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REPORT ON THE SECOND PHASE OF THE  
SEISMIC PROGRAM ACROSS THE SUPERIOR-CHURCHILL  
BOUNDARY ZONE IN SOUTHERN CANADA

Z. Hajnal,  
58 pp. including 20 illustrations

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Cooperative Near Vertical Incident Reflection  
and Refraction Seismic Surveys Across  
the Superior-Churchill Boundary Zone  
in Southern Canada

Location, Outline of Objectives, Field Procedures,  
Field Parameters  
Tape Formats and Preliminary Computer Results

DSS Contract No: OSU79-00033


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## CONTENTS

|   | Page |
|---|------|
| INTRODUCTION .....                            | 1    |
| OUTLINE OF OBJECTIVES .....                   | 2    |
| 1979 REFRACTION SURVEY .....                  | 3    |
| a) Survey Lines .....                         | 3    |
| b) Shot Receiver Location .....               | 4    |
| c) Shot Point Information .....               | 19   |
| d) Field Procedures, Instrumentation .....    | 19   |
| e) Refraction Data, Tape Format .....         | 26   |
| 1979 REFLECTION SURVEY .....                  | 30   |
| a) Survey Line .....                          | 30   |
| b) Field Parameters .....                     | 30   |
| 1) Seismic line .....                         | 30   |
| 2) Shot point .....                           | 31   |
| c) Drilling .....                             | 31   |
| d) Instrumentation, Shooting Procedures ..... | 36   |
| e) Corrections .....                          | 36   |
| 1) Static corrections .....                   | 36   |
| 2) Normal moveout correction .....            | 40   |
| f) Data Tape Format .....                     | 40   |
| MISCELLANEOUS .....                           | 42   |
| a) Personnel .....                            | 42   |
| 1) Refraction survey .....                    | 42   |
| 2) Reflection survey .....                    | 42   |
| b) Permits .....                              | 42   |
| c) Clean up .....                             | 42   |
| d) Timing .....                               | 43   |
| e) Weather .....                              | 43   |
| PRELIMINARY RESULTS .....                     | 44   |
| I. Refraction lines .....                     | 44   |
| a) Travel time interpretation .....           | 44   |
| b) North-south models .....                   | 45   |
| c) East-west models .....                     | 49   |
| REFERENCES .....                              | 58   |

## TABLES

| TABLE |   | PAGE  |
|-------|---|---|
| 1     | Line-A Receiver and Shot Locations        | 5   |
| 2     | Line-A Shot-Receiver Distances            | 8   |
| 3     | Line-B Receiver and Shot Locations        | 10  |
| 4     | Line-B Shot-Receiver Distances            | 13  |
| 5     | Line-C Receiver and Shot Location         | 15  |
| 6     | Line-C Shot-Receiver Distances            | 18  |
| 7     | 1979 - Shot Times                         | 20  |
| 8     | Instrumentation Setup                     | 27  |
| 9     | Refraction Data, Digital Tape Format      | 29  |
| 10    | Observers Notes                           | Back pocket  |
| 11    | Reflection Profile Station Elevations     | 32  |
| 12    | Elevation and Weathering Corrections      | 37  |
| 13    | Reflection Data, Digital Tape Format      | 41  |
| 14    | Refraction Velocities and Intercept Times | 46  |

# FIGURES

| FIGURE |   | PAGE          |
|--------|---|---------------|
| 1      | 1979-1977 All <u>Seismic Lines Location Map</u> | Back Pocket ( |
| 2      | Line-A Location Map                             | Back Pocket   |
| 3      | Line-B Location Map                             | Back Pocket ) |
| 4      | Line-C Location Map                             | Back Pocket   |
| 5      | Shot Points 9 and 13                            | 21            |
| 6      | Shot Points 11 and 12                           | 22            |
| 7      | Shot Points 14 and 17                           | 23            |
| 8      | Shot Points 16 and 18                           | 24            |
| 9      | Shot Points 19 and 20                           | 25            |
| 10     | Reflection Line Location Map                    | Back Pocket   |
| 11     | CDP Coverage                                    | Back Pocket   |
| 12     | Line-A, NS, Vertical Component Section          | 53            |
| 13     | Line-A, SN, Vertical Component Section          | 54            |
| 14     | Line-B, NS, Vertical Component Section          | 55            |
| 15     | Line B, SN, Vertical Component Section          | 56            |
| 16     | Line C, EW, Vertical Component Section          | 57            |
| 17     | North-South Crustal Models                      | Back Pocket   |
| 18     | East-West Crustal Model                         | Back Pocket   |
| 19     | Uninterpreted Reflection Profile                | Back Pocket   |
| 20     | Interpreted Reflection Profile                  | Back Pocket   |

## INTRODUCTION

En août 1979, le groupe CO-CRUST\* a poursuivi l'exécution de son programme coopératif de sondages sismiques dans le sud du Manitoba et de la Saskatchewan. La première étape des travaux a commencé en juillet 1977, et ses résultats ont été divulgués par Green et Stephenson (1978) et par Green et ass. (1980). Cette étude avait pour objectif de découvrir la nature de la zone limitrophe située entre les provinces tectoniques Churchill et Supérieur du Bouclier canadien. Green et Stephenson (1978) ont décrit les caractéristiques géologiques de surface de la zone de transition, ainsi que les anomalies géophysiques connexes.

Le présent rapport contient une brève description des objectifs, l'emplacement géographique de la partie visée par l'étude en 1979, les méthodes de travail utilisées sur le terrain, les paramètres du terrain, le format des rubans porteurs des données numériques, et un court résumé de l'interprétation préliminaire.

\* Consortium for Crustal Reconnaissance Using Seismic Techniques  
(Groupe de sondage sismique de la croûte terrestre)

## INTRODUCTION

In August 1979 the CO-CRUST\* group continued its cooperative seismic survey program in the southern part of Manitoba and Saskatchewan. The first phase of the project was undertaken in July 1977 and its findings were reported by Green and Stephenson (1978) and Green et al. (1980). The rationale of the study was to obtain information about the nature of the boundary zone between the Churchill and Superior Tectonic Provinces of the Canadian Shield. The surface geological characteristics of the transition zone and the associated geophysical anomalies were described by Green and Stephenson (1978).

This report includes a brief outline of the objectives, the geographic setting of the 1979 portion of the survey, field procedures, field parameters, digital data tape formats, and a short summary of the preliminary interpretation.

\* Consortium for Crustal Reconnaissance Using Seismic Techniques.

## OUTLINE OF OBJECTIVES

The Nelson Front or Churchill Superior Boundary zone is located in the Canadian Shield, extending south southwest for about 1600 km from the west coast of Hudson Bay. Green and Stephenson (1978) prepared a detailed description of the associated geologic features as well as the magnetic and gravity anomalies. A systematic presentation was provided of the economic and scientific significance of the boundary zone and the subsequent parts of the Churchill and Superior provinces. Green et al. (1979), compiling recent magnetic and gravity information, extended the boundary zone southwards to the Canada-U.S.A. border.

The continental dimensions of the Nelson Front, its association with significant mineral deposits and its location between two major tectonic regions of the Canadian Shield make it an excellent target area for a comprehensive crustal seismic investigation. The decision to locate the survey in the southern segment of the boundary zone was based on several factors. All of these were described by Green and Stephenson (1978).



1979 REFRACTION SURVEYa) Survey Lines

Three refraction lines A, B, and C (Figure 1) were completed in this phase of the program. Line A (Figure 2) was located in a north-south direction in the vicinity of Manitoba Highway 83 along approximate longitude of  $101^{\circ} 02'W$ . Its position between stations 19 to 34 is along the projected Superior Boundary (Green et al. 1979). From site 18 to 1 the line segment is in the boundary zone (Figure 1).

Line B (Figure 1 and 3) was also in a north-south direction but located along Highway 35 in Saskatchewan. Its longitudinal position is approximately  $103^{\circ}45'W$ . According to the present understanding of the regional geology it was positioned well within the eastern portion of the Churchill Province.

Both lines A and B were reversed. Line C (Figure 1 and 4) which starts near Carlyle, Saskatchewan, extends east-west along Highway 13 as far as Assiniboia at its western end. This line was not reversed. It was shot only from its western end. This profile is an extension of the 1977 east-west line into the Churchill Province. The line is along latitude  $49^{\circ}40'$ , and between longitudes  $102^{\circ}$  and  $106^{\circ}W$ . All recording sites were selected along roads such that any lines do not deviate from straight lines more than  $\pm 2$  km (Figures 2, 3, and 4). The average separation between recording stations is 8 km.

101 4940  
106

b) Shot and Receiver Locations

The latitude, longitude, and elevation of all recording sites and shot locations were taken from 1:50,000 topographic maps. The accuracy of the provided coordinates is in the range of  $\pm 0.0005^{\circ}$ .

The elevations have an estimated error of  $\pm 4.00$  m.

All the necessary information is tabulated in the following tables:

Table-1

Line-A, latitude, longitude, and elevation of shot and receiver locations.

Table-2

Line-A, distances between shot and receiver sites.

Table-3

Line-B, latitude, longitude, and elevation of shot and receiver locations.

Table-4

Line-B, distances between shot and receiver sites.

Table-5

Line-C, latitude, longitude, and elevation of shot and receiver locations.

Table-6

Line-C, distances between shot and receiver sites.

TABLE 1  
REFRACTION RECEIVER LOCATIONS - LINE A

## GAINSBOROUGH-ROBLIN

| STATION | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------|----------------------------------|-----------------------------------|-----------|--------|
|         |                                  |                                   | feet      | meters |
| 1       | 49.0289 <sup>o</sup>             | 101.1031 <sup>o</sup>             | 1480      | 451    |
| 2       | 49.0869                          | 101.1041                          | 1495      | 456    |
| 3       | 49.1557                          | 101.0885                          | 1487      | 453    |
| 4       | 49.2254                          | 101.0923                          | 1487      | 453    |
| 5       | 49.2908                          | 101.1035                          | 1500      | 457    |
| 6       | 49.3530                          | 101.1020                          | 1500      | 463    |
| 7       | 49.4289                          | 101.1184                          | 1520      | 463    |
| 8       | 49.5027                          | 101.1097                          | 1535      | 468    |
| 8A      | 49.5263                          | 101.1040                          | 1537      | 468    |
| 9       | 49.5751                          | 101.1048                          | 1520      | 463    |
| 10      | 49.6475                          | 101.1097                          | 1515      | 462    |
| 11      | 49.7394                          | 101.1097                          | 1550      | 473    |
| 12      | 49.8128                          | 101.1099                          | 1580      | 482    |
| 13      | 49.8716                          | 101.0987                          | 1605      | 489    |
| 14      | 49.9460                          | 101.1031                          | 1600      | 488    |
| 15      | 50.0193                          | 101.1030                          | 1570      | 479    |
| 16      | 50.0932                          | 101.1143                          | 1540      | 469    |
| 17      | 50.1643                          | 101.1254                          | 1525      | 465    |
| 18      | 50.2408                          | 101.1000                          | 1525      | 465    |

| STATION | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------|----------------------------------|-----------------------------------|-----------|--------|
|         |                                  |                                   | feet      | meters |
| 19      | 50.3143 <sup>o</sup>             | 101.1060 <sup>o</sup>             | 1570      | 479    |
| 20      | 50.3580                          | 101.1070                          | 1650      | 503    |
| 21      | 50.4470                          | 101.1202                          | 1715      | 523    |
| 22      | 50.5059                          | 101.1070                          | 1760      | 536    |
| 23      | 50.5500                          | 101.1540                          | 1780      | 542    |
| 23A     | 50.5888                          | 101.0903                          | 1810      | 551    |
| 24      | 50.6365                          | 101.1822                          | 1825      | 556    |
| 24A     | 50.6833                          | 101.1557                          | 1825      | 556    |
| 25      | 50.7383                          | 101.1535                          | 1862      | 567    |
| 26      | 50.8009                          | 101.1830                          | 1880      | 573    |
| 27      | 50.8860                          | 101.1830                          | 1980      | 604    |
| 28      | 50.9629                          | 101.1712                          | 2005      | 611    |
| 29      | 51.0369                          | 101.1849                          | 1900      | 579    |
| 30      | 51.1134                          | 101.1756                          | 1975      | 602    |
| 31      | 51.1695                          | 101.1805                          | 1915      | 584    |
| 32      | 51.2280                          | 101.1761                          | 1850      | 564    |
| 33      | 51.2546                          | 101.1719                          | 1800      | 548    |
| 33A     | 51.2843                          | 101.1858                          | 1950      | 594    |
| 34      | 51.3398                          | 101.1761                          | 2000      | 609    |

| STATION                   | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------------------------|----------------------------------|-----------------------------------|-----------|--------|
|                           |                                  |                                   | feet      | meters |
| NORTH END SHOT HOLE ARRAY |                                  |                                   |           |        |
| S4                        | 51.3579 <sup>o</sup>             | 101.1691 <sup>o</sup>             | 2025      | 617    |
| SOUTH END SHOT HOLE ARRAY |                                  |                                   |           |        |
| S4                        | 49.0077 <sup>o</sup>             | 101.1088 <sup>o</sup>             | 1500      | 457    |

## LINE A - SHOT HOLE ARRAY AT NORTH END

| RECEIVER<br>NUMBER | DISTANCE (KM.) | RECEIVER<br>NUMBER | DISTANCE (KM.) |
|--------------------|----------------|--------------------|----------------|
| 1.0                | 259.110        | 19.0               | 116.183        |
| 2.0                | 252.659        | 20.0               | 111.323        |
| 3.0                | 245.033        | 21.0               | 101.395        |
| 4.0                | 237.277        | 22.0               | 94.885         |
| 5.0                | 229.987        | 23.0               | 89.885         |
| 6.0                | 223.073        | 23.5               | 85.742         |
| 7.0                | 214.611        | 24.0               | 80.262         |
| 8.0                | 206.415        | 24.5               | 75.056         |
| 8.5                | 203.800        | 25.0               | 68.940         |
| 9.0                | 198.372        | 26.0               | 61.975         |
| 10.0               | 190.314        | 27.0               | 52.509         |
| 11.0               | 180.095        | 28.0               | 43.946         |
| 12.0               | 171.933        | 29.0               | 35.730         |
| 13.0               | 165.416        | 30.0               | 27.206         |
| 14.0               | 157.135        | 31.0               | 20.976         |
| 15.0               | 148.986        | 32.0               | 14.460         |
| 16.0               | 140.746        | 33.0               | 11.494         |
| 17.0               | 132.819        | 33.5               | 8.271          |
| 18.0               | 124.370        | 34.0               | 2.072          |

ALL DISTANCES CALCULATED WITH RESPECT TO SHOT HOLE AT  $51.3579^{\circ} \pm .0005^{\circ}$  LATITUDE,  $101.1691^{\circ} \pm .0005^{\circ}$  LONGITUDE, AT THE NORTH END OF THE LINE.

