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NOTES FOR USERS OF SOFTWARE

FOR THE CANADIAN GEOMAGNETIC REFERENCE FIELD

by

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Geological Survey of Canada

Internal Report No. 90-2

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MAR - 7 1990

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INTRODUCTION

The Canadian Geomagnetic Reference Field is a mathematical model of the geomagnetic field over Canada produced by the Geophysics Division of the Geological Survey of Canada at regular intervals, normally every 2.5 years. The latest model is for epoch 1990 and is referred to as CGRF 1990. By using the CGRF a user can calculate values of magnetic declination (or any other element of the magnetic field) at any location in Canada and adjacent areas.

The CGRF actually consists of a set of spherical harmonic coefficients in conjunction with a set of spherical cap harmonic coefficients. The spherical harmonic coefficients are those of the global International Geomagnetic Reference Field 1985 (IGRF 1985) (Barraclough, 1985) and the spherical cap harmonic coefficients are those derived for the residual field relative to the IGRF 1985 evaluated at 1990. That is, the spherical cap coefficients give an estimate of the difference between the true field and the field given by the global model over the Canadian region. Mathematically, this can be expressed as follows:

$$F_{\text{resid}} = F_{\text{obs}} - F_{\text{igrf}}$$

and

$$F_{\text{schm}} = F_{\text{resid}} - F_{\text{diff}}$$

where F_{obs} is the observed field, F_{igrf} is that part of the field modelled by the IGRF, F_{resid} is the residual field relative to the IGRF, F_{schm} is that part of the residual

field modelled by the spherical cap harmonic model, and F_{diff} is the part of the residual field which cannot be calculated by the model. Adding the two fields F_{igrf} and F_{schm} gives the Canadian Geomagnetic Reference Field for 1990 (CGRF 1990):

$$F_{\text{cgrf}} = F_{\text{igrf}} + F_{\text{schm}}$$

and

$$F_{\text{obs}} = F_{\text{cgrf}} + F_{\text{diff}}$$

where F_{cgrf} is the field calculated from the Canadian Geomagnetic Reference Field.

The method of spherical cap harmonic analysis has been described by Haines (1985), and the development of the CGRF has been described by Haines and Newitt (1986) and Newitt and Haines (1989).

The IGRF coefficients are listed in Appendix 1 and the spherical cap harmonic coefficients are listed in Appendix 2. (The file of IGRF coefficients also contains coefficients for epochs back to 1945.)

DETAILS

The subroutines described in this section and listed in full in Appendix 3 use the CGRF 1990 coefficients to calculate values of magnetic declination for a given location and time. We will give only a brief description of how the different subroutines are used. A detailed description of the computer software developed for spherical cap harmonic analysis, including many of the subroutines listed here, is given by Haines (1988). We will give a

brief summary of those programs and subroutines which are necessary for the calculation of magnetic declination values.

Program DECPROG is a simple driver program which produces a list of declination and annual change values at 5 x 5 degree grid intervals over Canada. A sample output is given in the appendix so that the user may verify that his program is operating correctly. The declination values are returned by Subroutine CALDEC. Inputs to this subroutine are FLAT and FLON, the geodetic latitude and longitude in degrees; longitude is positive east and latitude is positive north. ALT is the altitude above sea level in kilometres and YEAR is the year. The valid time span of the CGRF is 1960 to 1995. If a year outside these limits is entered, the value of declination will contain extrapolation errors. The input parameter L provides the subroutine with information about the coefficients used in calculating the declination. It should be set equal to 1 for the CGRF 1990 coefficients.

The output parameters of CALDEC are D and DSV. D is the magnetic declination in degrees. DSV is the annual change in minutes per year. In both cases, a positive value is easterly, and a negative value is westerly.

Subroutine CALDEC in turn calls several other subroutines which perform the actual calculations. All these subroutines are listed in the appendix. The first calls to FIELD, SCHNEV and SPHIT (an entry point in

subroutine SPHNEWF) read the two sets of coefficients and also return FLATO, FLONO and THETA which define the pole of rotation and radius of the spherical cap. For the CGRF 1990 the pole of rotation is 65° N, 85° W, and THETA is 30°. Note that the subroutines expect to find the CGRF residual coefficients in a file named SCHCOEF.90, and the IGRF coefficients in a file named IGRF4585.BYYEAR. If the user wishes to use other names for these files, changes must be made to the OPEN statements in FIELD and SCHNEV.

Subroutine GEOCENTF converts geodetic coordinates to geocentric coordinates, and SPHNEWF rotates the coordinates to a system centered on FLATO,FLONO.

FIELD calculates the north, east and vertical components of the magnetic field using the IGRF 1985 coefficients. This is a world model of the magnetic field. If the desired location is within the spherical cap for which the CGRF is valid, SCHNEV is called after the call to FIELD. SCHNEV calculates residual values of the magnetic field using the CGRF residual coefficients. These residual values are rotated back to a geographic coordinate system by subroutine SPHNEWF (entry point SPHOLDF). They are then added to the IGRF magnetic field values to produce a more detailed description of the magnetic field over Canada than can be produced by a world model alone. GEOCINV converts geocentric values back to geodetic values. Finally, declination is calculated from the north and east components of the magnetic field. Note that two calls to SCHNEV are

made, one using YEAR and the second using YEAR + DELT, where DELT=1, so that annual change values can be determined.

If the desired location is outside the valid area of the CGRF (more than THETA degrees from FLATO,FLONO), declination values are calculated using the IGRF alone.

Users who have occasion to use components of the magnetic field other than declination, such as horizontal intensity or total intensity, may obtain them by adding the necessary code and changing the output parameters in CALDEC. Contact the authors of this report for details.

The program and subroutines just described have been written in VAX FORTRAN and have been run successfully on a VAX 11/750 and on a MicroVAX II. Users of other systems may have to make software modifications appropriate to their systems.

POINTS TO REMEMBER

- 1) Latitude and longitude must be entered in degrees. East longitude is positive, west longitude is negative.
Altitude must be in kilometers above sea level.
- 2) Outside the area for which the CGRF is valid (more than 30 degrees from 65° N, 85° W), the subroutine will return declination values calculated using the IGRF 1985.
- 3) The valid time span of the CGRF 1985 is from 1960 to 1995.
- 4) The program and subroutines have been written in VAX FORTRAN.

- 5) The files containing the CGRF and IGRF coefficients must be named SCHCOEF.90 and IGRF4585.BYYEAR respectively. If you received the software and coefficients on a floppy disk, the latter filename may have been truncated to IGRF4585.BYY by DOS. Either rename it when you transfer the program to your own computer, or change the OPEN statement in FIELD.
- 5) New versions of the CGRF will be available at least every five years and possibly more frequently. Users should check periodically on the availability of a new model.
- 6) For further information, or if problems are encountered, contact the authors at: Geophysics Division, Geological Survey of Canada, 1 Observatory Cres, Ottawa, Ont, K1A 0Y3;
phone, 613-995-5545 (LRN)
613-995-0754 (GVH).

