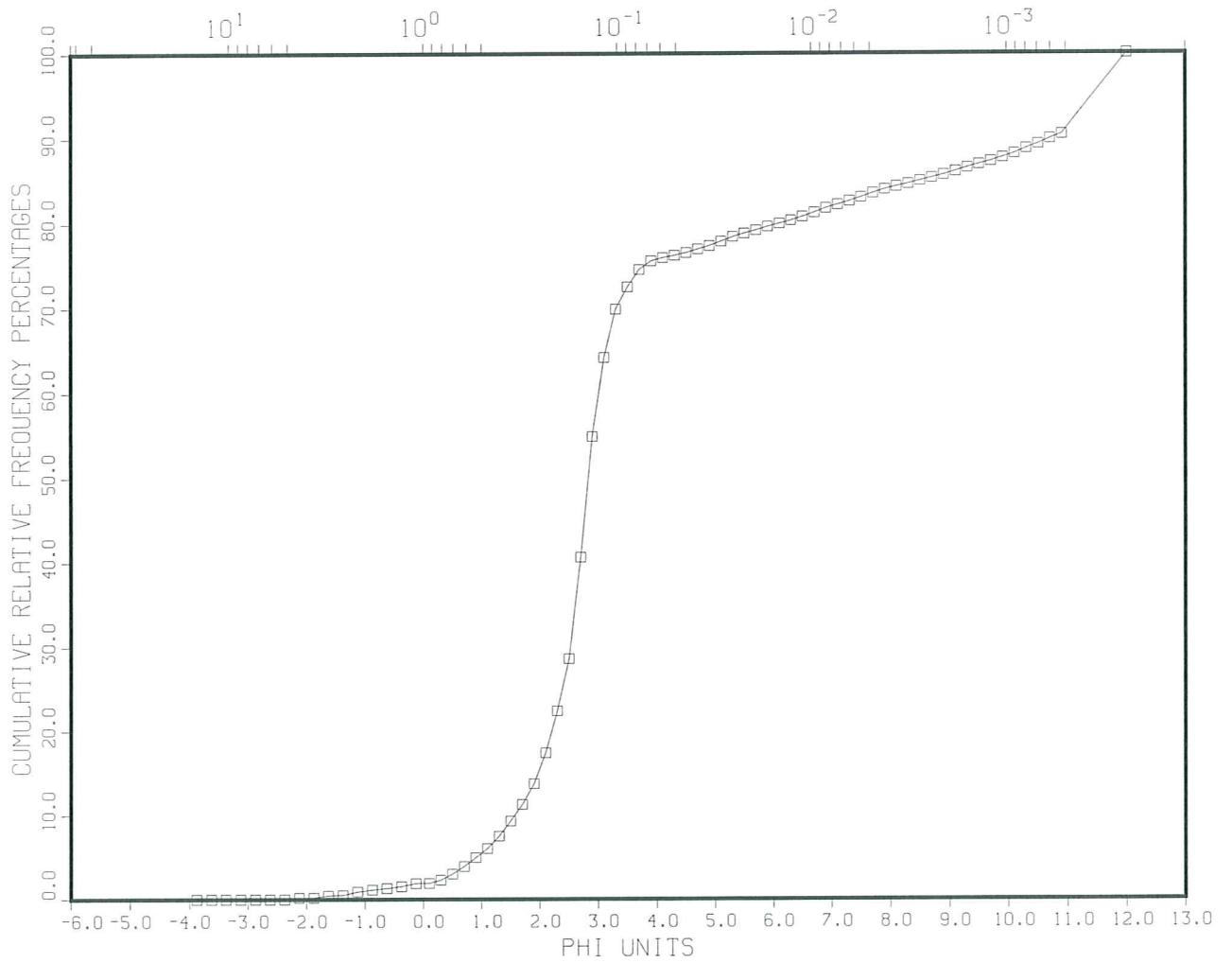
#### Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
1.73	90.42	2.36	5.49	7.85

#### Statistical Measures

Mean	Deviation	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
2.63	2.27	11.56	2.75

GS1-97-4442-4445, RD011423, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
5: 2:1998  
11423  
72  
GS1-97-4442-4445  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011423  
SWF00425  
4.44200000000000E+0003  
4.44500000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.20	0.20
3.67e+00	-1.88	0.00	0.20
3.08e+00	-1.62	0.25	0.45
2.59e+00	-1.38	0.05	0.49
2.18e+00	-1.12	0.41	0.90
1.83e+00	-0.88	0.22	1.12
1.54e+00	-0.62	0.18	1.30
1.30e+00	-0.38	0.23	1.53
1.09e+00	-0.12	0.36	1.88
9.33e-01	0.10	0.02	1.90
8.12e-01	0.30	0.40	2.30
7.07e-01	0.50	0.70	3.00
6.16e-01	0.70	0.90	3.90
5.36e-01	0.90	1.05	4.95
4.67e-01	1.10	1.06	6.02
4.06e-01	1.30	1.48	7.50
3.54e-01	1.50	1.82	9.32
3.08e-01	1.70	1.98	11.30
2.68e-01	1.90	2.46	13.76
2.33e-01	2.10	3.68	17.44
2.03e-01	2.30	4.96	22.40
1.77e-01	2.50	6.25	28.65
1.54e-01	2.70	12.02	40.67
1.34e-01	2.90	14.27	54.95
1.17e-01	3.10	9.34	64.28
1.02e-01	3.30	5.65	69.93
8.84e-02	3.50	2.59	72.52
7.69e-02	3.70	2.03	74.55
6.70e-02	3.90	1.01	75.56
5.83e-02	4.10	0.38	75.94
5.08e-02	4.30	0.27	76.22
4.42e-02	4.50	0.32	76.53
3.85e-02	4.70	0.43	76.96
3.35e-02	4.90	0.40	77.35
2.92e-02	5.10	0.52	77.87
2.54e-02	5.30	0.54	78.42
2.21e-02	5.50	0.40	78.82
1.92e-02	5.70	0.38	79.20
1.67e-02	5.90	0.43	79.62
1.46e-02	6.10	0.35	79.97
1.27e-02	6.30	0.37	80.34



1.10e-02	6.50	0.44	80.79
9.62e-03	6.70	0.48	81.27
8.37e-03	6.90	0.52	81.79
7.29e-03	7.10	0.40	82.19
6.35e-03	7.30	0.41	82.60
5.52e-03	7.50	0.45	83.05
4.81e-03	7.70	0.48	83.53
4.19e-03	7.90	0.44	83.97
3.64e-03	8.10	0.34	84.31
3.17e-03	8.30	0.30	84.61
2.76e-03	8.50	0.37	84.97
2.40e-03	8.70	0.34	85.32
2.09e-03	8.90	0.34	85.66
1.82e-03	9.10	0.42	86.08
1.59e-03	9.30	0.43	86.51
1.38e-03	9.50	0.39	86.90
1.20e-03	9.70	0.37	87.27
1.05e-03	9.90	0.44	87.71
9.11e-04	10.10	0.46	88.17
7.93e-04	10.30	0.60	88.77
6.91e-04	10.50	0.54	89.31
6.01e-04	10.70	0.62	89.93
5.23e-04	10.90	0.53	90.46
2.44e-04	12.00	9.54	100.00

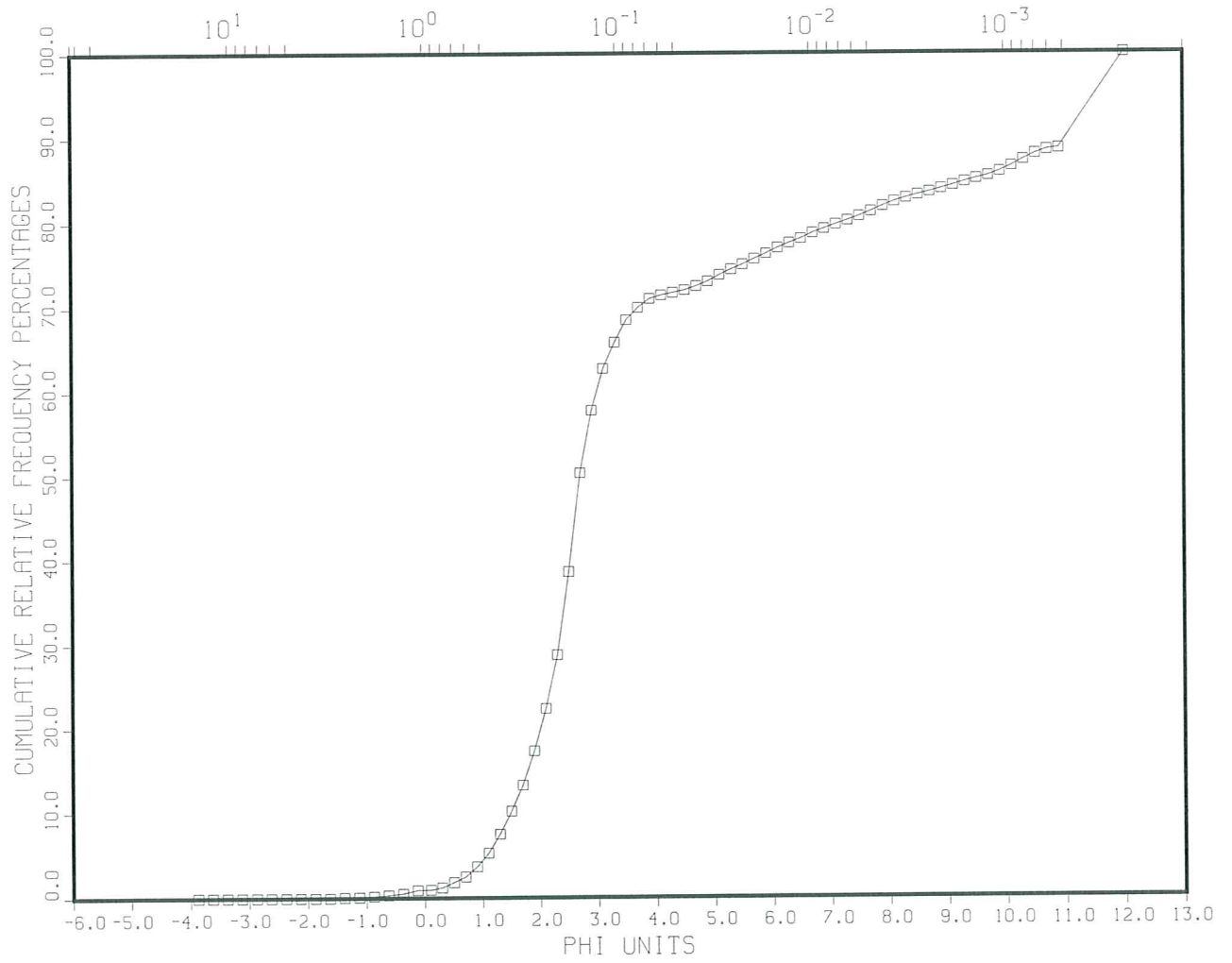
#### Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.90	74.66	8.41	16.03	24.44

#### Statistical Measures

Mean	Deviation	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.19	3.30	3.79	1.40

GS1-97-4514-4519, RD011424, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
5: 2:1998  
11424  
72  
GS1-97-4514-4519  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011424  
SWF00425  
4.514000000000000E+0003  
4.519000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.00	0.00
2.59e+00	-1.38	0.07	0.07
2.18e+00	-1.12	0.04	0.11
1.83e+00	-0.88	0.08	0.20
1.54e+00	-0.62	0.14	0.34
1.30e+00	-0.38	0.19	0.53
1.09e+00	-0.12	0.40	0.92
9.33e-01	0.10	0.02	0.95
8.12e-01	0.30	0.27	1.22
7.07e-01	0.50	0.61	1.83
6.16e-01	0.70	0.62	2.45
5.36e-01	0.90	1.18	3.63
4.67e-01	1.10	1.60	5.23
4.06e-01	1.30	2.25	7.47
3.54e-01	1.50	2.74	10.22
3.08e-01	1.70	3.05	13.27
2.68e-01	1.90	4.07	17.33
2.33e-01	2.10	5.04	22.37
2.03e-01	2.30	6.44	28.81
1.77e-01	2.50	9.82	38.63
1.54e-01	2.70	11.73	50.36
1.34e-01	2.90	7.43	57.78
1.17e-01	3.10	4.95	62.74
1.02e-01	3.30	3.09	65.83
8.84e-02	3.50	2.65	68.48
7.69e-02	3.70	1.46	69.94
6.70e-02	3.90	1.05	71.00
5.83e-02	4.10	0.41	71.41
5.08e-02	4.30	0.29	71.70
4.42e-02	4.50	0.31	72.00
3.85e-02	4.70	0.46	72.46
3.35e-02	4.90	0.56	73.02
2.92e-02	5.10	0.74	73.77
2.54e-02	5.30	0.65	74.42
2.21e-02	5.50	0.57	74.99
1.92e-02	5.70	0.66	75.64
1.67e-02	5.90	0.62	76.27
1.46e-02	6.10	0.66	76.93
1.27e-02	6.30	0.58	77.51

1.10e-02	6.50	0.52	78.03
9.62e-03	6.70	0.66	78.69
8.37e-03	6.90	0.51	79.20
7.29e-03	7.10	0.51	79.71
6.35e-03	7.30	0.47	80.17
5.52e-03	7.50	0.51	80.68
4.81e-03	7.70	0.56	81.24
4.19e-03	7.90	0.62	81.86
3.64e-03	8.10	0.54	82.40
3.17e-03	8.30	0.43	82.82
2.76e-03	8.50	0.36	83.19
2.40e-03	8.70	0.36	83.54
2.09e-03	8.90	0.37	83.91
1.82e-03	9.10	0.39	84.30
1.59e-03	9.30	0.42	84.72
1.38e-03	9.50	0.37	85.09
1.20e-03	9.70	0.35	85.44
1.05e-03	9.90	0.50	85.93
9.11e-04	10.10	0.64	86.58
7.93e-04	10.30	0.75	87.33
6.91e-04	10.50	0.67	88.00
6.01e-04	10.70	0.48	88.47
5.23e-04	10.90	0.16	88.64
2.44e-04	12.00	11.36	100.00