## LINE A - SHOT HOLE ARRAY AT SOUTH END

| RECEIVER<br>NUMBER | DISTANCE (KM.) | RECEIVER<br>NUMBER | DISTANCE (KM.) |
|--------------------|----------------|--------------------|----------------|
| 1.0                | 2.394          | 19.0               | 145.327        |
| 2.0                | 8.815          | 20.0               | 150.188        |
| 3.0                | 16.526         | 21.0               | 160.090        |
| 4.0                | 24.241         | 22.0               | 166.640        |
| 5.0                | 31.487         | 23.0               | 171.577        |
| 6.0                | 38.406         | 23.5               | 175.867        |
| 7.0                | 46.850         | 24.0               | 181.245        |
| 8.0                | 55.053         | 24.5               | 186.405        |
| 8.5                | 57.678         | 25.0               | 192.520        |
| 9.0                | 63.106         | 26.0               | 199.528        |
| 10.0               | 71.158         | 27.0               | 208.992        |
| 11.0               | 81.379         | 28.0               | 217.526        |
| 12.0               | 89.543         | 29.0               | 225.778        |
| 13.0               | 96.086         | 30.0               | 234.272        |
| 14.0               | 104.360        | 31.0               | 240.519        |
| 15.0               | 112.513        | 32.0               | 247.019        |
| 16.0               | 120.733        | 33.0               | 249.973        |
| 17.0               | 128.647        | 33.5               | 253.296        |
| 18.0               | 137.152        | 34.0               | 259.456        |

ALL DISTANCES CALCULATED WITH RESPECT TO SHOT HOLE AT  $49.0077^{\circ} \pm .0005^{\circ}$  LATITUDE,  $101.1088^{\circ} \pm .0005^{\circ}$  LONGITUDE, AT THE SOUTH END OF THE LINE

TABLE 3

## REFRACTION RECEIVER LOCATIONS - LINE B

## N-S BROMHEAD-KELLIHER REFRACTION LINE

| STATION | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------|----------------------------------|-----------------------------------|-----------|--------|
|         |                                  |                                   | feet      | meters |
| 1       | 49.0361 <sup>o</sup>             | 103.8524 <sup>o</sup>             | 2275      | 693    |
| 2       | 49.0861                          | 103.8512                          | 2250      | 686    |
| 2A      | 49.1256                          | 103.8525                          | 2100      | 640    |
| 3       | 49.1714                          | 103.8512                          | 2025      | 617    |
| 4       | 49.2562                          | 103.8500                          | 2000      | 610    |
| 5       | 49.3182                          | 103.8405                          | 1975      | 602    |
| 6       | 49.3729                          | 103.8520                          | 1975      | 602    |
| 7       | 49.4586                          | 103.8500                          | 1925      | 587    |
| 8       | 49.5204                          | 103.8349                          | 1900      | 579    |
| 9       | 49.5753                          | 103.8353                          | 1875      | 571    |
| 10      | 49.6368                          | 103.8397                          | 1875      | 571    |
| 11      | 49.6918                          | 103.8540                          | 1887      | 575    |
| 12      | 49.7534                          | 103.8500                          | 1925      | 587    |
| 13      | 49.8083                          | 103.8413                          | 1950      | 594    |
| 14      | 49.8724                          | 103.8500                          | 1950      | 594    |
| 15      | 49.9206                          | 103.8505                          | 1950      | 594    |
| 16      | 50.0179                          | 103.8421                          | 1975      | 602    |
| 17      | 50.0727                          | 103.8513                          | 1975      | 602    |
| 18      | 50.1580                          | 103.8423                          | 2020      | 616    |
| 19      | 50.1891                          | 103.8524                          | 2075      | 632    |



| STATION | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------|----------------------------------|-----------------------------------|-----------|--------|
|         |                                  |                                   | feet      | meters |
| 20      | 50.2833 <sup>o</sup>             | 103.8368 <sup>o</sup>             | 2175      | 663    |
| 21      | 50.3672                          | 103.8368                          | 2175      | 663    |
| 22      | 50.4540                          | 103.8504                          | 2200      | 670    |
| 23      | 50.5393                          | 103.8368                          | 2125      | 648    |
| 24      | 50.6251                          | 103.8425                          | 1975      | 602    |
| 24A     | 50.6712                          | 103.8530                          | 1900      | 579    |
| 25      | 50.7171                          | 103.8558                          | 1875      | 571    |
| 26      | 50.7696                          | 103.8409                          | 1875      | 571    |
| 27      | 50.8338                          | 103.8385                          | 1925      | 587    |
| 28      | 50.9193                          | 103.8500                          | 2000      | 610    |
| 29      | 51.0052                          | 103.8427                          | 2075      | 632    |
| 30      | 51.0908                          | 103.8427                          | 2150      | 655    |
| 31      | 51.1833                          | 103.8389                          | 2150      | 655    |
| 32      | 51.2688                          | 103.8429                          | 2212      | 674    |
| 32A     | 51.3080                          | 103.8567                          | 2225      | 678    |
| 33      | 51.3390                          | 103.8528                          | 2225      | 678    |
| 34      | 51.4010                          | 103.8532                          | 2250      | 686    |

| STATION                   | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------------------------|----------------------------------|-----------------------------------|-----------|--------|
|                           |                                  |                                   | feet      | meters |
| NORTH END SHOT HOLE ARRAY |                                  |                                   |           |        |
| S4                        | 51.4475°                         | 103.8542°                         | 2206      | 672.4  |
| SOUTH END SHOT HOLE ARRAY |                                  |                                   |           |        |
| S1                        | 49.0232°                         | 103.8512°                         | 2300      | 701    |

TABLE 4

## LINE B - SHOT HOLE ARRAY AT NORTH END

| RECEIVER<br>NUMBER | DISTANCE (KM.) | RECEIVER<br>NUMBER | DISTANCE (KM.) |
|--------------------|----------------|--------------------|----------------|
| 1.0                | 268.235        | 19.0               | 139.994        |
| 2.0                | 262.675        | 20.0               | 129.521        |
| 2.5                | 258.282        | 21.0               | 120.189        |
| 3.0                | 253.188        | 22.0               | 110.527        |
| 4.0                | 243.757        | 23.0               | 101.045        |
| 5.0                | 236.863        | 24.0               | 91.497         |
| 6.0                | 230.778        | 24.5               | 86.365         |
| 7.0                | 221.246        | 25.0               | 81.259         |
| 8.0                | 214.377        | 26.0               | 75.424         |
| 9.0                | 208.271        | 27.0               | 68.285         |
| 10.0               | 201.429        | 28.0               | 58.765         |
| 11.0               | 195.309        | 29.0               | 49.215         |
| 12.0               | 188.457        | 30.0               | 39.693         |
| 13.0               | 182.353        | 31.0               | 29.413         |
| 14.0               | 175.221        | 32.0               | 19.897         |
| 15.0               | 169.860        | 32.5               | 15.521         |
| 16.0               | 159.039        | 33.0               | 12.072         |
| 17.0               | 152.942        | 34.0               | 5.174          |
| 18.0               | 143.456        |                    |                |

ALL DISTANCES CALCULATED WITH RESPECT TO SHOT HOLE AT  $51.4475^{\circ} \pm .0005^{\circ}$   
 LATITUDE,  $103.8542^{\circ} \pm .0005^{\circ}$  LONGITUDE, AT THE NORTH END OF THE LINE.

## LINE B - SHOT HOLE ARRAY AT SOUTH END

| RECEIVER<br>NUMBER | DISTANCE (KM.) | RECEIVER<br>NUMBER | DISTANCE (KM.) |
|--------------------|----------------|--------------------|----------------|
| 1.0                | 1.437          | 19.0               | 129.676        |
| 2.0                | 6.995          | 20.0               | 140.158        |
| 2.5                | 11.389         | 21.0               | 149.491        |
| 3.0                | 16.482         | 22.0               | 159.143        |
| 4.0                | 25.913         | 23.0               | 168.635        |
|                    |                | 23.5               | 173.813        |
| 5.0                | 32.818         | 24.0               | 178.178        |
| 6.0                | 38.892         | 24.5               | 183.305        |
| 7.0                | 48.424         | 25.0               | 188.411        |
| 8.0                | 55.310         | 26.0               | 194.253        |
| 9.0                | 61.414         | 27.0               | 201.396        |
| 10.0               | 68.249         | 28.0               | 210.905        |
| 11.0               | 74.361         | 29.0               | 220.462        |
| 12.0               | 81.213         | 30.0               | 229.986        |
| 13.0               | 87.322         | 31.0               | 240.277        |
| 14.0               | 94.449         | 32.0               | 249.789        |
| 15.0               | 99.810         | 32.5               | 254.150        |
| 16.0               | 110.635        | 33.0               | 257.598        |
| 17.0               | 116.728        | 34.0               | 264.496        |
| 18.0               | 126.218        |                    |                |

ALL DISTANCES WITH RESPECT TO SHOT HOLE AT  $49.0232^{\circ} \pm .0005^{\circ}$   
 LATITUDE,  $103.8512^{\circ} \pm .0005^{\circ}$  LONGITUDE, AT THE SOUTH END OF THE  
 LINE.

TABLE 5  
REFRACTION RECEIVER LOCATIONS - LINE C

## CARLYLE-LIMERICK

| STATION | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------|----------------------------------|-----------------------------------|-----------|--------|
|         |                                  |                                   | feet      | meters |
| 0       | 49.6216 <sup>o</sup>             | 102.0913 <sup>o</sup>             | 2087      | 636    |
| 1       | 49.6375                          | 102.1858                          | 2050      | 625    |
| 2       | 49.6363                          | 102.3204                          | 2050      | 625    |
| 3       | 49.6351                          | 102.4333                          | 2050      | 625    |
| 4       | 49.6370                          | 102.5418                          | 2025      | 617    |
| 5       | 49.6191                          | 102.6567                          | 1975      | 602    |
| 6       | 49.6368                          | 102.7921                          | 2012      | 613    |
| 7       | 49.6370                          | 102.8851                          | 2012      | 613    |
| 8       | 49.6368                          | 102.9256                          | 2025      | 617    |
| 9       | 49.6365                          | 103.0883                          | 2000      | 610    |
| 10      | 49.6368                          | 103.2020                          | 2025      | 617    |
| 11      | 49.6363                          | 103.3098                          | 2000      | 610    |
| 12      | 49.6368                          | 103.4241                          | 2000      | 610    |
| 13      | 49.6368                          | 103.5383                          | 2000      | 610    |
| 14      | 49.6368                          | 103.6530                          | 1975      | 602    |
| 15      | 49.6368                          | 103.7676                          | 1900      | 579    |
| 16      | 49.6368                          | 103.8383                          | 1875      | 571    |
| 17      | 49.6368                          | 103.9691                          | 1900      | 579    |
| 18      | 49.6365                          | 104.1045                          | 1912      | 583    |
| 18A     | 49.6261                          | 104.1706                          | 1962      | 598    |

| STATION | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|---------|----------------------------------|-----------------------------------|-----------|--------|
|         |                                  |                                   | feet      | meters |
| 19      | 49.6246 <sup>o</sup>             | 104.2383 <sup>o</sup>             | 2012      | 613    |
| 20      | 49.6397                          | 104.3333                          | 2100      | 640    |
| 21      | 49.6248                          | 104.4206                          | 2137      | 651    |
| 22      | 49.6413                          | 104.5340                          | 2125      | 648    |
| 23      | 49.6415                          | 104.6242                          | 2200      | 670    |
| 24      | 49.6368                          | 104.7570                          | 2387      | 727    |
| 24A     | 49.6371                          | 104.805                           | 2400      | 731    |
| 25      | 49.6369                          | 104.8717                          | 2387      | 727    |
| 26      | 49.6368                          | 104.9858                          | 2325      | 709    |
| 27      | 49.6368                          | 105.1216                          | 2375      | 724    |
| 28      | 49.6368                          | 105.2550                          | 2350      | 716    |
| 29      | 49.6368                          | 105.3863                          | 2525      | 770    |
| 30      | 49.6370                          | 105.6358                          | 2312      | 705    |
| 31      | 49.6383                          | 105.7535                          | 2300      | 701    |
| 32      | 49.6383                          | 105.8677                          | 2325      | 708    |
| 33      | 49.6393                          | 105.9080                          | 2350      | 716    |
| 34      | 49.6358                          | 106.0231                          | 2475      | 754    |

| STATION                  | LATITUDE<br>(decimal of degrees) | LONGITUDE<br>(decimal of degrees) | ELEVATION |        |
|--------------------------|----------------------------------|-----------------------------------|-----------|--------|
|                          |                                  |                                   | feet      | meters |
| WEST END SHOT HOLE ARRAY |                                  |                                   |           |        |
| S4                       | 49.6373 <sup>o</sup>             | 106.0707 <sup>o</sup>             | 2450      | 746.7  |

