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MANAGEMENT PERSPECTIVE

This report describes a two-dimensional contaminant fate and transport model and its application to the lower Athabasca River. This is one of the major deliverables of a multiyear project funded by the Interdepartmental Panel on Energy R&D (PERD) and Environment Canada to study the aquatic impact of oil sands and heavy oil operations in northeastern Alberta. The Athabasca tar sands contain a substantial part of Canada's oil supply. A number of nitrogen-, and sulphur-PAC's (polycyclic aromatic compounds) as well as their alkyl derivatives have been identified in tar sands plants process streams and emissions. Some of these PAC's are known mutagens and carcinogens. The fate and persistence of these chemicals downstream of tar sands plants on the Athabasca River have been examined using a combination of field and laboratory data collection coupled with computer simulation modelling. The model, ATHMOD2, is expected to be used in future environmental impact assessments which are required as a result of industry expansion. It can easily be applied to other toxic substances and rivers to consider continuous and single spill discharges where incomplete mixing required two-dimensional analysis. It has been designed to operate within the Windows environment and has a user friendly input interface coupled with sophisticated model output visualization features.

SOMMAIRE À L'INTENTION DE LA DIRECTION

Le présent rapport décrit un modèle bidimensionnel de transport et de devenir d'un contaminant et son utilisation pour le bassin inférieur de la rivière Athabasca. Il s'agit là de l'un des principaux travaux d'un projet étalé sur plusieurs années et financé par le Groupe interministériel de recherche et d'exploitation énergétiques (GRDE) et Environnement Canada, projet qui vise à étudier l'impact de l'exploitation des sables bitumineux et des huiles lourdes sur le milieu aquatique dans le nord-est de l'Alberta. Les sables bitumineux de l'Athabasca représentent une fraction importante de l'approvisionnement en pétrole du Canada. Un certain nombre de CAP (composés aromatiques polycycliques) azotés et sulfurés, ainsi que leurs dérivés alkylés, ont été décelés dans les circuits et les émissions des procédés de traitement de ces sables. On sait que certains de ces composés sont mutagènes et cancérigènes. Le devenir et la persistance desdits composés en aval des usines de sables bitumineux sur la rivière Athabasca ont été examinés grâce à la collecte de données sur le terrain et en laboratoire, combinée à une simulation par modélisation sur ordinateur. On prévoit utiliser le modèle, ATHMOD2, pour de futures évaluations de l'impact environnemental, rendues nécessaires par l'expansion de l'industrie. Il peut facilement s'appliquer à d'autres substances toxiques et à d'autres rivières, pour évaluer les déversements continus et temporaires là où un mélange incomplet nécessite une analyse bidimensionnelle. Concu pour fonctionner en Windows, le modèle présente une interface d'entrée conviviale, combinée à une visualisation sophistiquée à la sortie.

RÉSUMÉ

Le bassin inférieur de la rivière Athabasca traverse les gisements de sables bitumineux de l'Athabasca dans le nord de l'Alberta. Deux usines d'extraction et de traitement de ces sables sont exploitées près de la rivière, en aval de Fort McMurray. Les effluents de l'une des usines (Suncor) sont déversés dans la rivière et contiennent de faibles concentrations de composés aromatiques polycycliques (CAP). Par suite de l'expansion de l'industrie, il faudra procéder à plusieurs évaluations de l'impact environnemental. Pour obtenir un outil d'évaluation de ces CAP, on a élaboré un modèle bidimensionnel de devenir des contaminants et on l'a appliqué à une portion de 120 km de la rivière Athabasca, en aval de Fort McMurray. L'étalonnage hydraulique du modèle a été effectué à l'aide de sodium et de chlorure provenant d'un affluent majeur, utilisés comme traceurs. Deux groupes de composés ont été modélisés : 1) les CAP provenant de l'effluent de Suncor; 2) les CAP provenant de sources naturelles ou de base. Les concentrations de CAP étaient généralement < 1 ng/L, nécessitant de grands volumes pour l'extraction et des méthodes d'analyse très sensibles. Les processus, comme le partage sédiments/eau et la biodégradation, ont été évalués à partir d'expériences sur le terrain utilisant l'eau et les sédiments en suspension de la rivière. La majeure partie des composés avaient des demi-vies d'environ 36 heures, ce qui présentait une bonne corrélation avec la cinétique de décomposition déterminée par étalonnage du modèle selon les concentrations mesurées dans la rivière.

A Two-Dimensional Contaminant Fate and Transport Model for the Lower Athabasca River

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Abstract

The lower Athabasca River flows through the Athabasca Oil Sands deposits in northeastern Alberta. Two oil sands mining/extraction/upgrading plants operate near the river downstream of Fort McMurray. Effluents from one of the plants (Suncor) is discharged to the river and contains low concentrations of polycyclic aromatic compounds (PAC's). Several environmental impact assessments are required as a result of industry expansion. To provide an assessment tool for the PAC's, a two-dimensional contaminant fate model has been developed and applied to a 120 km portion of the Athabasca River downstream from Fort McMurray. Hydraulic calibration of the model was carried out using sodium and chloride from a major tributary as tracers. Two groups of compounds were modelled: (1) PAC's from the Suncor effluent, and (2) PAC's from natural/background sources. PAC concentrations in the river were typically < 1 ng/L, requiring large volume extractions and highly sensitive analytical methods of analysis. Processes such as sedimentwater partitioning and biodegradation were determined from field experiments using river water and suspended sediment. The majority of the compounds showed half-lives of approximately 36 hours, which matched very well with decay kinetics determined through model calibration to measured river concentrations.

INTRODUCTION

The area in the lower Athabasca river watershed of northeastern Alberta contains an extensive oil sands deposit. A significant partion of Canada's petroleum production is derived from the extraction and upgrading operations that are carried out by Suncor, Inc. and Syncrude Canada Ltd. A multiyear project was started in 1989 to study the possible impact of these oil sands extraction and upgrading operations on aquatic ecosystems along the Athabasca River. The project is funded by the National Water Research Institute and the Interdepartmental Panel for Energy Research and Development (PERD). One of the goals of this project was to develop predictive models which can be used to examine the fate and transport of effluents from the oil sands extraction plants. These include polycyclic aromatic hydrocarbons (PAH's), which are naturally found in the area, as well as thiophenes and quinolines. PAH's may be acutely toxic or genotoxic, which is dependent upon the number and configuration of the fused benzene rings and the presence or absence of other chemicals (Heitkamp and Cerniglia 1989). Also, many of the metabolites of PAH's are known to be mutagenic, carcinogenic, or both (Bumpus 1989). Many of these chemicals appear on the CEPA (Canadian Environmental Protection Act) priority substance list and have been identified as persistent, bioaccumulative, and toxic subtances. Chemicals that meet or exceed criteria for toxicity, bioaccumulation and persistence, which were detected in effluents in this study include fluoranthene, phenanthrene, acridine, and pyrene. Toxicity testing on 21 quinoline derivatives (Birkholz et al., 1990) demonstrated that all compounds are moderately toxic according to the Microtox assay.

Based upon the results of the first 2 years of reconnaissance work to characterize the Athabasca

River system, a preliminary, one dimensional chemical fate model was developed and tested (Booty et al., 1991) for phenols downstream of Ft. McMurray to the delta at Lake Athabasca. Subsequent field data indicated that the river does not mix well across its width (Bourbonniere, R.A., 1992). Consequently, a 2-dimensional model (ATHMOD2) was developed to simulate the distribution of chemicals within the river.

MODEL DESCRIPTION

ATHMOD2 is a two-dimensional model that considers contaminant concentrations along the longitudinal or downstream direction as well as the lateral or cross-stream direction. In this model it is assumed that there is no vertical concentration gradient. The model is a modified version of TWODIFIN (OMOE,1988). TWODIFIN is an acronym for TWO-Dimensional FINite-time model. ATHMOD2 is designed to consider continuous and single spill discharge scenarios. It is also modified to incorporate additional in-river decay processes required to model toxic organic compounds such as PAH's. In addition, the model has been coupled with a new user interface and has been compiled using Visual Basic so that the original Fortran 77 code runs within the Windows environment. A description of the new interface is described in the next section.

The model is based upon a stream tube concept which was developed by Yotsukura and Cobb, 1972; Yotsukura and Sayre, 1976; Yotsukura and Sayre, 1977. In this model, the channel is divided into a number of strips called stream tubes so that the discharge within each stream tube is the same. The model uses a cumulative partial discharge, q, at a selected cross section instead of the actual lateral discharge, q, as the independent variable. In this case, the cross sectional concentration distributions c(x,q) predicted by the model are functions of q. By knowing the relation between q and y at each transect, the distributions can be transformed into c(x,y) distributions.

The 2-D convective-dispersion equation for a non-conservative material in the far field region of the mixing zone can be expressed in the form:

$$\frac{\delta c}{\delta t} + u \frac{\delta c}{\delta x} = e_x \frac{\delta^2 c}{\delta x^2} + u D_y \frac{\delta^2 c}{\delta q^2} - K_d c$$

where x = longitudinal coordinate (m)

y = lateral coordinate (m) from the reference bank

q = cumulative partial discharge (m³/s)

t = time(s)

u = velocity of flow in the x direction (m/s)

e_x = longitudinal dispersion coefficient (m²/s)

 $D_v = lateral diffusion factor (m⁵/s²)$

 K_d = first order decay rate coefficient (1/s)

c = concentration at point (x,q) at time (t)

The solution to equation (1) for a constant effluent discharge and concentration is:

$$C = \frac{u\exp\frac{ux}{(2e_x)}}{4\sqrt{\pi e_x e_q}} \sum_{i=1}^{n} \left\{ (\Delta w) \left[\frac{\exp(-2\sqrt{ab})}{(ab)^{1/4}} \left\{ erf\left(\sqrt{\frac{a}{t-t_j}} - \sqrt{b(t-t_j)}\right) - erf\left(\sqrt{\frac{a}{t-t_i}} - \sqrt{b(t-t_i)}\right) \right\} \right] \right\}$$

where
$$a = (x^2/4e_x) + ((q_s - q)^2/4e_q)$$

 $b = (u^2/4e_x) + K_d$

and u = velocity of flow (m/s)

x = distance downstream from the source (m)

t = time(s)

t_i = time of beginning of release (s)

t_i = time of end of release (s)

w = rate of release of mass (1/s)

e_r = longitudinal dispersion coefficient (m²/s)

 e_q = transverse diffusion coefficient (m⁶/s³)

The transverse diffusion coefficient is calculated in the model using the relation:

$$e_a = \beta Q^2 u/b$$

where Q is the total discharge for a reach and β is a dimensionless factor which is calculated from tracer studies (Booty, 1994).

The river is divided longitudinally into reaches and stream tubes. Each reach is assumed to have reasonably constant hydrodynamic characteristics. The model allows for up to 15 reaches and 15 stream tubes. The important parameters having longitudinal variabilities of concern include width, depth, velocity, decay rate, and stream bed material. These variabilities are considered in equation 1 and in the ATHMOD2 model the decay term K_d has been expanded to include expressions for volatilization, biodegradation, photolysis, oxidation, and hydrolysis. To take into account the variation of the hydrodynamic parameters from reach to reach, moving averages are determined that approximate the effective values of river width, depth, and velocity of flow. In order to scale the depth, width, and velocity to different flow conditions, Leopold-Maddock relationships are used (Leopold and Maddock, 1953). The model uses Bansal's equation (Bansal, M.K., 1971) to compute the dispersion coefficients if they are not available from tracer studies.

ATHMOD2 USER INTERFACE

The interface consists of a number of windows which allow the user to create the input data set for the model, edit the input data, edit the views of the river including the placement of the transects, and select options for viewing the output data. By selecting the file menu the user can create a new input data file, open an existing input data file, or save the file.

Typically the first step in setting up the model is to select the positions of the transects that will

define the reaches along the river. The user interface provides a number of windows that allow the user to view the river at different scales. The Large Map Window is the top portion of the screen shown in Figure 1. It is a scrollable map of the Athabasca River. The user is given a view that is approximately 25 km wide by 9 km high. The Small Map Window, which is the bottom portion of the screen shown in Figure 1, gives the user the view of the entire portion of the river that is being modelled. A box that is proportional in scale to the Large Map Window can be used to scroll within the Large Map Window. The user can easily add a transect by clicking on the Add Transect button and dragging it onto the Athabasca River map. Once the transect icon has been placed on the map, the user can still modify the location of the transect by dragging the transect icon to the desired location. The user also has the ability to manually enter a transect by using the Edit Transect option. This allows the user to type in exactly how far down the river the transect is from the starting reference point. This menu option also allows the user to enter the transect data into a new transect created from the drag and drop Add Transect operation.