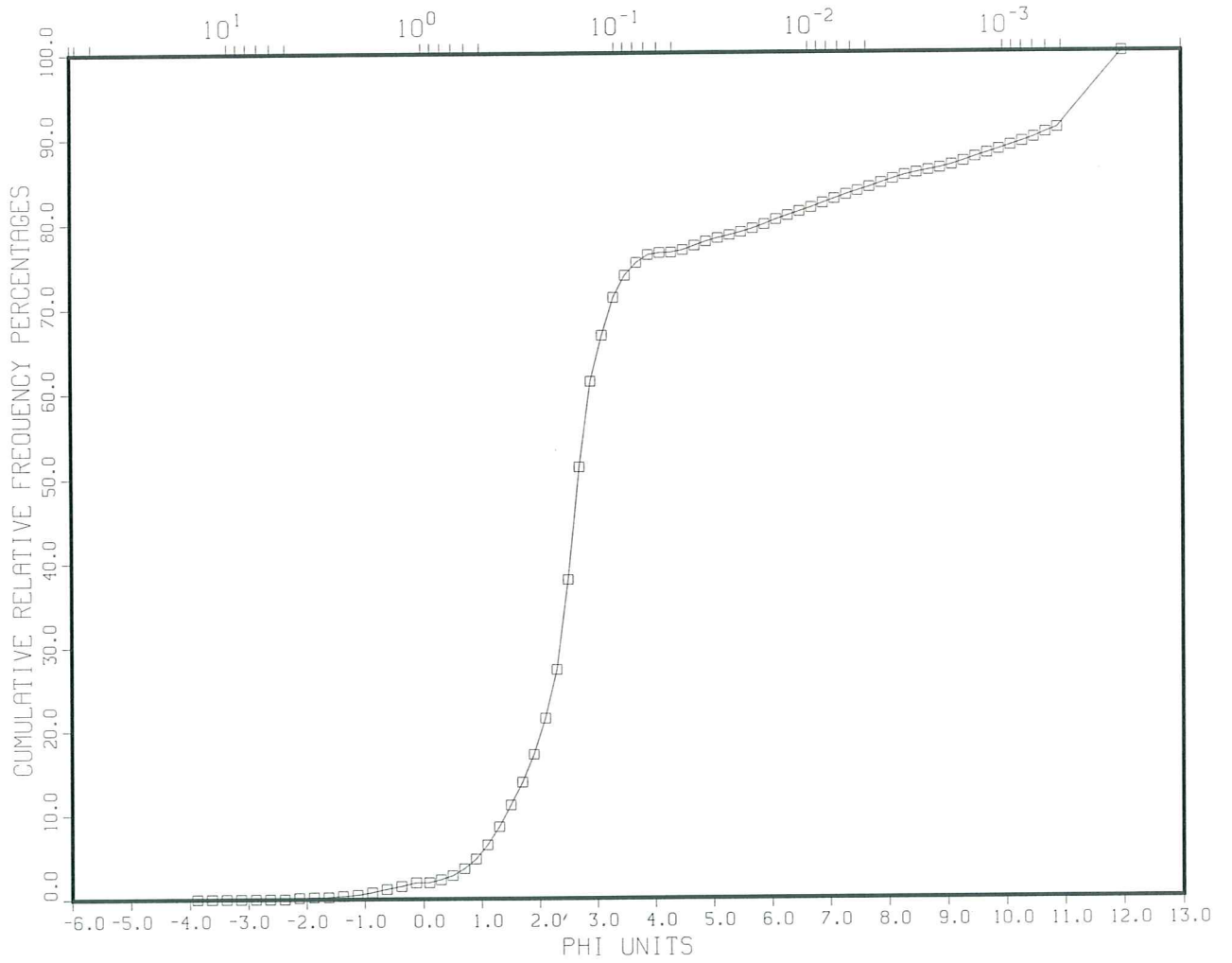
Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.11	70.88	10.86	18.14	29.00

Statistical Measures

Mean	Deviation	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.38	3.48	3.20	1.27

GS1-97-4598-4602, RD011425, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
6: 2:1998  
11425  
72  
GS1-97-4598-4602  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011425  
SWF00425  
4.598000000000000E+0003  
4.602000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.17	0.17
3.67e+00	-1.88	0.07	0.24
3.08e+00	-1.62	0.00	0.24
2.59e+00	-1.38	0.11	0.36
2.18e+00	-1.12	0.13	0.49
1.83e+00	-0.88	0.30	0.79
1.54e+00	-0.62	0.38	1.17
1.30e+00	-0.38	0.33	1.50
1.09e+00	-0.12	0.44	1.94
9.33e-01	0.10	0.00	1.94
8.12e-01	0.30	0.34	2.28
7.07e-01	0.50	0.47	2.75
6.16e-01	0.70	0.81	3.56
5.36e-01	0.90	1.15	4.71
4.67e-01	1.10	1.68	6.39
4.06e-01	1.30	2.16	8.55
3.54e-01	1.50	2.58	11.13
3.08e-01	1.70	2.70	13.83
2.68e-01	1.90	3.31	17.14
2.33e-01	2.10	4.31	21.45
2.03e-01	2.30	5.82	27.27
1.77e-01	2.50	10.69	37.95
1.54e-01	2.70	13.33	51.28
1.34e-01	2.90	10.06	61.34
1.17e-01	3.10	5.42	66.76
1.02e-01	3.30	4.47	71.22
8.84e-02	3.50	2.57	73.79
7.69e-02	3.70	1.50	75.29
6.70e-02	3.90	0.91	76.20
5.83e-02	4.10	0.23	76.43
5.08e-02	4.30	0.05	76.48
4.42e-02	4.50	0.27	76.76
3.85e-02	4.70	0.52	77.27
3.35e-02	4.90	0.50	77.77
2.92e-02	5.10	0.40	78.18
2.54e-02	5.30	0.34	78.52
2.21e-02	5.50	0.36	78.88
1.92e-02	5.70	0.42	79.30
1.67e-02	5.90	0.50	79.80
1.46e-02	6.10	0.57	80.37
1.27e-02	6.30	0.47	80.84



1.10e-02	6.50	0.48	81.31
9.62e-03	6.70	0.47	81.78
8.37e-03	6.90	0.51	82.29
7.29e-03	7.10	0.50	82.79
6.35e-03	7.30	0.50	83.29
5.52e-03	7.50	0.43	83.72
4.81e-03	7.70	0.43	84.15
4.19e-03	7.90	0.50	84.65
3.64e-03	8.10	0.46	85.11
3.17e-03	8.30	0.43	85.54
2.76e-03	8.50	0.30	85.84
2.40e-03	8.70	0.28	86.12
2.09e-03	8.90	0.26	86.38
1.82e-03	9.10	0.36	86.74
1.59e-03	9.30	0.43	87.17
1.38e-03	9.50	0.49	87.66
1.20e-03	9.70	0.45	88.10
1.05e-03	9.90	0.43	88.54
9.11e-04	10.10	0.47	89.01
7.93e-04	10.30	0.44	89.45
6.91e-04	10.50	0.48	89.93
6.01e-04	10.70	0.59	90.51
5.23e-04	10.90	0.53	91.05
2.44e-04	12.00	8.95	100.00

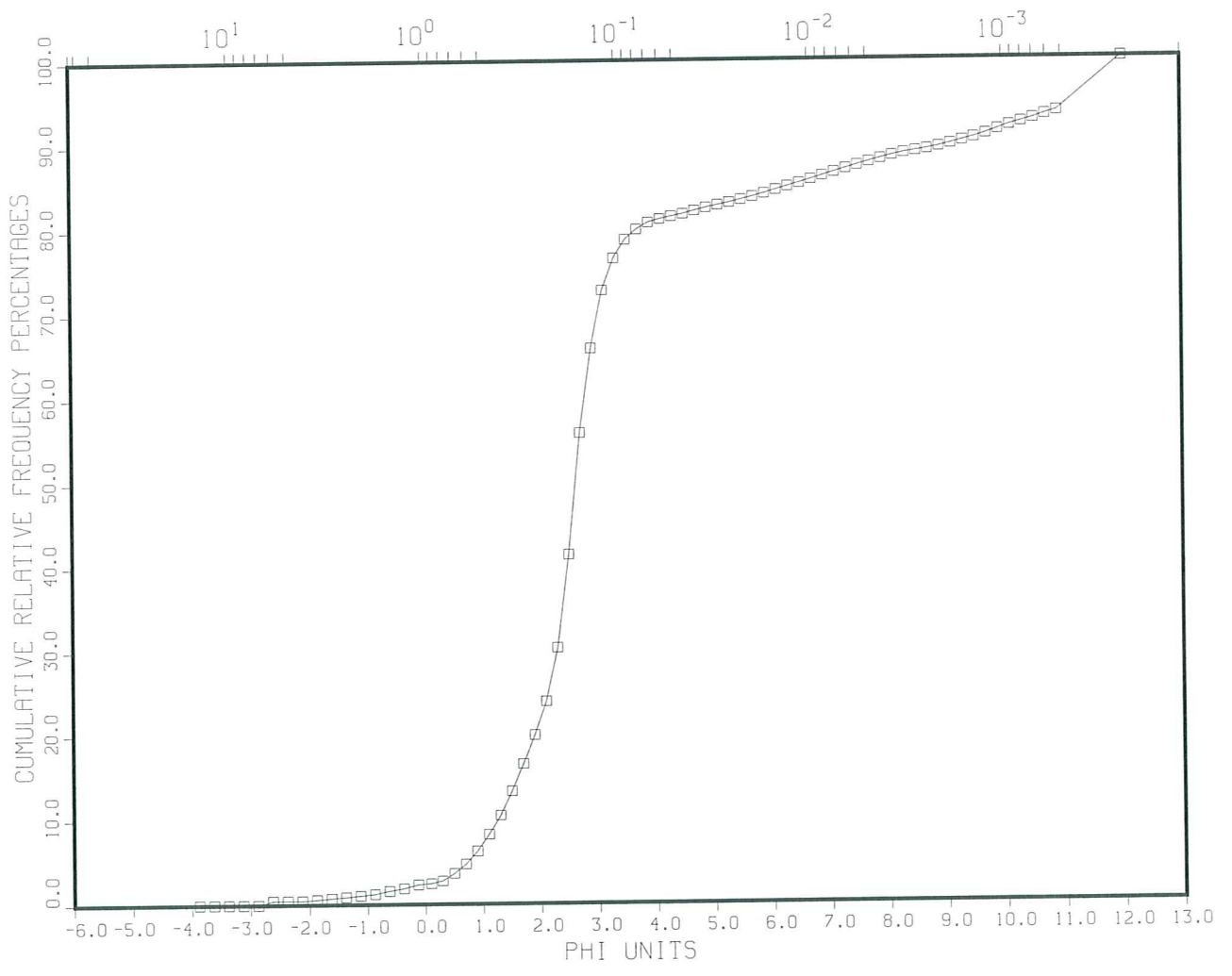
#### Grain Size Breakdown

	%	%	%	%	%
Gravel	0.49	Sand	75.71	Silt	8.45
		Clay	15.35	Mud	23.80

#### Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.05	3.28	3.92	1.45

GS1-97-4691-4695, R0011426, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
6: 2:1998  
11426  
72  
GS1-97-4691-4695  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011426  
SWF00425  
4.691000000000000E+0003  
4.695000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.47	0.47
5.19e+00	-2.38	0.00	0.47
4.36e+00	-2.12	0.00	0.47
3.67e+00	-1.88	0.12	0.59
3.08e+00	-1.62	0.15	0.74
2.59e+00	-1.38	0.13	0.87
2.18e+00	-1.12	0.17	1.05
1.83e+00	-0.88	0.17	1.22
1.54e+00	-0.62	0.36	1.58
1.30e+00	-0.38	0.29	1.87
1.09e+00	-0.12	0.44	2.31
9.33e-01	0.10	0.13	2.43
8.12e-01	0.30	0.33	2.76
7.07e-01	0.50	0.87	3.63
6.16e-01	0.70	1.11	4.74
5.36e-01	0.90	1.53	6.26
4.67e-01	1.10	1.98	8.24
4.06e-01	1.30	2.24	10.49
3.54e-01	1.50	2.89	13.38
3.08e-01	1.70	3.21	16.58
2.68e-01	1.90	3.39	19.98
2.33e-01	2.10	4.00	23.97
2.03e-01	2.30	6.37	30.34
1.77e-01	2.50	11.06	41.40
1.54e-01	2.70	14.47	55.87
1.34e-01	2.90	10.04	65.91
1.17e-01	3.10	6.85	72.76
1.02e-01	3.30	3.78	76.54
8.84e-02	3.50	2.19	78.73
7.69e-02	3.70	1.22	79.95
6.70e-02	3.90	0.81	80.75
5.83e-02	4.10	0.41	81.16
5.08e-02	4.30	0.30	81.46
4.42e-02	4.50	0.28	81.75
3.85e-02	4.70	0.38	82.12
3.35e-02	4.90	0.35	82.48
2.92e-02	5.10	0.30	82.78
2.54e-02	5.30	0.29	83.07
2.21e-02	5.50	0.34	83.41
1.92e-02	5.70	0.33	83.74
1.67e-02	5.90	0.37	84.12
1.46e-02	6.10	0.42	84.53
1.27e-02	6.30	0.41	84.94