TABLE 6

## LINE C - SHOT HOLE ARRAY AT WEST END

| RECEIVER<br>NUMBER | DISTANCE (KM.) | RECEIVER<br>NUMBER | DISTANCE (KM.) |
|--------------------|----------------|--------------------|----------------|
| 0.0                | 287.477        | 18.5               | 137.275        |
| 1.0                | 280.600        | 19.0               | 132.388        |
| 2.0                | 270.884        | 20.0               | 125.498        |
| 3.0                | 262.734        | 21.0               | 119.219        |
| 4.0                | 254.893        | 22.0               | 111.000        |
| 5.0                | 246.649        | 23.0               | 104.485        |
| 6.0                | 236.818        | 24.0               | 94.897         |
| 7.0                | 230.101        | 24.5               | 91.429         |
| 8.0                | 227.176        | 25.0               | 86.611         |
| 9.0                | 215.426        | 26.0               | 78.369         |
| 10.0               | 207.214        | 27.0               | 68.560         |
| 11.0               | 199.429        | 28.0               | 58.923         |
| 12.0               | 191.173        | 29.0               | 49.439         |
| 13.0               | 182.924        | 30.0               | 31.416         |
| 14.0               | 174.640        | 31.0               | 22.913         |
| 15.0               | 166.363        | 32.0               | 14.664         |
| 16.0               | 161.256        | 33.0               | 11.755         |
| 17.0               | 151.808        | 34.0               | 3.443          |
| 18.0               | 142.029        |                    |                |

ALL DISTANCES CALCULATED WITH RESPECT TO SHOT HOLE AT  $49.6373^{\circ} \pm .0005^{\circ}$   
LATITUDE,  $106.0707^{\circ} \pm .0005^{\circ}$  LONGITUDE, AT THE WEST END OF THE LINE.



c) Shot Point Information

All shot holes were drilled to a depth of 30.48 m. The average load per hole was 200 kg of 60% Geogel (46 cm x 13 cm sticks).

A minimum of two shots was fired at every shot point. The smaller shot was 400 kg in two holes, the larger shot was 1200 kg in six.

Table 7 provides the shot numbers, as they were referred to on the data tapes, the exact timing of the shots, and the charge sizes. Shots 10 and 15 are mis-fires, therefore, this information is not part of the regular data set. The locations of the shot point with respect to their relevant refraction line are shown in Figures 1, 2, 3, and 4.

The shot hole configurations are illustrated on Figures 5, 6, 7, 8, and 9. These diagrams also reveal the point of reference for the individual shot points.

All shots were timed to a recording of the standard WWV time code signal.

d) Field Procedures; Instrumentation

The instrumentation for the refraction survey was provided by the Earth Physics Branch of the Canada Department of Energy, Mines and Resources (EMR) and by the Department of Geophysics, University of Western Ontario (UWO). EMR fielded twelve recording systems. UWO provided seven field units plus a spare back-up unit that was also deployed for three shots.

All recording systems were pre-programmed to a set of specific recording times. The EMR stations recorded one vertical and one horizontal component. The horizontal components in most cases were

Shot Times  
Refraction Survey 1979  
CO-CRUST

| Location                                    | Shot No. | Date    | Hr. | Time M. | Sec.     | Charge size kg. |      |
|---|----------|---------|-----|---------|----------|-----------------|------|
| Line #A                                     |          |         |     |         |          |                 |      |
| Hwy #83<br>Manitoba Roblin<br>North End     | 9        | Aug. 15 | 05: | 59.97   | .01      | 400             |      |
| Hwy #83<br>South end Melita                 | 10       | Aug. 15 | 06: | 31:     | 06.183   | 0.003           | 200  |
| "   | 11       | Aug. 15 | 07: | 31:     | 04.488   | 0.003           | 1000 |
| "   | 12       | Aug. 16 | 06: | 31:     | 02.925 + | 0.003           | 425  |
| Hwy #83<br>North End Roblin                 | 13       | Aug. 17 | 06: | 00.97   | 0.1      | 1200            |      |
| Line #B                                     |          |         |     |         |          |                 |      |
| Hwy #35<br>Saskatchewan Leross<br>North End | 14       | Aug. 18 | 06: | 01.97   | 0.1      | 350             |      |
| Hwy #35<br>South End Oungre                 | 15       | Aug. 18 | 06: | 31:     | 03.145   | 0.003           | 400  |
| "   | 16       | Aug. 19 | 07: | 31:     | 02.819   | 0.003           | 983  |
| Hwy #35<br>North End Leross                 | 17       | Aug. 20 | 06: | 00.97   | 0.01     | 1249            |      |
| Hwy #35<br>South End Oungre                 | 18       | Aug. 20 | 06: | 31:     | 02.582   | 0.003           | 250  |
| Line #C                                     |          |         |     |         |          |                 |      |
| Hwy #13<br>West End Assiniboia<br>Sask.     | 19       | Aug. 21 | 06: | 01:     | 03.458   | 0.03            | 250  |
| "   | 20       | Aug. 21 | 21: | 01:     | 02.749   | 0.003           | 1375 |