REFERENCES

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APPENDIX 1

INTERNATIONAL REMAGNETIC REFERENCE FIELD COEFFICIENTS
1945 - 1985

10 1985.00 6371.200 6378.160 298.250IGRF 1945 TO 1985 WITH 85 TIME TERMS
 1 0 -30634.0 0.0 -30571.0 0.0 -30507.0 0.0 -30411.0
 0.0 -30334.0 0.0 -30220.0 0.0 -30100.0 0.0 -29992.0
 0.0 -29877.0 0.0 23.2 0.0
 1 1 -2240.0 5806.0 -2241.0 5807.0 -2134.0 5796.0 -2162.0
 5780.0 -2119.0 5776.0 -2068.0 5737.0 -2013.0 5675.0 -1956.0
 5604.0 -1903.0 5497.0 10.0 -24.5
 2 0 -1215.0 0.0 -1330.0 0.0 -1432.0 0.0 -1546.0
 0.0 -1662.0 0.0 -1781.0 0.0 -1902.0 0.0 -1997.0
 0.0 -2073.0 0.0 -13.7 0.0
 2 1 2972.0 -1700.0 2978.0 -1813.0 2995.0 -1896.0 3007.0
 -1948.0 2997.0 -2016.0 3000.0 -2047.0 3010.0 -2067.0 3027.0
 -2129.0 3045.0 -2191.0 3.4 -11.5
 2 2 1588.0 497.0 1579.0 388.0 1567.0 263.0 1572.0
 209.0 1594.0 114.0 1611.0 25.0 1632.0 -68.0 1663.0
 -200.0 1691.0 -309.0 7.0 -20.2
 3 0 1274.0 0.0 1293.0 0.0 1308.0 0.0 1307.0
 0.0 1297.0 0.0 1287.0 0.0 1276.0 0.0 1281.0
 0.0 1300.0 0.0 5.1 0.0
 3 1 -1833.0 -512.0 -1878.0 -485.0 -1955.0 -487.0 -1987.0
 -421.0 -2038.0 -404.0 -2091.0 -366.0 -2144.0 -333.0 -2180.0
 -336.0 -2208.0 -312.0 -4.6 5.3
 3 2 1225.0 185.0 1271.0 228.0 1293.0 235.0 1288.0
 230.0 1292.0 240.0 1278.0 251.0 1260.0 262.0 1251.0
 271.0 1244.0 284.0 -0.6 2.3
 3 3 926.0 -5.0 890.0 -67.0 897.0 -73.0 879.0
 -130.0 856.0 -165.0 838.0 -196.0 830.0 -223.0 833.0
 -252.0 835.0 -296.0 0.1 -10.8
 4 0 980.0 0.0 975.0 0.0 964.0 0.0 962.0
 0.0 957.0 0.0 952.0 0.0 946.0 0.0 938.0
 0.0 937.0 0.0 0.1 0.0
 4 1 771.0 155.0 795.0 171.0 794.0 167.0 804.0
 150.0 804.0 148.0 800.0 167.0 791.0 191.0 782.0
 212.0 780.0 233.0 -0.6 3.8
 4 2 544.0 -280.0 532.0 -306.0 510.0 -275.0 492.0
 -272.0 479.0 -269.0 461.0 -266.0 438.0 -265.0 398.0
 -257.0 363.0 -250.0 -7.8 2.2
 4 3 -408.0 -68.0 -402.0 -51.0 -392.0 -44.0 -392.0
 1.0 -390.0 13.0 -395.0 26.0 -405.0 39.0 -419.0
 53.0 -426.0 68.0 -1.4 2.5
 4 4 300.0 -158.0 310.0 -184.0 292.0 -249.0 267.0
 -254.0 252.0 -269.0 234.0 -279.0 216.0 -288.0 199.0
 -297.0 169.0 -298.0 -6.8 0.9
 5 0 -286.0 0.0 -255.0 0.0 -232.0 0.0 -236.0
 0.0 -219.0 0.0 -216.0 0.0 -218.0 0.0 -218.0
 0.0 -215.0 0.0 1.3 0.0
 5 1 341.0 -14.0 355.0 -8.0 360.0 14.0 358.0
 12.0 358.0 19.0 359.0 26.0 356.0 31.0 357.0
 46.0 356.0 47.0 0.1 0.1
 5 2 207.0 80.0 201.0 101.0 237.0 111.0 229.0
 121.0 254.0 128.0 262.0 139.0 264.0 148.0 261.0
 150.0 253.0 148.0 -1.5 -0.2

5	3	-25.0	-65.0	-3.0	-95.0	-13.0	-90.0	-34.0
-115.0	-31.0	-126.0	-42.0	-139.0	-59.0	-152.0	-74.0	
-151.0	-94.0	-155.0	-3.2	-0.1				
5	4	-156.0	-114.0	-160.0	-100.0	-176.0	-111.0	-153.0
-106.0	-157.0	-97.0	-160.0	-91.0	-159.0	-83.0	-162.0	
-78.0	-161.0	-75.0	0.1	0.6				
5	5	-88.0	83.0	-76.0	73.0	-68.0	77.0	-64.0
83.0	-62.0	81.0	-56.0	83.0	-49.0	88.0	-48.0	
92.0	-48.0	95.0	-0.1	0.0				
6	0	68.0	0.0	57.0	0.0	47.0	0.0	47.0
0.0	45.0	0.0	43.0	0.0	45.0	0.0	48.0	
0.0	52.0	0.0	1.4	0.0				
6	1	67.0	9.0	50.0	-1.0	57.0	-7.0	56.0
-13.0	61.0	-11.0	64.0	-12.0	66.0	-13.0	66.0	
-15.0	65.0	-16.0	-0.3	-0.4				
6	2	6.0	118.0	15.0	100.0	4.0	101.0	-3.0
106.0	8.0	100.0	15.0	100.0	28.0	99.0	42.0	
93.0	50.0	90.0	1.7	-1.1				
6	3	-244.0	18.0	-261.0	52.0	-250.0	46.0	-241.0
55.0	-228.0	68.0	-212.0	72.0	-198.0	75.0	-192.0	
71.0	-186.0	69.0	0.6	-0.8				
6	4	-12.0	-9.0	8.0	-7.0	12.0	-16.0	3.0
-26.0	4.0	-32.0	2.0	-37.0	1.0	-41.0	4.0	
-43.0	4.0	-50.0	0.0	-2.3				
6	5	14.0	-12.0	8.0	-17.0	13.0	-6.0	4.0
-10.0	1.0	-8.0	3.0	-6.0	6.0	-4.0	14.0	
-2.0	17.0	-4.0	0.9	-0.5				
6	6	-100.0	-42.0	-108.0	-21.0	-105.0	-21.0	-108.0
-16.0	-111.0	-7.0	-112.0	1.0	-111.0	11.0	-108.0	
17.0	-102.0	20.0	1.2	-0.1				
7	0	72.0	0.0	67.0	0.0	80.	0.0	72.0
0.0	75.0	0.0	72.0	0.0	71.0	0.0	72.0	
0.0	75.0	0.0	0.2	0.0				
7	1	-61.0	-42.0	-48.0	-44.0	-66.0	-52.0	-52.0
-53.0	-57.0	-61.0	-57.0	-70.0	-56.0	-77.0	-59.0	
-82.0	-61.0	-82.0	-0.6	0.2				
7	2	6.0	-39.0	-3.0	-18.0	2.0	-37.0	4.0
-25.0	4.0	-27.0	1.0	-27.0	1.0	-26.0	2.0	
-27.0	2.0	-26.0	-0.5	1.0				
7	3	6.0	2.0	16.0	-6.0	4.0	6.0	11.0
-8.0	13.0	-2.0	14.0	-4.0	16.0	-5.0	21.0	
-5.0	24.0	-1.0	0.8	1.1				
7	4	-44.0	-1.0	-38.0	-8.0	-46.0	-1.0	-20.0
3.0	-26.0	6.0	-22.0	8.0	-14.0	10.0	-12.0	
16.0	-6.0	23.0	1.0	1.9				
7	5	-2.0	25.0	1.0	32.0	-15.0	29.0	-4.0
28.0	-6.0	26.0	-2.0	23.0	0.0	22.0	1.0	
18.0	4.0	17.0	0.4	0.3				
7	6	18.0	-19.0	9.0	-18.0	8.0	-20.0	15.0
-16.0	13.0	-23.0	13.0	-23.0	12.0	-23.0	11.0	
-23.0	9.0	-21.0	-0.5	0.2				
7	7	27.0	-23.0	11.0	-22.0	14.0	-12.0	6.0
-18.0	1.0	-12.0	-2.0	-11.0	-5.0	-12.0	-2.0	
-10.0	0.0	-6.0	-0.1	0.9				