1.10e-02	6.50	0.39	85.32
9.62e-03	6.70	0.42	85.74
8.37e-03	6.90	0.43	86.17
7.29e-03	7.10	0.42	86.59
6.35e-03	7.30	0.41	87.00
5.52e-03	7.50	0.40	87.40
4.81e-03	7.70	0.38	87.79
4.19e-03	7.90	0.36	88.15
3.64e-03	8.10	0.36	88.51
3.17e-03	8.30	0.29	88.81
2.76e-03	8.50	0.22	89.02
2.40e-03	8.70	0.22	89.24
2.09e-03	8.90	0.28	89.52
1.82e-03	9.10	0.34	89.86
1.59e-03	9.30	0.36	90.22
1.38e-03	9.50	0.36	90.57
1.20e-03	9.70	0.43	91.01
1.05e-03	9.90	0.50	91.50
9.11e-04	10.10	0.49	92.00
7.93e-04	10.30	0.40	92.39
6.91e-04	10.50	0.39	92.78
6.01e-04	10.70	0.47	93.25
5.23e-04	10.90	0.41	93.66
2.44e-04	12.00	6.34	100.00

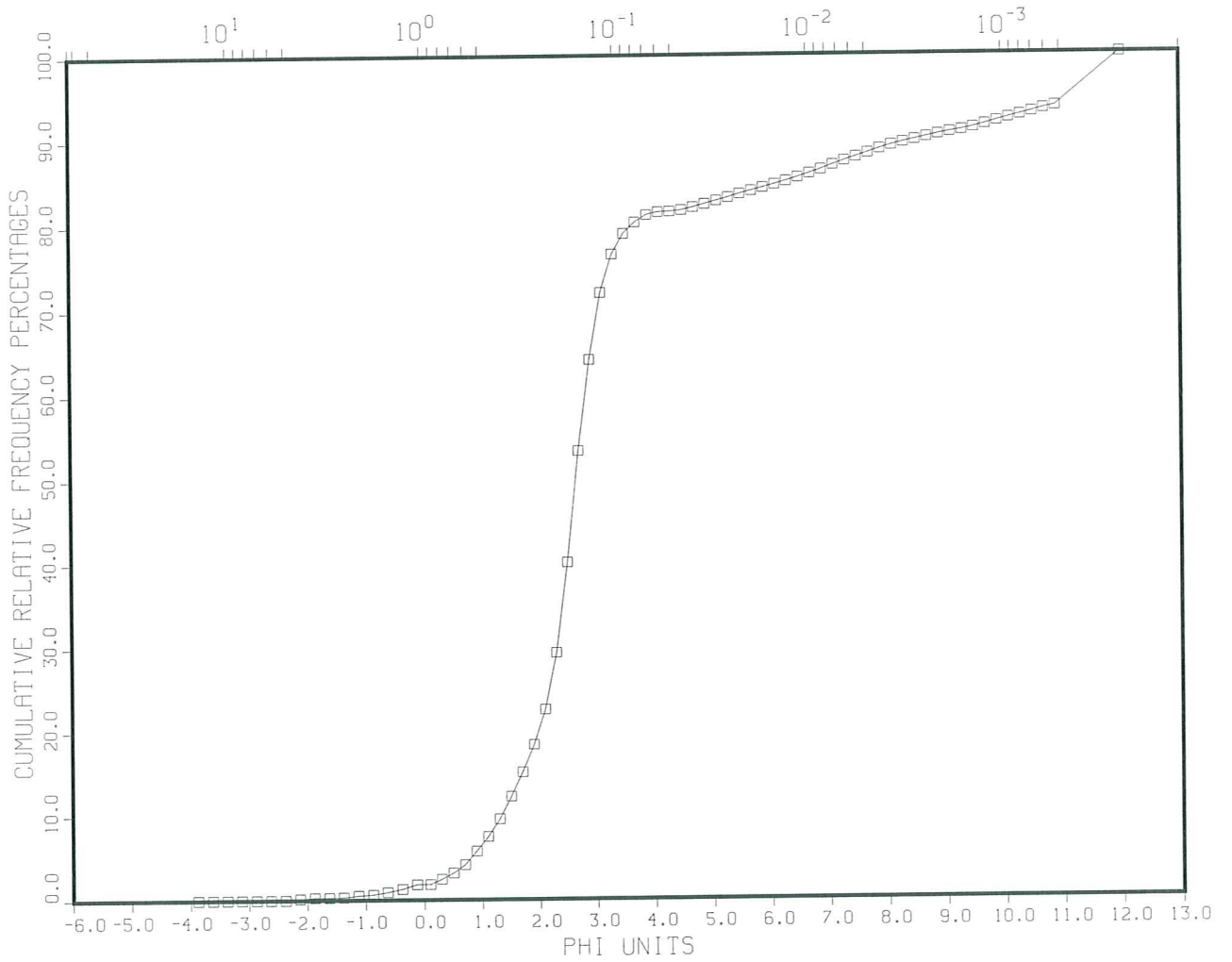
#### Grain Size Breakdown

	%	%	%	%	%
Gravel	1.05	Sand	79.71	Silt	7.40
		Clay	11.85	Mud	19.25

#### Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
3.63	3.01	5.10	1.68

GS1-97-4760-4764, RD011427, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
6: 2:1998  
11427  
72  
GS1-97-4760-4764  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011427  
SWF00425  
4.760000000000000E+0003  
4.764000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.17	0.17
3.67e+00	-1.88	0.12	0.29
3.08e+00	-1.62	0.00	0.29
2.59e+00	-1.38	0.03	0.32
2.18e+00	-1.12	0.20	0.51
1.83e+00	-0.88	0.11	0.63
1.54e+00	-0.62	0.28	0.90
1.30e+00	-0.38	0.37	1.27
1.09e+00	-0.12	0.54	1.81
9.33e-01	0.10	0.02	1.83
8.12e-01	0.30	0.62	2.44
7.07e-01	0.50	0.73	3.17
6.16e-01	0.70	0.96	4.14
5.36e-01	0.90	1.63	5.76
4.67e-01	1.10	1.71	7.47
4.06e-01	1.30	2.11	9.58
3.54e-01	1.50	2.70	12.28
3.08e-01	1.70	2.92	15.20
2.68e-01	1.90	3.27	18.47
2.33e-01	2.10	4.19	22.66
2.03e-01	2.30	6.75	29.41
1.77e-01	2.50	10.72	40.13
1.54e-01	2.70	13.26	53.40
1.34e-01	2.90	10.76	64.15
1.17e-01	3.10	7.87	72.02
1.02e-01	3.30	4.51	76.53
8.84e-02	3.50	2.42	78.96
7.69e-02	3.70	1.34	80.30
6.70e-02	3.90	0.88	81.18
5.83e-02	4.10	0.32	81.50
5.08e-02	4.30	0.06	81.56
4.42e-02	4.50	0.16	81.72
3.85e-02	4.70	0.31	82.03
3.35e-02	4.90	0.39	82.41
2.92e-02	5.10	0.38	82.80
2.54e-02	5.30	0.38	83.18
2.21e-02	5.50	0.42	83.60
1.92e-02	5.70	0.36	83.96
1.67e-02	5.90	0.35	84.31
1.46e-02	6.10	0.38	84.69
1.27e-02	6.30	0.39	85.08



1.10e-02	6.50	0.42	85.50
9.62e-03	6.70	0.46	85.96
8.37e-03	6.90	0.46	86.41
7.29e-03	7.10	0.53	86.94
6.35e-03	7.30	0.49	87.43
5.52e-03	7.50	0.44	87.87
4.81e-03	7.70	0.46	88.33
4.19e-03	7.90	0.46	88.79
3.64e-03	8.10	0.41	89.20
3.17e-03	8.30	0.35	89.55
2.76e-03	8.50	0.30	89.85
2.40e-03	8.70	0.31	90.16
2.09e-03	8.90	0.30	90.46
1.82e-03	9.10	0.27	90.73
1.59e-03	9.30	0.22	90.95
1.38e-03	9.50	0.29	91.25
1.20e-03	9.70	0.37	91.61
1.05e-03	9.90	0.39	92.00
9.11e-04	10.10	0.37	92.37
7.93e-04	10.30	0.34	92.71
6.91e-04	10.50	0.35	93.07
6.01e-04	10.70	0.37	93.44
5.23e-04	10.90	0.29	93.73
2.44e-04	12.00	6.27	100.00

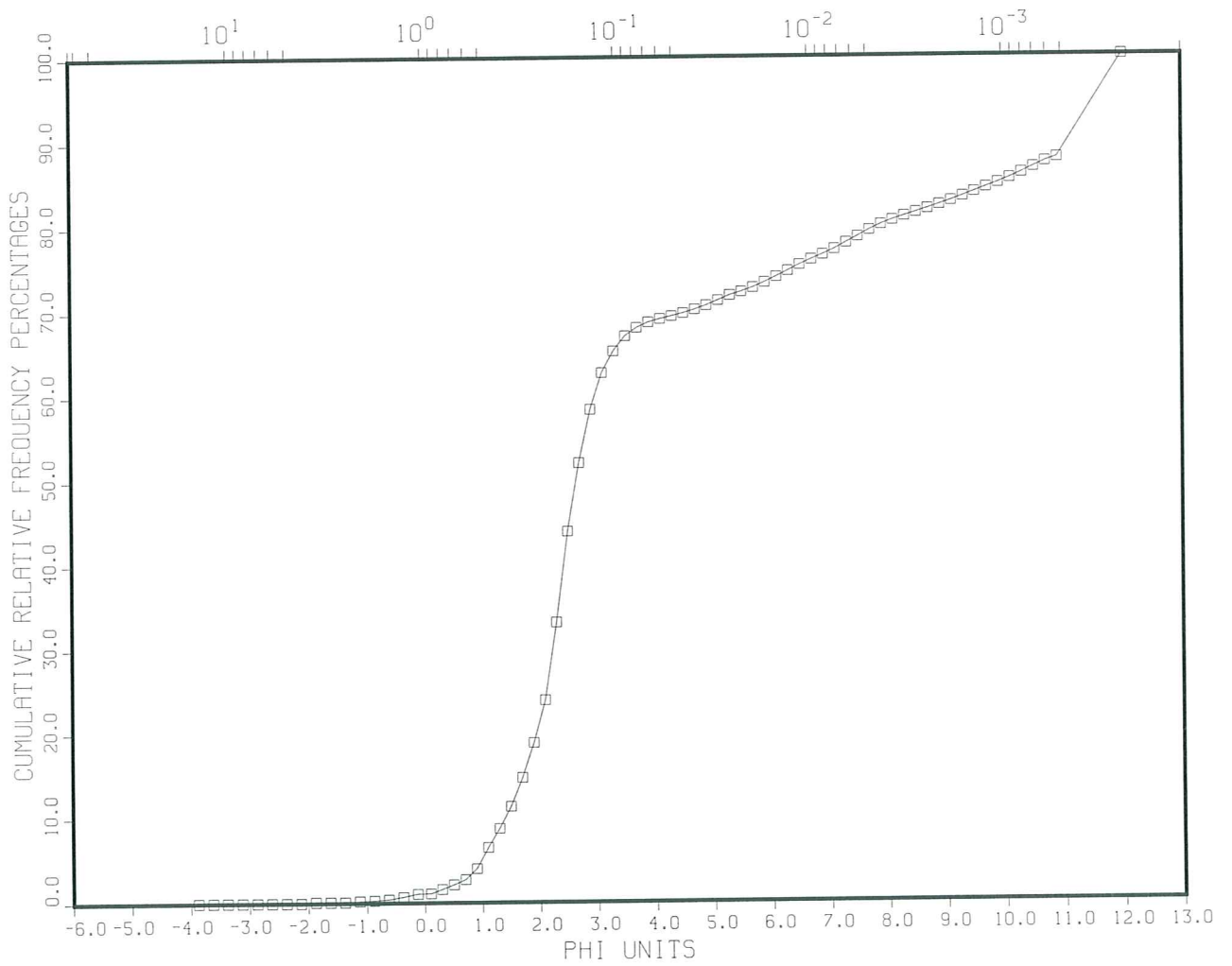
#### Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.51	80.67	7.61	11.21	18.82

#### Statistical Measures

Mean	Deviation	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
3.65	2.93	5.35	1.78

GS1-97-4790-4795, RD011428, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
 6: 2:1998  
 11428  
 72  
 GS1-97-4790-4795  
 97NORSKALD  
 970001  
 G. SONNICHSEN  
 TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
 RD011428  
 SWF00425  
 4.790000000000000E+0003  
 4.795000000000000E+0003  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 53292  
 GS1-97  
 GS1-97  
 BOREHOLE  
 BOREHOLE  
 46:27.72  
 -48:29.27  
 92.90  
 n lines for future expansion  
 #

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.11	0.11
3.08e+00	-1.62	0.00	0.11
2.59e+00	-1.38	0.00	0.11
2.18e+00	-1.12	0.12	0.22
1.83e+00	-0.88	0.07	0.29
1.54e+00	-0.62	0.11	0.40
1.30e+00	-0.38	0.29	0.69
1.09e+00	-0.12	0.36	1.05
9.33e-01	0.10	0.03	1.07
8.12e-01	0.30	0.51	1.58
7.07e-01	0.50	0.53	2.12
6.16e-01	0.70	0.60	2.72
5.36e-01	0.90	1.30	4.01
4.67e-01	1.10	2.47	6.48
4.06e-01	1.30	2.23	8.71
3.54e-01	1.50	2.60	11.31
3.08e-01	1.70	3.42	14.73
2.68e-01	1.90	4.12	18.86
2.33e-01	2.10	5.11	23.96
2.03e-01	2.30	9.24	33.21
1.77e-01	2.50	10.73	43.93
1.54e-01	2.70	8.18	52.11
1.34e-01	2.90	6.28	58.39
1.17e-01	3.10	4.34	62.73
1.02e-01	3.30	2.58	65.31
8.84e-02	3.50	1.77	67.08
7.69e-02	3.70	0.98	68.06
6.70e-02	3.90	0.63	68.69
5.83e-02	4.10	0.39	69.08
5.08e-02	4.30	0.32	69.40
4.42e-02	4.50	0.34	69.74
3.85e-02	4.70	0.41	70.16
3.35e-02	4.90	0.49	70.64
2.92e-02	5.10	0.58	71.22
2.54e-02	5.30	0.60	71.82
2.21e-02	5.50	0.41	72.24
1.92e-02	5.70	0.48	72.72
1.67e-02	5.90	0.60	73.33
1.46e-02	6.10	0.67	73.99
1.27e-02	6.30	0.70	74.69