Selecting "Parameters" from the model menu activates the model setup window (Figure 2). This window allows the user to display and modify the:

Title of the study
Pollutant name
Model resolution
Days to run the model
Number of stream tubes
Fraction of flow between the bank and discharge pipe
Delta value for estimating the number of bank images
Tolerance level to determine degree of mixedness
Background concentration of the pollutant
Use of Leopold-Maddock relationship
Use of longitudinal dispersion coefficient

Selecting "Edit Transect" from the model menu activates the window (Figure 3) which allows the user to view and modify the input data for each reach and associated transects. The parameters include:

Distance from the outfall
Longitudinal dispersion coefficient
Transverse dispersion coefficient
Leopold-Maddock constants (width, depth, and velocity)
Reach design temperature and stream flow
Reach length and channel geometry (width-depth profile)
Flow velocity
Decay rate

By selecting "Decay Rate" with the mouse, a new window appears (Figure 4), which allows the user to supply individual decay reaction rate values, which include:

Volatilization
Photolysis
Oxidation
Benthic biodegradation

Hydrolysis Metabolization

The final step involves entering the effluent discharge data. The parameters that may be modified within the Effluent Discharge window (Figure 5) are:

Source data time interval Number of intervals

For each time interval:
Time

Discharge rate Concentration

When the input file has been created and saved the model may be run by selecting "Run model" from the Model menu. The results of the model run are then displayed directly on the Pollutant Concentration window view of the river, as shown in Figure 6. The x axis represents the distance down the river and the y axis represents the stream tubes. The vertical lines represent the transects at which water flow and chemistry are observed. By moving the mouse cursor to any point on the screen, the reach number, stream tube number, distance from the outfall, and concentration of the contaminant is shown.

The View Data Window (Figure 7) may be selected to display the model output data in tabular form. The user may also cut and paste the data into any Windows spreadsheet.

EXPERIMENTAL

Collection and Field Processing of Samples

A schematic of the sampling strategy is shown in Figure 8. Calibration of a two-dimensional model requires lateral data (transects) at a number of points upstream and downstream from the source (Suncor wastewater discharge to the Athabasca River). Seven transects were sampled at five points across the river at approximately 0.1, 0.3, 0.5, 0.7 and 0.9 of the distance from the left bank (Sites A, B, C, D, and E). These transects were upstream of the Horse River (only a four-point transect was sampled here), and at km 33.3, 40.2, 53.9, 60.0, 90.1, and 131.9 from the reference point for the model. The Suncor discharge is at km 37.8.

River water was pumped from 0.5 m depth through an Alfa-Laval MAB-103 continuous-flow centrifuge using PTFE-lined tubing. Centrifugate was collected and extracted (see below) and the suspended sediment was removed from the centrifuge bowls and frozen. In order to sample one transect per day and obtain sufficient suspended sediment, it was necessary to use two boats and three centrifuges.

Water (centrifugate) samples (20 L) were extracted onsite by stirring with dichloromethane (DCM) in a stainless vessel following appropriate pH adjustment (pH 12 for base/neutral extract followed

by pH 2 for acid extract). Diphenyl-d₁₀ was added as a recovery standard. The method is described in more detail in Fox (1986) and in Brownlee et al. (1995). Suncor wastewater samples (4 L, collected by Suncor staff) were extracted in a separatory funnel at pH 12 with three portions of DCM, the pH adjusted to 2 and extracted with a further three portions of DCM. All extracts were shipped to the National Water Research Institute in Burlington for laboratory analysis.

Laboratory Analyses -- Quantitation of Base/Neutral Compounds

Water was separated from the DCM extracts, the extracts dried by passing through combusted (450°C) sodium sulfate and concentrated on a rotary evaporator. The extracts were then transferred to graduated 15 mL tubes and further evaporated under an argon stream. A portion was solvent-exchanged into toluene and chrysene-d₁₂ was added as an internal standard. The extract was then analyzed by gas chromatography-mass spectrometry (GC-MS) in the single ion mode (SIM). Each sample was injected five times using a different method for each injection depending on the target compound(s) being quantitated. The different groups quantitated were: polycyclic aromatic hydrocarbons (PAHs), alkylated PAHs, benzothiophenes, quinolines, and miscellaneous (aromatic amines, phenanthrene, diphenyl-d₁₀). For the river water samples results were corrected based on diphenyl-d₁₀ recoveries.

The instrument used was a Hewlett-Packard model 5890 gas chromatograph connected to a Hewlett-Packard model 5791 mass selective detector operating in electron impact mode at 70 eV. The column was a 30 m x 0.25 mm capillary coated with 0.25 µm of DB-5ms, helium carrier at ca. 35 cm/s (constant flow mode). The temperature program was 80-245°C at 3°C/min to 245°C, then at 4°C/min to 280°C with ten minute hold. A 1µL sample was injected by splitless injection.

Average relative standard deviation for sampling and analysis was 15% (n=30), based on results for eight of the compounds in duplicate samples collected at four of the transects.

Laboratory Analyses -- Identification of Base/Neutral Compounds

Prior to establishing the target list of base/neutral compounds to quantitate, Suncor wastewater base/neutral extracts were examined qualitatively by GC-MS. Several compounds could be identified by comparison of retention times and spectra with authentic materials available at the time. In other cases, we had to rely on comparison with library spectra and estimates of likely retention times. In one case (2,4-dimethylbenzothiophene) authentic material was only obtained after the quantitation had been completed. The mass spectra for the 2,4-DMBTP in the effluent and for the standard are shown in Figures 9 and 10 respectively. The qualitative results for all of the compounds are summarized in Table 1.

Table 1. Information available for identification of compounds quantitated in Suncor effluent and Athabasca River, May, 1993.

· ·							
Compound		Std. ^a	RT Match TIC ^b	RT Match XIC ^c	Spec. Match		RI Lit. ⁶
7-Methylquinoline	•	Y	Y	Y	Y	227.47	231.37 ¹
2,4-Dimethylquinoline		Y	Ÿ	Y	Y	242.69	`.
Trimethylquinoline Isomer (1st)	N			$\mathbf{Y}^{\mathbf{f}}$			
Trimethylquinoline Isomer (2nd)	N			$\mathbf{Y}^{\mathbf{f}}$			
Acridine		Y	Y	Y	\mathbf{Y}	303.71	304.04 ¹
Benzoquinoline Isomer		N			Y ^g	307.56	307.94 ¹
3/4-Methylbenzothiophene	Ÿ	Y	·Y	· Y	220.06	5	220.55 ²
2,4-Dimethylbenzothiophene	\hat{N}^h	, Ÿ	Y	Y	238.02	2	238.39 ²
Naphthalene	Y	Y					
Phenanthrene ⁱ	Ÿ	. Y					
Fluoranthene	Y	· Y					
Pyrene ⁱ	-	Y	Y		- - -		

^a Authentic material available (Y)/unavailable (N) for quantitation.

The concentrations of the organic compounds in the Suncor wastewater and the Athabasca River collected during May of 1993 for the sites shown in Figure 8 are presented in Appendix A.

Water Column Disappearance Experiments

To 2 L amber glass wide mouth bottles were added 400 mL of Athabasca River sediment and 2000 mL of unfiltered Athabasca River water followed by 100 mL of an aqueous solution of the test compounds 7-methylquinoline, 2,4-dimethylquinoline, 3-methylbenzothiophene, acridine and pyrene to give a nominal initial concentration of 500 ng/L of each test compound. The jars were closed with caps that were driled with holes to accommodate stirring paddles. The bottle contents were stirred gently at room temperature with a mechanical stirrer motor. At 0, 1, 2, 4 and 7 days, the

^b Retention time match with standard for the Total Ion Chromatogram.

^c Retention time match with standard for 3-4 ions in Extracted Ion Chromatogram.

^d Experimental Retention Index.

^e Literature Retention Index; Ref. 1 Vassilaros et al. (1982); Ref 2 Andersson (1986).

Assigned on the basis of m/z 171 ion and match with library spectrum.

⁸ Retention Index and library spectrum match for benzo[f]quinoline or phenanthridine.

h Authentic material was available for identification.

Assigned on basis of quantitation ion and retention time.

water from one bottle was extracted with DCM (3 x 100 mL). The extracts were worked up and analyzed in the laboratory in the same manner as the large volume extracts except that diphenylamine (1 μ g/mL) was used as the internal standard. The results are shown in Figure 11.

MODEL APPLICATION and CALIBRATION

Data collected during the 1993 sampling year was used to calibrate the model. Major ion chemistry and flow data were used to determine the transverse mixing characteristics of the river reaches (Booty, 1994). Daily loadings for the Suncor effluent were available for the period of May 25-31. As seen in Appendix A for the Suncor wastewater, the daily loadings are not constant as both discharge rates and concentrations of the chemicals vary. Due to sampling logistics, the sampling of river concentrations were carried out at different transects on different days as the crews moved downstream. Consequently, model outputs have been selected which most closely match the measured values with respect to time of travel in the river. Model predicted vs measured results are also examined with and without decay reaction kinetics.

2,4-Dimethylbenzothiophene

2,4-DMBTP is one of the compounds in the Suncor watestream that does not occur naturally in the river. This is seen in Appendix A where 2,4-DMBTP is a non-detect (ND) at the u/s Horse River site and at transect 1 (km 33.5), both of which are upstream of the Suncor wastestream discharge. The background value for the model runs was set to 0.0 ng/L. An error analysis was carried out using the results of replicate analyses of river water samples for each compound. The overall average residual standard deviation of 15% was used for the determination of the error bars which are shown in all of the following figures for the observed data.

At transect 2 (km 40.2), as shown in Figure 12, the model significantly underestimates the concentration in the first 2 stream tubes. The Suncor wastestream enters the river close to the left bank, and in the model it is equally input to the 1st and second stream tubes. The model predicted concentrations in the other 8 stream tubes match the observed data almost exactly. This is a result of the fact that the there is very little lateral mixing between the discharge point at km 37.8 and transect 2 at km 40.2. In the model, it is assumed that the effluent is at the same temperature and has the same buoyancy as the river water. However, this was determined well after the sampling had been completed to not be the case. The effluent is much warmer than the river water and more buoyant. Early exploratory sampling for major ions indicated that the river was vertically mixed and so subsequent sampling was not carried out at different depths, but only in the top 0.5 metres. Consequently, we believe that the higher measured concentrations than those predicted by the model are due to incomplete vertical mixing of the effluent.

At transect 3 (53.9 km) (Figure 12), the pollutant still does not appear to be completely vertically mixed. However, the effect of lateral diffusion is obvious from the measured data and is well predicted by the model.

At transect 4 (60.0 km) (Figure 13) the model predicted and measured concentrations match extremely well. By this point it appears that the chemical is vertically mixed within the river. By transect 5 (90.1 km) (Figure 13) the model begins to overpredict the concentrations on the left side of the river. The higher measured concentration at 0.9 from the left bank must be due to analytical error or contamination as there is no source of 2,4-DMBTP to account for such an anomaly.

At transect 6 (131.9 km) (Figure 14) the model overpredicts the concentrations across the entire river. This is assumed to be due to the decay of the chemical in the system with time. No experimental decay data were available for this compound so the overall decay rate (t1/2 = 36 hrs) was determined through calibration of the model with the observed data. However, this value is close to that found for 3-methylbenzothiophene (t1/2 = 32 hrs) through experimental studies (Figure 11).

As expected, the model predictions at transects 2 and 3 (Figure 15) are virtually identical to those simulated with the decay set to zero (Figure 12). The model predicted concentrations at transect 4 (Figure 16) with decay are not quite as close of a match to the measured data as they are for decay set to zero. However, at transect 5 (Figure 16) the model predicted concentrations across the river match the measured data extremely well as compared to those without decay kinetics (Figure 13). The model predicted concentrations across the river at transect 6 (Figure 17) match the measured data much more closely than those in Figure (14) with no decay. It is also interesting to note that after 98 kms of travel the 2,4-DMBTP has still not completely mixed laterally across the river. It is also apparent that for the model to more accurately simulate the decay of 2,4-DMBTP between transects 5 and 6 needs to be higher than it is in the previous reaches. The model was run again with t1/2 = 36 hrs for the reaches upstream of transect 5 and the value of t1/2 downstream was calibrated to give the best fit to the data at transect 6. A value of t1/2 = 12 hrs was found to give the best fit to the observed data (Figure 18). Further experimental work in this reach of the river is required to determine if this is a reasonable rate of decay.

7-Methylquinoline

This compound was only found in one sample (Appendix A; Site B, u/s Horse River) at a very low concentration (0.273 ng/L) upstream of the Suncor wastestream discharge. It is therefore not considered to have a significant natural source. The background concentration for the modelling was set at 0.1 ng/l (detection limit).

As is the case with the 2,4-DMBTP, the measured concentrations of 7-methylquinoline on the left bank of the river at transects 2 and 3 (Figure 19) are substantially higher than the model predicted values due to incomplete vertical mixing of the Suncor wastestream in the river. At transects 3 and 4 (Figure 20) the model predicted concentrations match the measured values within the range of uncertainty of the analytical methods. However, at transect 6 (Figure 21) with the decay term set to zero, the model overpredicts the measured concentrations.

The model was run again with the decay term set to the measured value of t1/2 = 36 hrs. For transects 2 and 3 (Figure 22) the model results are virtually the same as for no decay (Figure 19). At transect 4 (Figure 23) the model predicts a minor decrease in the concentrations in the first 2 stream tubes only as compared to the run with no decay (Figure 20). However, at transect 5 (Figure 23) the predicted concentrations are substantially lower than those determined with zero decay (Figure 20).