8	0	15.0	0.0	16.0	0.0	5.0	0.0	6.0
0.0		13.0	0.0	14.0	0.0	14.0	0.0	18.0
0.0		21.0	0.0	0.7	0.0			
8	1	5.0	-7.0	4.0	2.0	17.0	12.0	4.0
7.0		5.0	7.0	6.0	7.0	6.0	6.0	
7.0		6.0	7.0	0.0	0.1			
8	2	-12.0	9.0	-8.0	-2.0	-3.0	1.0	-3.0
-16.0		-4.0	-12.0	-2.0	-15.0	-1.0	-16.0	0.0
-18.0		0.0	-21.0	0.3	-1.0			
8	3	-21.0	0.0	-31.0	-3.0	-30.0	10.0	-13.0
5.0		-14.0	9.0	-13.0	6.0	-12.0	4.0	-11.0
4.0		-11.0	5.0	0.4	0.1			
8	4	18.0	-13.0	15.0	-7.0	14.0	-20.0	-5.0
-19.0		0.0	-16.0	-3.0	-17.0	-8.0	-19.0	-7.0
-22.0		-9.0	-25.0	-0.3	-0.8			
8	5	16.0	5.0	8.0	6.0	27.0	5.0	10.0
5.0		8.0	4.0	5.0	6.0	4.0	6.0	4.0
9.0		2.0	11.0	-0.3	0.2			
8	6	-14.0	26.0	-17.0	27.0	-15.0	34.0	-6.0
23.0		-1.0	24.0	0.0	21.0	0.0	18.0	3.0
16.0		4.0	12.0	0.1	-0.8			
8	7	1.0	1.0	7.0	-6.0	1.0	4.0	15.0
-2.0		11.0	-3.0	11.0	-6.0	10.0	-10.0	6.0
-13.0		4.0	-16.0	-0.5	-0.1			
8	8	10.0	-19.0	13.0	-22.0	12.0	-19.0	5.0
-18.0		4.0	-17.0	3.0	-16.0	1.0	-17.0	-1.0
-15.0		-6.0	-10.0	-0.8	1.3			
9	0	0.0	0.0	0.0	0.0	0.0	0.0	13.0
0.0		8.0	0.0	8.0	0.0	7.0	0.0	5.0
0.0		5.0	0.0	0.0	0.0			
9	1	0.0	0.0	0.0	0.0	0.0	0.0	5.0
-22.0		10.0	-22.0	10.0	-21.0	10.0	-21.0	10.0
-21.0		10.0	-21.0	0.0	0.0			
9	2	0.0	0.0	0.0	0.0	0.0	0.0	4.0
14.0		2.0	15.0	2.0	16.0	2.0	16.0	1.0
16.0		1.0	16.0	0.0	0.0			
9	3	0.0	0.0	0.0	0.0	0.0	0.0	-12.0
5.0		-13.0	7.0	-12.0	6.0	-12.0	7.0	-12.0
9.0		-12.0	9.0	0.0	0.0			
9	4	0.0	0.0	0.0	0.0	0.0	0.0	14.0
-5.0		10.0	-4.0	10.0	-4.0	10.0	-4.0	9.0
-5.0		9.0	-5.0	0.0	0.0			
9	5	0.0	0.0	0.0	0.0	0.0	0.0	5.0
0.0		-1.0	-5.0	-1.0	-5.0	-1.0	-5.0	-3.0
-6.0		-3.0	-6.0	0.0	0.0			
9	6	0.0	0.0	0.0	0.0	0.0	0.0	-2.0
11.0		-1.0	10.0	0.0	10.0	-1.0	10.0	-1.0
9.0		-1.0	9.0	0.0	0.0			
9	7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10.0		5.0	10.0	3.0	11.0	4.0	11.0	7.0
10.0		7.0	10.0	0.0	0.0			
9	8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.0		1.0	-4.0	1.0	-2.0	1.0	-3.0	2.0
-6.0		2.0	-6.0	0.0	0.0			

APPENDIX 2

Spherical Cap Harmonic Coefficients Used for
the Canadian Geomagnetic Reference Field 1990

65.00	-85.00	30.00	6371.2	66.3333		
1	0	0	2 16 4	0 -1		
I 0 0 0.0000	0.100000E+01	0.000000E+00	0.000000E+00	0.000000E+00		
0.805212E+03	0.000000E+00	-0.213366E+04	0.000000E+00	0.000000E+00		
-0.442117E+04	0.000000E+00	-0.231748E+04	0.000000E+00	0.000000E+00		
I 1 0 4.0837	0.100000E+01	0.393952E+01	0.000000E+00	0.000000E+00		
0.288157E+03	0.000000E+00	0.276897E+03	0.000000E+00	0.000000E+00		
-0.643388E+03	0.000000E+00	-0.480977E+03	0.000000E+00	0.000000E+00		
I 1 1 3.1196	0.253621E+01	-0.152553E+03	-0.350967E+02			
0.658761E+03	0.333090E+03	-0.169371E+03	-0.304683E+03			
0.000000E+00	-0.493076E+03	0.136406E+03	-0.159062E+03			
I 2 0 6.8354	0.100000E+01	0.000000E+00	0.000000E+00	0.000000E+00		
-0.124345E+03	0.000000E+00	-0.223119E+03	0.000000E+00	0.000000E+00		
-0.208055E+03	0.000000E+00	-0.122209E+03	0.000000E+00	0.000000E+00		
I 2 1 6.8354	0.517746E+01	0.452437E+03	0.507498E+02			
-0.291487E+03	-0.382857E+03	0.000000E+00	-0.486984E+02			
0.000000E+00	-0.133601E+03	0.123905E+02	-0.741942E+02			
I 2 2 5.4928	0.612537E+01	0.132779E+02	-0.188386E+03			
0.142083E+03	0.282898E+03	0.000000E+00	-0.175786E+03			
-0.590835E+02	0.000000E+00	0.000000E+00	0.956235E+02			
I 3 0 10.0385	0.100000E+01	0.000000E+00	0.000000E+00	0.000000E+00		
0.293542E+02	0.000000E+00	0.470950E+02	0.000000E+00	0.000000E+00		
0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00		
I 3 1 9.7121	0.721601E+01	-0.768652E+03	-0.774457E+02			
0.256738E+03	0.366483E+03	0.000000E+00	0.000000E+00	0.000000E+00		
-0.106881E+03	0.000000E+00	-0.783833E+02	0.000000E+00	0.000000E+00		
I 3 2 9.3733	0.170110E+02	-0.171574E+02	0.569208E+03			
0.000000E+00	-0.244150E+03	0.000000E+00	0.724967E+02			
0.000000E+00	-0.661285E+02	-0.340082E+01	-0.395611E+02			
I 3 3 7.7524	0.154891E+02	0.170846E+02	-0.333048E+01			
-0.187627E+03	0.749742E+02	-0.887667E+02	0.729314E+01			
0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00		
I 4 0 12.9083	0.100000E+01	0.000000E+00	0.000000E+00	0.000000E+00		
0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00		
0.144852E+02	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00		
I 4 1 12.9083	0.947928E+01	0.995386E+03	0.636325E+02			
-0.154933E+03	-0.291324E+03	0.000000E+00	0.000000E+00	0.000000E+00		
0.963486E+01	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00		
I 4 2 12.3720	0.290691E+02	0.830277E+01	-0.113427E+04			
0.000000E+00	0.248416E+03	0.000000E+00	-0.378451E+02			
0.000000E+00	0.000000E+00	0.000000E+00	0.122722E+02			
I 4 3 11.8074	0.533354E+02	-0.234119E+02	0.000000E+00			
0.122009E+03	-0.380616E+02	0.000000E+00	0.000000E+00			
0.000000E+00	0.000000E+00	0.323442E+02	0.000000E+00			
I 4 4 9.9589	0.398615E+02	0.000000E+00	-0.558992E+01			
-0.136597E+02	0.276629E+02	0.178351E+02	0.000000E+00			
0.000000E+00	-0.671208E+01	0.000000E+00	0.000000E+00			
I 5 0 16.0248	0.100000E+01	0.102724E+01	0.000000E+00			
0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00			
0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00			
I 5 1 15.8215	0.115415E+02	-0.101329E+04	-0.382369E+02			
0.750231E+02	0.191267E+03	0.000000E+00	0.000000E+00			
0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00			