# SHOT HOLE ARRAY - LINE A - SHOTS 9 AND 13

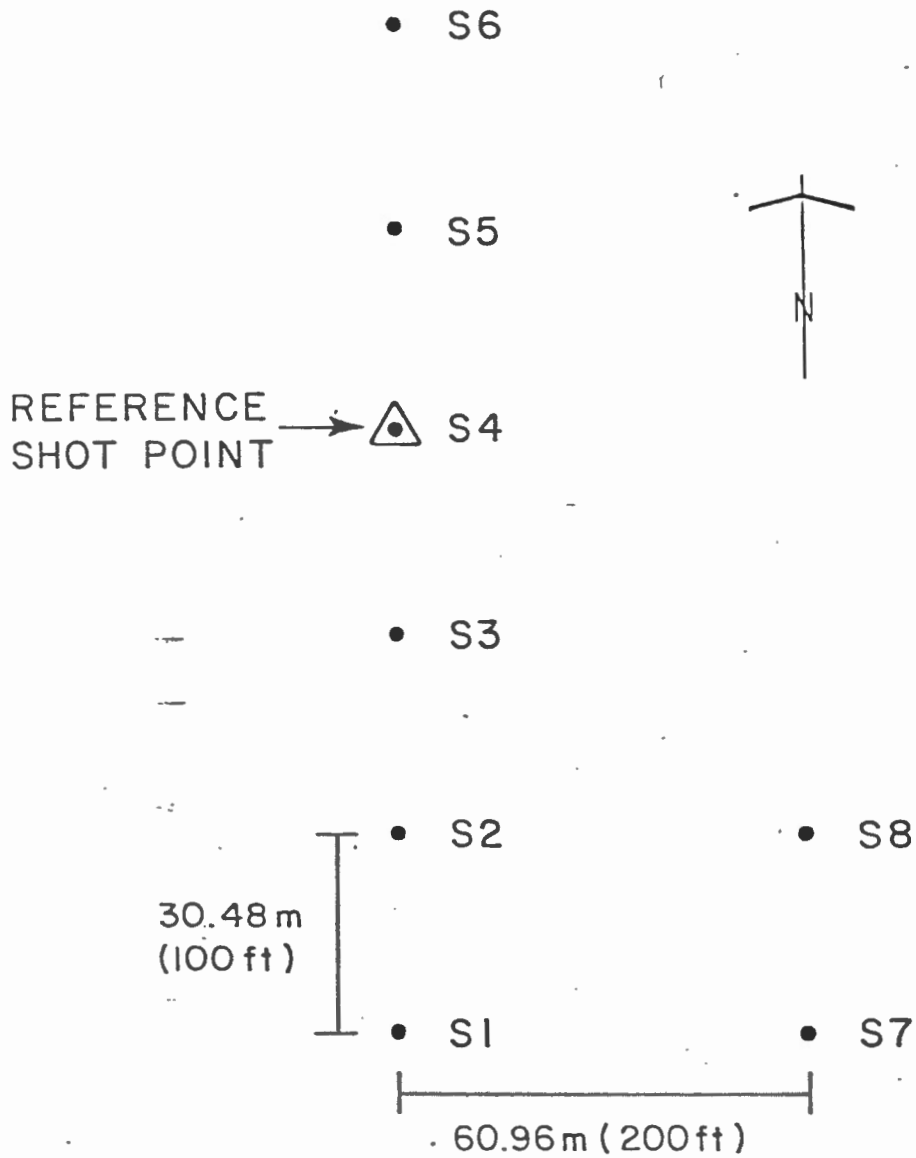


FIGURE 5

# SHOT HOLE ARRAY - LINE A - SHOTS II AND 12

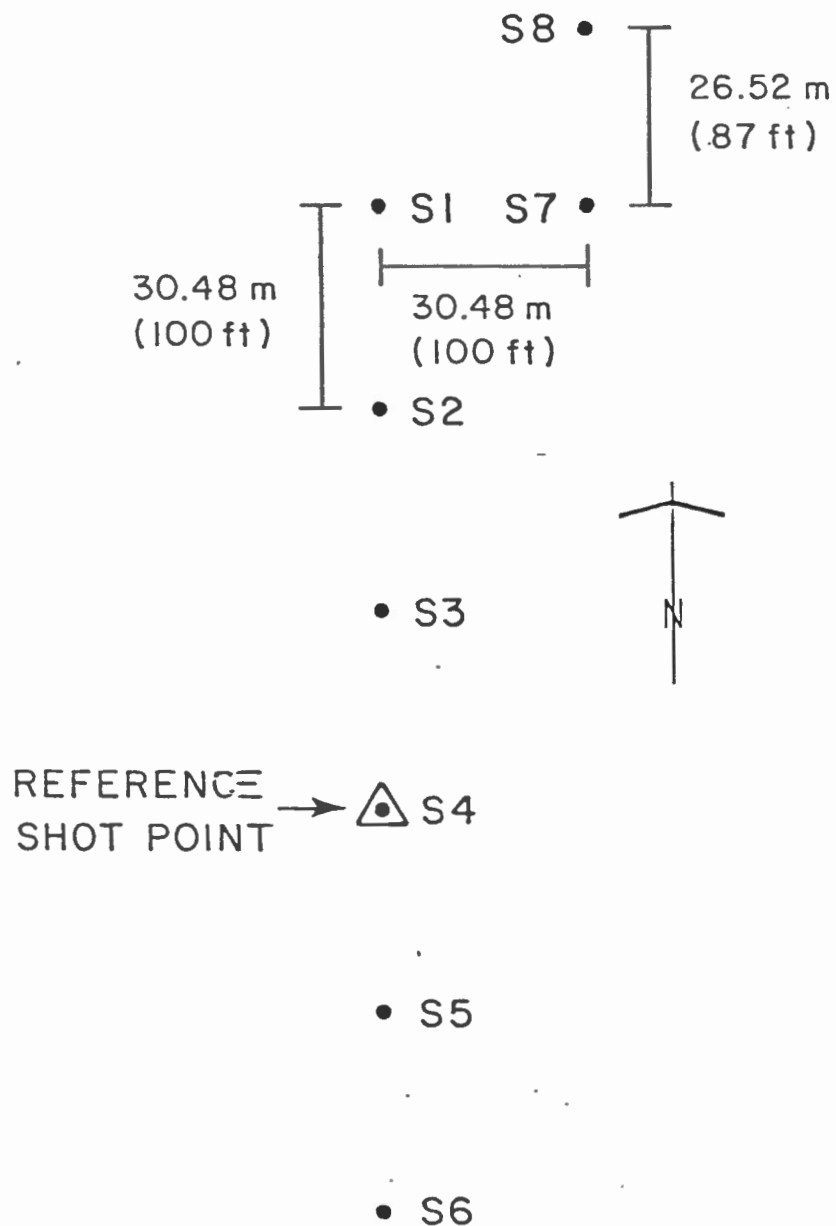


FIGURE 6

# SHOT HOLE ARRAY - LINE B - SHOTS 14 AND 17

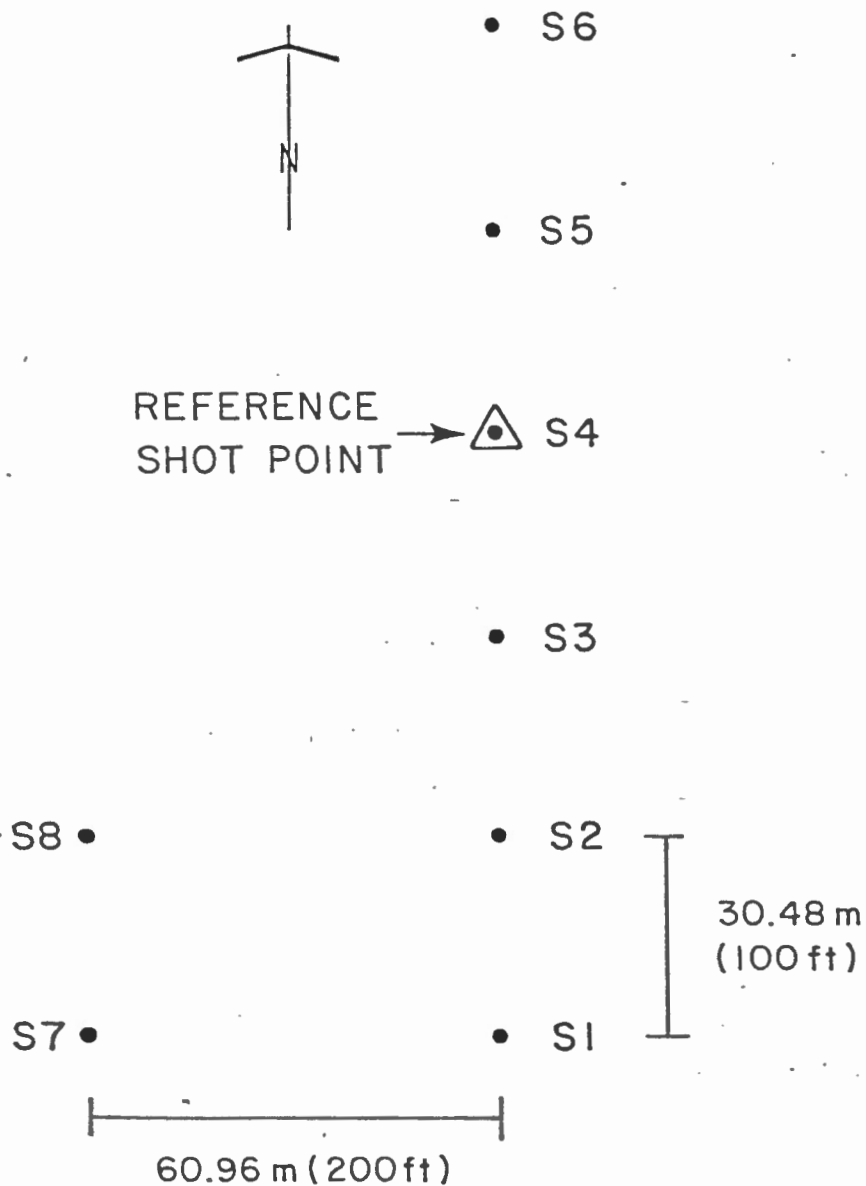


FIGURE 7

# SHOT HOLE ARRAY - LINE B - SHOTS 16 AND 18

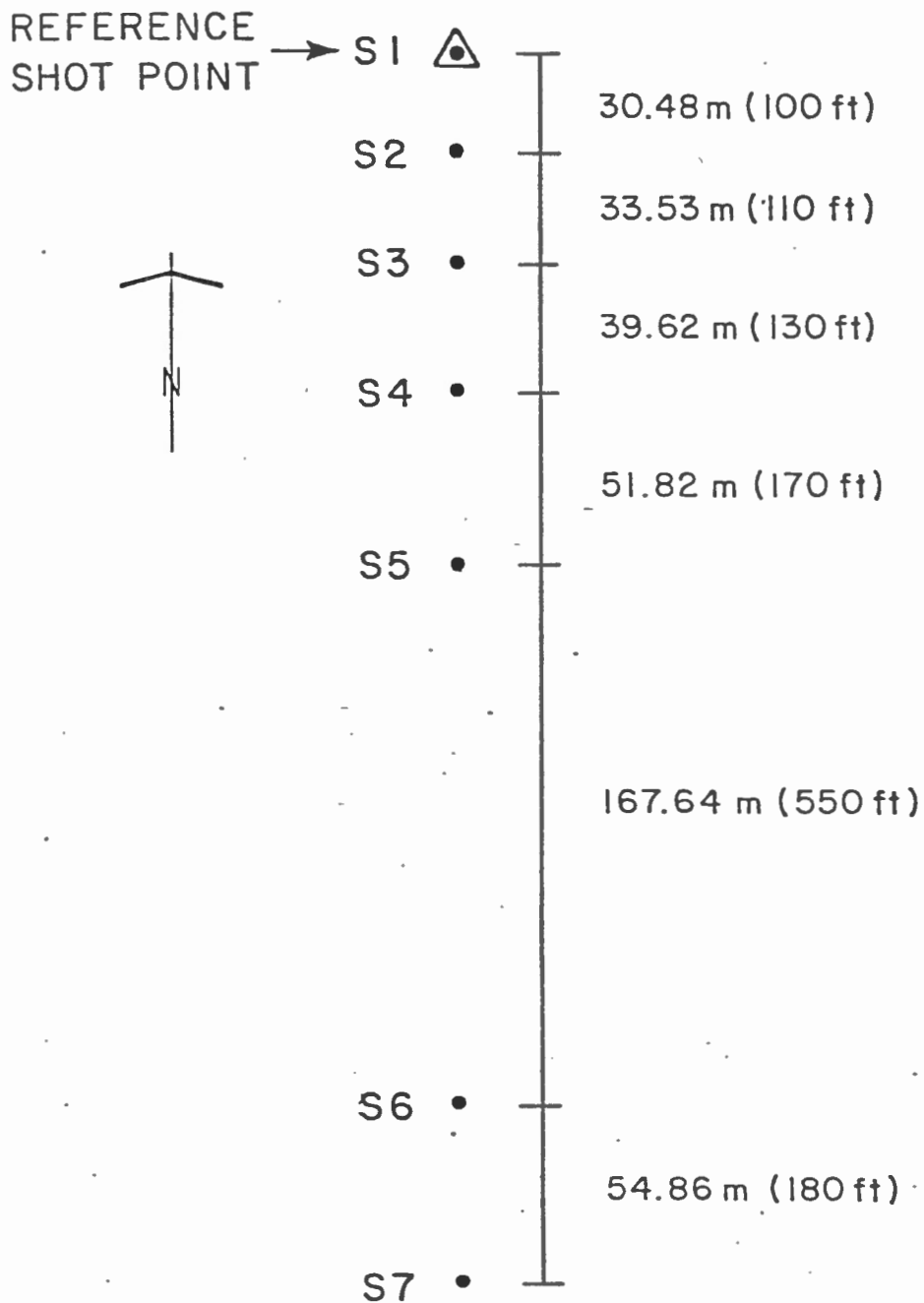


FIGURE 8

SHOT HOLE ARRAY - LINE C -  
SHOTS 19 AND 20

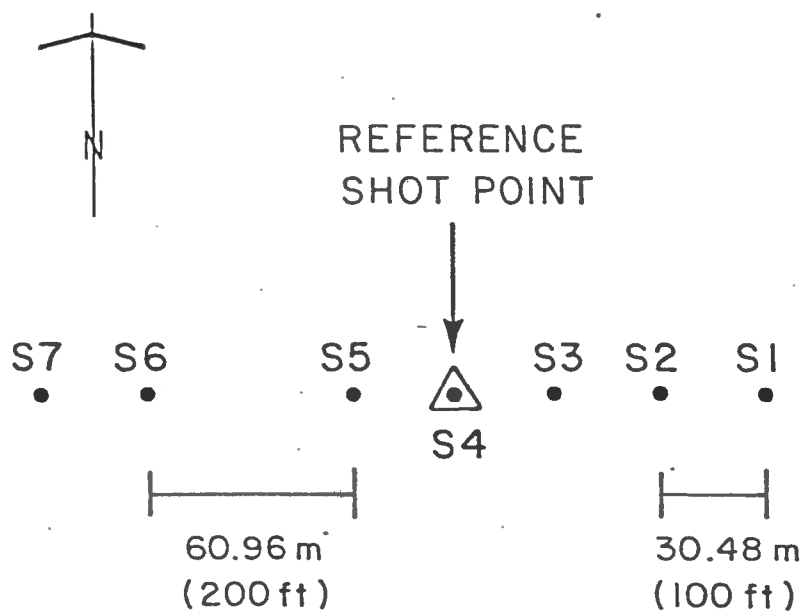


FIGURE 9

set in the shot direction. UWO sites observed one vertical and two horizontal seismometers. These horizontal components were set N/S and E/W.

Nineteen stations were occupied within one set-up and one shot was fired into this array from each end of the line. Thus every set-up recorded one small and one large charge.

Table 8 indicates the instrumentation of the individual recording sites for all three lines.

All EMR stations recorded digitally. The UWO stations recorded FM analog signals. The EMR data digital interval was 0.01667 sec. The UWO data was digitized in the laboratory. The digital interval on this set of data was not constant, it varied between 0.0172 to 0.0163 sec. The sampling interval of each individual trace was indicated on the trace header of the digital data. For accurate timing and plotting of these data this additional variable must be recognized.

#### e) Refraction Data, Tape Format

All 1979 refraction data were compiled on a single digital tape. The total set of information is condensed in 10 digital files. Specific details of the format are described in Table 9. One file contains all the headers for each individual trace for a single line. This is followed by the file that contains all the data traces for that specific line. The first three data samples contain the following information: receiver number, shot number, component number.

Component numbers are: 1 vertical  
3 N/S  
4 E/W.



TABLE 8

## INSTRUMENTATION SETUP

| <u>LINE A</u> |      | <u>LINE B</u> |      |
|---------------|------|---------------|------|
| ST            | CREW | ST            | CREW |
| 1.0           | UWO  | 1.0           | EMR  |
| 2.0           | UWO  | 2.0           | EMR  |
| 3.0           | UWO  | 2.5           | EMR  |
| 4.0           | UWO  | 3.0           | EMR  |
| 5.0           | UWO  | 4.0           | EMR  |
| 6.0           | UWO  | 5.0           | EMR  |
| 7.0           | UWO  | 6.0           | EMR  |
| 8.0           | EMR  | 7.0           | EMR  |
| 8.5           | EMR  | 8.0           | EMR  |
| 9.0           | EMR  | 9.0           | EMR  |
| 10.0          | EMR  | 10.0          | EMR  |
| 11.0          | EMR  | 11.0          | EMR  |
| 12.0          | EMR  | 12.0          | UWO  |
| 13.0          | EMR  | 13.0          | UWO  |
| 14.0          | EMR  | 14.0          | UWO  |
| 15.0          | EMR  | 15.0          | UWO  |
| 16.0          | EMR  | 16.0          | UWO  |
| 17.0          | EMR  | 17.0          | UWO  |
| 18.0          | EMR  | 18.0          | UWO  |
| 19.0          | UWO  | 19.0          | UWO  |
| 20.0          | UWO  | 20.0          | UWO  |
| 21.0          | UWO  | 21.0          | UWO  |
| 22.0          | UWO  | 22.0          | UWO  |
| 23.0          | UWO  | 23.0          | UWO  |
| 23.5          | UWO  | 24.0          | EMR  |
| 24.0          | EMR  | 24.5          | EMR  |
| 24.5          | EMR  | 25.0          | EMR  |
| 25.0          | EMR  | 26.0          | EMR  |
| 26.0          | EMR  | 27.0          | EMR  |
| 27.0          | EMR  | 28.0          | EMR  |
| 28.0          | EMR  | 29.0          | EMR  |
| 29.0          | EMR  | 30.0          | EMR  |
| 30.0          | EMR  | 31.0          | EMR  |
| 31.0          | EMR  | 32.0          | EMR  |
| 32.0          | EMR  | 32.5          | EMR  |
| 33.0          | EMR  | 33.0          | EMR  |
| 33.5          | EMR  | 34.0          | EMR  |
| 34.0          | EMR  |               |      |

TABLE 8

## INSTRUMENTATION SETUP

LINE C

| ST   | CREW |
|------|------|
| 0.0  | UWO  |
| 1.0  | UWO  |
| 2.0  | UWO  |
| 3.0  | UWO  |
| 4.0  | UWO  |
| 5.0  | UWO  |
| 6.0  | UWO  |
| 7.0  | UWO  |
| 8.0  | EMR  |
| 9.0  | EMR  |
| 10.0 | EMR  |
| 11.0 | EMR  |
| 12.0 | EMR  |
| 13.0 | EMR  |
| 14.0 | EMR  |
| 15.0 | EMR  |
| 16.0 | EMR  |
| 17.0 | EMR  |
| 18.0 | EMR  |
| 18.5 | UWO  |
| 19.0 | UWO  |
| 20.0 | UWO  |
| 21.0 | UWO  |
| 22.0 | UWO  |
| 23.0 | UWO  |
| 24.0 | UWO  |
| 24.5 | EMR  |
| 25.0 | EMR  |
| 26.0 | EMR  |
| 27.0 | EMR  |
| 28.0 | EMR  |
| 29.0 | EMR  |
| 30.0 | EMR  |
| 31.0 | EMR  |
| 32.0 | EMR  |
| 33.0 | EMR  |
| 34.0 | EMR  |

TABLE 9

## TAPE CHARACTERISTICS - COCRUST '79 REFRACTION DATA

## 1. Tape holds 10 files:

| File # | Contents   |
|--------|--|
| 1      | Alpha numeric record headers for<br>Line A - N.S. (S.P. at N. end) |
| 2      | Data - Line A - N.S.   |
| 3      | Headers - Line A - S.N.  |
| 4      | Data - Line A - S.N.   |
| 5      | Headers - Line B - N.S.  |
| 6      | Data - Line B - N.S.   |
| 7      | Headers - Line B - S.N.  |
| 8      | Data - Line B - S.N.   |
| 9      | Headers - Line C   |
| 10     | Data - Line C  |

2. Each trace is made up of 7200 digital samples

3. 1600 BPI

4. Record Length - 80 Bytes

5. Block Size - 4800 Bytes

6. Headers written as follows:

```

      INTEGER IHDR (200)
      WRITE (10,40) (IHDR(I), I = 1,200)
      40 FORMAT (20A4)

```

7. Data written as follows:

```

      REAL TRACE (7200)
      WRITE (10,50) (TRACE(I), I = 1,7200)
      50 FORMAT (5E16.6)

```

8. IBM floating point format

9. Tape contains No Labels

Brian Reilkoff  
June 12, 1980

## 1979 REFLECTION SURVEY

### a) Survey Line

The reflection survey was conducted along Manitoba Provincial Highway 255 in an east-west direction. This line represents the direct continuation of the 1977 survey (Figure 1 and 10). The rationale for the location and the direction was well documented by Green and Stephenson (1978).