At transect 6 (Figure 24) the predicted concentrations give a much better fit to the measured data than for the model run with zero decay (Figure 21).

2,4-Dimethylquinoline

As seen in Appendix A, this compound is found at significant concentrations at both transects upstream of the Suncor wastewater stream discharge and is one of the major components in the wastewater stream.

Running the model with decay set to zero, at transect 2 (Figure 25), as was the case for the other compounds, the model underpredicts the concentration measured at the left side of the river due to the lack of vertical mixing of the effluent. However, by transect 3 (Figure 25), the model predicted and observed concentrations are beginning to approach one another. An even better match is seen at transect 4 (Figure 26). The model predicted versus observed data also match very well at transect 5 (Figure 26). The trend of the observed data at transect 6 (Figure 27) do not match the model predicted trend and indicate that there may be an additional source or sources of 2,4-dimethylquinoline along this stretch of the river. This is also obvious in that the water column disappearance kinetics studies (Figure 11) indicated that 2,4-dimethylquinoline should have a decay rate of t1/2 = 48 hrs. If this was used the model would greatly underestimate the measured river concentrations at the different transects. Unfortunately tributary loads of this compound downstream of the Suncor wastestream discharge are not known.

Pyrene

Pyrene is a minor component of the Suncor effluent (Appendix A) and is actually found at lower concentrations in the Athabasca River below the Suncor effluent discharge than upstream (Appendix A). Consequently, as a compound with natural soyrces along the river, the mixing of the Suncor effluent in the river is masked and can not be simulated with the model without the tributary loadings (Figures 28-30).

Benzoquinoline Isomer

This compound was not present in detectable quantities at the u/s Horse River transect (Appendix A). However, at mile 20.8 (km 33.3) is was detected at all sites except A. There is no known source of this compound between these two transects to explain the increase in concentration. Benzoquinoline is also a significant component of the Suncor waste stream (Appendix A). The model predicted (decay set to zero) versus observed concentrations downstream of the effluent dischrage are shown in Figures 31-33. Again due to incomplete vertical mixing of the effluent within the river, the model predicted concentrations on the left bank of the river are significantly less than the observed values. However, by transect 6 (Figure 33) the model overpredicts the observed concentrations, indicating that here had been loss of the compound between transects 5 and 6. No experimental water column disappearance kinetics data were obtained for this compound. A

decay value of t1/2 = 36 hrs was determined through calibration of the model with the observed concentrations. The results are shown in Figures 34-36.

CONCLUSIONS

- 1) The Suncor effluent remains incompletely vertically mixed in the Athabasca River for a distance of 16 to 22 km downstream of the discharge point for the various compounds. All of the compounds studied were found to be incompletely mixed across the river for at least 100 km downstream of the Suncor discharge.
- 2) 2,4-Dimethylbenzothiophene, 2,4-Dimethylquinoline and 7-Methylquinoline were found to be the best tracers of the Suncor effluent. They had no significant natural sources along the river and were major components of the Suncor wastestream.
- 3) The two-dimensional transport and fate model ATHMOD2 was successfully used to simulate the lateral mixing and decay of most of the Suncor wastestream compounds along the 120 km stretch of river downstream of Ft. McMurray. The experimental water column disappearance rates determined for the compounds were confirmed to be correct through calibration of the model with the observed data.
- 4) For those compounds with natural sources along the river and which were not major components of the Suncor wastestream, the downstream concentrations could not be accurately predicted by the model. Samples from the major tributaries have been collected but have not yet been analyzed for the compounds with natural sources. This data could be used as input to the model in order to more accurately simulate their transport and fate in the river. Further calibration and verification of the model requires another complete set of data collected during different flow conditions and effluent loadings.

ACKNOWLEDGEMENTS

We thank S.B. Smith and R. Neureuther, Technical Operations, National Water Research Institute, for providing field support. The contribution of S.B. Smith is especially appreciated for organizing the complex field logistics required in order to sample one transect per day. We also thank J. Lussenburg and the other Suncor staff who provided the daily samples of Suncor wastewater for us. Finally, we gratefully acknowledge the financial support from PERD.

REFERENCES

Andersson, J.T. 1986. Gas chromatographic retention indices for all C₁- and C₂-alkylated benzothiophenes and their dioxides on three different stationary phases. J. Chromatog. 354:83-98.

Bansal, M.K. 1971. Dispersion in Natural Streams. Journal of Hydraulics Division, ASCE, 97 (HY11): 1867-1886.

Birkholz, D. A., Coutts, R.T., Hrudey, S.E., Danell, R.W., and Lockhart, W.L. 1990. Aquatic Toxicology of Alkyl-Quinolines. Wat. Res. Vol. 24, No.1, pp. 67-73.

Booty, W.G. 1994. Mixing Characteristics of the Athabasca River using Conservative Ions. NWRI Contribution No. 94-152.

Brownlee, B.G., S.L. Kenefick, G.A. MacInnis and S.E. Hrudey. 1995. Characterization of odorous compounds from bleached kraft pulp mill effluent. Wat. Sci. Tech. 31(11):35-40.

Bumpus, J.A. 1989. Biodegradation of polycylcic aromatic hydrocarbons by Phanerochaete chrysosporium. Appl. Environ. Microbiol. 55:154-158.

Fox, M.E. 1986. A Practical Sampling and Extraction System for the Quantitative Analysis of Subng/L of Organochlorine Contaminants in Filtered Water and Suspended Solids, National Water Research Institute Contribution No. 86-41, Environment Canada, Burlington, Ontario, 13 pp.

Heitkamp, M.A. and Cernilglia, C.E. 1989. Polycyclic aromatic hydrocarbon degradation by a Mycobacterium sp. in microcosms containing sediemnt and twater from a pristine ecosystem. Appl. Environ. Microbiol. 55:1968-1973.

Leopold, L.B. and Maddock, T. 1953. The Hydraulic Geometry of Stream Channels and Some Physiographic Implications, Professional Paper 252, U.S. Geological Survey, Washington, DC.

Vassilaros, D.L., R.C. Kong, D.W. Later and M.L. Lee. 1982. Linear retention index system for polycyclic aromatic compounds. Critical evaluation and additional indices. *J. Chromatog.* 252:1-20.

Yotsukura, N., 1977. Derivation of Solute-Transport Equations for a Turbulent Natural-Channel Flow. Journal of Research, U.S. Geological Survey, 5(3), p277-284.

Yotsukura, N. and Cobb, E.D. 1972. Transverse Diffusion of Solutes in Natural Streams. U.S. Geological Survey Professional Paper 582-C, U.S. Gov't Printing Office, Washington, D.C. 19 pp.

Yotsukura, N. and Sayre, W.W. 1976. Transverse Mixing in Natural Channels. Water Resources Research, 12(4), 695-704.

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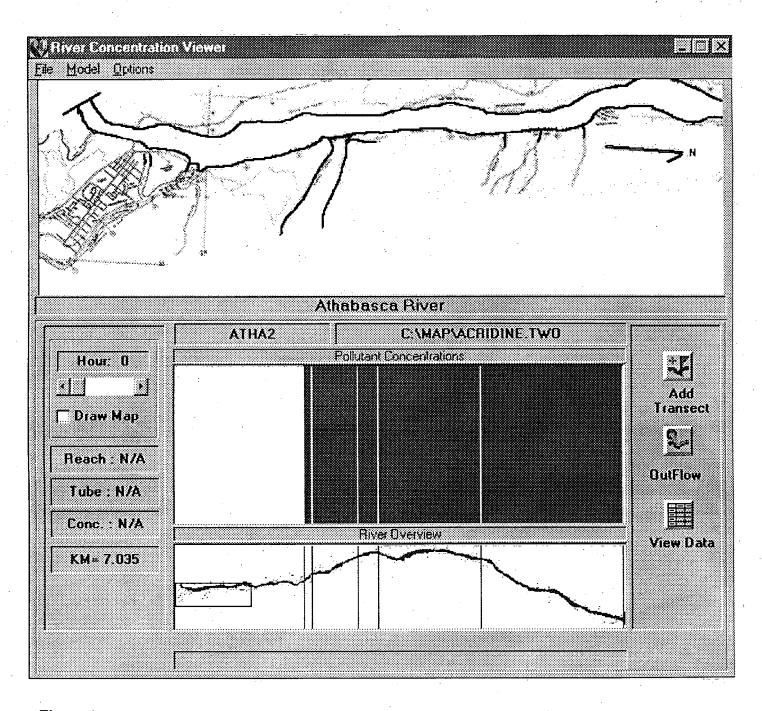


Figure 1

Title of Model	
Athabasca River Mixing Study May , 1993	
Pollutant Title	
Acridine Data May 1993	
Resolution of Model (hours) 6 Number	er of Stream Tubes 10
Simulation Length (Days) 15.0 bank to	n of flow between .9
	value for estimating .001
□ Leopold-Maddock Relationship	
7	nce level to .1 nine mixedness
OK Cancel Outfall	round concentration .08

Figure 2

	Transect			
Downstream distance of transect from iver zero (0) reference (km)		Transect# 40.200		
Longitudinal dispersion c	coefficient (m2/s)	0		
Transverse dispersion factor		.00039		
Leopola-M	ieddock Experients	Reach Design		
Width	.05	Temperature (C)		
Depth	18	20		
Velocity	.45	Stream Flow (m3/s)		
	ch Reference Data	766		
Temperature (C)	20	1.77		
Stream Flow (m3/s)	766			
Channel Width (m)	330	Next		
Channel Depth (m)	1.73	Previous		
Channel Velocity (m/s)	1.36			
Decay Rate (s-1)	.0005628	New		
Adsorption (?)		Delete		
		Save Exit		

Figure 3

— Reaction F	Rates
Volatilization (s-1)	.0003
Photolysis (s-1)	.00009
Oxidation (s-1)	.000002
Benthic Biodegradation (s-1)	.00017
Hydolysis (s-1)	.0000006
Metabolization (s-1)	.0000002
<u>o</u> k <u>c</u>	ancel