I	5	2	15.6154	0.456895E+02	0.000000E+00	0.177861E+04
			0.000000E+00	-0.187180E+03	0.000000E+00	0.000000E+00
			0.115898E+02	0.000000E+00	0.137648E+02	0.000000E+00
I	5	3	14.9180	0.105995E+03	0.135495E+02	0.000000E+00
			-0.104855E+03	0.235087E+02	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	-0.260955E+02	0.000000E+00
I	5	4	14.1778	0.162625E+03	0.000000E+00	0.000000E+00
			0.247057E+02	-0.457641E+01	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	5	5	12.1334	0.103486E+03	-0.200459E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	6	1	18.9364	0.137460E+02	0.779207E+03	0.123826E+02
			-0.224413E+02	-0.857139E+02	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	6	2	18.5830	0.641554E+02	0.000000E+00	-0.217468E+04
			0.000000E+00	0.994581E+02	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	6	3	18.2219	0.190927E+03	-0.410011E+01	-0.371005E+01
			0.642951E+02	-0.944535E+01	0.000000E+00	0.000000E+00
			-0.182973E+02	0.000000E+00	0.000000E+00	0.000000E+00
I	6	4	17.3910	0.364976E+03	0.253005E+01	0.000000E+00
			-0.188470E+02	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	6	5	16.5041	0.486587E+03	0.000000E+00	0.000000E+00
			0.000000E+00	0.267181E+01	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	6	6	14.2861	0.270001E+03	0.000000E+00	-0.466811E+01
			0.000000E+00	-0.409800E+01	0.391241E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	-0.526934E+01
I	7	1	21.8702	0.158221E+02	-0.464803E+03	0.000000E+00
			0.000000E+00	0.258820E+02	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	7	2	21.7210	0.870680E+02	0.000000E+00	0.211087E+04
			0.000000E+00	-0.305952E+02	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	7	3	21.2461	0.300181E+03	0.000000E+00	0.000000E+00
			-0.247740E+02	0.000000E+00	-0.732047E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	7	4	20.7588	0.734755E+03	0.000000E+00	0.000000E+00
			0.981816E+01	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	7	5	19.8121	0.121018E+04	0.000000E+00	0.281860E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	7	6	18.7979	0.143591E+04	-0.456082E+01	0.236503E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	8	1	24.9514	0.180025E+02	0.182408E+03	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	8	2	24.6858	0.111915E+03	0.000000E+00	-0.165732E+04
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

I	8	4	23.8390	0.126951E+04	0.000000E+00	0.663180E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	8	7	21.0663	0.419235E+04	-0.134438E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	8	8	18.5472	0.185281E+04	0.000000E+00	-0.207342E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	9	1	27.8979	0.200874E+02	-0.408884E+02	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	9	2	27.7807	0.1411168E+03	0.000000E+00	0.988606E+03
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	9	4	27.0470	0.209140E+04	0.401427E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	9	5	26.3784	0.501966E+04	0.000000E+00	-0.143431E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	10	2	30.7474	0.172387E+03	0.000000E+00	-0.455496E+03
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	10	3	30.5325	0.876491E+03	0.000000E+00	-0.757373E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	10	4	30.0829	0.318566E+04	-0.259024E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	10	8	26.8711	0.384162E+05	0.155144E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	10	10	22.7683	0.127842E+05	0.000000E+00	-0.229285E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	11	0	34.0120	0.100000E+01	0.123425E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	11	2	33.8193	0.207993E+03	0.564711E+00	0.137241E+03
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	11	4	33.2235	0.471946E+04	0.000000E+00	-0.416833E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	11	9	29.1761	0.117952E+06	0.000000E+00	0.158920E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	11	10	27.7627	0.996787E+05	0.134952E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	12	1	36.9669	0.265041E+02	0.276942E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

I	12	2	36.7886	0.245582E+03	0.000000E+00	-0.218306E+02
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	12	6	35.2710	0.625103E+05	0.171012E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	12	8	33.7718	0.242271E+06	0.000000E+00	0.795277E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	12	12	26.9619	0.884337E+05	0.000000E+00	-0.310819E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	13	0	40.0102	0.100000E+01	-0.531003E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	13	4	39.3438	0.922032E+04	0.428681E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	13	6	38.4664	0.104918E+06	-0.684041E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	13	9	36.1810	0.834895E+06	-0.587816E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	13	12	32.1619	0.802105E+06	0.444168E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	1	42.9715	0.307525E+02	-0.102928E+01	-0.400819E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	3	42.6643	0.236389E+04	0.000000E+00	-0.779218E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	4	42.3494	0.123446E+05	-0.972213E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	5	42.0320	0.506746E+05	-0.409944E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	6	41.5359	0.165915E+06	0.000000E+00	0.102912E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	8	40.3169	0.100244E+07	0.000000E+00	-0.202692E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	9	39.5844	0.188373E+07	0.000000E+00	0.177718E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	12	35.9940	0.321758E+07	-0.888707E+01	-0.172721E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	14	13	34.3470	0.226154E+07	-0.104301E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

I	15	2	45.8662	0.379827E+03	-0.606618E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	4	45.4313	0.163099E+05	0.992168E+01	-0.729867E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	7	44.1294	0.751154E+06	0.527667E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	8	43.5694	0.186492E+07	0.000000E+00	0.161684E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	9	42.7989	0.381372E+07	0.000000E+00	-0.384056E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	10	42.0100	0.667923E+07	0.000000E+00	0.395886E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	11	40.9382	0.938057E+07	0.198927E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	12	39.8232	0.111063E+08	0.941816E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	13	38.2408	0.953823E+07	0.000000E+00	-0.178600E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	14	36.5239	0.635452E+07	0.000000E+00	-0.582115E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	15	15	33.2160	0.161204E+07	0.000000E+00	-0.919449E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	0	48.9749	0.100000E+01	0.307120E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	1	48.9749	0.350000E+02	0.000000E+00	0.598322E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	3	48.7056	0.350375E+04	0.000000E+00	-0.391360E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	4	48.4311	0.210193E+05	-0.452871E+01	0.121919E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	5	48.1549	0.995458E+05	0.000000E+00	0.279807E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	6	47.7278	0.380260E+06	0.000000E+00	0.281341E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	7	47.2962	0.121828E+07	0.000000E+00	0.964958E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

I	16	9	46.0801	0.742617E+07	0.000000E+00	0.269312E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	11	44.4162	0.232234E+08	-0.149749E+01	0.798591E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	12	43.2911	0.307483E+08	-0.529923E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	13	42.1198	0.345010E+08	0.000000E+00	0.185191E+01
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	14	40.4771	0.281031E+08	0.924275E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
I	16	15	38.6935	0.178002E+08	-0.107275E+01	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
			0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