The 1979 survey was relocated 1.609 km south of line 3 of the 1977 program. This move made it possible to conduct the entire survey as a continuous profile. The first shot point was located at the NE corner of Section 2, Township 9, Range 25 W1. The final recording site was at the NW corner of section 5, Township 9, Range 28 W1. The first shot point is 1.609 km south of station 210 of the 1977 survey. This provides a 10 km overlap of the two surveys. The total length of the seismic profile is 37.01 km. Details of the position of the line are illustrated in Figure 5.

### b). Field Parameters

Table 10 consists of the observers' notes which provide most of the pertinent information. Some of the main values are:

#### 1) Seismic line

|                                |        |
|--------------------------------|--------|
| Seismometer group spacing      | 200 m  |
| Number of geophone groups/shot | 48     |
| Geophones interval             | 7.62 m |
| Number of geophones/station    | 18     |

|  |                    |
|--|--------------------|
| Group length                           | 129.54 m           |
| Geophone type                          | Mark Products L-15 |
| Standard frequency                     | 8 Hz               |
| Total number of receiver locations     | 190                |
| Group layout                           | linear             |
| 2). Shot Point                         |                    |
| Shot point spacing                     | 400 m              |
| Number of shot/spread                  | 24                 |
| Total number of shots                  | 82                 |
| Explosives (60% Geogel, 46cm. x 13cm.) | 33 kg              |
| Shot hole depth                        | 15.24 m            |

The survey geometry followed the following pattern: minimum offset was 400 m, maximum 9300 m. Shots were fired from the east end of the line. Shooting at every second receiver location and following the above pattern provided a 12-fold common depth point (CDP) survey for the line. Figure 11 reveals the exact CDP coverage at the individual sites. Every shot point and receiver site was established by a local survey. The elevation of each location above sea level was determined by high quality leveling. Table 11 contains the individual station elevation values.

### c) Drilling

Drilling was contracted to Graham Drilling Ltd. from Bredenbury, Saskatchewan. Shot hole drilling was done in the road allowance alongside the road.

TABLE 11

## REFLECTION PROFILE - STATION ELEVATIONS

| STATION | ELEVATION | STATION | ELEVATION (meters) |
|---------|-----------|---------|--------------------|
| 1       | 433.523   | 26      | 431.134            |
| 2       | 433.968   | 27      | 431.396            |
| 3       | 433.874   | 28      | 431.097            |
| 4       | 437.982   | 29      | 431.225            |
| 5       | 438.254   | 30      | 431.365            |
| 6       | 436.099   | 31      | 431.228            |
| 7       | 437.025   | 32      | 430.963            |
| 8       | 437.242   | 33      | 430.567            |
| 9       | 435.983   | 34      | 430.612            |
| 10      | 434.890   | 35      | 430.981            |
| 11      | 433.435   | 36      | 430.902            |
| 12      | 433.005   | 37      | 431.085            |
| 13      | 432.831   | 38      | 431.210            |
| 14      | 433.000   | 39      | 431.262            |
| 15      | 431.390   | 40      | 431.615            |
| 16      | 431.100   | 41      | 432.188            |
| 17      | 430.999   | 42      | 433.045            |
| 18      | 430.999   | 43      | 432.883            |
| 19      | 431.173   | 44      | 431.902            |
| 20      | 431.222   | 45      | 431.487            |
| 21      | 431.344   | 46      | 431.487            |
| 22      | 431.240   | 47      | 431.853            |
| 23      | 431.213   | 48      | 431.978            |
| 24      | 431.073   | 49      | 432.209            |
| 25      | 431.100   | 50      | 433.624            |

| STATION | ELEVATION | STATION | ELEVATION (meters) |
|---------|-----------|---------|--------------------|
| 51      | 432.462   | 81      | 435.958            |
| 52      | 432.456   | 82      | 436.720            |
| 53      | 432.398   | 83      | 438.107            |
| 54      | 432.420   | 84      | 440.406            |
| 55      | 432.493   | 85      | 444.292            |
| 56      | 432.880   | 86      | 448.833            |
| 57      | 433.365   | 87      | 449.202            |
| 58      | 433.383   | 88      | 449.153            |
| 59      | 433.600   | 89      | 449.495            |
| 60      | 433.224   | 90      | 450.476            |
| 61      | 433.167   | 91      | 450.089            |
| 62      | 433.374   | 92      | 448.394            |
| 63      | 433.740   | 93      | 447.913            |
| 64      | 433.910   | 94      | 447.870            |
| 65      | 433.554   | 95      | 449.156            |
| 66      | 433.291   | 96      | 449.473            |
| 67      | 433.578   | 97      | 450.287            |
| 68      | 433.709   | 98      | 451.589            |
| 69      | 433.612   | 99      | 452.783            |
| 70      | 433.352   | 100     | 453.658            |
| 71      | 433.654   | 101     | 454.396            |
| 72      | 433.895   | 102     | 455.655            |
| 73      | 433.883   | 103     | 456.322            |
| 74      | 434.066   | 104     | 456.270            |
| 75      | 434.160   | 105     | 457.081            |
| 76      | 434.529   | 106     | 457.547            |
| 77      | 434.169   | 107     | 457.365            |
| 78      | 434.057   | 108     | 458.608            |
| 79      | 434.517   | 109     | 459.702            |
| 80      | 435.041   | 110     | 458.224            |

| STATION | ELEVATION | STATION | ELEVATION (meters) |
|---------|-----------|---------|--------------------|
| 111     | 457.282   | 141     | 477.591            |
| 112     | 457.648   | 142     | 477.871            |
| 113     | 458.596   | 143     | 478.740            |
| 114     | 460.495   | 144     | 479.713            |
| 115     | 461.772   | 145     | 480.255            |
| 116     | 461.370   | 146     | 480.913            |
| 117     | 463.305   | 147     | 481.493            |
| 118     | 463.912   | 148     | 482.239            |
| 119     | 464.015   | 149     | 484.443            |
| 120     | 464.000   | 150     | 484.217            |
| 121     | 465.061   | 151     | 484.845            |
| 122     | 465.865   | 152     | 484.644            |
| 123     | 465.792   | 153     | 485.232            |
| 124     | 465.795   | 154     | 484.522            |
| 125     | 466.283   | 155     | 483.215            |
| 126     | 466.692   | 156     | 484.035            |
| 127     | 467.018   | 157     | 482.081            |
| 128     | 467.350   | 158     | 479.280            |
| 129     | 468.624   | 159     | 478.426            |
| 130     | 469.846   | 160     | 477.021            |
| 131     | 471.151   | 161     | 475.762            |
| 132     | 471.879   | 162     | 474.400            |
| 133     | 472.690   | 163     | 470.636            |
| 134     | 473.498   | 164     | 469.029            |
| 135     | 474.647   | 165     | 467.158            |
| 136     | 475.253   | 166     | 465.070            |
| 137     | 476.040   | 167     | 464.131            |
| 138     | 476.640   | 168     | 463.823            |
| 139     | 477.055   | 169     | 463.503            |
| 140     | 477.189   | 170     | 463.787            |



| STATION | ELEVATION | STATION | ELEVATION (meters) |
|---------|-----------|---------|--------------------|
| 171     | 464.195   |         |                    |
| 172     | 465.302   |         |                    |
| 173     | 467.268   |         |                    |
| 174     | 467.258   |         |                    |
| 175     | 467.420   |         |                    |
| 176     | 468.490   |         |                    |
| 177     | 468.136   |         |                    |
| 178     | 466.627   |         |                    |
| 179     | 468.170   |         |                    |
| 180     | 469.584   |         |                    |
| 181     | 472.727   |         |                    |
| 182     | 474.628   |         |                    |
| 183     | 479.460   |         |                    |
| 184     | 485.178   |         |                    |
| 185     | 487.760   |         |                    |
| 186     | 492.273   |         |                    |
| 187     | 496.458   |         |                    |
| 188     | 499.884   |         |                    |
| 189     | 503.389   |         |                    |
| 190     | 505.432   |         |                    |

d) Instrumentation; Shooting Procedures

The data were recorded with a Texas Instruments model DFS III 48 trace seismic system. Record length was 20 seconds; sampling rate was 2 msec. This recording system is equipped with binary gain ranging amplifiers with fifteen 2 to 1 gain steps, providing a 90 db dynamic range and giving a total range of 32,768:1.

The shooting procedure was conducted with an Input/Output Incorporated Model DEC 200 FM decoding system. The FM pulse, generated remotely by the shooter, triggered the entire recording system thus providing an accurate zero time as well as transmitting the uphole time to the recording truck.

e) Corrections

Attached to this report are two seismic sections which represent a preliminary interpretation of the reflection data (Figures 19 and 20). Two sets of corrections were applied to the data. These are static corrections that include elevation and weathering corrections and normal moveout corrections.

1) Static corrections

The static corrections were computed to effectively place all the shots and receivers to a common datum of 380 m above the sea level. This is the same elevation used as datum for the 1977 program.

The actual corrections are listed in Table 12. The large receiver spacing and long spread length made the first break information ineffective for weathering corrections. Chevron Standard Ltd. of Calgary recorded an exploration seismic line over the same

TABLE 12

1979 Reflection Data, Elevation and Weathering Corrections  
(Datum = 380.09 m A.S.L.)

| STA. | RCR STAT.<br>SEC. | SHOT STAT.<br>SEC. | STA. | RCR STAT.<br>SEC. | SHOT STAT.<br>SEC. |
|------|-------------------|--------------------|------|-------------------|--------------------|
| 1    | .034              | .019               | 31   | .034              | .019               |
| 2    | .034              |                    | 32   | .034              |                    |
| 3    | .034              | .019               | 33   | .034              | .019               |
| 4    | .034              |                    | 34   | .034              |                    |
| 5    | .034              | .019               | 35   | .034              | .019               |
| 6    | .034              |                    | 36   | .034              |                    |
| 7    | .034              | .019               | 37   | .034              | .019               |
| 8    | .034              |                    | 38   | .034              |                    |
| 9    | .034              | .019               | 39   | .034              | .019               |
| 10   | .034              |                    | 40   | .034              |                    |
| 11   | .034              | .019               | 41   | .034              | .019               |
| 12   | .034              |                    | 42   | .034              |                    |
| 13   | .034              | .019               | 43   | .034              | .019               |
| 14   | .034              |                    | 44   | .034              |                    |
| 15   | .034              | .019               | 45   | .034              | .019               |
| 16   | .034              |                    | 46   | .034              |                    |
| 17   | .034              | .019               | 47   | .034              | .019               |
| 18   | .034              |                    | 48   | .034              |                    |
| 19   | .034              | .019               | 49   | .034              | .019               |
| 20   | .034              |                    | 50   | .034              |                    |
| 21   | .034              | .019               | 51   | .034              | .019               |
| 22   | .034              |                    | 52   | .034              |                    |
| 23   | .034              | .019               | 53   | .034              | .019               |
| 24   | .034              |                    | 54   | .034              |                    |
| 25   | .034              | .019               | 55   | .034              | .019               |
| 26   | .034              |                    | 56   | .034              |                    |
| 27   | .034              | .019               | 57   | .034              | .019               |
| 28   | .034              |                    | 58   | .034              |                    |
| 29   | .034              | .019               | 59   | .034              | .019               |
| 30   | .034              |                    | 60   | .034              |                    |

| STA. | RCR STAT.<br>SEC. | SHOT STAT.<br>SEC. | STA. | RCR STAT.<br>SEC. | SHOT STAT.<br>SEC. |
|------|-------------------|--------------------|------|-------------------|--------------------|
| 61   | .034              | .019               | 95   | .037              | .023               |
| 62   | .034              |                    | 96   | .040              |                    |
| 63   | .034              | .019               | 97   | .039              | .026               |
| 64   | .034              |                    | 98   | .042              |                    |
| 65   | .034              | .019               | 99   | .042              | .030               |
| 66   | .034              |                    | 100  | .041              |                    |
| 67   | .034              | .019               | 101  | .036              | .024               |
| 68   | .031              |                    | 102  | .039              |                    |
| 69   | .031              | .017               | 103  | .040              | .028               |
| 70   | .034              |                    | 104  | .046              |                    |
| 71   | .031              | .019               | 105  | .042              | .030               |
| 72   | .032              |                    | 106  | .039              |                    |
| 73   | .033              | .021               | 107  | .044              | .032               |
| 74   | .034              |                    | 108  | .046              |                    |
| 75   | .034              | .020               | 109  | .046              | .033               |
| 76   | .033              |                    | 110  | .045              |                    |
| 77   | .034              | .019               | 111  | .045              | .033               |
| 78   | .034              |                    | 112  | .045              |                    |
| 79   | .032              | .020               | 113  | .044              | .032               |
| 80   | .034              |                    | 114  | .044              |                    |
| 81   | .032              | .018               | 115  | .051              | .035               |
| 82   | .033              |                    | 116  | .049              |                    |
| 83   | .036              | .024               | 117  | .049              | .037               |
| 84   | .040              |                    | 118  | .047              |                    |
| 85   | .045              | .026               | 119  | .047              | .034               |
| 86   | .045              |                    | 120  | .049              |                    |
| 87   | .046              | .027               | 121  | .048              | .035               |
| 88   | .043              |                    | 122  | .049              |                    |
| 89   | .040              | .027               | 123  | .055              | .036               |
| 90   | .048              |                    | 124  | .049              |                    |
| 91   | .044              | .028               | 125  | .051              | .037               |
| 92   | .038              |                    | 126  | .050              |                    |
| 93   | .042              | .028               | 127  | .049              | .036               |
| 94   | .038              |                    | 128  | .052              |                    |