Figure 4

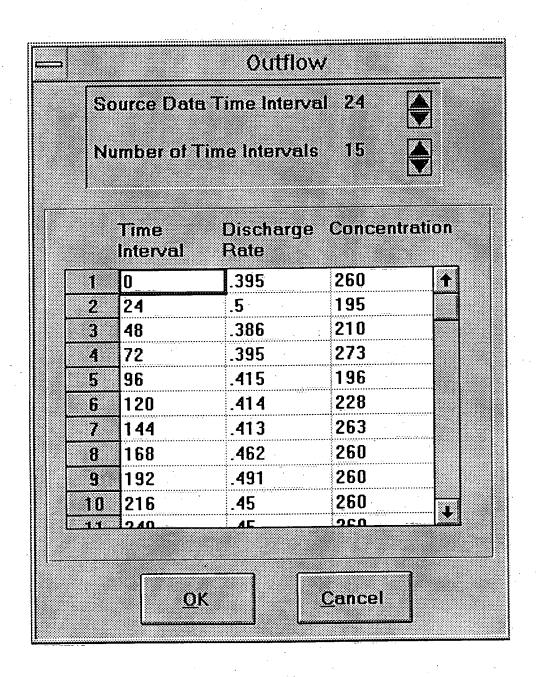


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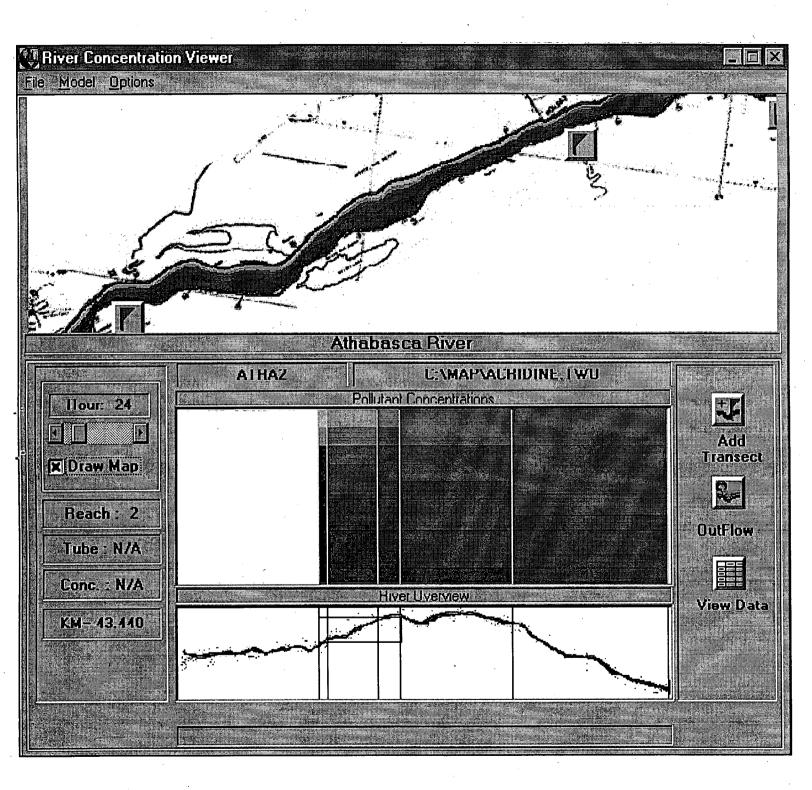
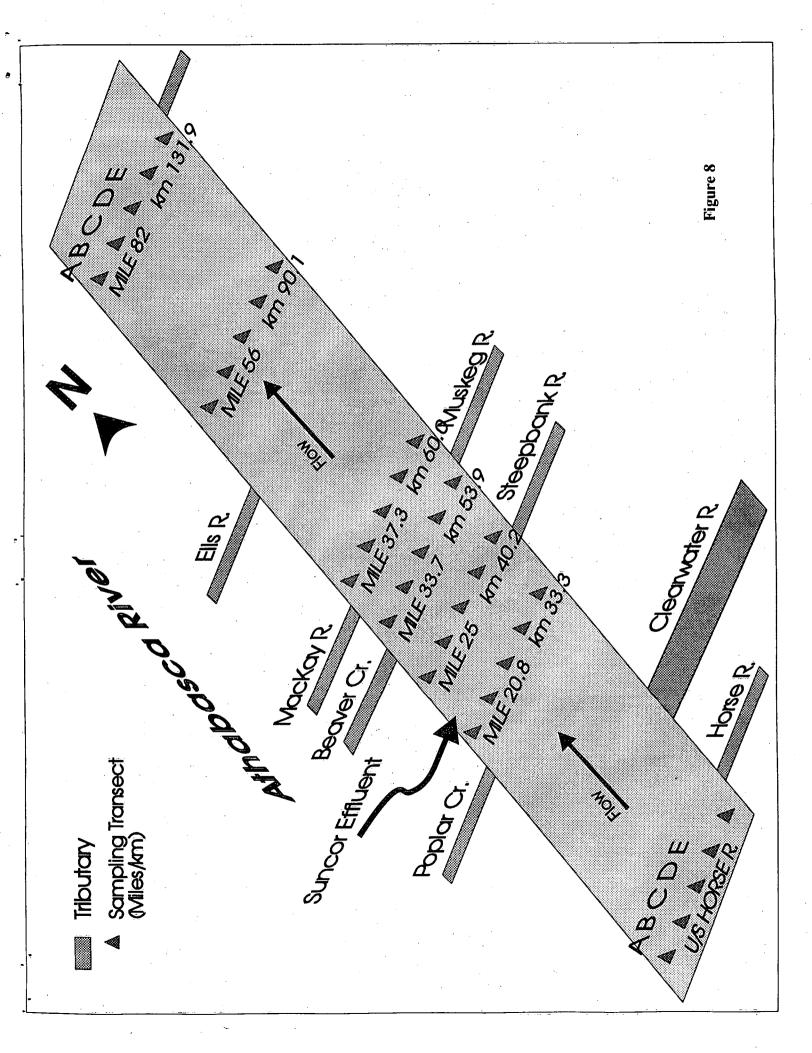


Figure 6

_		ATHA2	Data		¥
Transect	Hour	Tube 6	Tube 7	Tube 8	Tube
	0	0.0800	0.0800	0.0800	0.0800
	6	0.0800	0.0805	0.1020	5.6025
l	12	0.0800	0.0805	0.1020	5.5785
l	18	0.0800	0.0805	0.1015	5.5085
	24	0.0800	0.0805	0.1010	5.3925
	30	0.0800	0.0805	0.1005	5.2215
l	36	0.0800	0.0805	0.0995	5.0120
l	42	0.0800	0.0805	0.0990	4.7910
1	48	0.0800	0.0805	0.0980	4.5585
1	54	0.0800	0.0805	0.0980	4.6165
1	60	0.0800	0.0805	0.0995	4.9725
1	66	0.0800	0.0805	0.1010	5.3325
1	72	0.0800	0.0805	0.1025	5.6965
1	78	0.0800	0.0805	0.1025	5.7090
1	84	0.0800	0.0805	0.1010	5.3630
l	90	0.0800	0.0805	0.0995	5.0065
1	96	0.0800	0.0805	0.0980	4.6400
1	102	0.0800	0.0805	0.0980	4.5425
					-

Figure 7



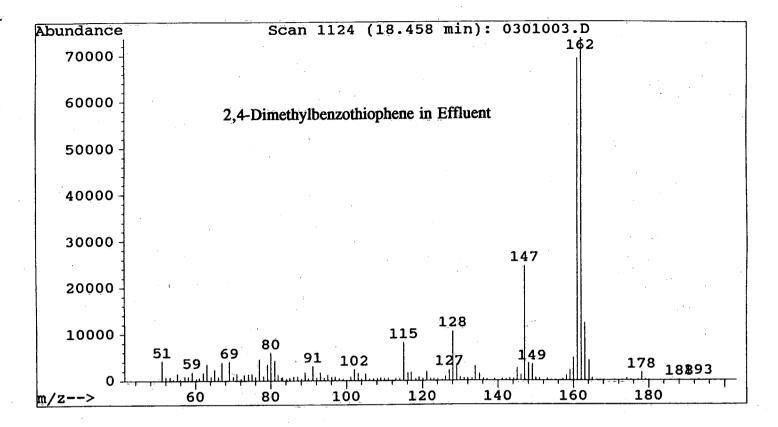


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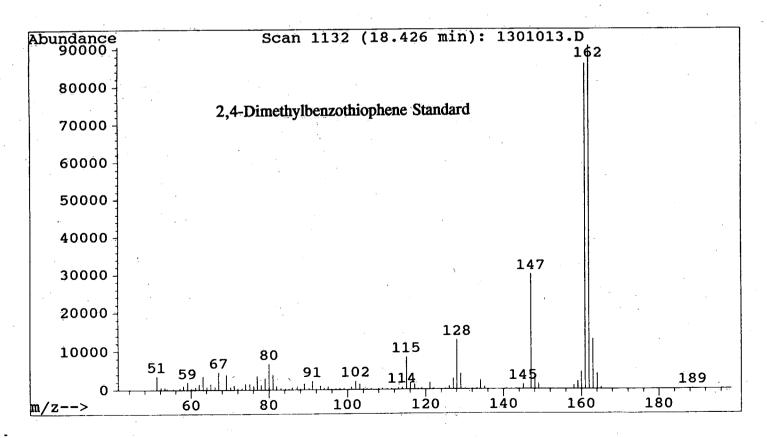
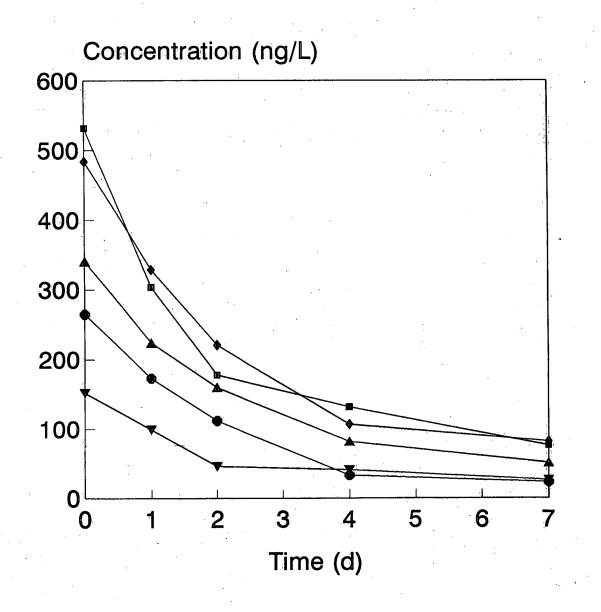


Figure 10

Water Column Disappearance Kinetics



Test Compound

- Pyrene
- → Acridine
- **★** 2,4-DiMeQuinoline
- ◆ 7-MeQuinoline
- **▼** 3-MeBenzothiophene