APPENDIX 3

PROGRAM DECPROG

SUBROUTINE CALDEC

SUBROUTINE GEOCENF

SUBROUTINE SCHNEV

SUBROUTINE LEGFUN

SUBROUTINE FIELD

SUBROUTINE SPHENWF

```
PROGRAM DECPROG
C
C THIS PROGRAM IS A SIMPLE DRIVER PROGRAM TO CALCULATE AND LIST
C MAGNETIC FIELD VALUES
C IN ITS MOST BASIC FORM THE PROGRAM AND ITS ASSOCIATED SUBROUTINES
C FORM THE BASIC SOFTWARE WHICH IS PASSED ON TO OUTSIDE AGENCIES
C
C L.R. NEWITT FEB 23, 1989
C
C REVISED TO USE THE CGRF90 FEB 26, 1990
C
C
L=1
ALT=0.0
YEAR=1990.
DO 10 FLAT=40.,85,5
DO 10 FLON=-50.,-145.,-5.
CALL CALDEC(FLAT,FLON,ALT,YEAR,L,D,DSV)
10 PRINT 1, FLAT,FLON,YEAR,D,DSV
1 FORMAT(1H ,3F10.1,F10.2,F8.1)
STOP
END
```

```

SUBROUTINE CALDEC(FLAT,FLON,ALT,YEAR,L,D,DSV)
DATA IENTER /0/
DELT=1.
RF=6371.2
NMAX=10
IF(IENTER.NE.0)GO TO 10
IENTER=1
LF=1
CALL FIELD(DUM,DUM,DUM,DUM,NMAX,LF,DUM,DUM,DUM)
CALL SCHNEV(DUM,DUM,DUM,DUM,0,FLATO,FLONO,THETA)
CALL SPHITF(FLATO,FLONO,DUM,DUM,DUM,DUM,DUM,DUM)
TCGRF=1990.
CAPLAT=90.-THETA
10 CONTINUE
CALL GEOCENF(FLAT,ALT,DUM,DUM,GCLAT,R,DUM,DUM)
CALL SPHNEWF(GCLAT,FLON,DUM,DUM,FLATR,FLONR,DUM,DUM)
IF(FLATR.LT.CAPLAT)THEN
CALL FIELD(GCLAT,FLON,R-RF,YEAR+DELT,NMAX,LF,BN2,Y2,BV2)
CALL FIELD(GCLAT,FLON,R-RF,YEAR,NMAX,LF,BN,Y,BV)
PRINT 100
100 FORMAT(1H , 'FOLLOWING POINT OUTSIDE AREA OF CGRF; CALCULATED USING
* IGRF')
ELSE
IF(YEAR.LT.1990.)THEN
CALL FIELD(GCLAT,FLON,R-RF,TCGRF,NMAX,LF,XR,YR,ZR)
CALL SCHNEV(FLATR,FLONR,R,(YEAR+DELT)/30.,L,BNR2,BER2,BV2)
CALL SPHOLDF(DUM,DUM,BN2,BE2,DUM,DUM,BNR2,BER2)
BN2=BN2+XR
Y2=BE2+YR
BV2=BV2+ZR
CALL SCHNEV(FLATR,FLONR,R,YEAR/30.,L,BNR,BER,BV)
CALL SPHOLDF(DUM,DUM,BN,BE,DUM,DUM,BNR,BER)
BN=BN+XR
Y=BE+YR
BV=BV+ZR
ELSE
DELUP=YEAR-TCGRF
CALL FIELD(GCLAT,FLON,R-RF,TCGRF,NMAX,LF,XR,YR,ZR)
CALL SCHNEV(FLATR,FLONR,R,(TCGRF+DELT)/30.,L,BNR2,BER2,BV2)
CALL SPHOLDF(DUM,DUM,BN2,BE2,DUM,DUM,BNR2,BER2)
CALL SCHNEV(FLATR,FLONR,R,TCGRF/30.,L,BNR,BER,BV)
CALL SPHOLDF(DUM,DUM,BN,BE,DUM,DUM,BNR,BER)
BN=BN+XR
Y=BE+YR
BV=BV+ZR
BN2=BN2+XR
Y2=BE2+YR
BV2=BV2+ZR
DELBN=BN2-BN
DELY=Y2-Y
DELBV=BV2-BV
BN=DELBN*DELUP+BN

```

```
Y=DELY*DELUP+Y
BV=DELBV*DELUP+BV
BN2=DELBN+BN
Y2=DELY+Y
BV2=DELBV+BV
ENDIF
END IF
CALL GEOCINV(DUM,DUM,X2,Z2,DUM,DUM,BN2,BV2)
CALL GEOCINV(DUM,DUM,X,Z,DUM,DUM,BN,BV)
H=SQRT(X*X+Y*Y)
H2=SQRT(X2*X2+Y2*Y2)
D=0.
IF(H.NE.0.)D=ATAN2D(Y,X)
D2=0.
IF(H2.NE.0.)D2=ATAN2D(Y2,X2)
DSV=D2-D
IF(DSV.GT.180.)DSV=DSV-180.
IF(DSV.LT.-180.)DSV=DSV+360.
DSV=DSV*60./DELT
RETURN
END
```

```

SUBROUTINE GEOCENF (GDLAT,GDALT,X,Z,GCLAT,R,BN,BV)

C   CONVERT FROM GEODETIC TO GEOCENTRIC COORDINATES, AND
C   CONVERT GEODETIC COMPONENTS X,Z TO GEOCENTRIC COMPONENTS BN,BV.

C   KAULA 1964 ELLIPSOID, RECOMMENDED BY I.A.U., 1964
DATA A/6378.160/, ESQ/.00669454/

SLAT = SIND(GDLAT)
CLAT = COSD(GDLAT)
FN = A/SQRT(1.-ESQ*SLAT**2)
FNPH = FN + GDALT
WC = FNPH*CLAT
ZC = (FNPH-ESQ*FN)*SLAT
R = SQRT(WC**2+ZC**2)
IF(WC.LT.ABS(ZC))THEN
    GCLAT=ACOSD(WC/R)
    IF(ZC. LT .0.)GCLAT=-GCLAT
ELSE
    GCLAT = ASIND(ZC/R)
ENDIF
D = GDLAT - GCLAT
SD = SIND(D)
CD = COSD(D)
BN = X*CD - Z*SD
BV = X*SD + Z*CD
RETURN

C   CONVERT BACK FROM GEOCENTRIC BN,BV TO GEODETIC X,Z.
C   THIS CALL MUST FOLLOW A CALL TO GEOCENF

ENTRY GEOCINV
X = BN*CD + BV*SD
Z = BV*CD - BN*SD
RETURN

END

```

SUBROUTINE SCHNEV (FLAT,FLON,R,T,L,BN,BE,BV)

C WHEN L IS POSITIVE:
C COMPUTES SPHERICAL CAP HARMONIC (GEOCENTRIC) FIELD COMPONENTS
C HORIZONTAL NORTH BN, HORIZONTAL EAST BE, AND VERTICAL DOWNWARD BV.
C WHEN L IS NEGATIVE:
C COMPUTES GENERAL FUNCTION BV, ITS HORIZONTAL NORTH DERIVATIVE BN,
C AND ITS HORIZONTAL EAST DERIVATIVE BE, ON SPHERICAL CAP SURFACE.
C NOTE THAT THESE ARE METRICAL DERIVATIVES, AND BE IS THE
C LONGITUDINAL DERIVATIVE DIVIDED BY SIN(COLATITUDE).

C FLAT,FLON,R ARE GEOCENTRIC SPHERICAL CAP LATITUDE, LONGITUDE, RADIAL
C DISTANCE; T IS TIME.

C L = 0 ON FIRST CALL: RETURNS SPHERICAL CAP POLE POSITION FLATO,FLONO
C AND HALF-ANGLE THETA AS BN,BE, AND BV AFTER INITIALIZATION.
C ON SUBSEQUENT CALLS: ACTS AS L=1.
C 1 COMPUTES POTENTIAL FIELD COMPONENTS FROM INTERNAL COEFFICIENTS.
C 2 COMPUTES POTENTIAL FIELD COMPONENTS FROM EXTERNAL COEFFICIENTS.
C 3 COMPUTES FIELD FROM BOTH INTERNAL AND EXTERNAL COEFFICIENTS.
C -1 COMPUTES GENERAL FUNCTION BV AND DERIVATIVES BN WITH RESPECT TO
C LATITUDE AND BE WITH RESPECT TO LONGITUDE DIVIDED BY COS(LAT)
C (R IS DUMMY VARIABLE IN THIS CASE).
C NOTE: SUBROUTINE IS INITIALIZED DURING FIRST CALL REGARDLESS OF L.