| STA. | RCR STAT.<br>SEC. | SHOT STAT.<br>SEC. | STA. | RCR STAT.<br>SEC. | SHOT STAT.<br>SEC. |
|------|-------------------|--------------------|------|-------------------|--------------------|
| 129  | .052              | .039               | 163  | .054              | .039               |
| 130  | .051              |                    | 164  | .054              |                    |
| 131  | .050              | .037               | 165  | .053              | .038               |
| 132  | .052              |                    | 166  | .052              |                    |
| 133  | .049              | .037               | 167  | .051              | .036               |
| 134  | .054              |                    | 168  | .051              |                    |
| 135  | .053              | .041               | 169  | .051              |                    |
| 136  | .053              |                    | 170  | .051              |                    |
| 137  | .055              | .043               | 171  | .051              |                    |
| 138  | .056              |                    | 172  | .052              |                    |
| 139  | .056              | .043               | 173  | .053              |                    |
| 140  | .057              |                    | 174  | .053              |                    |
| 141  | .058              | .044               | 175  | .053              |                    |
| 142  | .057              |                    | 176  | .053              |                    |
| 143  | .058              | .045               | 177  | .053              |                    |
| 144  | .059              |                    | 178  | .052              |                    |
| 145  | .058              | .045               | 179  | .053              |                    |
| 146  | .060              |                    | 180  | .054              |                    |
| 147  | .061              | .046               | 181  | .057              |                    |
| 148  | .062              |                    | 182  | .058              |                    |
| 149  | .062              | .048               | 183  | .060              |                    |
| 150  | .060              |                    | 184  | .063              |                    |
| 151  | .063              | .048               | 185  | .064              |                    |
| 152  | .065              |                    | 186  | .066              |                    |
| 153  | .062              | .048               | 187  | .068              |                    |
| 154  | .063              |                    | 188  | .070              |                    |
| 155  | .061              | .047               | 189  | .071              |                    |
| 156  | .060              |                    | 190  | .072              |                    |
| 157  | .061              | .046               |      |                   |                    |
| 158  | .060              |                    |      |                   |                    |
| 159  | .060              | .045               |      |                   |                    |
| 160  | .059              |                    |      |                   |                    |
| 161  | .058              | .043               |      |                   |                    |
| 162  | .057              |                    |      |                   |                    |

locality. The corrections computed from these data were adapted for the present program. The data provide excellent quality information and at most receiver locations direct correlation could be made between the two survey sites. The replacement velocity for the upper till section was 1.859 km/sec and for the underlying Cretaceous beds 2.133 km/sec.

## 2) Normal moveout corrections

The velocity function used for NMO correction was taken from two sources. For the sedimentary section Chevron Standard Ltd. released the values which they adopted to process the exploration data. Beyond the Phanerozoic-Precambrian contact the function used by Sereda (1978) for the Sifton site (Figure 1) in Manitoba was adapted. This information was reproduced on Figure 21; where curve 'c' represents the pertinent velocity function.

## f) Data Tape Format

The raw reflection data are provided in shot sort form. The sampling rate of the data on the tape is 4 msec. The format of the information, as transcribed on the submitted tape, is illustrated in detail in Table 13.

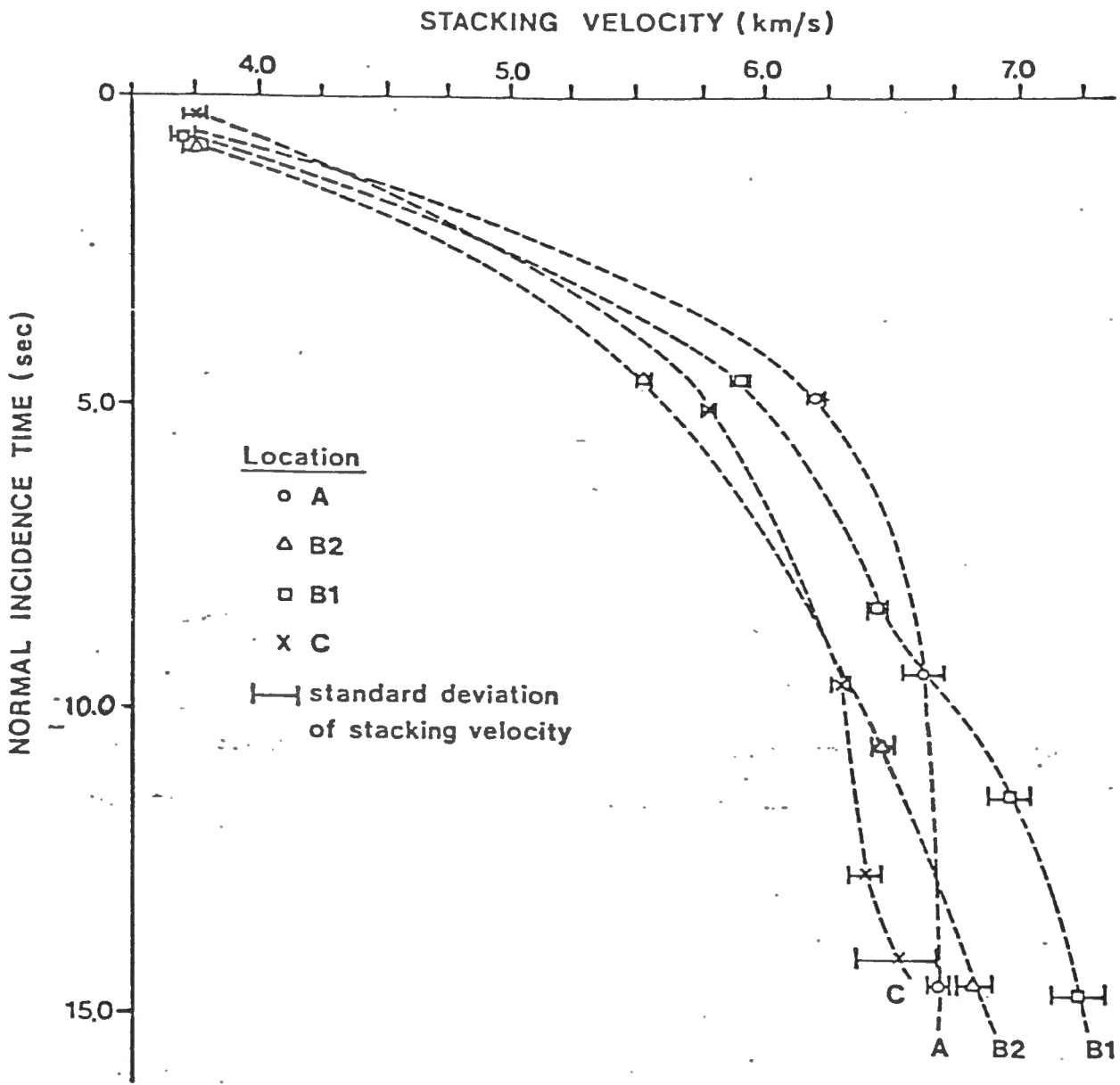


Figure 21 - Crustal stacking velocity functions.

TABLE 13

## TAPE CHARACTERISTICS: EMR1 &amp; EMR2

1. Tapes hold the "shot sorts"
2. Both tapes are 1600 BPI
3. EMR1 contains 2 files:
  - first file holds a tape header
  - second file contains data
4. EMR2 contains 1 file of data
5. Tape header:

| Byte # | Contents | Description            |
|--------|----------|------------------------|
| 0-3    | 'CC79'   | Project                |
| 4-7    | 'UofS'   | Crew                   |
| 8-11   | 1.0      | Line #                 |
| 12-15  | 82.0     | # of shots             |
| 16-19  | 48.0     | # traces/shot          |
| 20-23  | 4.0      | Sampe rate (msec.)     |
| 24-27  | 5000.0   | # Samples/trace        |
| 28-31  | 3936.0   | Total # traces in line |
| 32-35  | 0.0      |                        |
| 36-39  | 0.0      |                        |

6. Each trace has a header written onto it:

| Byte # | Description                 |
|--------|-----------------------------|
| 0-3    | Shot # (1-82)               |
| 4-7    | Trace # (1-48)              |
| 8-11   | Shot position (1-167)       |
| 12-15  | Receiver # (1-190)          |
| 16-19  | Offset in meters (400-9800) |
| 20-23  | Shot depth (meters)         |
| 24-27  | Charge size (kilograms)     |
| 28-31  | Digital filter passband     |
| 32-35  | 0.0                         |
| 36-39  | 0.0                         |

7. Record Length = Blocksize = 20000 Bytes
8. Tapeheader & data are in binary IBM floating point format:

```

      REAL TRACE (5000)
      WRITE (10,20) (TRACE(I), I=1,5000)
20  FORMAT (5000 A4)

```

9. Tape contains NO LABELS



## MISCELLANEOUS

a) Personnel1) Refraction Survey

| Supervisor     | Organization                  | Number of crew |
|----------------|-------------------------------|----------------|
| Dr. A. Mair    | Earth Physics Branch          | 4              |
| Dr. R.F. Mereu | University of Western Ontario | 2              |

2) Reflection Survey

| Supervisor    | Organization               | Number of crew |
|---------------|----------------------------|----------------|
| Dr. Z. Hajnal | University of Saskatchewan | 6              |
|               | University of Manitoba     | 3              |
|               | University of Alberta      | 2              |

b) PermitsManitoba

Geophysical License No. 155

Road Allowance Permit No. 151

Saskatchewan

License to Conduct Geophysical Exploration No. 1089

Geophysical Crew Certificate No. 41

c) Clean Up

Along the reflection line several holes were cratered on account of loose unconsolidated, fine-grained sand near the surface.

B. Williamson Construction Company of Pierson, Manitoba, was

contracted to fill the holes and repair all effects of the shot hole drilling.

d) Timing

The reflection survey was conducted in the time period of August 1 to August 10, 1979. Approximately 2.5 days were lost due to poor weather and waiting for the driller.

The refraction program was undertaken between August 14 and 21, 1979. One day was lost due to blaster box malfunction and lack of finished holes.

e) Weather

During the reflection survey period there was one rainy stormy day and the heavy lightning the following day prevented field operations. The weather at the time of the refraction program was ideal. With the exception of the last shot all explosions were fired in the early morning hours, in an almost completely windless environment.

## PRELIMINARY RESULTS

### I. Refraction lines

Computer plots of the vertical component refraction records are shown in Figures 12 to 16. All records were plotted with a reduced time scale. The time reduction was trace offset divided by a velocity of 6.8 km/sec. The data quality is very high. Excellent signal to noise ratio is indicated on every line. The maximum amplitude on all plotted traces was set to 2.54 cm, therefore the sections indicate only relative amplitude variation. The first break information is very well recognizable and arrival times were determined on the majority of the records with an accuracy of 0.01 sec. or better. All sections reveal some uneven gaps in between traces. This occurrence is a result of technical problems encountered when reading several EMR digital magnetic cassette tapes. The data presented on the above sections represent the unfiltered raw information as recovered from field records.

#### a) Travel Time Interpretation

Figures 12-16 indicate the initial attempt to interpret the first arrival information. Apparent velocities and intercept times were computed from linear least-square fits of the data. The linearity of the data is illustrated by the rather high correlation coefficient obtained in all cases. The lowest correlation coefficient was 0.9913

on the last segment of line C. Although the correlation appears to be good, the variation of velocities within reversed profiles and from line to line, as well as the appearance of a complex set of large amplitude secondary arrivals on all the sections, illustrate that the crustal picture in the area is much more complex than the first arrivals indicate. The present results are very preliminary and will require significant modifications after an analysis of later events and some experimentation with modelling.

Velocities and intercept times are shown in Table 14.

#### b) North-South Models

Although the velocity information of the different line segments shows considerable lateral heterogeneity there is enough similarity in character between them that as a first approximation the crust is assumed to be formed by a set of layers separated by dipping interfaces. For this type of analysis of the data equations derived by Masuda (1975) were adopted. Figure 17 presents a rudimentary interpretation of all north south lines. On the premises of Green et al. (1979, 1980) respecting the interpretation of magnetic gravity and seismic data, the 1977 profile was located in the Superior Province -- line A mainly in the eastern margin of the boundary zone and line B in the Churchill Province. In spite of the apparent different geological regions, with the exception of the sedimentary layers, all sections show a south to north dip within the crust. A near 6.0 km/sec uppermost crustal layer exists in all the regions. It is thinnest in

TABLE 14

## Line A

| LAYER NUMBER | RECORDS USED IN LEAST SQUARES           | NUMBER OF RECORDS | LEAST SQUARE APPARENT VELOCITIES (KM/S) | LEAST SQUARE INTERCEPT (SEC.) | CORRELATION COEFFICIENT | COMMENTS   |
|--------------|---|-------------------|---|-------------------------------|-------------------------|------------|
| 1            |   | V LOG             | 3.62                                    |                               |                         |            |
| 2            | 245, 260, 290                           | 3                 | $6.09 \pm 0.001$                        | $0.55 \pm 0.01$               | 0.9999                  | RELIABLE   |
| 3            | 180 to 230<br>235, 240                  | 8                 | $6.25 \pm 0.002$                        | $0.76 \pm 0.05$               | 0.9998                  | RELIABLE   |
| 4            | 90, 110 to 130<br>160, 170              | 6                 | $6.32 \pm 0.001$                        | $1.20 \pm 0.45$               | 0.9994                  | RELIABLE   |
| 5            | 20 to 60                                | 5                 | $8.05 \pm 0.006$                        | $8.61 \pm 0.61$               | 0.9998                  | RELIABLE   |
| -----        |   |                   |   |                               |                         |            |
| 1            |   | V LOG             | 3.62                                    |                               |                         |            |
| 2            | 20, 30                                  | 2                 | $5.75 \pm 0.020$                        | $0.81 \pm 0.12$               | 1.0000                  | UNRELIABLE |
| 3            | 40 to 120                               | 9                 | $6.30 \pm 0.002$                        | $0.85 \pm 0.11$               | 0.9996                  | RELIABLE   |
| 4            | 160 to 230<br>235, 240, 245<br>250, 260 | 13                | $6.34 \pm 0.002$                        | $1.09 \pm 0.20$               | 0.9997                  | RELIABLE   |
| 5            | 280 to 310,<br>335                      | 5                 | $8.06 \pm 0.010$                        | $8.52 \pm 0.75$               | 0.9991                  | RELIABLE   |
| -----        |   |                   |   |                               |                         |            |