Figure 11

Figure 12

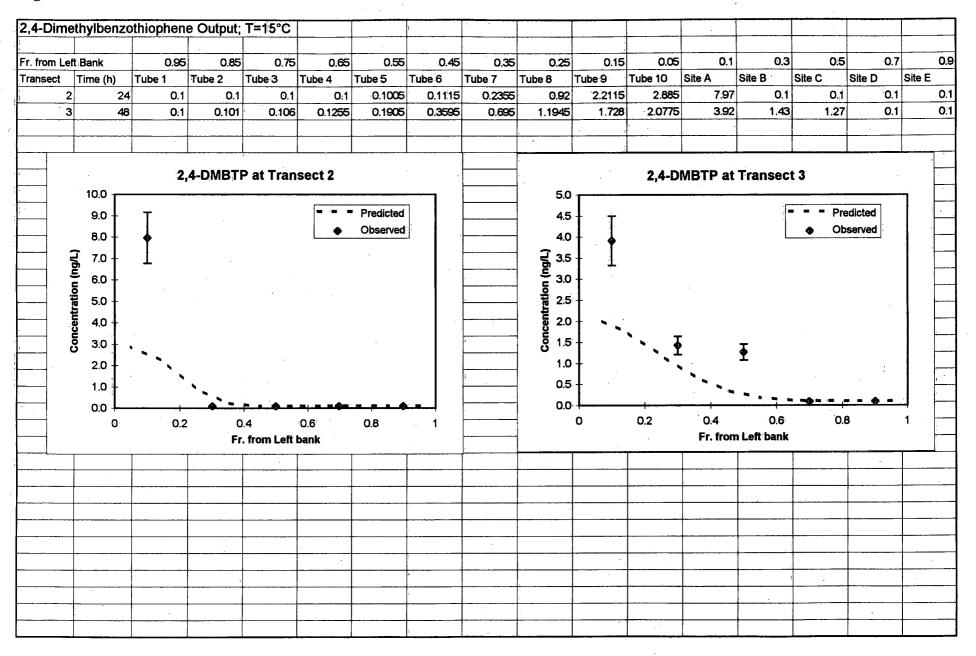


Figure 13

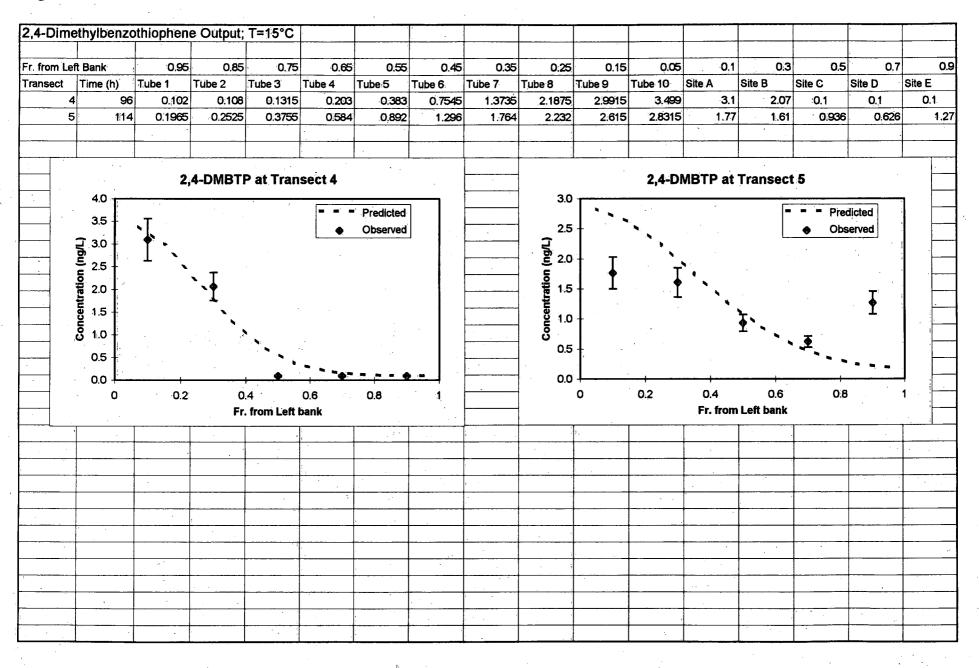


Figure 14

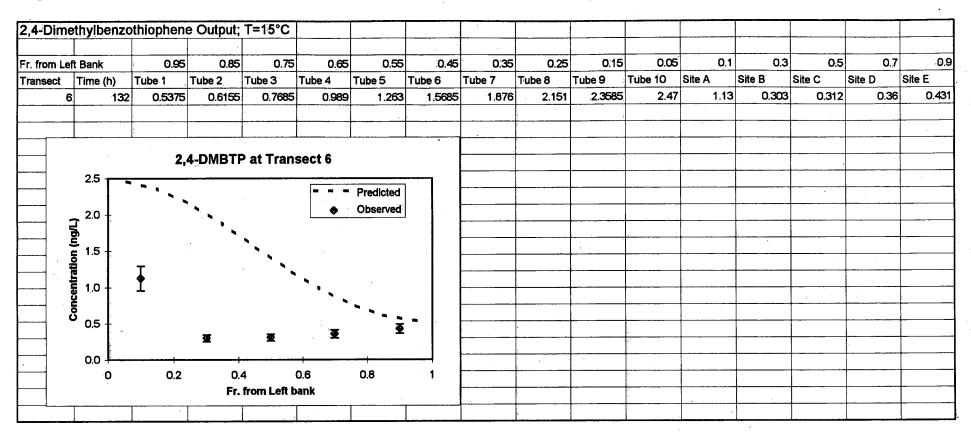


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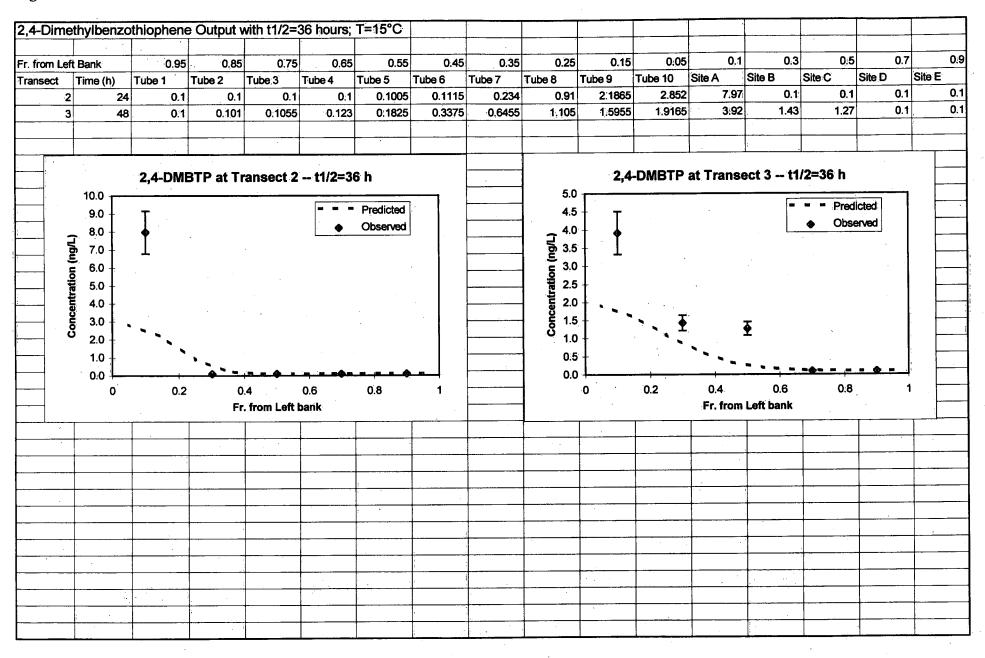


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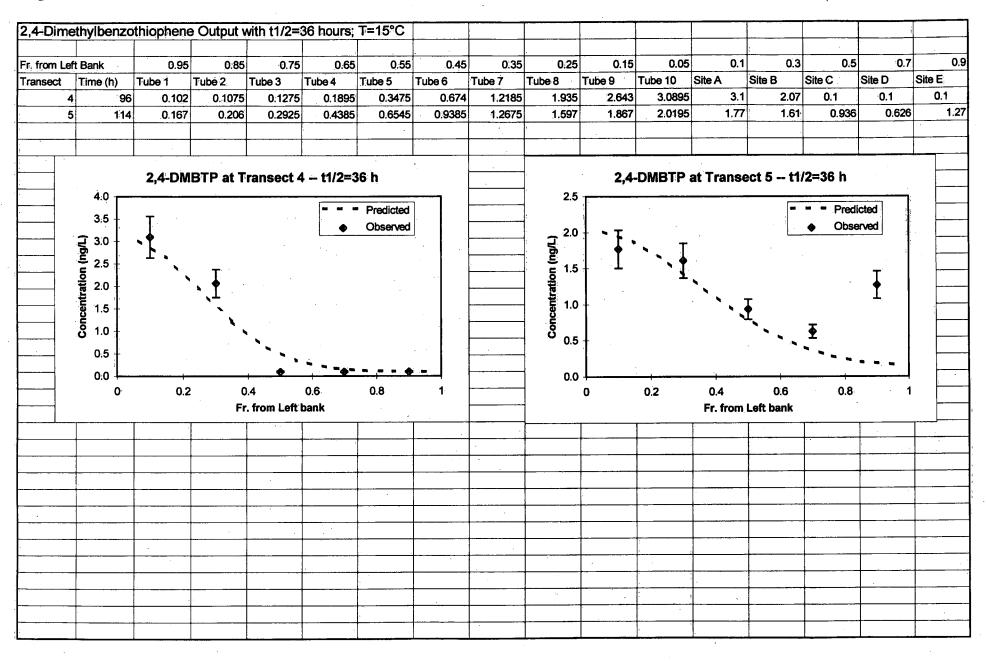
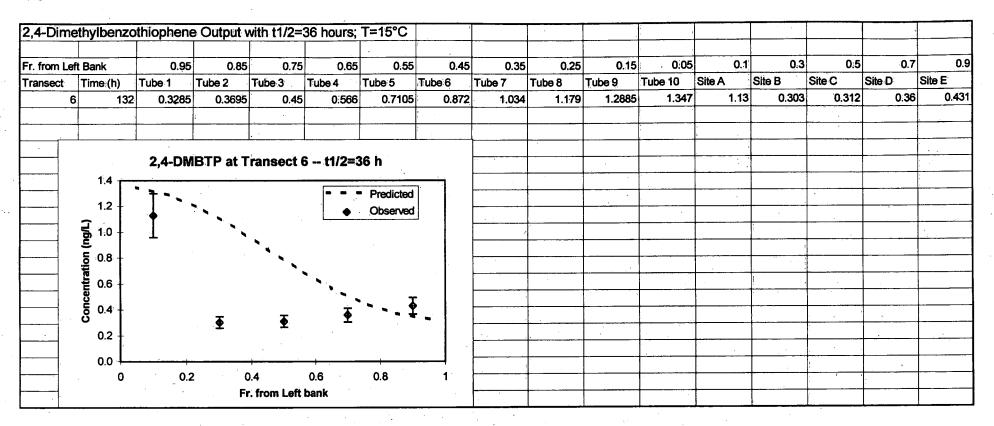


Figure 17



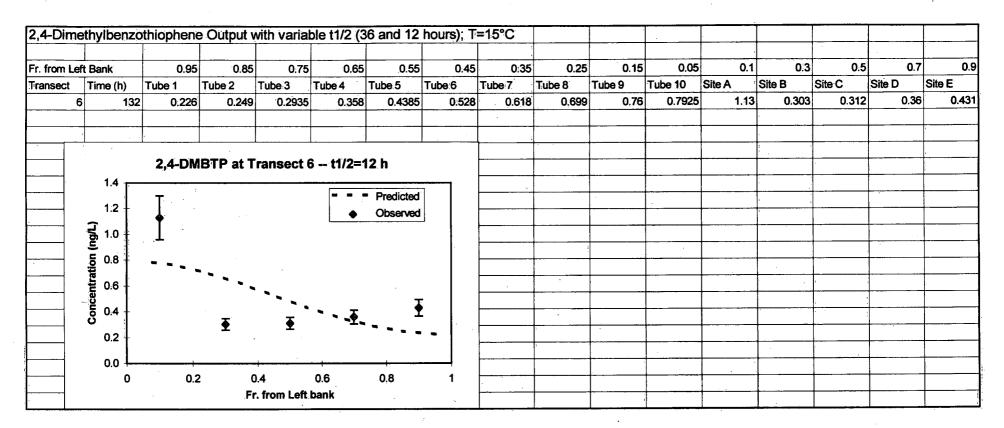


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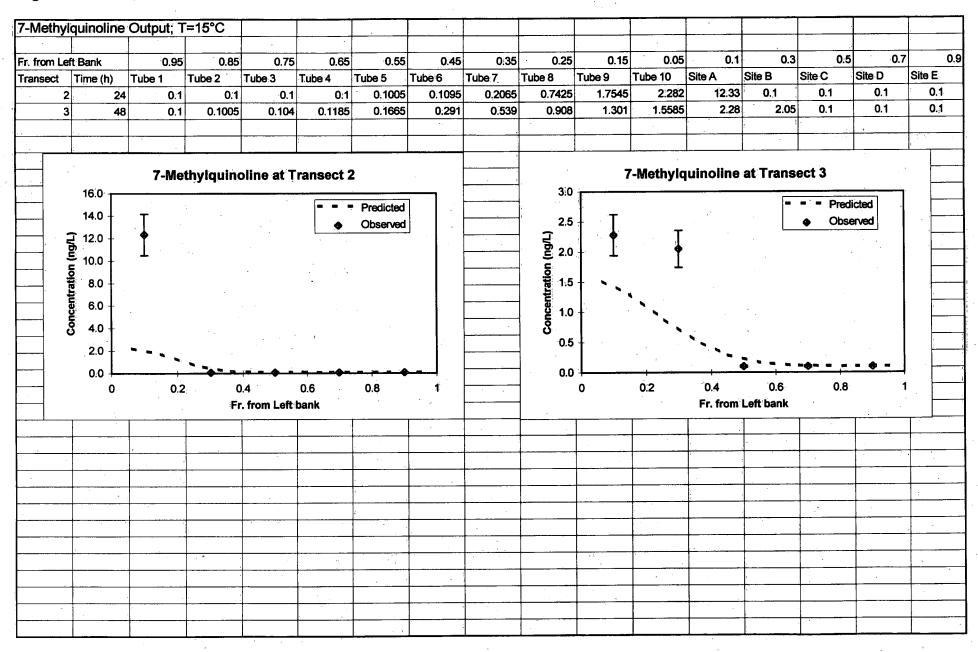


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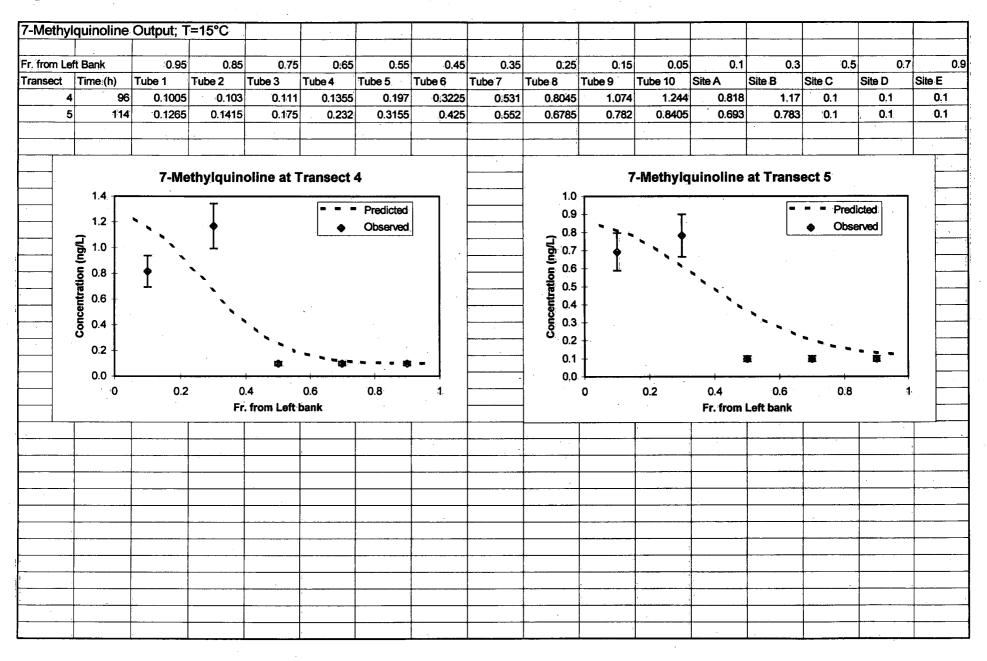