C SUBPROGRAM USED: LEGFUN

PARAMETER (KDIM=16,LDIM=16) SET UP
DIMENSION FN(0:KDIM,0:KDIM), CONST(0:KDIM,0:KDIM)
DIMENSION CML(KDIM), SML(KDIM)
DIMENSION GNM(0:LDIM), HNM(0:LDIM)
DIMENSION DELT(0:LDIM)
DIMENSION BINT(0:KDIM,0:KDIM,0:LDIM), BEXT(0:KDIM,0:KDIM,0:LDIM)
CHARACTER*1 IE
DATA IENTER /0/

IF (IENTER .NE. 0) GO TO 100

IENTER = 1
C READ COEFFICIENT FILE
IT1 = 85
OPEN (UNIT=IT1,FILE='SCHCOEF.90',STATUS='OLD')
READ (IT1,240,END=999) FLATO,FLONO,THETA,RE,TZERO
READ (IT1,241,END=999) IFIT,ICEN,IREF,IB,KINT,LINT,KEXT,LEXT
240 FORMAT (F8.2,F9.2,F7.2,F8.1,F10.4)
241 FORMAT(8I5)
KMAX = MAX(KINT,KEXT)
IF (KMAX .GT. KDIM) GO TO 999
KT = MAX(LINT,LEXT)
IF (KT .GT. LDIM) GO TO 999
247 READ (IT1,250,END=280) IE,N,M,FNN,CON,(GNM(J),HNM(J),J=0,KT)
250 FORMAT (1X,A1,2I3,F9.4,E15.6,<KT+1>(E15.6,E15.6))

```

IF (N .LT. 0) GO TO 280
IF (M .LT. 0) GO TO 280
IF (N .GT. KMAX) GO TO 247
IF (M .GT. KMAX) GO TO 247
IF (IE .EQ. 'I') THEN
  IF (N .GT. KINT) GO TO 247
  LJ = LINT
ELSE
  IF (N .GT. KEXT) GO TO 247
  LJ = LEXT
END IF
FN(N,M) = FNN
CONST(N,M) = CON
IF (M .GT. 0) GO TO 300
DO 301 J=0,LJ
IF (IE .EQ. 'I') THEN
  BINT(N,M,J) = GNM(J)
ELSE
  BEXT(N,M,J) = GNM(J)
END IF
301 CONTINUE
GO TO 247
300 CONTINUE
DO 302 J=0,LJ
IF (IE .EQ. 'I') THEN
  BINT(N,M,J) = GNM(J)
  BINT(M-1,N,J) = HNM(J)
ELSE
  BEXT(N,M,J) = GNM(J)
  BEXT(M-1,N,J) = HNM(J)
END IF
302 CONTINUE
GO TO 247
280 CLOSE (UNIT=IT1,STATUS='KEEP')

IF (L .NE. 0) GO TO 100
BN = FLATO
BE = FLONO
BV = THETA
T = TZERO
RETURN

100 IF (L .GE. 0) THEN
  IF (IFIT .LT. 0) GO TO 999
  AOR = RE/R
  AR = AOR**2
  IF (L .GT. 1) GO TO 107
ELSE
  IF (IFIT .GE. 0) GO TO 999
  AR = -1.
  END IF
KT = LINT
GO TO 109

```

```

107 IF (KEXT .GT. 0) AOR3 = AOR*AR
    IF (L .GT. 2) GO TO 108
    KT = LEXT
    GO TO 109
108 KT = MAX (LINT,LEXT)
109 DELT(0) = 1.
    IF (KT .LE. 0) GO TO 103
    DEL = T - TZERO
    DO 102 I=1,KT
102 DELT(I) = DELT(I-1)*DEL
103 X = 0.
    Y = 0.
    Z = 0.
    IF (L .EQ. 2) GO TO 106
    IF (KINT .LT. 0) GO TO 106
    GTI = 0.
    DO 105 I=0,LINT
105 GTI = GTI + BINT(0,0,I)*DELT(I)
    Z = -AR*GTD
106 COLAT = 90. - FLAT
    DO 150 N=1,KMAX
    IF (N .GT. 1) GO TO 115
    CL = COSD(FLON)
    SL = SIND(FLON)
    CML(1) = CL
    SML(1) = SL
    GO TO 120
115 SML(N) = SL*CML(N-1) + CL*SML(N-1)
    CML(N) = CL*CML(N-1) - SL*SML(N-1)
120 CONTINUE
    DO 150 M=0,N
    IF (IB .EQ. 2) GO TO 121
    NMM = N - M
    IF ((NMM/2)*2 .NE. NMM) GO TO 150
121 FFN = FN(N,M)
    CALL LEGFUN (M,FFN,CONST(N,M),COLAT,P,DP,PMS,0)
    IF (L .GE. 0) THEN
        AR = AOR**(FFN+2.)
    ELSE
        AR = 1.
        FFN = -2.
        DP = -DP
        PMS = -PMS
        END IF
    IF (M .NE. 0) GO TO 130
    BT1 = 0.
    BT3 = 0.
    BT = 0.
    IF (L .EQ. 2) GO TO 123
    IF (N .GT. KINT) GO TO 123
    GTI = 0.
    DO 122 I=0,LINT
122 GTI = GTI + BINT(N,M,I)*DELT(I)

```

```

BT1 = AR*GTI
BT3 = BT1
123 IF (L .LE. 1) GO TO 125
    IF (N .GT. KEXT) GO TO 125
    GTE = 0.
    DO 124 I=0,LEXT
124 GTE = GTE + BEXT(N,M,I)*DELT(I)
    BT = AOR3/AR*GTE
    BT1 = BT1 + BT
125 X = X + BT1*DP
    Z = Z - (FFN*(BT3-BT)+BT3)*P
    GO TO 150
130 BT1 = 0.
    BT2 = 0.
    BT3 = 0.
    BT = 0.
    IF (L .EQ. 2) GO TO 133
    IF (N .GT. KINT) GO TO 133
    GTI = 0.
    HTI = 0.
    DO 132 I=0,LINT
        GTI = GTI + BINT(N,M,I)*DELT(I)
132 HTI = HTI + BINT(M-1,N,I)*DELT(I)
    BT1 = AR*(GTI*CML(M) + HTI*SML(M))
    BT2 = AR*(GTI*SML(M) - HTI*CML(M))
    BT3 = BT1
133 IF (L .LE. 1) GO TO 135
    IF (N .GT. KEXT) GO TO 135
    GTE = 0.
    HTE = 0.
    DO 134 I=0,LEXT
        GTE = GTE + BEXT(N,M,I)*DELT(I)
134 HTE = HTE + BEXT(M-1,N,I)*DELT(I)
    RA = AOR3/AR
    BT = RA*(GTE*CML(M) + HTE*SML(M))
    BT1 = BT1 + BT
    BT2 = BT2 + RA*(GTE*SML(M) - HTE*CML(M))
135 X = X + BT1*DP
    Y = Y + BT2*PMS
    Z = Z - (FFN*(BT3-BT)+BT3)*P
150 CONTINUE
    BN = X
    BE = Y
    BV = Z
    RETURN

999 STOP
END

```

```

SUBROUTINE LEGFUN (M,FN,CONST,COLAT,P,DP,PMS,IPRT)

C      SERIES FORM FOR ASSOCIATED LEGENDRE FUNCTION P, ITS DERIVATIVE DP,
C      AND THE FUNCTION PMS=P*M/SIN(COLAT), IN POWERS OF (1-COS(COLAT))/2.
C      INTEGRAL ORDER M, REAL DEGREE FN, NORMALIZING CONSTANT CONST.
C      COLATITUDE COLAT IN DEGREES.
C      IPRT = 0      NO PRINT-OUT
C                  1      PRINT PARAMETERS AND P SERIES
C                  2      PRINT PARAMETERS AND DP SERIES
C                  3      PRINT PARAMETERS AND BOTH P AND DP SERIES
C                 -1      PRINT PARAMETERS ONLY
C      INPUT M,FN,CONST,COLAT,IPRT.    OUTPUT P,DP,PMS.
C      REAL*8  FNN,AL,DX,A,B,PNM,DPNM

PARAMETER (JMAX=60)
DIMENSION AM(JMAX), BM(JMAX)

IF (COLAT .LT. 60.) THEN
    X = SIND(COLAT/2.)**2
    C = 1. - 2.*X
ELSE
    C = COSD(COLAT)
    X = (1. - C)/2.
    END IF
S = SIND(COLAT)
FNN = FN*(FN+1.)
IF (M .GT. 1) GO TO 20
IF (M .LT. 0) STOP
AL = CONST
GO TO 50
20 AL = CONST*S** (M-1)

50 PNM = AL
DPNM = 0.
DX = X
J = 0

100 J = J + 1
JPM = J + M
B = AL*((JPM-1)-FNN/JPM)
DPNM = DPNM + B
A = (B*DX)/J
PNM = PNM + A
AL = A

C      STORE P OR DP SERIES FOR PRINTOUT.
IF (IPRT .LE. 0) GO TO 150
IF (IPRT .EQ. 2) GO TO 145
AM(J) = A
IF (IPRT .EQ. 1) GO TO 150
145 BM(J) = B