## Line B

| LAYER NUMBER | RECORDS USED IN LEAST SQUARES         | NUMBER OF RECORDS | LEAST SQUARE APPARENT VELOCITIES (KM/S) | LEAST SQUARE INTERCEPT (SEC.) | CORRELATION COEFFICIENT | COMMENTS |
|--------------|---------------------------------------|-------------------|---|-------------------------------|-------------------------|----------|
| 1            |                                       | V LOG             | 4.0                                     | 0                             |                         |          |
| 2            | 260, 280<br>300, 330                  | 4                 | $6.05 \pm 0.001$                        | $0.29 \pm 0.26$               | 0.9996                  | RELIABLE |
| 3            | 170 to 240                            | 9                 | $6.37 \pm 0.004$                        | $1.14 \pm 0.14$               | 0.9998                  | RELIABLE |
| 4            | 100, 110, 130<br>to 160               | 6                 | $6.49 \pm 0.004$                        | $1.69 \pm 0.06$               | 1.0000                  | RELIABLE |
| 5            | 10 to 70                              | 8                 | $8.26 \pm 0.001$                        | $8.22 \pm 0.41$               | 0.9993                  | RELIABLE |
| -----        |                                       |                   |   |                               |                         |          |
| 1            |                                       | V LOG             | 3.20                                    | 0                             |                         |          |
| 2            | 20, 25, 30<br>to 70                   | 7                 | $6.05 \pm 0.001$                        | $1.57 \pm 0.05$               | 0.9997                  | RELIABLE |
| 3            | 100, 110, 130<br>to 200               | 10                | $6.38 \pm 0.003$                        | $2.09 \pm 0.33$               | 0.9984                  | RELIABLE |
| 4            | 220, 230, 235<br>240, 245, 260<br>270 | 7                 | $6.49 \pm 0.005$                        | $2.36 \pm 0.26$               | 0.9998                  | RELIABLE |
| 5            | 280, 290, 310<br>330, 340             | 5                 | $8.26 \pm 0.011$                        | $9.05 \pm 1.67$               | 0.9951                  | RELIABLE |
| -----        |                                       |                   |   |                               |                         |          |

## Line C

| LAYER NUMBER | RECORDS USED IN LEAST SQUARES | NUMBER OF RECORDS | LEAST SQUARE APPARENT VELOCITIES (KM/S) | LEAST SQUARE INTERCEPT (SEC.) | CORRELATION COEFFICIENT | COMMENTS   |
|--------------|-------------------------------|-------------------|---|-------------------------------|-------------------------|------------|
| 1            |                               | V LOG             | 3.2                                     | 0                             |                         |            |
| 2            | 240, 245, 250 to 270          | 10                | $6.07 \pm 0.001$                        | $1.40 \pm 0.11$               | 0.9995                  | RELIABLE   |
| 3            | 170, 180, 185, 190 to 230     | 8                 | $6.56 \pm 0.001$                        | $2.82 \pm 0.17$               | 0.9998                  | RELIABLE   |
| 4            | 90, 110, 130, 150             | 4                 | $6.65 \pm 0.001$                        | $3.21 \pm 0.29$               | 0.9999                  | UNRELIABLE |
| 5            | 0 to 70                       | 8                 | $7.99 \pm 0.005$                        | $8.97 \pm 1.76$               | 0.9913                  | RELIABLE   |

---

the boundary zone. The underlying intermediate layer reveals significant velocity heterogeneity or anisotropy from east to west, starting with 6.21 km/sec in the east and reaching 6.38 km/sec in the Churchill Province. The lowest crustal layer appears also heterogeneous as it has the highest velocity in the Superior Province and the lowest in the boundary zone, where it reaches over 29 km in thickness.

The Moho is apparently dipping to the south in the Superior Province; to the north in the boundary zone; and is relatively flat in the Churchill Province. The upper mantle velocity in the Churchill Province appears anomalously high. The first break information does not reveal, on any of the 1979 profiles, a 7 km/sec type of lower crustal layer. This zone, however, was recognized in many parts of the Superior Province (Hall and Hajnal, 1973) and also in the Churchill Province (Chandra and Cumming, 1972). Preliminary modelling by Green et al. (1980) seems to indicate that this lower crustal zone may appear as a hidden layer in the boundary zone region.

### c) East-west models

Except for the upper most crust the subsurface sampled by the east-west line lies within the boundary zone, mainly in the Churchill Province (Figure 18). The complications of the reversed segment of the 1977 line were described by Green et al. (1980). The complexity of the travel time branches near the source on the east end of the line was interpreted as an indication of the start of the boundary zone. The near 6.04 km/sec uppermost layer was not observed on the west side of



the 1977 profile. It was observed, however, on line B and also on line C. It appears that this layer is rather thin, or perhaps does not exist in most parts of the transition zone. One interpretation of the related figures on line B and C is that this layer is relatively thin in the most easterly part of the Churchill Province and reaches a thickness of 13.7 km at the west end of line C. The second layers of line B and C with velocities of 6.38 km/sec and 6.56 km/sec are very likely inter-related but the different dip variations along the respective lines must be established first in order that the true velocity of this zone be determined. The lower crustal layer reaches a depth of 44 km at its most westerly point of study. If the observed velocities are true velocities, this layer is heterogeneous or anisotropic with an increasing value from east to west. The crust thickness is increasing to the west. It is 44 km just east of Assiniboia and 45 km near Swift Current, according to Chandra and Cumming (1972). They, however, reveal a 7.17 km/sec layer above the Moho that is not recognized on either line C or the 1977 part of the cross section. A more thorough analysis of the entire data set is necessary before correlation between the different layers of the different profiles is established with considerable confidence.

## II Reflection Profile

A standard, commercially processed form of the reflection data is presented in Figures 19 and 20.

Judging from the near-surface section of the profile the reflection data quality are rather good. The patterned nature of the

reflections from the top of the Paleozoic around 0.7 sec two way time is due to the influence of the long spread length. It was impossible to eliminate the effect of the first break wave components on these shallow events. The smooth correlation of the basement reflections around 1.0-1.1 sec illustrates that the static and dynamic corrections adopted from Chevron's exploration data are quite suitable to this crustal information.

The major processing sequences on the data are:

1) Time variant bandpass filter

8-50 Hz      0-4.00 sec.

8-25 Hz      4.00-20 sec.

2) Static corrections

3) NMO corrections

4) Predictive deconvolution

50 ms. prediction distance

200 ms. operator length

5) Automatic residual static correction

6) Stack

7) Time variant bandpass filter, same as before.

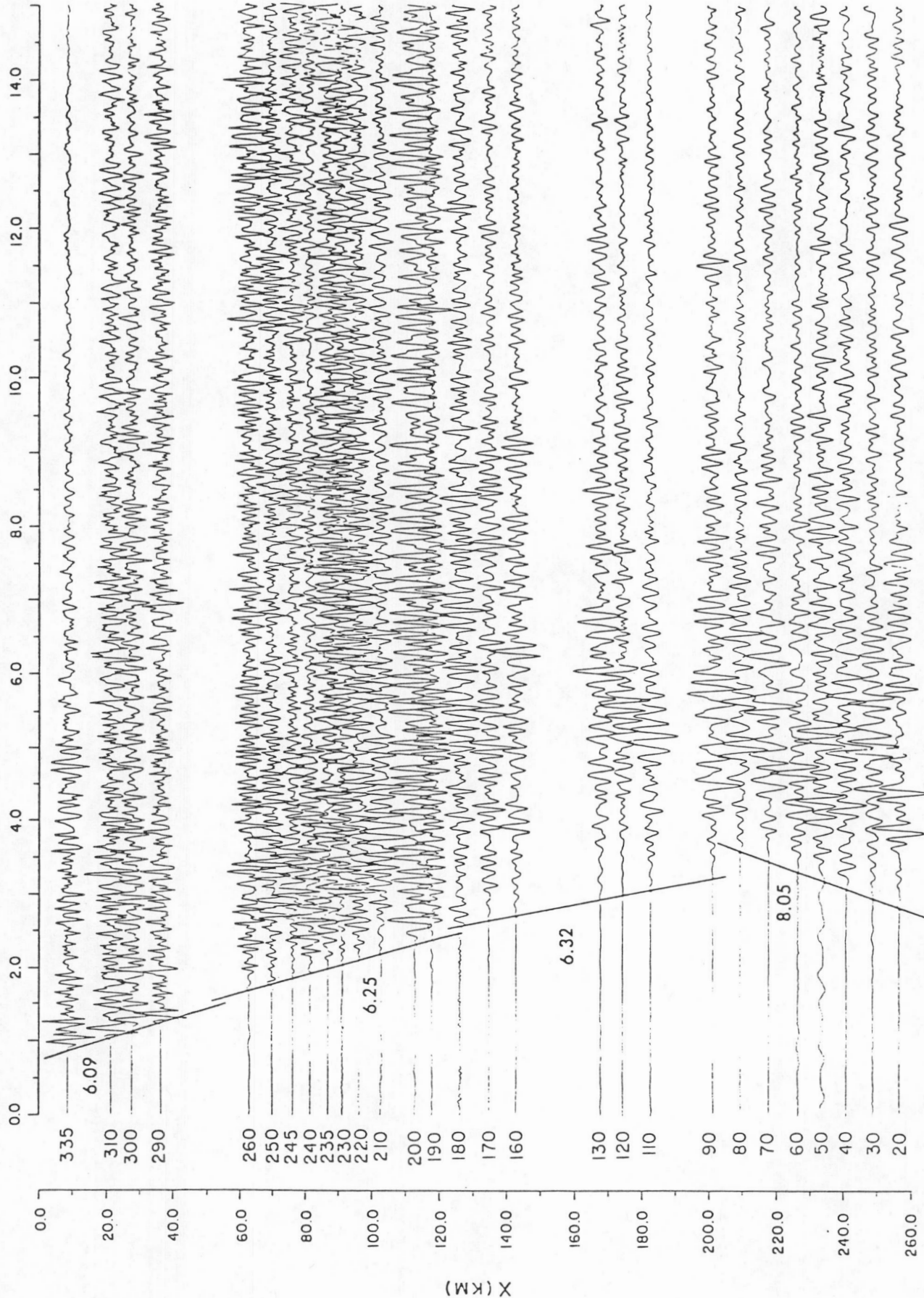
The deeper segment of the section reveals several sets of relatively continuous events. Large numbers of westerly dipping events were recognized between 4.0-10.8 sec. The origin of these arrivals requires further investigation. Some of them can be easily correlated over 10 km. Assuming normal crustal velocities in this area, they could originate from a depth of at least 12 km. They could also be

diffraction patterns or side sweeps from nearby, shallower sources. However, their visual characteristics appear to eliminate this possibility. The majority of these events appear to terminate abruptly between CDP points 91 and 117. East of this line the character of the section changes considerably. The general nature of it is not as coherent as the events to the west. On the west side of the profile again, but in deeper segments, several easterly dipping reflections are shown at 12.8 seconds to 20 seconds; some of these can also be easily correlated at a significant distance.

In general the section reveals an enormous amount of detail about the crust in this area. It shows that the crust is significantly disturbed. East of CDP point 91 the section is relatively transparent to acoustic waves. Green et al. (1979) described local magnetic and gravity anomalies in this region. It is possible that the seismic section is delineating this magnetically anomalous body. One can also postulate that the easterly termination of the dipping reflecting interfaces is the most westerly limit of the Superior Province in that area.

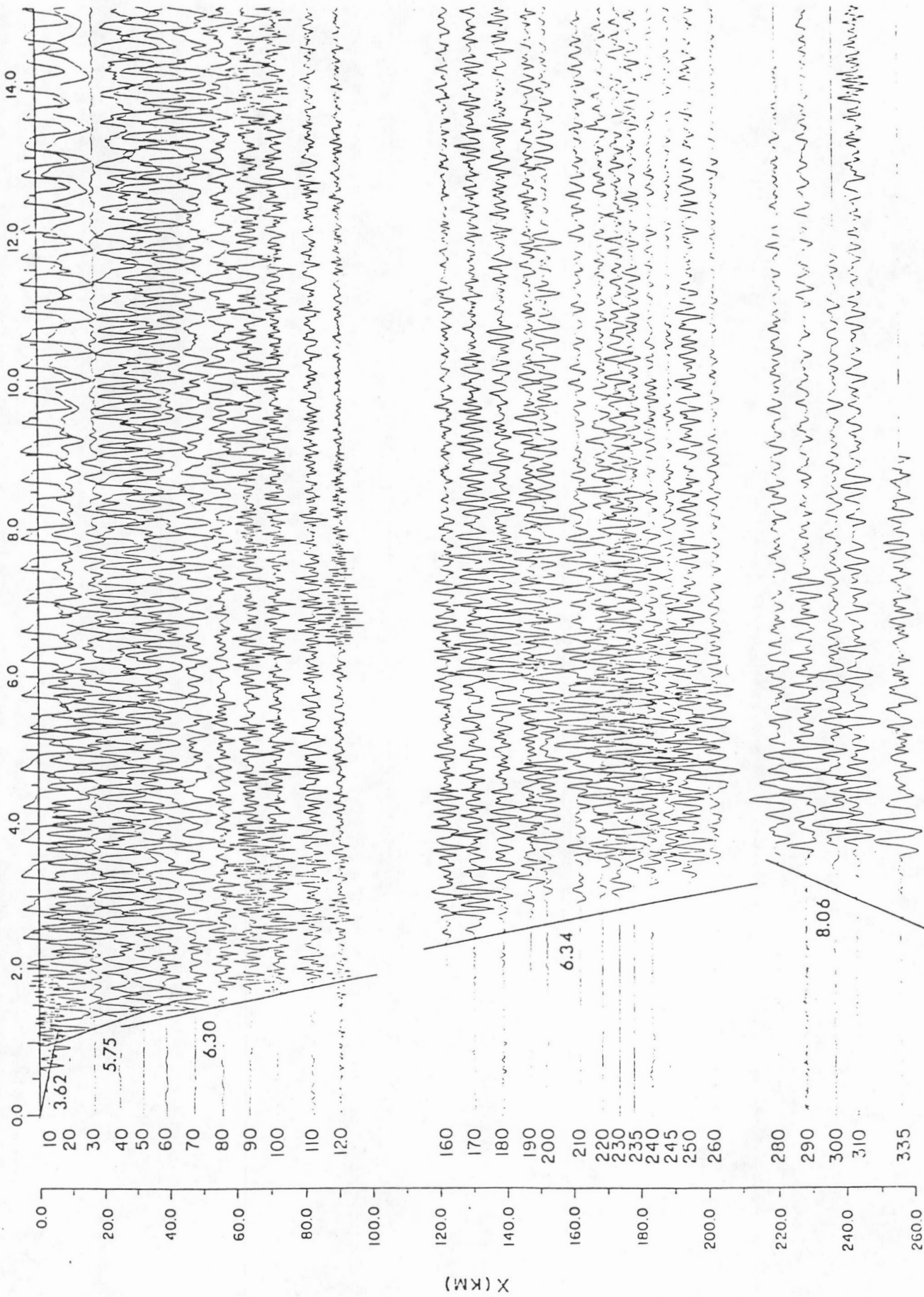
Attempts are being made for further analysis of this information. One of the first steps in this program will be migration of the data with several forms of migration algorithms. This test will very likely provide additional, perhaps convincing, evidence about the sources of these deep crustal reflection events.