1.10e-02	6.50	0.71	75.39
9.62e-03	6.70	0.62	76.01
8.37e-03	6.90	0.58	76.59
7.29e-03	7.10	0.62	77.21
6.35e-03	7.30	0.74	77.95
5.52e-03	7.50	0.73	78.68
4.81e-03	7.70	0.74	79.42
4.19e-03	7.90	0.65	80.07
3.64e-03	8.10	0.51	80.59
3.17e-03	8.30	0.45	81.04
2.76e-03	8.50	0.44	81.48
2.40e-03	8.70	0.44	81.91
2.09e-03	8.90	0.45	82.37
1.82e-03	9.10	0.47	82.84
1.59e-03	9.30	0.50	83.34
1.38e-03	9.50	0.52	83.87
1.20e-03	9.70	0.53	84.40
1.05e-03	9.90	0.50	84.90
9.11e-04	10.10	0.56	85.46
7.93e-04	10.30	0.63	86.09
6.91e-04	10.50	0.66	86.75
6.01e-04	10.70	0.65	87.40
5.23e-04	10.90	0.47	87.87
2.44e-04	12.00	12.13	100.00

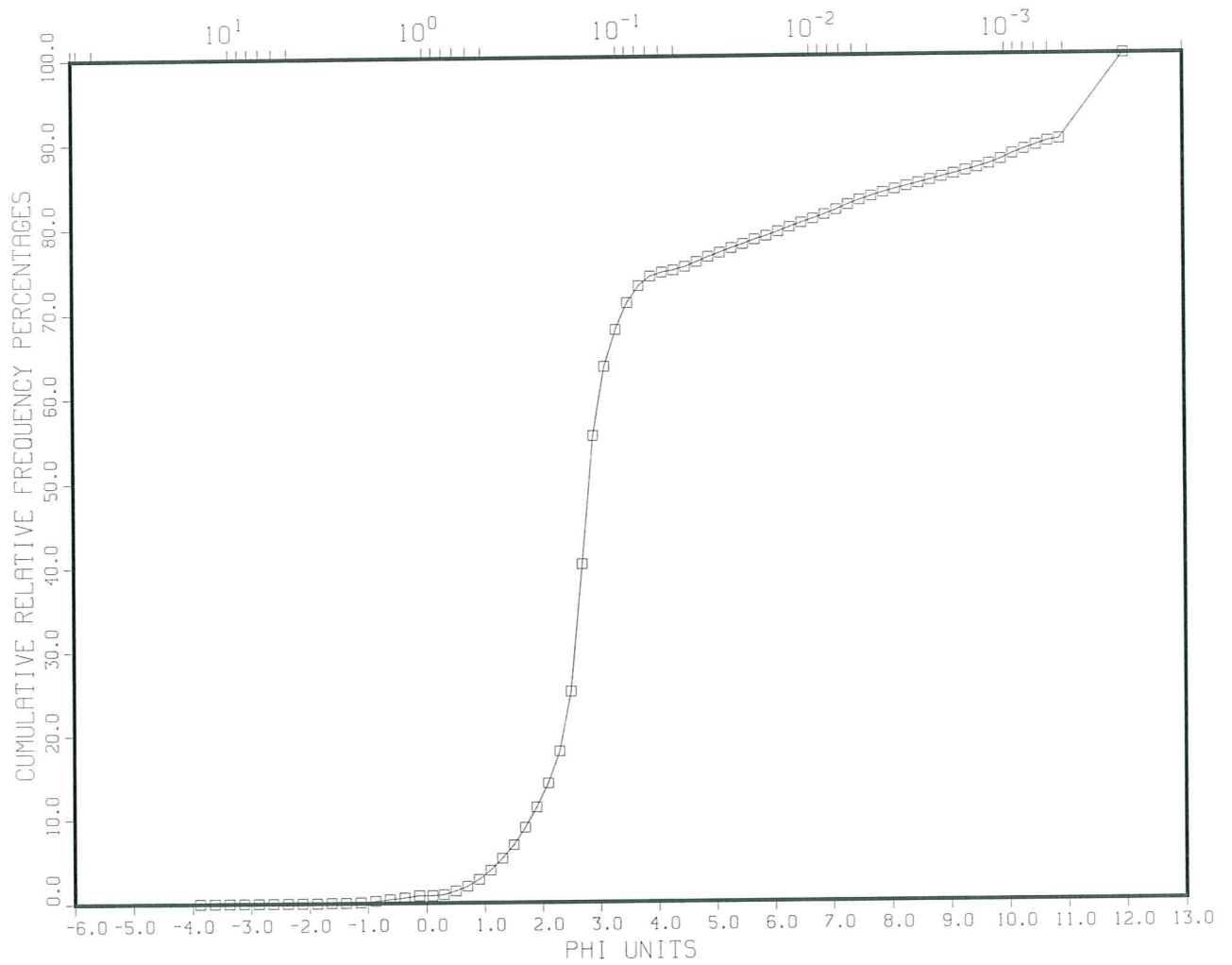
Grain Size Breakdown

	%	%	%	%	%
Gravel		Sand	Silt	Clay	Mud
	0.22	68.47	11.38	19.93	31.31

Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.49	3.62	2.81	1.13

GS1-97-4840-4845, RD011429, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
6: 2:1998  
11429  
72  
GS1-97-4840-4845  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011429  
SWF00425  
4.84000000000000E+0003  
4.84500000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.06	0.06
2.59e+00	-1.38	0.00	0.06
2.18e+00	-1.12	0.03	0.10
1.83e+00	-0.88	0.15	0.25
1.54e+00	-0.62	0.18	0.43
1.30e+00	-0.38	0.18	0.61
1.09e+00	-0.12	0.25	0.86
9.33e-01	0.10	0.00	0.86
8.12e-01	0.30	0.11	0.97
7.07e-01	0.50	0.42	1.39
6.16e-01	0.70	0.54	1.93
5.36e-01	0.90	0.81	2.75
4.67e-01	1.10	1.08	3.83
4.06e-01	1.30	1.41	5.24
3.54e-01	1.50	1.59	6.82
3.08e-01	1.70	2.06	8.89
2.68e-01	1.90	2.42	11.30
2.33e-01	2.10	2.86	14.16
2.03e-01	2.30	3.81	17.97
1.77e-01	2.50	7.12	25.09
1.54e-01	2.70	15.18	40.27
1.34e-01	2.90	15.11	55.38
1.17e-01	3.10	8.14	63.52
1.02e-01	3.30	4.36	67.88
8.84e-02	3.50	3.16	71.04
7.69e-02	3.70	1.97	73.01
6.70e-02	3.90	1.12	74.14
5.83e-02	4.10	0.46	74.59
5.08e-02	4.30	0.23	74.83
4.42e-02	4.50	0.41	75.24
3.85e-02	4.70	0.56	75.80
3.35e-02	4.90	0.58	76.38
2.92e-02	5.10	0.49	76.87
2.54e-02	5.30	0.52	77.39
2.21e-02	5.50	0.45	77.85
1.92e-02	5.70	0.53	78.38
1.67e-02	5.90	0.42	78.80
1.46e-02	6.10	0.50	79.29
1.27e-02	6.30	0.53	79.82



1.10e-02	6.50	0.50	80.33
9.62e-03	6.70	0.46	80.79
8.37e-03	6.90	0.50	81.29
7.29e-03	7.10	0.54	81.83
6.35e-03	7.30	0.61	82.44
5.52e-03	7.50	0.52	82.96
4.81e-03	7.70	0.47	83.43
4.19e-03	7.90	0.43	83.85
3.64e-03	8.10	0.38	84.24
3.17e-03	8.30	0.36	84.59
2.76e-03	8.50	0.34	84.94
2.40e-03	8.70	0.35	85.29
2.09e-03	8.90	0.36	85.65
1.82e-03	9.10	0.35	86.00
1.59e-03	9.30	0.36	86.36
1.38e-03	9.50	0.36	86.72
1.20e-03	9.70	0.40	87.12
1.05e-03	9.90	0.53	87.65
9.11e-04	10.10	0.62	88.27
7.93e-04	10.30	0.52	88.79
6.91e-04	10.50	0.47	89.26
6.01e-04	10.70	0.47	89.73
5.23e-04	10.90	0.22	89.95
2.44e-04	12.00	10.05	100.00

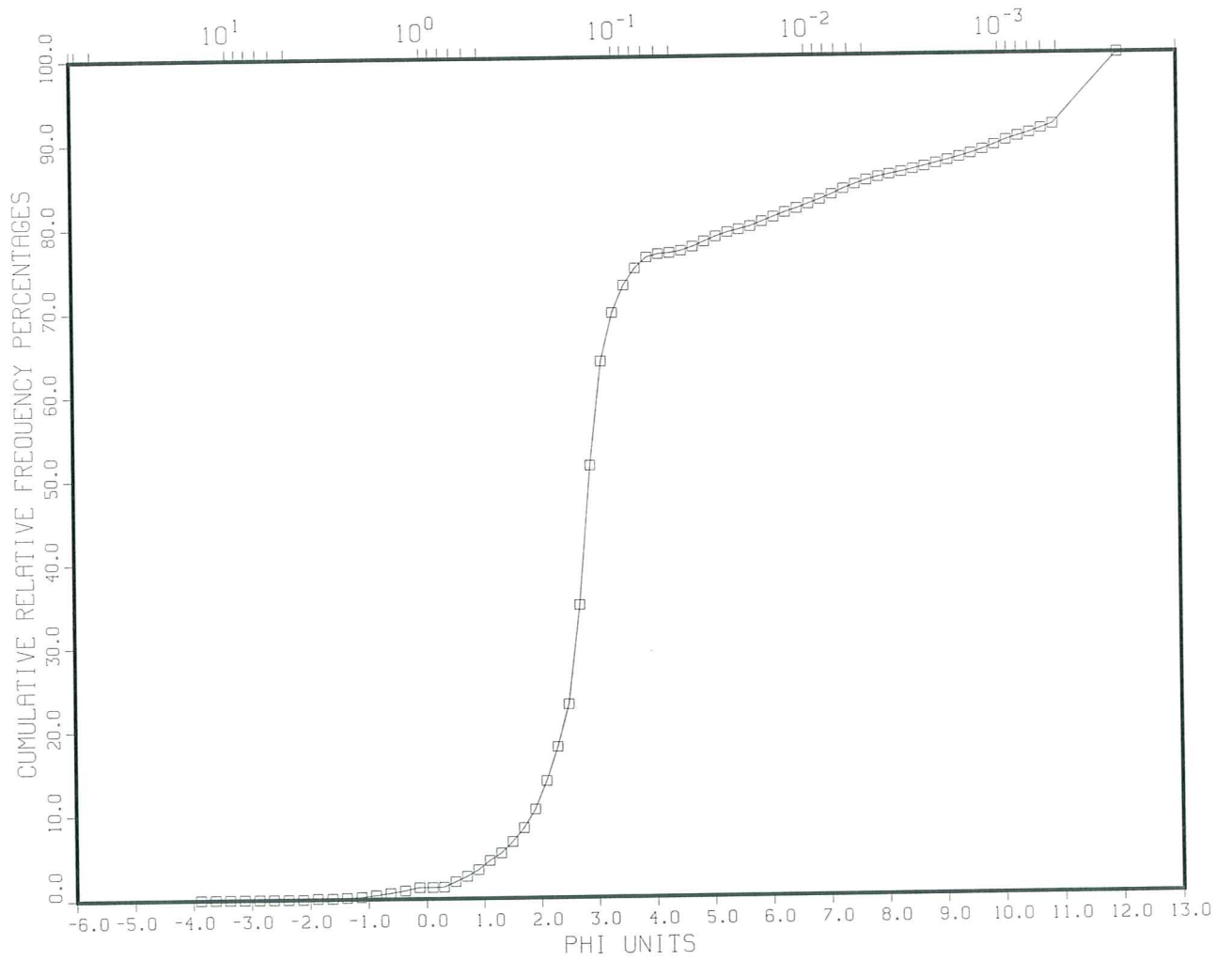
Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.10	74.04	9.72	16.15	25.86

Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.32	3.26	3.77	1.45

GS1-97-4884-4890, RD011430, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
6: 2:1998  
11430  
72  
GS1-97-4884-4890  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011430  
SWF00425  
4.884000000000000E+0003  
4.890000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.09	0.09
3.08e+00	-1.62	0.00	0.09
2.59e+00	-1.38	0.08	0.17
2.18e+00	-1.12	0.07	0.24
1.83e+00	-0.88	0.22	0.46
1.54e+00	-0.62	0.23	0.69
1.30e+00	-0.38	0.29	0.98
1.09e+00	-0.12	0.37	1.35
9.33e-01	0.10	0.00	1.35
8.12e-01	0.30	0.03	1.38
7.07e-01	0.50	0.62	2.00
6.16e-01	0.70	0.63	2.63
5.36e-01	0.90	0.78	3.40
4.67e-01	1.10	1.08	4.48
4.06e-01	1.30	0.87	5.36
3.54e-01	1.50	1.33	6.68
3.08e-01	1.70	1.62	8.30
2.68e-01	1.90	2.17	10.47
2.33e-01	2.10	3.38	13.86
2.03e-01	2.30	4.02	17.87
1.77e-01	2.50	5.06	22.94
1.54e-01	2.70	11.88	34.81
1.34e-01	2.90	16.66	51.47
1.17e-01	3.10	12.39	63.86
1.02e-01	3.30	5.78	69.64
8.84e-02	3.50	3.24	72.88
7.69e-02	3.70	2.02	74.90
6.70e-02	3.90	1.31	76.21
5.83e-02	4.10	0.38	76.59
5.08e-02	4.30	0.11	76.70
4.42e-02	4.50	0.24	76.95
3.85e-02	4.70	0.47	77.42
3.35e-02	4.90	0.61	78.02
2.92e-02	5.10	0.57	78.60
2.54e-02	5.30	0.48	79.08
2.21e-02	5.50	0.32	79.40
1.92e-02	5.70	0.36	79.77
1.67e-02	5.90	0.54	80.31
1.46e-02	6.10	0.53	80.84
1.27e-02	6.30	0.54	81.38

1.10e-02	6.50	0.44	81.82
9.62e-03	6.70	0.52	82.34
8.37e-03	6.90	0.52	82.86
7.29e-03	7.10	0.58	83.44
6.35e-03	7.30	0.64	84.08
5.52e-03	7.50	0.54	84.62
4.81e-03	7.70	0.48	85.09
4.19e-03	7.90	0.37	85.46
3.64e-03	8.10	0.29	85.75
3.17e-03	8.30	0.28	86.03
2.76e-03	8.50	0.31	86.34
2.40e-03	8.70	0.33	86.67
2.09e-03	8.90	0.36	87.03
1.82e-03	9.10	0.35	87.38
1.59e-03	9.30	0.37	87.75
1.38e-03	9.50	0.40	88.14
1.20e-03	9.70	0.47	88.61
1.05e-03	9.90	0.55	89.16
9.11e-04	10.10	0.56	89.72
7.93e-04	10.30	0.45	90.17
6.91e-04	10.50	0.40	90.57
6.01e-04	10.70	0.50	91.07
5.23e-04	10.90	0.50	91.57
2.44e-04	12.00	8.43	100.00

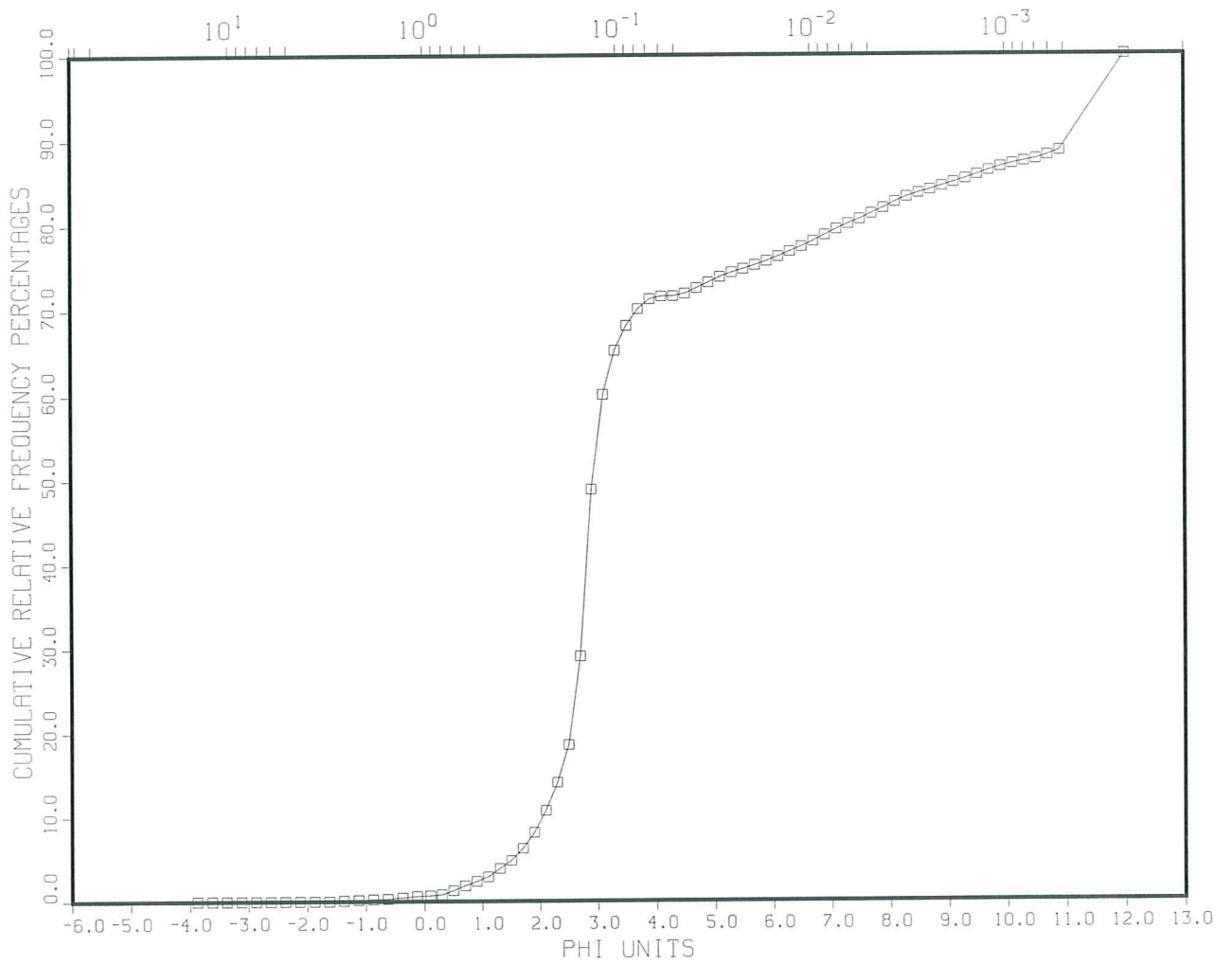
#### Grain Size Breakdown

	%	%	%	%	%
Gravel		Sand	Silt	Clay	Mud
	0.24	75.97	9.25	14.54	23.79

#### Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.20	3.12	4.19	1.53

GS1-97-4935-4940, RD011431, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
 6: 2:1998  
 11431  
 72  
 GS1-97-4935-4940  
 97NORSKALD  
 970001  
 G. SONNICHSEN  
 TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
 RD011431  
 SWF00425  
 4.935000000000000E+0003  
 4.940000000000000E+0003  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 53292  
 GS1-97  
 GS1-97  
 BOREHOLE  
 BOREHOLE  
 46:27.72  
 -48:29.27  
 92.90  
 n lines for future expansion  
 #

Results

Midpoints	PHI	Relative Frequency Percentages	Cumulative Frequency Percentages
1.47e+01	-3.88	0.00	0.00
1.23e+01	-3.62	0.00	0.00
1.04e+01	-3.38	0.00	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.00	0.00
2.59e+00	-1.38	0.08	0.08
2.18e+00	-1.12	0.09	0.17
1.83e+00	-0.88	0.07	0.24
1.54e+00	-0.62	0.04	0.28
1.30e+00	-0.38	0.14	0.42
1.09e+00	-0.12	0.16	0.58
9.33e-01	0.10	0.08	0.66
8.12e-01	0.30	0.12	0.79
7.07e-01	0.50	0.48	1.27
6.16e-01	0.70	0.58	1.85
5.36e-01	0.90	0.49	2.34
4.67e-01	1.10	0.55	2.89
4.06e-01	1.30	0.98	3.87
3.54e-01	1.50	0.95	4.82
3.08e-01	1.70	1.44	6.26
2.68e-01	1.90	1.90	8.16
2.33e-01	2.10	2.60	10.76
2.03e-01	2.30	3.34	14.10
1.77e-01	2.50	4.49	18.59
1.54e-01	2.70	10.51	29.10
1.34e-01	2.90	19.78	48.88
1.17e-01	3.10	11.25	60.13
1.02e-01	3.30	5.13	65.26
8.84e-02	3.50	2.90	68.16
7.69e-02	3.70	1.97	70.13
6.70e-02	3.90	1.16	71.29
5.83e-02	4.10	0.31	71.60
5.08e-02	4.30	0.03	71.63
4.42e-02	4.50	0.30	71.93
3.85e-02	4.70	0.63	72.56
3.35e-02	4.90	0.66	73.22
2.92e-02	5.10	0.64	73.85
2.54e-02	5.30	0.52	74.37
2.21e-02	5.50	0.41	74.79
1.92e-02	5.70	0.45	75.23
1.67e-02	5.90	0.47	75.70
1.46e-02	6.10	0.54	76.24
1.27e-02	6.30	0.59	76.83



1.10e-02	6.50	0.58	77.41
9.62e-03	6.70	0.62	78.03
8.37e-03	6.90	0.73	78.75
7.29e-03	7.10	0.68	79.44
6.35e-03	7.30	0.63	80.07
5.52e-03	7.50	0.53	80.61
4.81e-03	7.70	0.66	81.27
4.19e-03	7.90	0.64	81.90
3.64e-03	8.10	0.71	82.62
3.17e-03	8.30	0.61	83.23
2.76e-03	8.50	0.46	83.68
2.40e-03	8.70	0.37	84.05
2.09e-03	8.90	0.44	84.49
1.82e-03	9.10	0.43	84.92
1.59e-03	9.30	0.44	85.36
1.38e-03	9.50	0.48	85.84
1.20e-03	9.70	0.50	86.33
1.05e-03	9.90	0.44	86.77
9.11e-04	10.10	0.36	87.14
7.93e-04	10.30	0.27	87.41
6.91e-04	10.50	0.28	87.69
6.01e-04	10.70	0.44	88.12
5.23e-04	10.90	0.54	88.66
2.44e-04	12.00	11.34	100.00

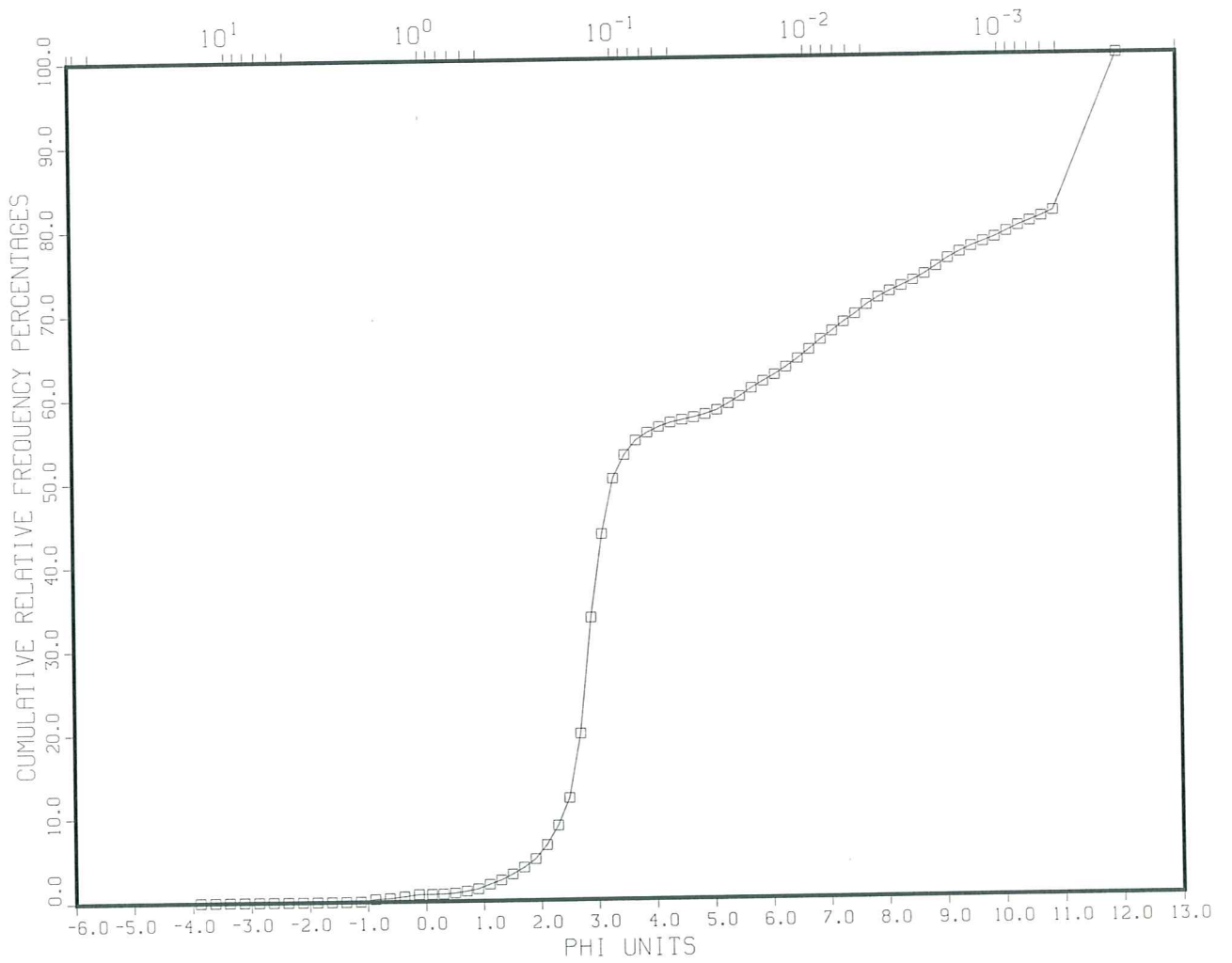
#### Grain Size Breakdown

	%	%	%	%	%
Gravel		Sand	Silt	Clay	Mud
	0.17	71.12	10.61	18.10	28.71

#### Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.60	3.33	3.33	1.31

GS1-97-5027-5033, R0011432, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
 6: 2:1998  
 11432  
 72  
 GS1-97-5027-5033  
 97NORSKALD  
 970001  
 G. SONNICHSEN  
 TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
 RD011432  
 SWF00425  
 5.027000000000000E+0003  
 5.033000000000000E+0003  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 53292  
 GS1-97  
 GS1-97  
 BOREHOLE  
 BOREHOLE  
 46:27.72  
 -48:29.27  
 92.90  
 n lines for future expansion  
 #