Figure 21

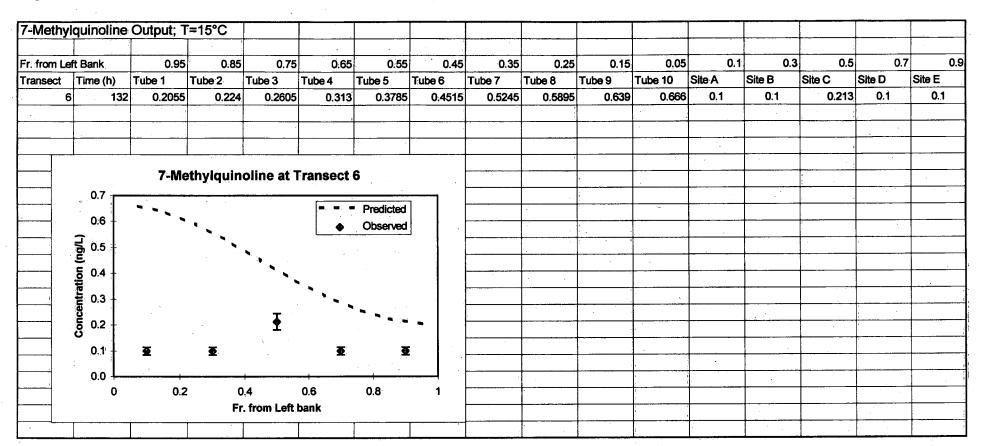
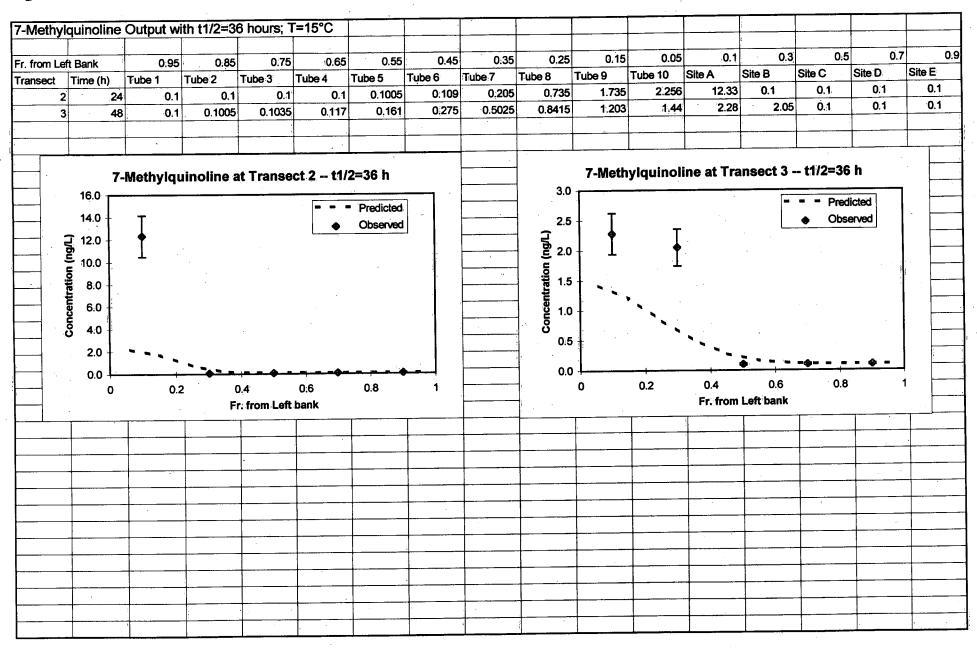