```

```

C      CHECK FOR TERMINATION OF SERIES.
150 ABSA = ABS(A)
      ABSB = ABS(B)
      IF (ABSB .GE. 1.E-7) GO TO 160
      IF (ABSA .LT. 1.E-7) GO TO 110
160 IF (ABSB .GE. 1.E+26) GO TO 105
      IF (ABSA .GE. 1.E+26) GO TO 105
C      CHANGE CHECK LIMITS ACCORDING TO ACCURACY DESIRED AND ACCORDING
C      TO WORD SIZE OF COMPUTER.
C      FOR 32-BIT WORD, DOUBLE PRECISION, E-7 AND E+9 GIVE 7 DIGITS ACCURACY.
C      FOR 60-BIT WORD, DOUBLE PRECISION, E-7 AND E+22 GIVE 7 DIGITS ACCURACY.
C      FOR 60-BIT WORD, SINGLE PRECISION, E-7 AND E+7 GIVE 7 DIGITS ACCURACY.
C      (DOUBLE OR SINGLE PRECISION REFER TO FNN,AL,A,B,PNM,DPNM)
      IF (J .LT. JMAX) GO TO 100
C      CONVERGENCE SLOW OR JMAX TOO SMALL
105 CONTINUE
C      NUMERICAL ERROR UNACCEPTABLY LARGE DUE TO ADDING OF
C      LARGE AND SMALL NUMBERS.
      PRINT 108, M,FN,CONST,J,A,B
108 FORMAT (//12H ** ERROR **/1X,I5,F10.5,E15.7,I5,2D15.7)
      STOP

C      SERIES TRUNCATED SUCCESSFULLY.
110 PS = PNM
      DPS = DPNM
      IF (M .NE. 0) GO TO 115
      PMS = 0.
      P = PS
      DP = DPS*S/2.
      GO TO 120
115 PMS = PS*M
      P = PS*S
      DP = DPS*S*S/2. + C*PMS
120 CONTINUE

C      PRINT TERMS OF SERIES
      IF (IPRT .EQ. 0) RETURN
      PRINT 125, M,FN,CONST,COLAT,P,DP,PMS,J
125 FORMAT (/1X,I5,F10.5,E20.12,F10.2,3F25.14,I5)
      IF (IPRT .LT. 0) RETURN
      IF (IPRT .EQ. 2) GO TO 135
      PRINT 130, (AM(I),I=1,J)
130 FORMAT (1X,16E8.1)
      IF (IPRT .EQ. 1) RETURN
135 PRINT 130, (BM(I),I=1,J)
      RETURN
      END

```

```

SUBROUTINE FIELD (DLAT,DLONG,ALT,TM,NMAX,L,BN,BE,BV)

C      GEOMAGNETIC FIELD COMPONENTS X,Y,Z, IN GAMMAS.
C      USES ANY SET OF COEFFICIENTS.
C      L POSITIVE READS A NEW SET OF COEFFICIENTS.
C

C*****MODIFIED TO CALCULATE VALUES INTERPOLATING BETWEEN DGRF MODELS
C FROM 1945 TO 1985
C VALUES FROM 1985 TO 1995 ARE CALCULATED USING IGRF TIME TERMS
C*****DEGREE10

PARAMETER (ND=11)                                     DEGREE10
DIMENSION P(ND,ND),G(ND,ND,9),H(ND,ND,9),DP(ND,ND),CONST(ND,ND),
*      SP(ND),CP(ND),SHMIT(ND,ND),GT(ND,ND),HT(ND,ND),
*      GTT(ND,ND),HTT(ND,ND),TG(ND,ND),TH(ND,ND),FM(ND),FN(ND)
DIMENSION AID(4), GGNM(9), HNNM(9)
DATA P(1,1)/0./

IF (P(1,1) .EQ. 1.) GO TO 9
P(1,1)=1.
IT = 75                                         TAPE 75
NDIM = ND
DP(1,1)=0.
SP(1)=0.
CP(1)=1.
RAD=57.295779513
SHMIT(1,1)=-1.
FM(1) = 0.
DO 20 N=2,NDIM
SHMIT(N,1)=SHMIT(N-1,1)*FLOAT (2*N-3)/FLOAT (N-1)
FN(N)=N
FM(N) = N - 1
J=2
DO 20 M=2,N
SHMIT(N,M)=SHMIT(N,M-1)*SQRT (FLOAT ((N-M+1)*J)/FLOAT (N+M-2))
20 J=1
DO 4 N=3,NDIM
NM2 = N-2
DO 4 M=1,NM2
4 CONST(N,M)=FLOAT ((N-2)**2-(M-1)**2)/FLOAT ((2*N-3)*(2*N-5))

9 IF (L .EQ. 0) GO TO 15
IF (L .LT. 0) GO TO 33
C COEFFICIENTS ARE FOR GEOCENTRIC COORDINATES
OPEN(UNIT=IT,FILE='IGRF4585.BYYEAR',STATUS='OLD')
READ (IT,27) J,K,TZERO,RE,A,FLAT,(AID(I),I=1,4)           TAPE 75
27 FORMAT (2I1,F8.2,3F10.3,4A10)

C      J      - ZERO IF COEFFICIENTS ARE FOR OBLATE EARTH
C                  - NON-ZERO IF COEFFICIENTS ARE FOR SPHERICAL EARTH.
C      K      - ZERO IF COEFFICIENTS ARE SCHMIDT NORMALIZED

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C          - NON-ZERO IF GAUSS NORMALIZED.
C      TZERO  - EPOCH YEAR OF COEFFICIENTS.
C      RE    - RADIUS OF EQUIVALENT SPHERICAL EARTH USED IN DERIVING
C                  THE COEFFICIENTS.
C      A     - SEMI-MAJOR AXIS OF GEODETIC ELLIPSOID.
C      FLAT  - FLATTENING OF ELLIPSOID.
C      AID   - IDENTIFICATION (MAXIMUM 40 CHARACTERS)

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```

MAXN=0
TEMP=0.
IF (J .NE. 0) GO TO 25
FLAT= 1.-1./FLAT
A2=A**2
A4=A**4
B2=(A*FLAT)**2
A2B2=A2*(1.-FLAT**2)
A4B4=A4*(1.-FLAT**4)
25 READ (IT,2) N,M,((GGNM(I),HHNM(I)),I=1,9),GTNM,HTNM           TAPE 75
2 FORMAT (2I5,20F10.1)
IF (N .LE. 0)      GO TO 3
IF (N .LT. NDIM)   GO TO 7
GO TO 25
7 N=N+1
M=M+1
MAXN= MAXO (N,MAXN)
DO 47 JK=1,9
G(N,M,JK)=GGNM(JK)
47 H(N,M,JK)=HHNM(JK)
GT(N,M)=GTNM
HT(N,M)=HTNM
TEMP=AMAX1(TEMP,ABS (GTNM))
GO TO 25
3 CONTINUE
IF (NMAX .LT. MAXN) GO TO 17
MAXNM1 = MAXN-1
STOP
17 IF (TEMP .NE. 0) GO TO 29
L = -L
GO TO 30
29 L=0
30 IF (K .NE. 0) GO TO 16
DO 32 N=2,MAXN
DO 32 M=1,N
DO 232 KK=1,9
G(N,M,KK)=G(N,M,KK)*SHMIT(N,M)
H(N,M,KK)=H(N,M,KK) *SHMIT(N,M)
232 CONTINUE
GT(N,M)=GT(N,M)*SHMIT(N,M)
32 HT(N,M)=HT(N,M)*SHMIT(N,M)
15 IF (TM .EQ. TLAST) GO TO 33
16 T=TM-TZERO
IF(TM.GE.TZERO)THEN
DO 22 N=2,MAXN

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DO 22 M=1,N
TG(N,M)=G(N,M,9)+T *GT(N,M)
TH(N,M)=H(N,M,9)+T *HT(N,M)
22 CONTINUE
ELSE
KT=T/5
DELT=(T-KT*5.)/5.
KKT=KT+9
DO 222 N=2,MAXN
DO 222 M=1,N
TG(N,M)=G(N,M,KKT)+DELT*(G(N,M,KKT)-G(N,M,KKT-1))
222 TH(N,M)=H(N,M,KKT)+DELT*(H(N,M,KKT)-H(N,M,KKT-1))
ENDIF
TLAST=TM

33 RLAT=DLAT/RAD
SINLA=SIN (RLAT)
RLONG=DLONG/RAD
CP(2)=COS (RLONG)
SP(2)=SIN (RLONG)
NMAXP1=NMAX+1
DO 10 M=3,NMAXP1
SP(M)=SP(2)*CP(M-1)+CP(2)*SP(M-1)
10 CP(M)=CP(2)*CP(M-1)-SP(2)*SP(M-1)
IF (J .EQ. 0) GO TO 59
R = RE + ALT
CT=SINLA
GO TO 21
59 SINLA2=SINLA*SINLA
DEN2=A2-A2B2*SINLA2
DEN=SQRT (DEN2)
COSLA = SQRT(1.-SINLA2)
IF (COSLA .NE. 0.) GO TO 18
THETA = 90./RAD
IF (SINLA .LT. 0.) THETA = -THETA
GO TO 19
18 ALTDEN = ALT*DEN
THETA = ATAN((ALTDEN+B2)/(ALTDEN+A2)*SINLA/COSLA)
19 R=SQRT (ALT*(ALT+2.*DEN)+(A4-A4B4*SINLA2)/DEN2)
CT=SIN (THETA)
21 STST = 1. - CT**2
ST = SQRT(STST)
CTST = CT*ST
AOR = RE/R
AR=AOR*AOR
BN=0.
BE=0.
BV=0.
DO 54 N=2,NMAXP1
SUMN=0.
SUME=0.
SUMV=0.
AR=AOR*AR