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.00	0.00
2.59e+00	-1.38	0.00	0.00
2.18e+00	-1.12	0.03	0.03
1.83e+00	-0.88	0.27	0.30
1.54e+00	-0.62	0.08	0.38
1.30e+00	-0.38	0.20	0.58
1.09e+00	-0.12	0.24	0.82
9.33e-01	0.10	0.01	0.82
8.12e-01	0.30	0.02	0.84
7.07e-01	0.50	0.11	0.95
6.16e-01	0.70	0.21	1.16
5.36e-01	0.90	0.25	1.41
4.67e-01	1.10	0.53	1.94
4.06e-01	1.30	0.49	2.43
3.54e-01	1.50	0.68	3.11
3.08e-01	1.70	0.80	3.91
2.68e-01	1.90	1.00	4.91
2.33e-01	2.10	1.63	6.53
2.03e-01	2.30	2.28	8.82
1.77e-01	2.50	3.25	12.07
1.54e-01	2.70	7.70	19.76
1.34e-01	2.90	13.79	33.56
1.17e-01	3.10	9.94	43.50
1.02e-01	3.30	6.65	50.14
8.84e-02	3.50	2.80	52.94
7.69e-02	3.70	1.72	54.66
6.70e-02	3.90	0.91	55.57
5.83e-02	4.10	0.68	56.25
5.08e-02	4.30	0.50	56.75
4.42e-02	4.50	0.30	57.05
3.85e-02	4.70	0.30	57.35
3.35e-02	4.90	0.35	57.70
2.92e-02	5.10	0.47	58.17
2.54e-02	5.30	0.77	58.94
2.21e-02	5.50	0.82	59.76
1.92e-02	5.70	0.96	60.73
1.67e-02	5.90	0.82	61.54
1.46e-02	6.10	0.76	62.30
1.27e-02	6.30	0.89	63.19

1.10e-02	6.50	1.00	64.20
9.62e-03	6.70	1.09	65.28
8.37e-03	6.90	1.16	66.44
7.29e-03	7.10	0.98	67.42
6.35e-03	7.30	1.05	68.47
5.52e-03	7.50	0.93	69.40
4.81e-03	7.70	1.07	70.47
4.19e-03	7.90	0.86	71.33
3.64e-03	8.10	0.71	72.04
3.17e-03	8.30	0.63	72.66
2.76e-03	8.50	0.64	73.31
2.40e-03	8.70	0.74	74.05
2.09e-03	8.90	0.91	74.96
1.82e-03	9.10	0.93	75.89
1.59e-03	9.30	0.75	76.64
1.38e-03	9.50	0.64	77.28
1.20e-03	9.70	0.53	77.81
1.05e-03	9.90	0.52	78.33
9.11e-04	10.10	0.66	78.99
7.93e-04	10.30	0.66	79.65
6.91e-04	10.50	0.54	80.20
6.01e-04	10.70	0.56	80.75
5.23e-04	10.90	0.64	81.39
2.44e-04	12.00	18.61	100.00

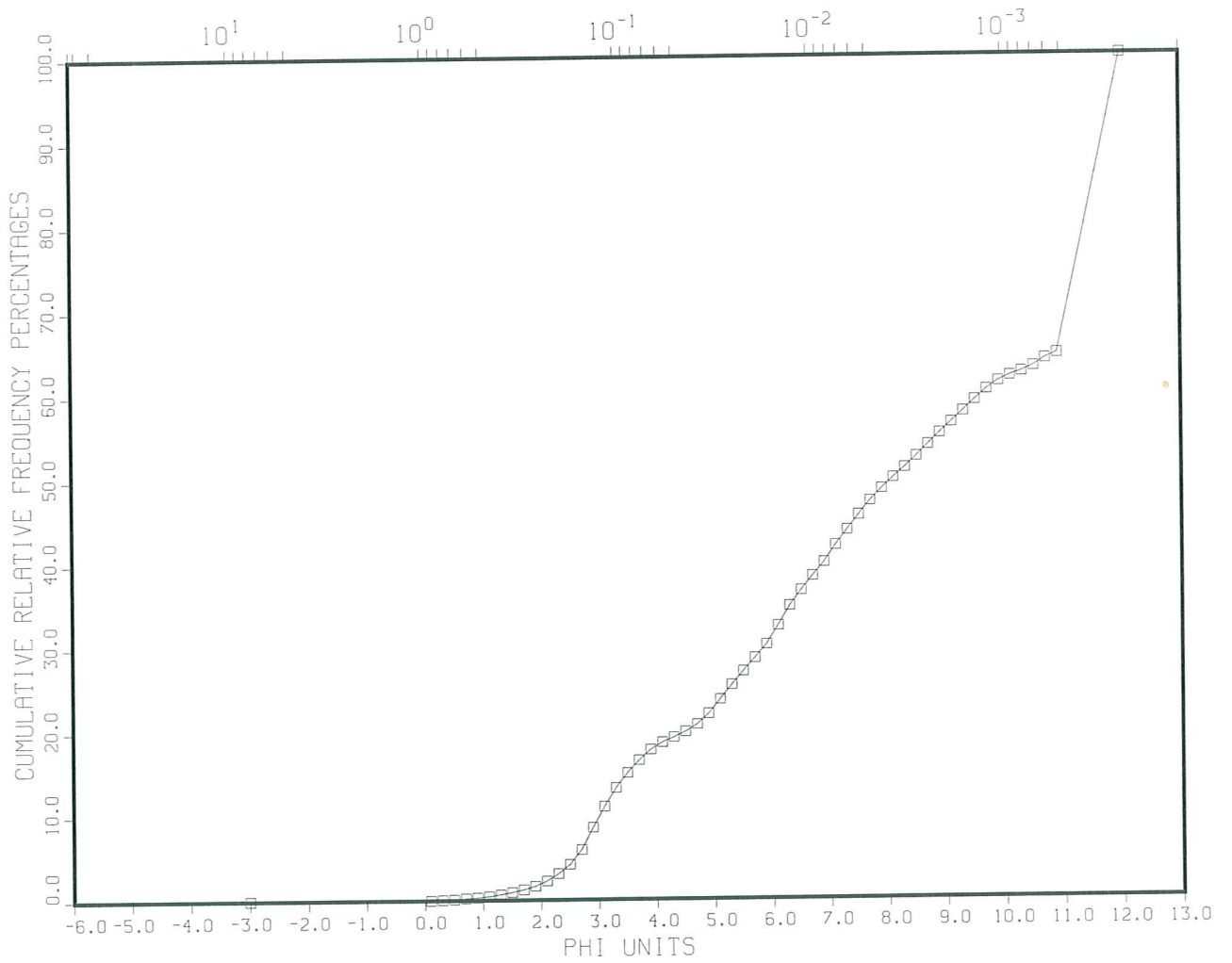
Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.03	55.55	15.75	28.67	44.43

Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
5.73	3.75	1.90	0.67

GS1-97-5082-5086, RD011433, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
 9: 2:1998  
 11433  
 57  
 GS1-97-5082-5086  
 97NORSKALD  
 970001  
 G. SONNICHSEN  
 TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
 RD011433  
 SWF00425  
 5.082000000000000E+0003  
 5.086000000000000E+0003  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 53292  
 GS1-97  
 GS1-97  
 BOREHOLE  
 BOREHOLE  
 46:27.72  
 -48:29.27  
 92.90  
 n lines for future expansion  
 #

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
8.00e+00	-3.00	0.00
9.33e-01	0.10	0.00
8.12e-01	0.30	0.06

7.07e-01	0.50	0.06	0.12
6.16e-01	0.70	0.11	0.23
5.36e-01	0.90	0.09	0.32
4.67e-01	1.10	0.13	0.45
4.06e-01	1.30	0.22	0.67
3.54e-01	1.50	0.26	0.93
3.08e-01	1.70	0.31	1.24
2.68e-01	1.90	0.41	1.64
2.33e-01	2.10	0.61	2.26
2.03e-01	2.30	0.86	3.11
1.77e-01	2.50	1.08	4.20
1.54e-01	2.70	1.75	5.94
1.34e-01	2.90	2.64	8.58
1.17e-01	3.10	2.47	11.05
1.02e-01	3.30	2.21	13.26
8.84e-02	3.50	1.81	15.08
7.69e-02	3.70	1.51	16.59
6.70e-02	3.90	1.28	17.87
5.83e-02	4.10	0.85	18.72
5.08e-02	4.30	0.59	19.31
4.42e-02	4.50	0.68	19.99
3.85e-02	4.70	0.85	20.84
3.35e-02	4.90	1.27	22.11
2.92e-02	5.10	1.71	23.81
2.54e-02	5.30	1.75	25.57
2.21e-02	5.50	1.61	27.18
1.92e-02	5.70	1.56	28.74
1.67e-02	5.90	1.59	30.33
1.46e-02	6.10	2.24	32.57
1.27e-02	6.30	2.38	34.95
1.10e-02	6.50	1.86	36.80
9.62e-03	6.70	1.70	38.50
8.37e-03	6.90	1.61	40.11
7.29e-03	7.10	2.02	42.13
6.35e-03	7.30	1.79	43.92
5.52e-03	7.50	1.73	45.65
4.81e-03	7.70	1.67	47.32
4.19e-03	7.90	1.42	48.74
3.64e-03	8.10	1.31	50.04
3.17e-03	8.30	1.21	51.25
2.76e-03	8.50	1.31	52.56
2.40e-03	8.70	1.39	53.95
2.09e-03	8.90	1.35	55.30
1.82e-03	9.10	1.28	56.57
1.59e-03	9.30	1.29	57.87



1.38e-03	9.50	1.31	59.17
1.20e-03	9.70	1.25	60.43
1.05e-03	9.90	0.97	61.40
9.11e-04	10.10	0.65	62.05
7.93e-04	10.30	0.48	62.53
6.91e-04	10.50	0.63	63.16
6.01e-04	10.70	0.89	64.05
5.23e-04	10.90	0.61	64.66
2.44e-04	12.00	35.34	100.00

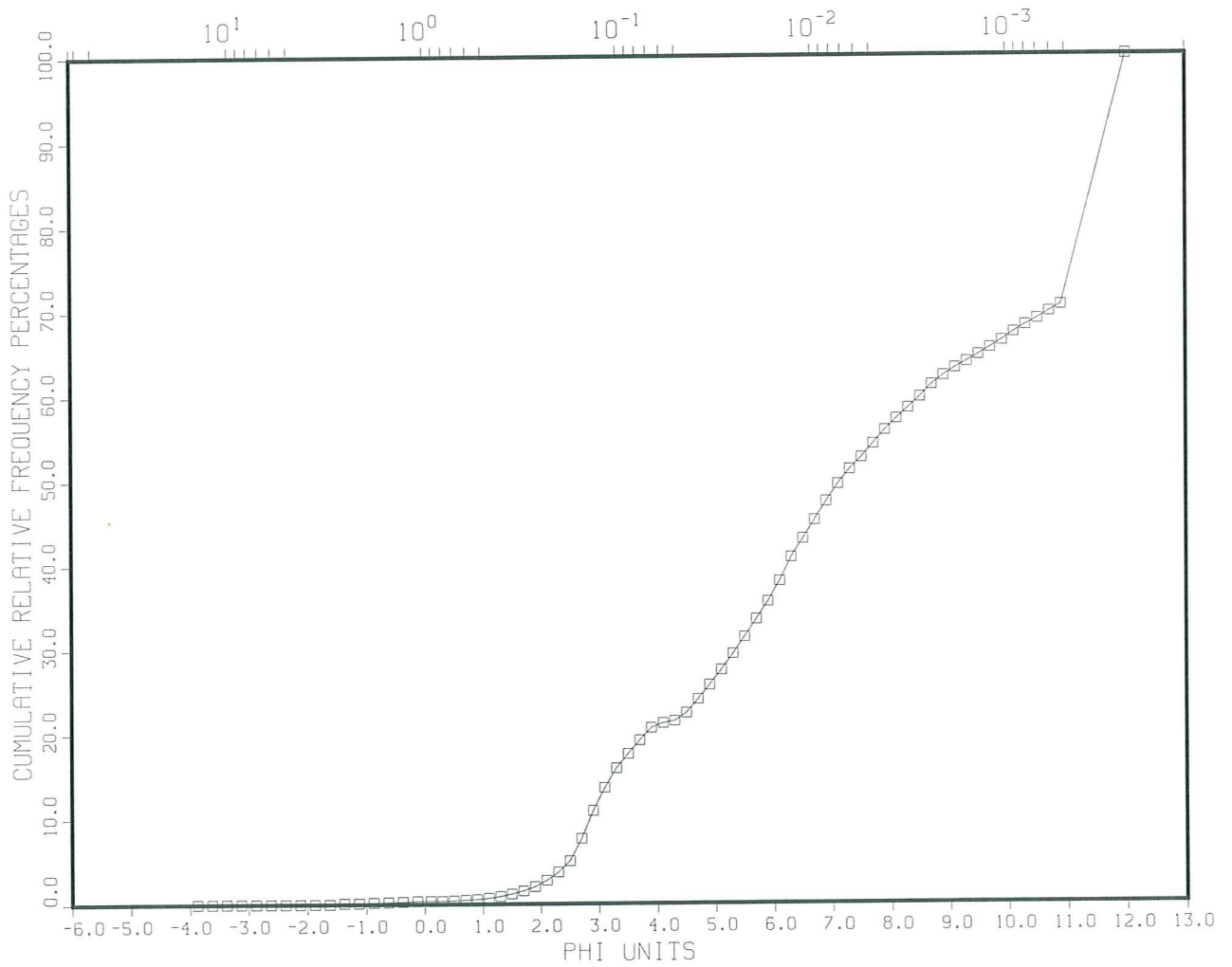
#### Grain Size Breakdown

	%	%	%	%	%
Gravel		Sand	Silt	Clay	Mud
	0.00	17.87	30.87	51.26	82.13

#### Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
8.17	3.46	1.67	-0.26

GS1-97-5101-5105, RD011434, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
 9: 2:1998  
 11434  
 72  
 GS1-97-5101-5105  
 97NORSKALD  
 970001  
 G. SONNICHSEN  
 TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
 RD011434  
 SWF00425  
 5.10100000000000E+0003  
 5.10500000000000E+0003  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 53292  
 GS1-97  
 GS1-97  
 BOREHOLE  
 BOREHOLE  
 46:27.72  
 -48:29.27  
 92.90  
 n lines for future expansion  
 #