Figure 22



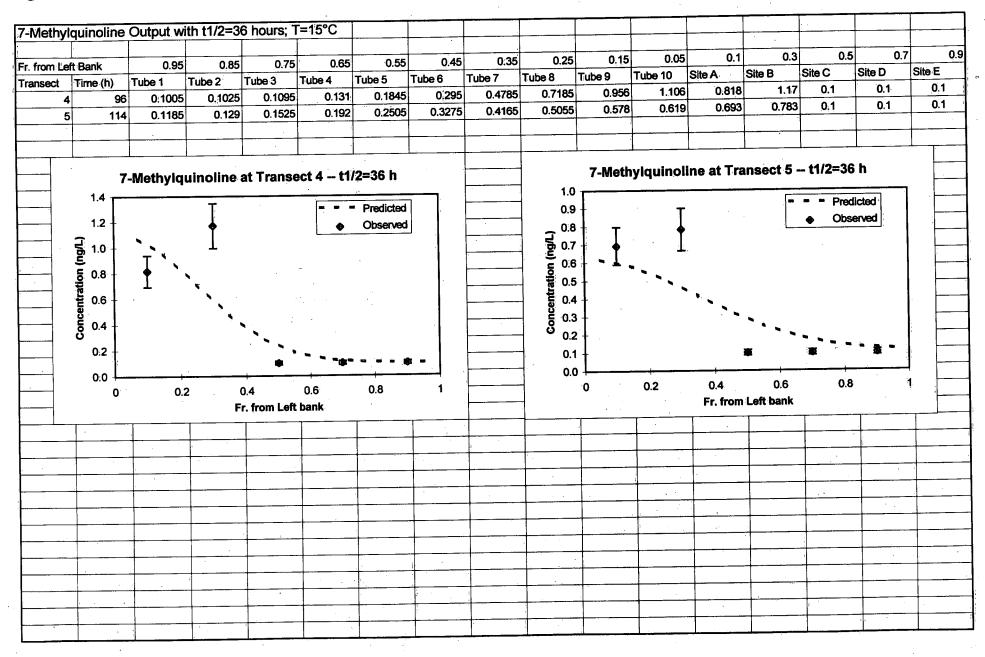


Figure 24

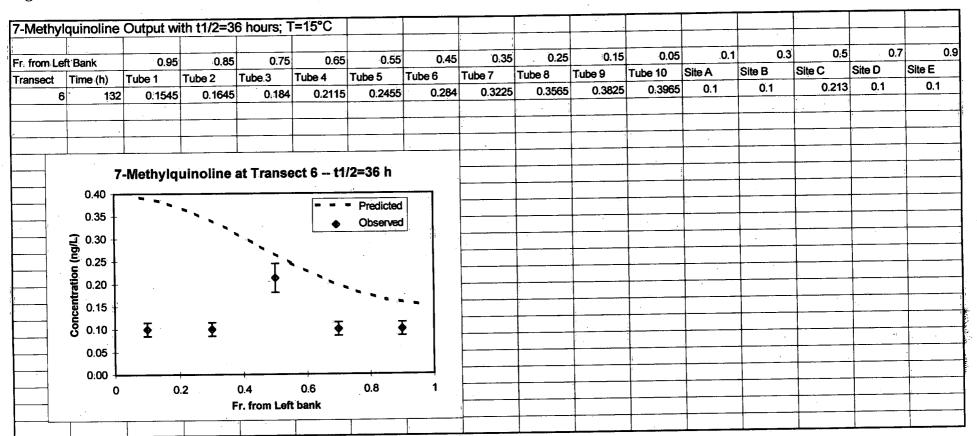


Figure 25

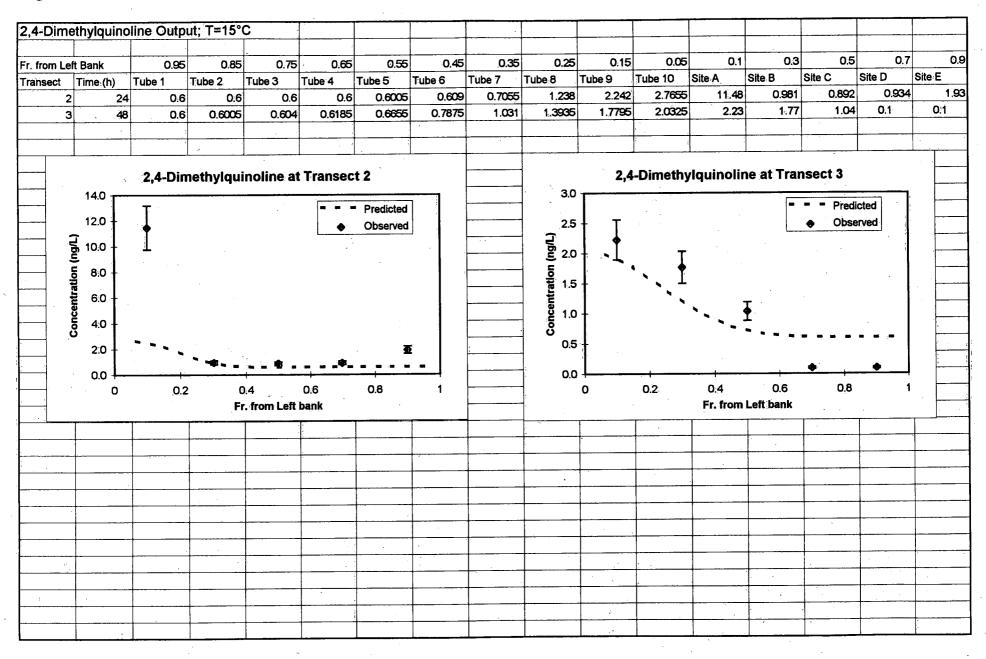


Figure 26

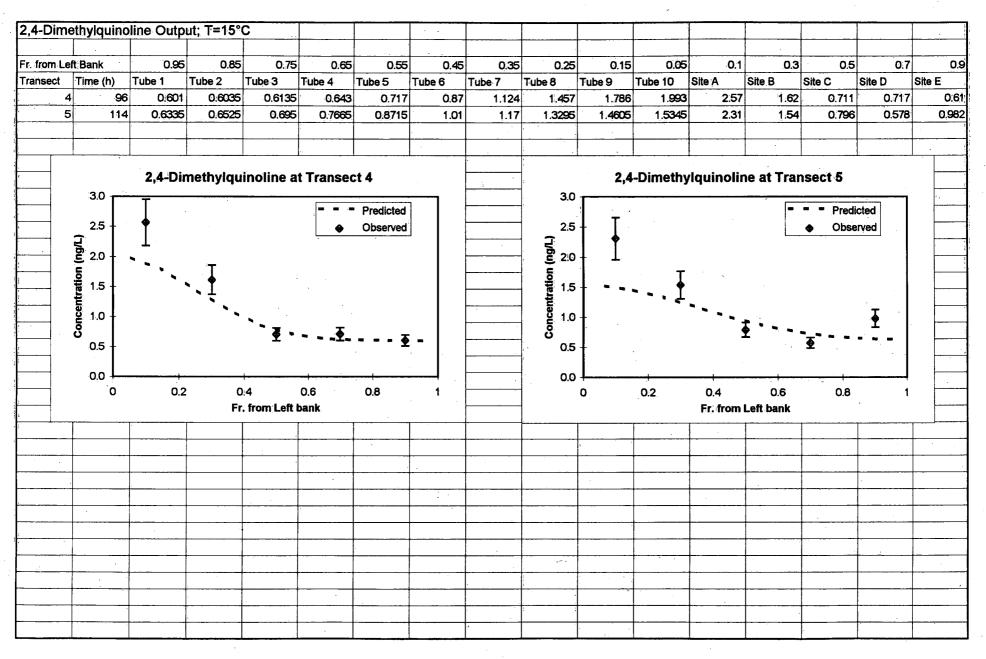


Figure 27

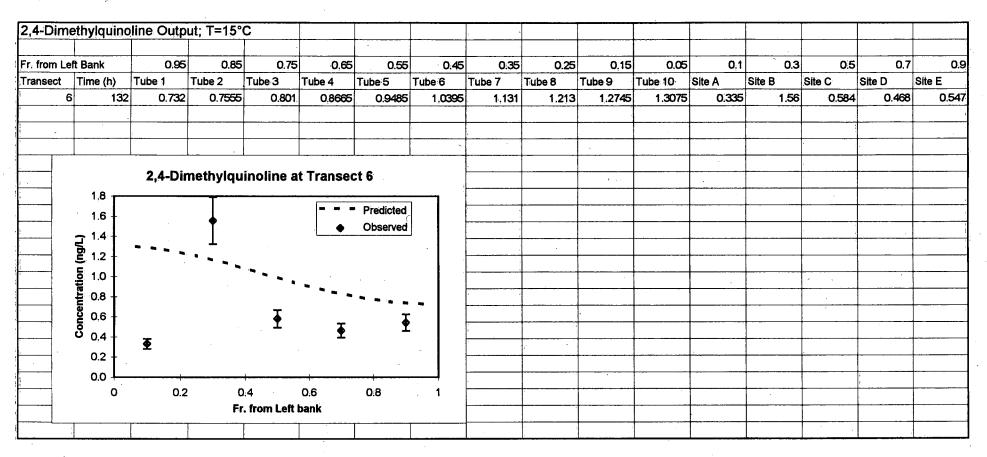


Figure 28

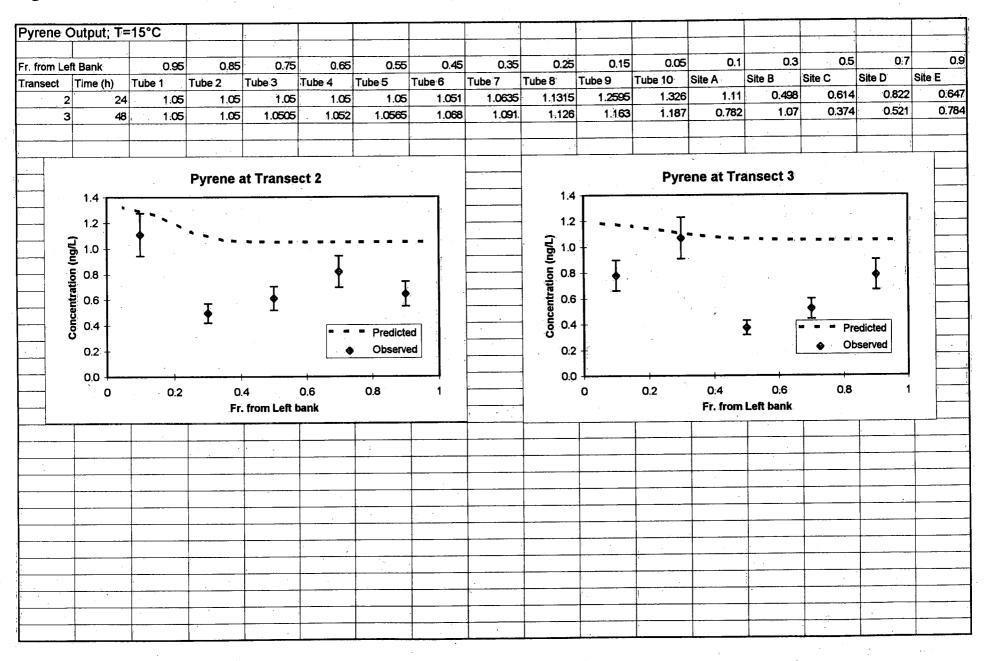


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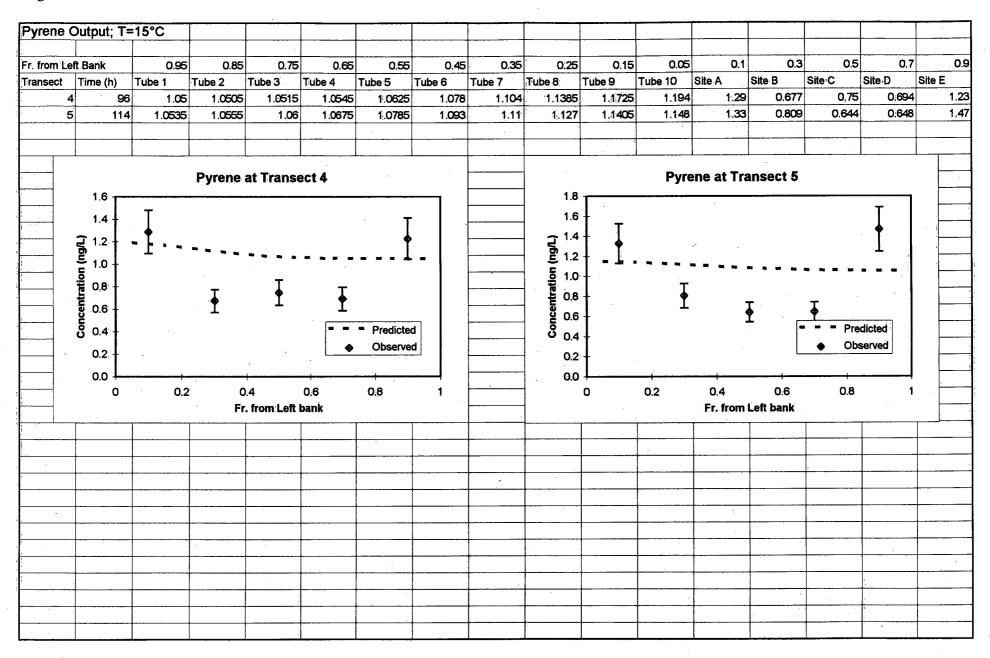
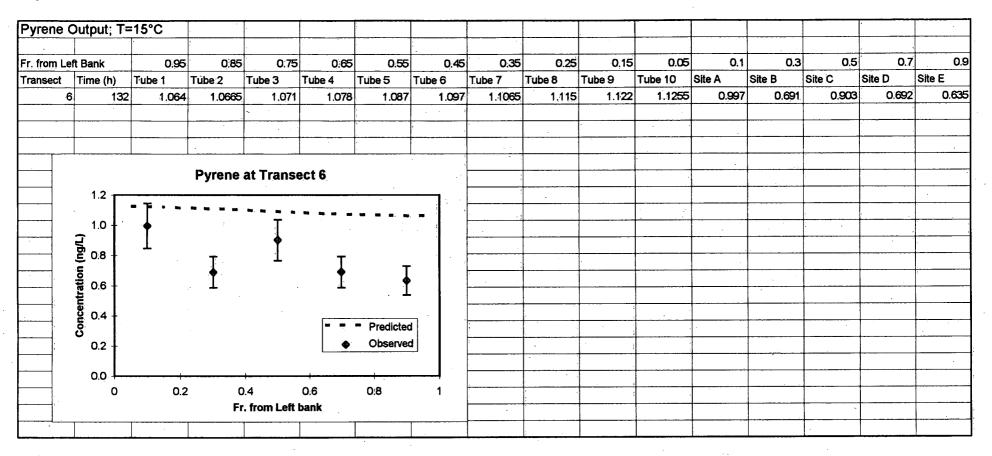


Figure 30



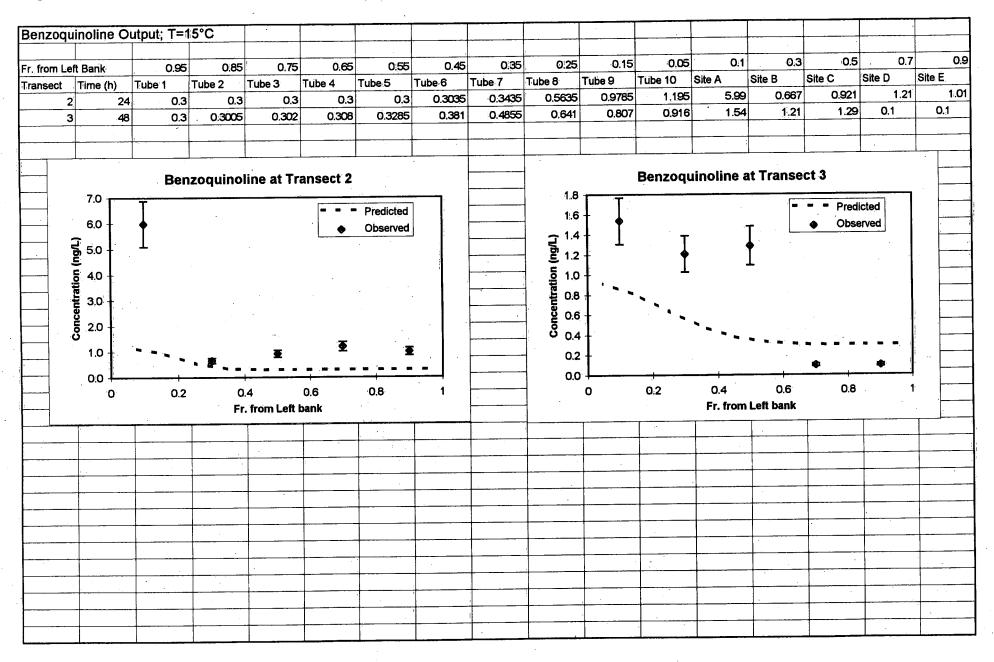


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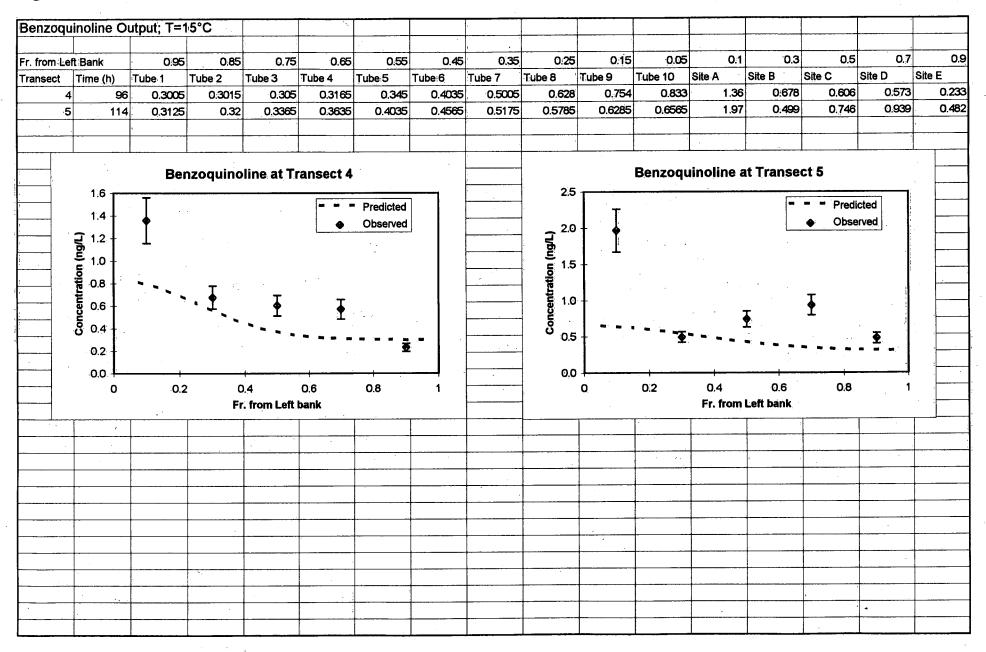
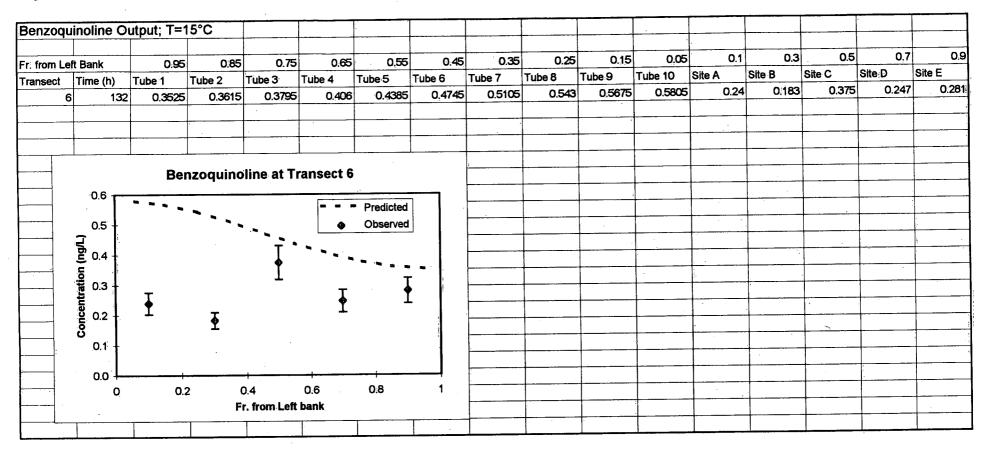
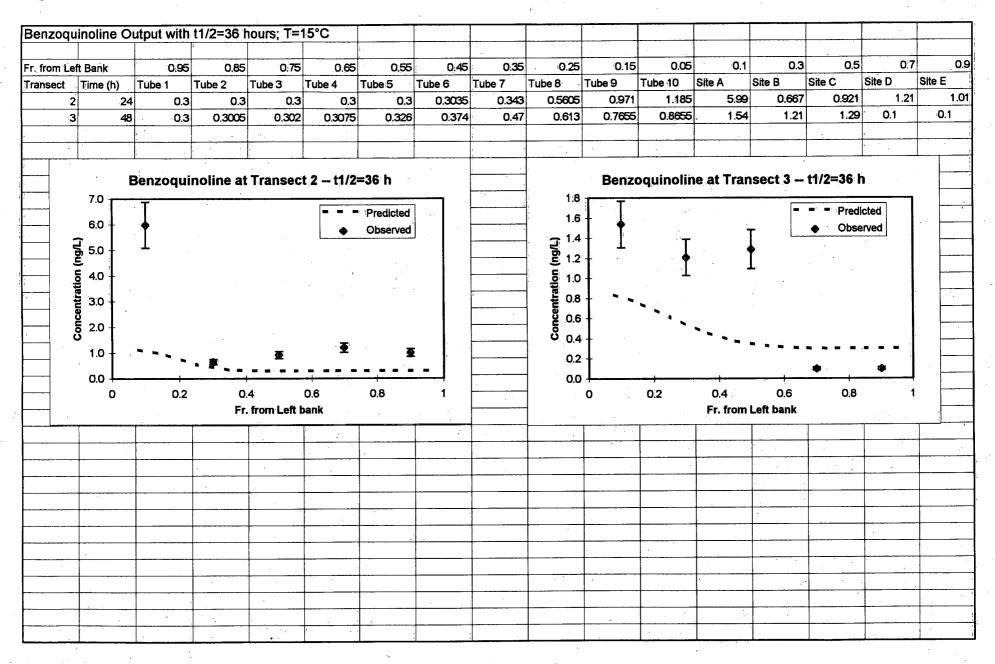