```

```

IF (N .GE. 3) GO TO 60
P(2,2) = 1.
DP(2,2) = CT
GO TO 61
60 P(N,N) = ST* P(N-1,N-1)
DP(N,N) = ST*DP(N-1,N-1) + CTST*P(N-1,N-1)
61 FACT = ST
DO 45 M=1,N
TEMP = TG(N,M)*CP(M) + TH(N,M)*SP(M)
IF (M .EQ. 2) FACT = STST
IF (M .LE. N-2) GO TO 12
IF (N .EQ. M) GO TO 13
P(N,M) = CT* P(N-1,M)
DP(N,M) = CT*DP(N-1,M) - FACT*P(N-1,M)
GO TO 13
12 P(N,M) = CT* P(N-1,M) - CONST(N,M)* P(N-2,M)
DP(N,M) = CT*DP(N-1,M) - CONST(N,M)*DP(N-2,M) - FACT*P(N-1,M)
13 SUMN = SUMN - DP(N,M)*TEMP
IF (M .EQ. 1) GO TO 45
SUME = SUME + P(N,M)*FM(M)*(-TG(N,M)*SP(M)+TH(N,M)*CP(M))
TEMP = TEMP*ST
45 SUMV = SUMV + P(N,M)*TEMP
BN = BN + SUMN*AR
BE = BE + SUME*AR
54 BV = BV + SUMV*AR*FN(N)
IF (J .NE. 0) GO TO 23
C      TRANSFORMS FIELD TO GEODETIC DIRECTIONS
SIND=SIN (RLAT-THETA )
COSD=SQRT (1.0-SIND*SIND)
TN=BN
BN=BN*COSD+BV*SIND
BV=BV*COSD-TN*SIND
23 RETURN
END

```

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SUBROUTINE SPHNEWF (FLAT1,FLON1,X1,Y1,FLAT2,FLON2,X2,Y2)

C   SUBROUTINE FOR TRANSFORMING GEOGRAPHIC COORDINATES (FLAT1,FLON1)
C   TO SPHERICAL COORDINATES (FLAT2,FLON2) ABOUT A NEW POLE (FLATO,FLONO).
C   FIELD COMPONENTS GEOGRAPHIC NORTH X1 AND EAST Y1 ARE ROTATED TO
C   NORTH X2 AND EAST Y2 IN THE NEW COORDINATE SYSTEM.
C   FLON2 = 0 IS THE MERIDIAN THROUGH THE SOUTH GEOGRAPHIC POLE.
C   ENTER NEW POLE BY CALLING EITHER SPHINF OR SPHITF.
C   DATA    FLATO/90./

IF (FLATO .LT. 90.) GO TO 100
FLAT2 = FLAT1
FLON2 = FLON1
GO TO 105
100 IF (FLATO .GT. -90.) GO TO 101
FLAT2 = -FLAT1
FLON2 = -FLON1
GO TO 107

101 IF (FLAT1 .LT. 90.) GO TO 102
131 FLAT2 = FLATO
FLON2 = 180.
ANG = FLONO-FLON1+180.
GO TO 103
102 IF (FLAT1 .GT. -90.) GO TO 104
132 FLAT2 = -FLATO
FLON2 = 0.
ANG = FLON1-FLONO
103 COSROT = COSD(ANG)
SINROT = SIND(ANG)
GO TO 225
104 DFLAT1 = FLAT1
SIN1 = SIND(DFLAT1)
COS1 = COSD(DFLAT1)
IF (COS1 .NE. 0.) GO TO 133
IF (SIN1 .GT. 0.) GO TO 131
GO TO 132
133 FLOND1 = FLON1 - FLONO
COSD1 = COSD(FLOND1)
SIN2 = SIN0*SIN1 + COS0*COS1*COSD1
IF (SIN2 .LT. 1.) GO TO 106
108 FLAT2 = 90.
FLON2 = 0.
105 X2 = X1
Y2 = Y1
COSROT = 1.
SINROT = 0.
RETURN
106 IF (SIN2 .GT. -1.) GO TO 110
109 FLAT2 = -90.
FLON2 = 0.

```

```

107 X2 = -X1
Y2 = -Y1
COSROT = -1.
SINROT = 0.
RETURN
110 DFLAT2 = ASIND(SIN2)
FLAT2 = DFLAT2
COS2 = COSD(DFLAT2)
IF (COS2 .NE. 0.) GO TO 111
IF (SIN2 .GT. 0.) GO TO 108
GO TO 109

111 PROD = SINO*SIN2
SIND1 = SIND(FLOND1)
IF (SIN1 .NE. PROD) GO TO 120
IF (SIND1 .GT. 0.) GO TO 115
112 FLON2 = -90.
SLON2 = -1.
GO TO 200
115 FLON2 = 90.
SLON2 = 1.
GO TO 200
120 SLON2 = (SIND1*COS1)/COS2
IF (SLON2 .LE. -1.) GO TO 112
IF (SLON2 .GE. 1.) GO TO 115
IF (SIN1 .LT. PROD) GO TO 125
FLON2 = 180. - ASIND(SLON2)
IF (FLON2 .GT. 180.) FLON2 = FLON2 - 360.
GO TO 200
125 FLON2 = ASIND(SLON2)

200 COSROT = (SINO-SIN1*SIN2)/COS1/COS2
SINROT = COSO*SLON2/COS1
225 X2 = X1*COSROT - Y1*SINROT
Y2 = X1*SINROT + Y1*COSROT
RETURN

C      TRANSFORM BACK FROM ROTATED COMPONENTS X2,Y2
C              TO GEOGRAPHIC COMPONENTS X1,Y1.

ENTRY SPHOLDF
X1 = X2*COSROT + Y2*SINROT
Y1 = Y2*COSROT - X2*SINROT
RETURN

C      INPUT NEW POLE POSITION FLATO,FLONO IN GEOGRAPHIC COORDINATES.
C      RETURN FLATO,FLONO AS FLAT1,FLON1.

ENTRY SPHINF
READ 10, FLATO,FLONO
10 FORMAT (2F10.0)
FLAT1 = FLATO
FLON1 = FLONO

```

GO TO 20

C DEFINE NEW POLE POSITION THROUGH CALL PARAMETERS FLAT1,FLON1.

ENTRY SPHITF
FLATO = FLAT1
FLONO = FLON1
20 CONTINUE
DFLATO = FLATO
SINO = SIND(DFLATO)
COSO = COSD(DFLATO)
RETURN

END