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.00	0.00
2.59e+00	-1.38	0.13	0.13
2.18e+00	-1.12	0.00	0.13
1.83e+00	-0.88	0.07	0.20
1.54e+00	-0.62	0.04	0.24
1.30e+00	-0.38	0.05	0.29
1.09e+00	-0.12	0.07	0.35
9.33e-01	0.10	0.00	0.35
8.12e-01	0.30	0.01	0.37
7.07e-01	0.50	0.05	0.42
6.16e-01	0.70	0.08	0.49
5.36e-01	0.90	0.07	0.56
4.67e-01	1.10	0.13	0.69
4.06e-01	1.30	0.21	0.90
3.54e-01	1.50	0.29	1.19
3.08e-01	1.70	0.36	1.55
2.68e-01	1.90	0.49	2.03
2.33e-01	2.10	0.73	2.77
2.03e-01	2.30	0.97	3.74
1.77e-01	2.50	1.29	5.03
1.54e-01	2.70	2.64	7.66
1.34e-01	2.90	3.28	10.94
1.17e-01	3.10	2.66	13.60
1.02e-01	3.30	2.31	15.91
8.84e-02	3.50	1.71	17.62
7.69e-02	3.70	1.62	19.24
6.70e-02	3.90	1.47	20.71
5.83e-02	4.10	0.55	21.26
5.08e-02	4.30	0.26	21.52
4.42e-02	4.50	0.94	22.46
3.85e-02	4.70	1.62	24.08
3.35e-02	4.90	1.67	25.75
2.92e-02	5.10	1.78	27.53
2.54e-02	5.30	1.91	29.44
2.21e-02	5.50	2.00	31.44
1.92e-02	5.70	2.09	33.53
1.67e-02	5.90	2.11	35.63
1.46e-02	6.10	2.41	38.04
1.27e-02	6.30	2.82	40.86

1.10e-02	6.50	2.19	43.05
9.62e-03	6.70	2.20	45.26
8.37e-03	6.90	2.20	47.45
7.29e-03	7.10	2.03	49.49
6.35e-03	7.30	1.75	51.23
5.52e-03	7.50	1.41	52.64
4.81e-03	7.70	1.63	54.27
4.19e-03	7.90	1.60	55.87
3.64e-03	8.10	1.35	57.23
3.17e-03	8.30	1.26	58.49
2.76e-03	8.50	1.29	59.77
2.40e-03	8.70	1.43	61.20
2.09e-03	8.90	1.05	62.25
1.82e-03	9.10	0.89	63.15
1.59e-03	9.30	0.74	63.89
1.38e-03	9.50	0.80	64.69
1.20e-03	9.70	0.82	65.51
1.05e-03	9.90	0.85	66.36
9.11e-04	10.10	0.97	67.33
7.93e-04	10.30	0.86	68.19
6.91e-04	10.50	0.74	68.93
6.01e-04	10.70	0.87	69.80
5.23e-04	10.90	0.79	70.59
2.44e-04	12.00	29.41	100.00

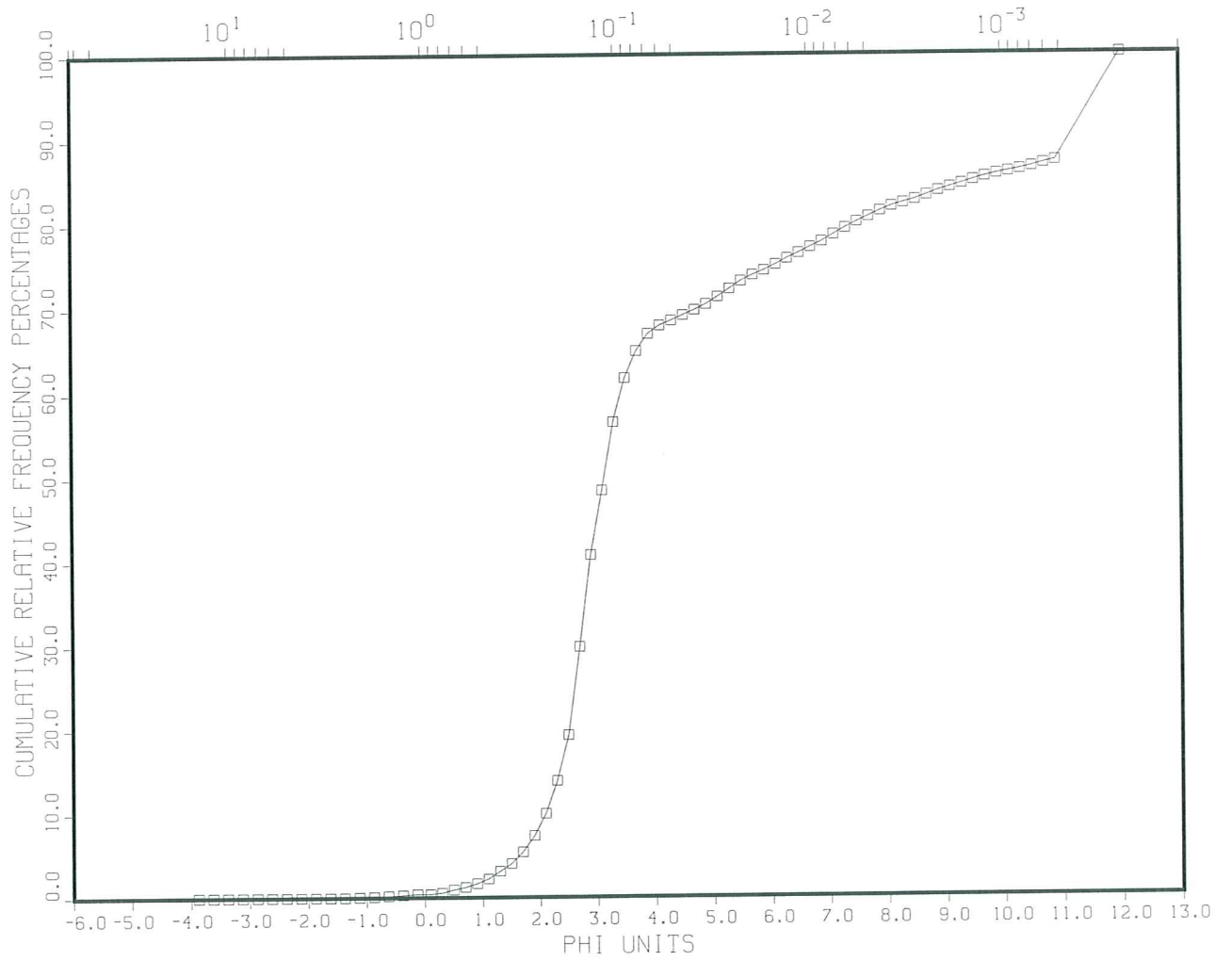
Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.13	20.58	35.17	44.13	79.29

Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
7.67	3.47	1.70	-0.06

GS1-97-5140-5144, RD011435, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
 9: 2:1998  
 11435  
 72  
 GS1-97-5140-5144  
 97NORSKALD  
 970001  
 G. SONNICHSEN  
 TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
 RD011435  
 SWF00425  
 5.14000000000000E+0003  
 5.14400000000000E+0003  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 53292  
 GS1-97  
 GS1-97  
 BOREHOLE  
 BOREHOLE  
 46:27.72  
 -48:29.27  
 92.90  
 n lines for future expansion  
 #

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.00	0.00
2.59e+00	-1.38	0.00	0.00
2.18e+00	-1.12	0.06	0.06
1.83e+00	-0.88	0.05	0.11
1.54e+00	-0.62	0.08	0.19
1.30e+00	-0.38	0.10	0.30
1.09e+00	-0.12	0.12	0.41
9.33e-01	0.10	0.00	0.41
8.12e-01	0.30	0.15	0.56
7.07e-01	0.50	0.37	0.92
6.16e-01	0.70	0.31	1.23
5.36e-01	0.90	0.43	1.66
4.67e-01	1.10	0.57	2.23
4.06e-01	1.30	0.91	3.14
3.54e-01	1.50	0.90	4.04
3.08e-01	1.70	1.40	5.44
2.68e-01	1.90	1.94	7.38
2.33e-01	2.10	2.64	10.02
2.03e-01	2.30	3.93	13.95
1.77e-01	2.50	5.43	19.38
1.54e-01	2.70	10.54	29.92
1.34e-01	2.90	10.94	40.86
1.17e-01	3.10	7.63	48.49
1.02e-01	3.30	8.17	56.66
8.84e-02	3.50	5.16	61.83
7.69e-02	3.70	3.19	65.02
6.70e-02	3.90	2.00	67.01
5.83e-02	4.10	0.97	67.98
5.08e-02	4.30	0.58	68.56
4.42e-02	4.50	0.62	69.18
3.85e-02	4.70	0.60	69.78
3.35e-02	4.90	0.68	70.46
2.92e-02	5.10	0.86	71.32
2.54e-02	5.30	0.96	72.27
2.21e-02	5.50	0.91	73.19
1.92e-02	5.70	0.69	73.87
1.67e-02	5.90	0.56	74.43
1.46e-02	6.10	0.69	75.12
1.27e-02	6.30	0.72	75.84



1.10e-02	6.50	0.63	76.47
9.62e-03	6.70	0.69	77.16
8.37e-03	6.90	0.65	77.81
7.29e-03	7.10	0.81	78.62
6.35e-03	7.30	0.77	79.39
5.52e-03	7.50	0.71	80.10
4.81e-03	7.70	0.64	80.73
4.19e-03	7.90	0.65	81.39
3.64e-03	8.10	0.55	81.94
3.17e-03	8.30	0.39	82.34
2.76e-03	8.50	0.38	82.72
2.40e-03	8.70	0.50	83.22
2.09e-03	8.90	0.51	83.73
1.82e-03	9.10	0.42	84.15
1.59e-03	9.30	0.40	84.55
1.38e-03	9.50	0.42	84.98
1.20e-03	9.70	0.39	85.37
1.05e-03	9.90	0.32	85.69
9.11e-04	10.10	0.28	85.97
7.93e-04	10.30	0.25	86.22
6.91e-04	10.50	0.31	86.53
6.01e-04	10.70	0.40	86.93
5.23e-04	10.90	0.32	87.25
2.44e-04	12.00	12.75	100.00

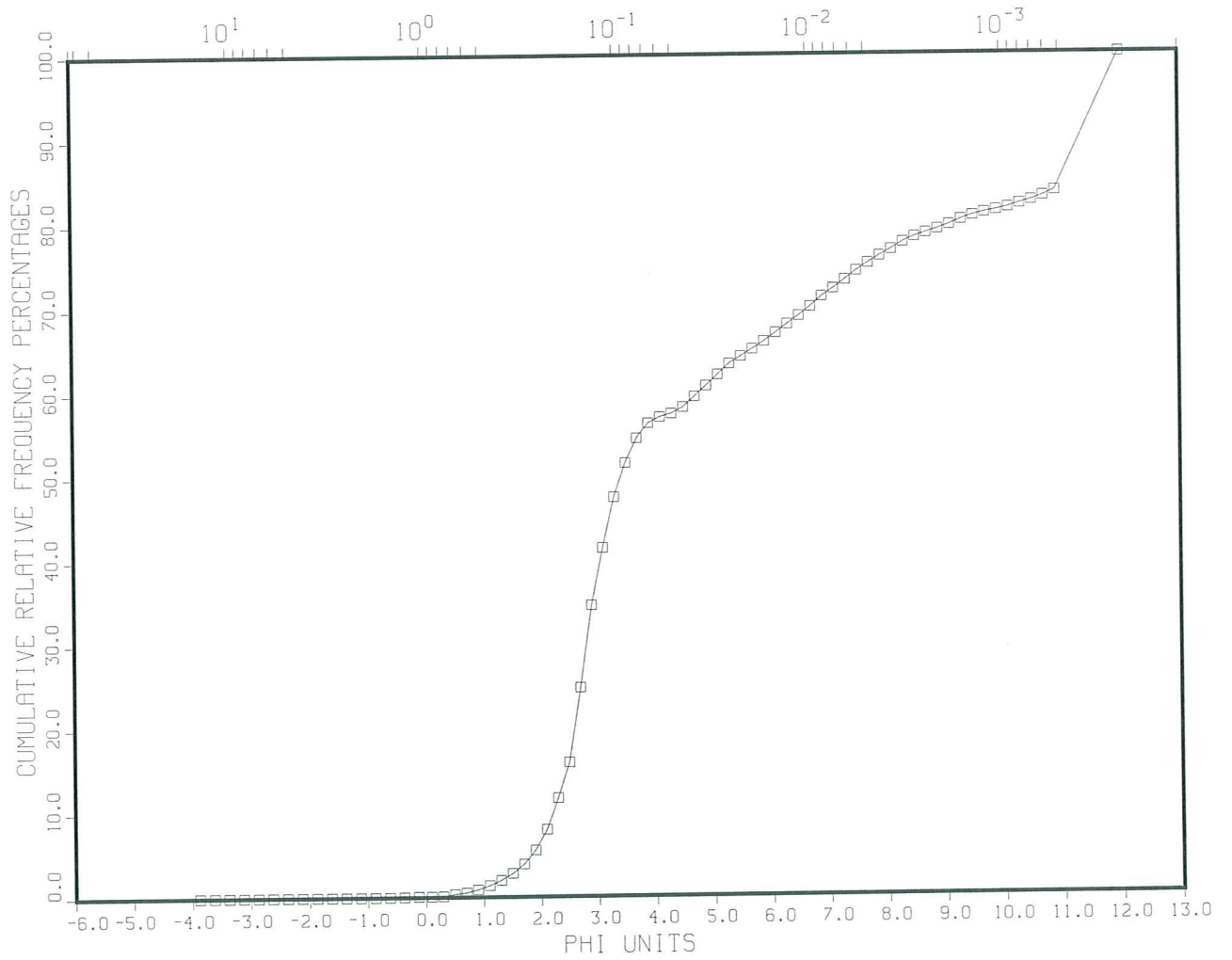
#### Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.06	66.96	14.37	18.61	32.99