Figure 33





There is the

Figure 35

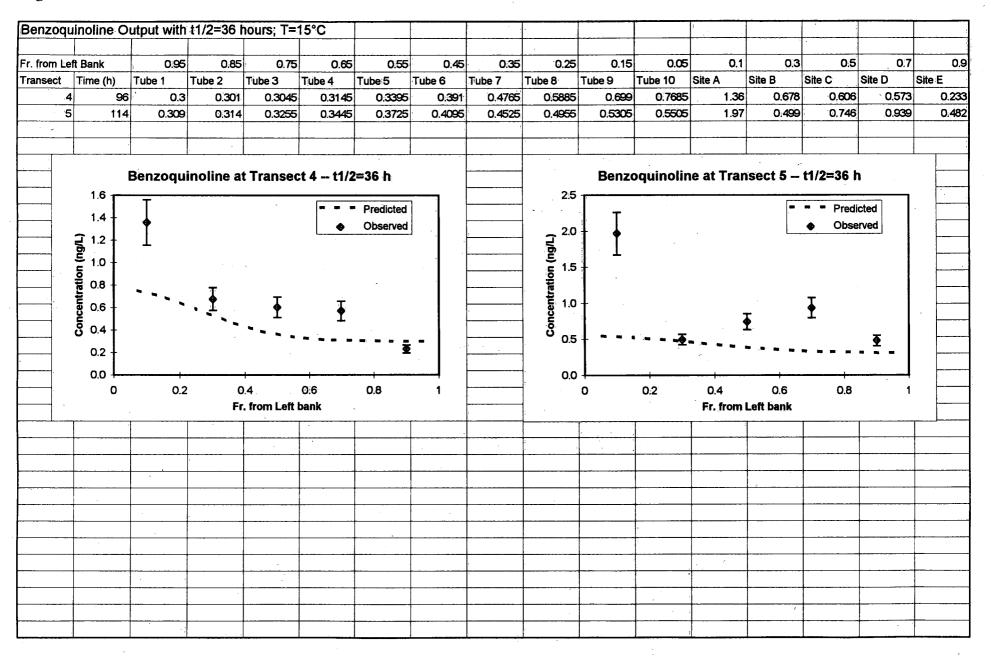
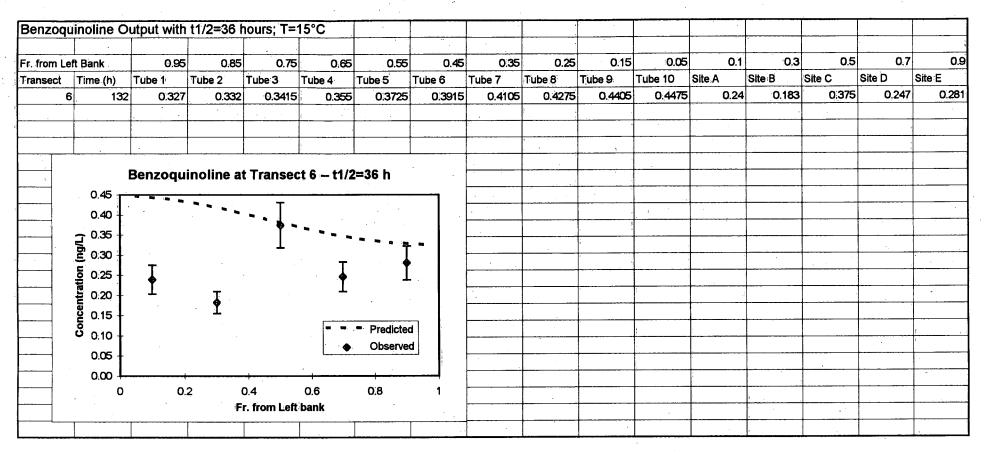


Figure 36



APPENDIX A

May 1993 Athabasca River Sampling Data

Filename "ARMAY93" Created M	aicii 20, 19:	30					
Organic compound concentration	s for Sunco	Wastewate	er and the A	thabasca F	River May/9	3	
Compound Name		Concentrat	ion in Sunc	or Wastewa	eter (ng/L)		
Compound Name	25-May	26-May	27-May	28-May	29-May	30-May	31-May
	25-Way	20-iviay	Zielviay	20-iviay	20-iviay	JO-IVIAY	O I - IVIA
7-Methylquinoline	863	694	815	918	596	611	659
2,4-Dimethylquinoline	833	692	799	1007	761	725	775
Trimethylquinoline Isomer (1st)	391	292	336	445	337	326	360
Trimethylquinoline Isomer (2nd)	246	196	225	300	234	219	249
Acridine	260	195	210	273	196	228	263
Benzoquinoline Isomer	295	293	344	414	282	339	490
3/4-Methylbenzothiophene	495	429	471	602	414	597	633
2,4-Dimethylbenzothiophene	855	920	1108	1873	2043	3726	4460
Naphthalene	ND	13.7	11.3	10.8	8.2	15.9	24.8
Phenanthrene	ND	4.3	3.4	6.5	4.2	7.9	8.8
Fluoranthene	ND	2.7	3.4	4.7	2.5	4.2	16.6
Pyrene	187	77	75.3	104	79.1	83	111
Discharge (m3/day)	34140	43192	33337	34120	35878	35738	35655
		Concentrat	ion (na/l\)	/s Horse D	May 22/93		
the state of the s	CH A (a)	Site B	Site C	Site D	iviay ZZ193		
	Site A (a)	Site D	Sile C	Sile D	,		
7 Mothylauinoline	ND	0.273	ND	ND			
7-Methylquinoline 2,4-Dimethylquinoline	1.84	2.34	1.52	4.07			
Trimethylquinoline Isomer (1st)	ND ND	ND	ND	ND			
Trimethylquinoline Isomer (2nd)	ND	ND	ND	ND			
Acridine	ND	ND	ND	ND		-	
Benzoquinoline Isomer	ND	ND	ND	ND			
3/4-Methylbenzothiophene	0.364	0.345	0.51	0.435			
2,4-Dimethylbenzothiophene	ND	ND	ND	ND			
Naphthalene	7.22	7.77	12.27	10.49			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
Phenanthrene	1.78		1.38	1.29			<u> </u>
Fluoranthene	0.718					· ·	*** ** * * * * * * * * * * * * * * * *
Pyrene	3.14			 			7
	,					8	
in the second		Concentrat	ion (ng/L) a	t Mile 20.8	(km 33.3) N	lay 24/93	
	Site A	Site B	Site C	Site D	Site E		
The standard of the standard o	ND	NO	MD	ND	ND		· · · · · · · · · · · · · · · · · · ·
7-Methylquinoline	ND	ND	ND 0.622	ND 0.548	ND 0.385		
2,4-Dimethylquinoline	0.666				0.385 ND		<u> </u>
Trimethylquinoline Isomer (1st)	ND	ND ND	ND ND	ND ND	ND		
Trimethylquinoline Isomer (2nd) Acridine	ND		ND	ND	ND		
	ND	ND	11.7				
Benzoquinoline Isomer	ND 0.604	0.233	0.255		ND		
3/4-Methylbenzothiophene	0.604	1.03	ND	ND ND	. ND		
2,4-Dimethylbenzothiophene	ND 27.65	ND 46.06	ND 8 04				
Naphthalene Phenanthrene	27.65		8.94				
ir nenanimene	1.48						
	O E 64	0.004	U E E 4	A 72	0.044		
Fluoranthene Pyrene	0.561 0.97	 	0.564 1.15				·

		Concentrati	on (ng/l \ a	Mile 25 /ki	n 40.2) May	26/93	
					Site E	20,00	
	Site A	Site B	Site C-U	Site D	Oile E		
	40.00	NO	ND	ND	ND		
7-Methylquinoline	12.33	ND 0.094	0.892	0.934	1.93		
2,4-Dimethylquinoline	11.48	0.981	0.692 ND	ND	ND		
Trimethylquinoline Isomer (1st)	2.99	ND	**		ND		
Trimethylquinoline Isomer (2nd)	1.3	0.268	0.161	ND	ND ND		
Acridine	2.94	ND	ND	ND 4 84			
Benzoquinoline Isomer	5.99	0.667	0.921	1.21	1.01		
3/4-Methylbenzothiophene	3.93	0.407	0.403	0.412	0.57		
2,4-Dimethylbenzothiophene	7.97	ND	ND	ND_	ND		
Naphthalene	5.51	3.54	12.2	13.67	19.1		
Phenanthrene	0.951	1.03	1.43	1.25	1.25		<i>.</i>
Fluoranthene	0.381	0.326	0.465	0.604	0.396		
Pyrene	1.11	0.498	0.614	0.822	0.647		
		Concentrat	ion (ng/L) a	t Mile 33.7	(km 53.9) M	ay 27/93	
	Site A		Site C-U	Site D	Site E		
	Outo is						
7-Methylquinoline	2.28	2.05	ND	ND.	ND	:	
	2.23		1.04	ND	ND		7
2,4-Dimethylquinoline	ND	ND	ND	ND	ND		· · · · · ·
Trimethylquinoline Isomer (1st)	ND	ND	ND	ND	ND		
Trimethylquinoline Isomer (2nd)	0.782	<u> </u>	ND	ND	ND		
Acridine	1		1.29		ND		-
Benzoquinoline Isomer	1.54		1.02		ND		
3/4-Methylbenzothiophene	1.78				ND	· ·	
2,4-Dimethylbenzothiophene	3.92		1,27				·
Naphthalene	3.79		16.94				
Phenanthrene	0.821		1.39				
Fluoranthene	0.416		0.387				
Pyrene	0.782	1.07	0.374	0.521	0.784		
		Concentrat		at Mile 37.3 (km 60.0) May 29/93		lay 29/93	
	Site A	Site B	Site C-U	Site D	Site E	·	1.2.
7-Methylquinoline	0.818	1.17		ND	ND		
2,4-Dimethylquinoline	2.57		0.711	0.717	0.61		
Trimethylquinoline Isomer (1st)	ND	ND	ND	ND	ND		
Trimethylquinoline Isomer (2nd)	ND	ND	ND	ND	ND		L
Acridine	0.418		ND	ND	ND		
Benzoquinoline Isomer	1.36	<u> </u>		0.573	0.233		
3/4-Methylbenzothiophene	1.4					····· · · · · · · · · · · · · · · · ·	
2,4-Dimethylbenzothiophene	3.1			ND	ND		
Naphthalene	21.36					· · · · · · · · · · · · · · · · · · ·	
	2.04					<u>-</u>	
Phenanthrene							
Fluoranthene	0.744						
Pyrene	1.29	0.677	0.75	U.094	1.23		
			ļ	<u> </u>			
	ļ		·				
	1	1					1

	T. 7	Concentrat	ion (ng/L) a	t Mile 56 (k	m 90.1) May	30/93	
				Site D	Site E		
	Ono.	<u> </u>	<u> </u>				200
7-Methylquinoline	0.693	0.783	ND	ND	ND		
2,4-Dimethylquinoline	2.31	1.54	0.796		0.982		
Trimethylquinoline Isomer (1st)	ND ND	ND ND	ND	ND	ND		
Trimethylquinoline Isomer (2nd)	ND ND	ND	ND	ND	ND		
	ND	ND	ND	ND	ND		
Acridine			0.746				
Benzoquinoline Isomer	1.97				0.462		
3/4-Methylbenzothiophene	1.28		0.579			-	
2,4-Dimethylbenzothiophene	1.77						
Naphthalene	30.07	9.94		n / . / /			:
Phenanthrene	1.5						· · · · · · · ·
Fluoranthene	0.756						
Pyrene	1.33	0.809	0.644	0.648	1.47		<u> </u>
						- 4 (0.0)	
				at Mile 82 (r	km 131.9) Ma	ıy 31/93	
	Site A		Site C	Site D-U	Site E		
							<u> </u>
7-Methylquinoline	ND	ND	0.213		ND		
2,4-Dimethylquinoline	0.335	1.56	0.584				
Trimethylquinoline Isomer (1st)	ND	ND	ND	ND	ND		
Trimethylquinoline Isomer (2nd)	ND	ND	ND	ND	ND		
Acridine	ND	ND	ND	ND	ND	, 1	
Benzoquinoline Isomer	0.24						
3/4-Methylbenzothiophene	0.576						*
2,4-Dimethylbenzothiophene	1.13		1				
	7.23						
Naphthalene	0.958				 		
Phenanthrene			4				
Fluoranthene	0.398						
Pyrene	0.997	0.691	0.500	Ú.UJZ	0.000		
		1			+		
Compound	Ret. Time		Quant.				
	minutes	lon m/z	Std. (b)		 		<u> </u>
		146	<u> </u>	<u> </u>	· · · · · · · · · · · · · · · · · · ·		<u> </u>
7-Methylquinoline	16.15						
2,4-Dimethylquinoline	19.35						-
Trimethylquinoline Isomer (1st)	23.56						
Trimethylquinoline Isomer (2nd)							
Acridine	32.58		·	,	1		
Benzoquinoline Isomer (c)	33.36						ļ
3/4-Methylbenzothiophene (d)	14.41				1		
2,4-Dimethylbenzothiophene	18.33						
Naphthalene	10.12						·
Phenanthrene	31.86	178		1			
Fluoranthene	40.91		2 Y				
Pyrene	42.48			†			
i yiong	+	<u>'</u>	1	 	1.		T
Footnotes:		+			1.	7	
produtotes.	l .						

a. Site A=left bank; Site C= centre; Site E=right bank of river. U=upper sample of an upper/lower depth pair.

b. Where standard was not available for quantitation, response for parent compound or isomer was used.
c. Formerly assigned as phenanthridine on the basis of mass spectral library match.

d. 3- and 4-Isomers have nearly identical retention times. Quantitation uncertain due to interfering peak.



DATE DUE REMINDER

1 : AUG 2003

Please do not remove this date due slip.



National Water Research Institute Environment Canada Canada Centre for Inland Waters

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