T-X/6.8 (SEC)



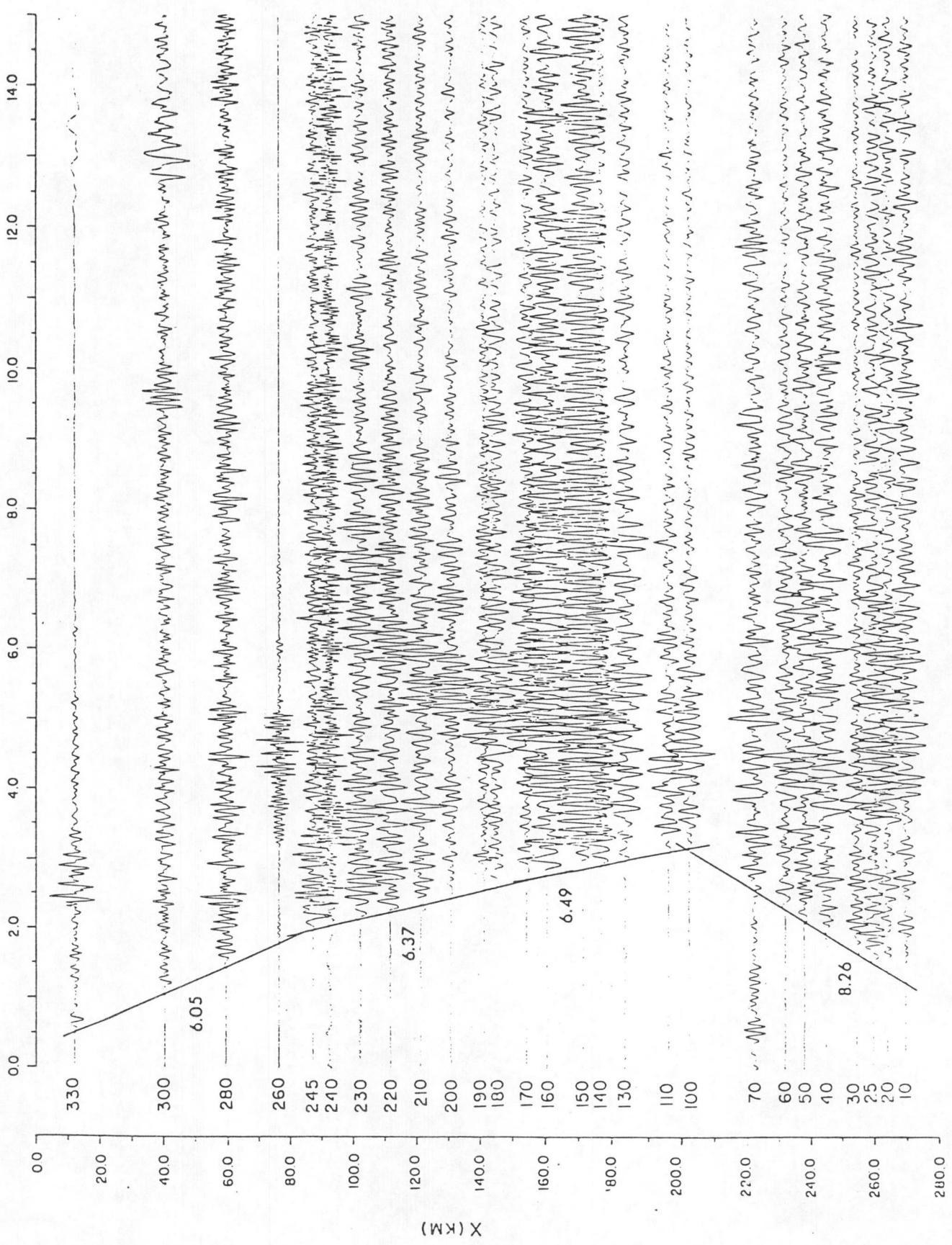
COCRUST '79 REFRACTION LINE A - NS-VERTICAL COMPONENT

T - X / 6.8 (SEC)



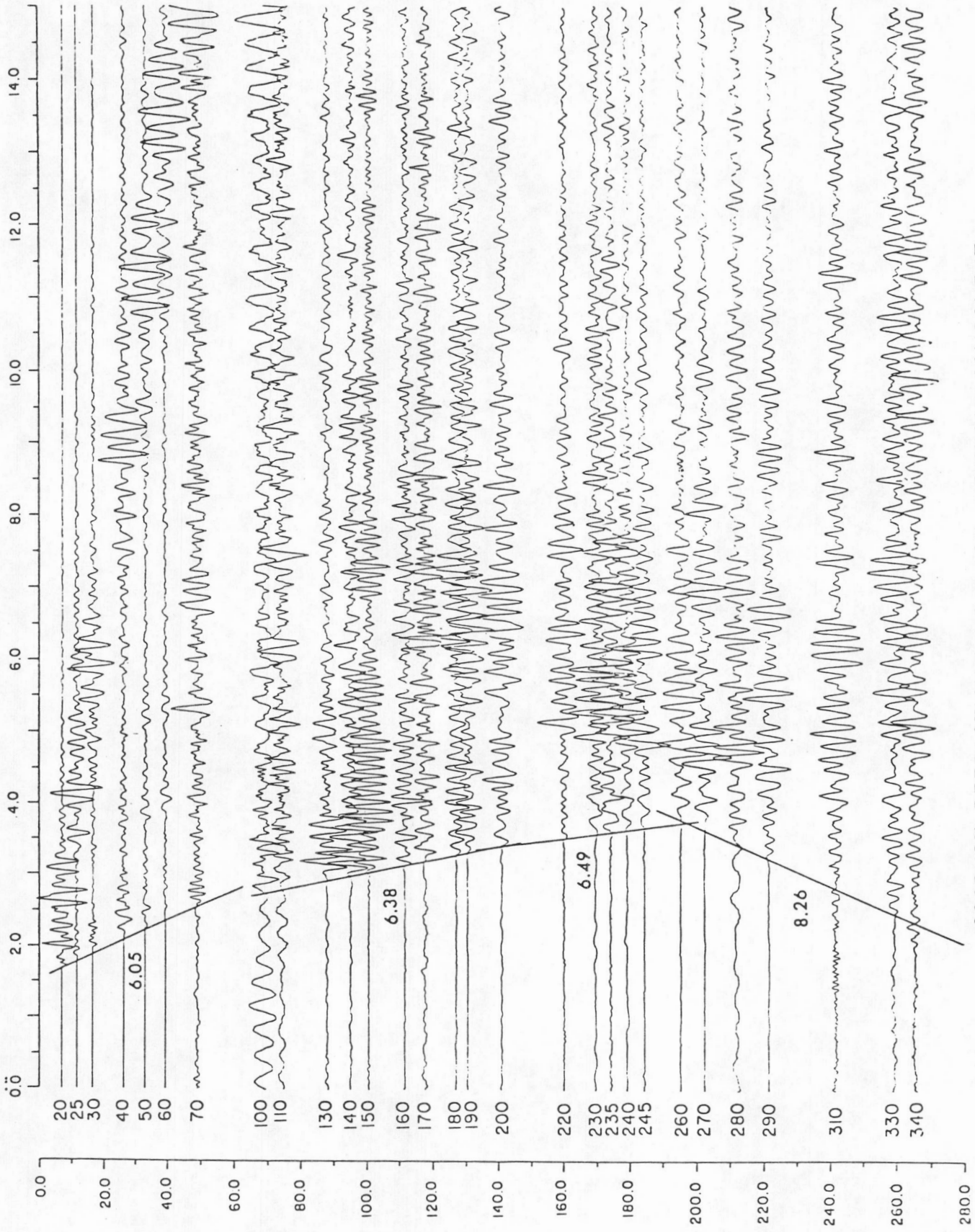
COCRUST '79 REFRACTION LINE A - SN - VERTICAL COMPONENT

T - X / 6.8 (SEC)



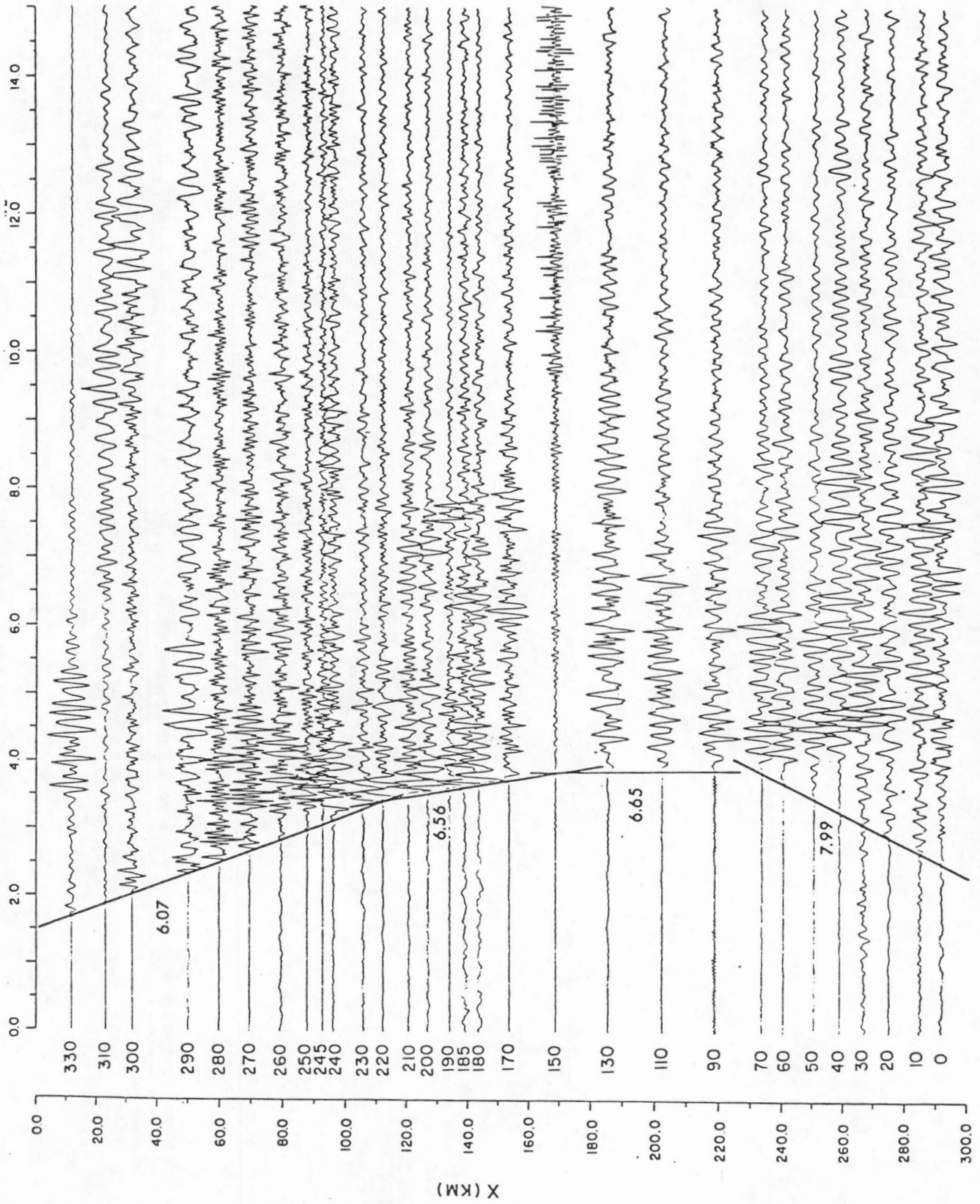
COCRUST '79 REFRACTION LINE B - NS - VERTICAL COMPONENT

T - X / 0.8 (SEC)



COCRUST REFRACTION LINE B - SN - VERTICAL COMPONENT

T - X / 6.8 (SEC)



COCRUST '79 REFRACTION LINE C - VERTICAL COMPONENT

ESC-1186-11



## REFERENCES

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