#### Statistical Measures

Mean	Standard	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
4.80	3.36	3.11	1.23

GS1-97-5160-5164, RD011436, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
9: 2:1998  
11436  
72  
GS1-97-5160-5164  
97NORSKALD  
970001  
G. SONNICHSEN  
TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
RD011436  
SWF00425  
5.160000000000000E+0003  
5.164000000000000E+0003  
0  
0  
0  
0  
0  
0  
0  
0  
0  
53292  
GS1-97  
GS1-97  
BOREHOLE  
BOREHOLE  
46:27.72  
-48:29.27  
92.90  
n lines for future expansion  
#

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.00	0.00
2.59e+00	-1.38	0.00	0.00
2.18e+00	-1.12	0.00	0.00
1.83e+00	-0.88	0.00	0.00
1.54e+00	-0.62	0.02	0.02
1.30e+00	-0.38	0.02	0.04
1.09e+00	-0.12	0.05	0.09
9.33e-01	0.10	0.00	0.09
8.12e-01	0.30	0.04	0.13
7.07e-01	0.50	0.22	0.35
6.16e-01	0.70	0.18	0.53
5.36e-01	0.90	0.36	0.89
4.67e-01	1.10	0.48	1.37
4.06e-01	1.30	0.61	1.98
3.54e-01	1.50	0.82	2.80
3.08e-01	1.70	1.10	3.90
2.68e-01	1.90	1.65	5.55
2.33e-01	2.10	2.43	7.98
2.03e-01	2.30	3.71	11.70
1.77e-01	2.50	4.20	15.90
1.54e-01	2.70	8.96	24.86
1.34e-01	2.90	9.78	34.64
1.17e-01	3.10	6.82	41.46
1.02e-01	3.30	6.07	47.53
8.84e-02	3.50	4.02	51.56
7.69e-02	3.70	2.97	54.52
6.70e-02	3.90	1.80	56.32
5.83e-02	4.10	0.73	57.05
5.08e-02	4.30	0.40	57.44
4.42e-02	4.50	0.76	58.20
3.85e-02	4.70	1.25	59.45
3.35e-02	4.90	1.27	60.72
2.92e-02	5.10	1.30	62.02
2.54e-02	5.30	1.29	63.32
2.21e-02	5.50	0.86	64.17
1.92e-02	5.70	0.85	65.02
1.67e-02	5.90	0.90	65.92
1.46e-02	6.10	1.00	66.92
1.27e-02	6.30	1.03	67.95

1.10e-02	6.50	1.00	68.95
9.62e-03	6.70	1.06	70.01
8.37e-03	6.90	1.22	71.23
7.29e-03	7.10	0.93	72.16
6.35e-03	7.30	1.03	73.18
5.52e-03	7.50	1.05	74.23
4.81e-03	7.70	0.92	75.15
4.19e-03	7.90	0.85	76.00
3.64e-03	8.10	0.75	76.75
3.17e-03	8.30	0.86	77.60
2.76e-03	8.50	0.60	78.20
2.40e-03	8.70	0.46	78.66
2.09e-03	8.90	0.43	79.10
1.82e-03	9.10	0.50	79.60
1.59e-03	9.30	0.61	80.20
1.38e-03	9.50	0.48	80.68
1.20e-03	9.70	0.35	81.03
1.05e-03	9.90	0.27	81.30
9.11e-04	10.10	0.30	81.60
7.93e-04	10.30	0.46	82.05
6.91e-04	10.50	0.40	82.45
6.01e-04	10.70	0.51	82.96
5.23e-04	10.90	0.61	83.57
2.44e-04	12.00	16.43	100.00

#### Grain Size Breakdown

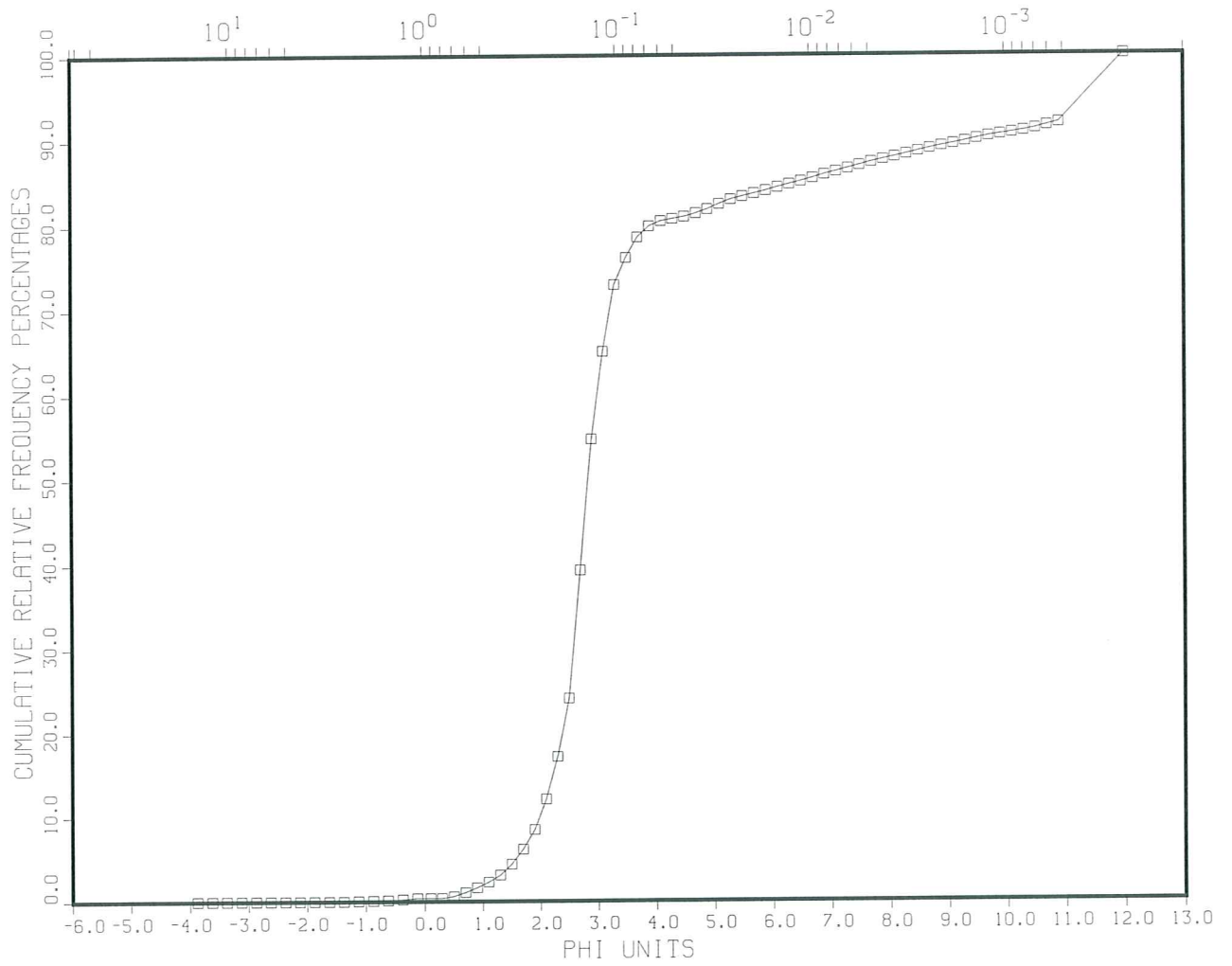
%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.00	56.32	19.68	24.00	43.68

#### Statistical Measures

##### Standard

Mean	Deviation	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )
5.45	3.57	2.26	0.87

GS1-97-5220-5224, RD011437, G. SONNICHSEN  
# ,00425, TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
MILLIMETER EQUIVALENTS



Calculation Results for  
The Sample with the Identifier:

V4.0  
 9: 2:1998  
 11437  
 72  
 GS1-97-5220-5224  
 97NORSKALD  
 970001  
 G. SONNICHSEN  
 TERRA NOVA DISCOVERY SITE, NE GRAND BANKS  
 RD011437  
 SWF00425  
 5.22000000000000E+0003  
 5.22400000000000E+0003  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 0  
 53292  
 GS1-97  
 GS1-97  
 BOREHOLE  
 BOREHOLE  
 46:27.72  
 -48:29.27  
 92.90  
 n lines for future expansion  
 #

Results

Midpoints	Relative	Cumulative
MM	PHI	Frequency
	Percentages	Percentages
1.47e+01	-3.88	0.00
1.23e+01	-3.62	0.00
1.04e+01	-3.38	0.00

8.72e+00	-3.12	0.00	0.00
7.34e+00	-2.88	0.00	0.00
6.17e+00	-2.62	0.00	0.00
5.19e+00	-2.38	0.00	0.00
4.36e+00	-2.12	0.00	0.00
3.67e+00	-1.88	0.00	0.00
3.08e+00	-1.62	0.00	0.00
2.59e+00	-1.38	0.00	0.00
2.18e+00	-1.12	0.05	0.05
1.83e+00	-0.88	0.04	0.10
1.54e+00	-0.62	0.04	0.14
1.30e+00	-0.38	0.09	0.23
1.09e+00	-0.12	0.15	0.38
9.33e-01	0.10	0.00	0.38
8.12e-01	0.30	0.00	0.38
7.07e-01	0.50	0.22	0.60
6.16e-01	0.70	0.47	1.07
5.36e-01	0.90	0.58	1.65
4.67e-01	1.10	0.65	2.30
4.06e-01	1.30	0.83	3.13
3.54e-01	1.50	1.29	4.41
3.08e-01	1.70	1.76	6.18
2.68e-01	1.90	2.32	8.50
2.33e-01	2.10	3.65	12.14
2.03e-01	2.30	5.06	17.20
1.77e-01	2.50	6.96	24.16
1.54e-01	2.70	15.21	39.37
1.34e-01	2.90	15.47	54.84
1.17e-01	3.10	10.34	65.18
1.02e-01	3.30	7.84	73.02
8.84e-02	3.50	3.18	76.21
7.69e-02	3.70	2.38	78.59
6.70e-02	3.90	1.31	79.90
5.83e-02	4.10	0.61	80.51
5.08e-02	4.30	0.24	80.75
4.42e-02	4.50	0.24	81.00
3.85e-02	4.70	0.38	81.38
3.35e-02	4.90	0.47	81.85
2.92e-02	5.10	0.59	82.45
2.54e-02	5.30	0.52	82.97
2.21e-02	5.50	0.35	83.32
1.92e-02	5.70	0.32	83.64
1.67e-02	5.90	0.34	83.98
1.46e-02	6.10	0.38	84.36
1.27e-02	6.30	0.35	84.71



1.10e-02	6.50	0.33	85.05
9.62e-03	6.70	0.38	85.43
8.37e-03	6.90	0.41	85.84
7.29e-03	7.10	0.35	86.20
6.35e-03	7.30	0.37	86.56
5.52e-03	7.50	0.37	86.93
4.81e-03	7.70	0.37	87.30
4.19e-03	7.90	0.32	87.62
3.64e-03	8.10	0.30	87.92
3.17e-03	8.30	0.32	88.23
2.76e-03	8.50	0.34	88.57
2.40e-03	8.70	0.32	88.89
2.09e-03	8.90	0.29	89.18
1.82e-03	9.10	0.27	89.45
1.59e-03	9.30	0.28	89.73
1.38e-03	9.50	0.31	90.04
1.20e-03	9.70	0.29	90.33
1.05e-03	9.90	0.21	90.54
9.11e-04	10.10	0.19	90.73
7.93e-04	10.30	0.22	90.95
6.91e-04	10.50	0.27	91.22
6.01e-04	10.70	0.36	91.58
5.23e-04	10.90	0.35	91.93
2.44e-04	12.00	8.07	100.00

Grain Size Breakdown

%	%	%	%	%
Gravel	Sand	Silt	Clay	Mud
0.05	79.85	7.72	12.38	20.10

Statistical Measures

Standard	Mean	Deviation	Kurtosis	Skewness
(PHI)	(PHI)	( No Dim. )	( No Dim. )	
	4.01	2.91	5.34	1.89