ENVIRONMENT CANADA CONSERVATION AND PROTECTION ENVIRONMENTAL PROTECTION PACIFIC AND YUKON REGION NORTH VANCOUVER, B.C.

BASELINE MONITORING

SNIP PROJECT

- July 21, 1990 -

Data Report DR 91-04

By Benoit Godin and Gerry Mitchell

August 1991

LIBRARY ENVIRONMENT CANADA CONSERVATION AND PROTECTION PACIFIC REGION

## TABLE OF CONTENTS

PAGE

| TABLE OF CONTENTS    | i          |
|----------------------|------------|
| INTRODUCTION         | _ <b>1</b> |
| MATERIAL AND METHODS | 3          |
| RESULTS              | 4          |
| REFERENCES           | 19         |

### INTRODUCTION

The Snip project is located at the confluence of the Iskut River and Bronson Creek. The mine is situated at an elevation of 180 to 680 metres on the north-west side of base of Johnny Mountain. The Snip property is drained by Monsoon Creek flowing northwardly towards the Iskut River. Dolly Varden char and Cutthroat trout are present in Monsoon Lake. Sockeye is known to spawning at the mouth of Bronson Creek and in the side channels in front of the Bronson Creek airstrip. There is no suitable fish habitat upstream of the Cominco property since the creek is characterised by a single channel with fast flows, large boulder and cascading falls. Salmon are utilising the lower 1 km of Sky Creek draining the west part of the property to the north west towards the Craig River. Small runs of chinook, pink and sockeye as well as cutthroat trout were identified (Figure 1).

The company is developing an underground mine. The gold and silver extraction will be performed by flotation. The tailings will be discharged in the tailings pond located in the headwaters of Monsoon Creek and Sky Creek.

### Site Description

| Station | Location   | Remarks                |
|---------|--|------------------------|
| 1       | Sky Creek at the mouth                           | Tea colour waters      |
| 2       | Bronson Creek upstream<br>of Cominco camp        | Influenced by glaciers |
| 3       | Monsoon Creek downstream                         | Tea colour waters      |
| 4       | Iskut River upstr <b>eam</b><br>of Bronson Creek | Influenced by glaciers |
| 5       | Iskut River downstream<br>of Monsoon Creek       | Influenced by glaciers |
| 6       | Mine adit  | Level 130              |
| 7       | Mine adit  | Level 180              |
| 8       | Mine adit  | Level 300              |

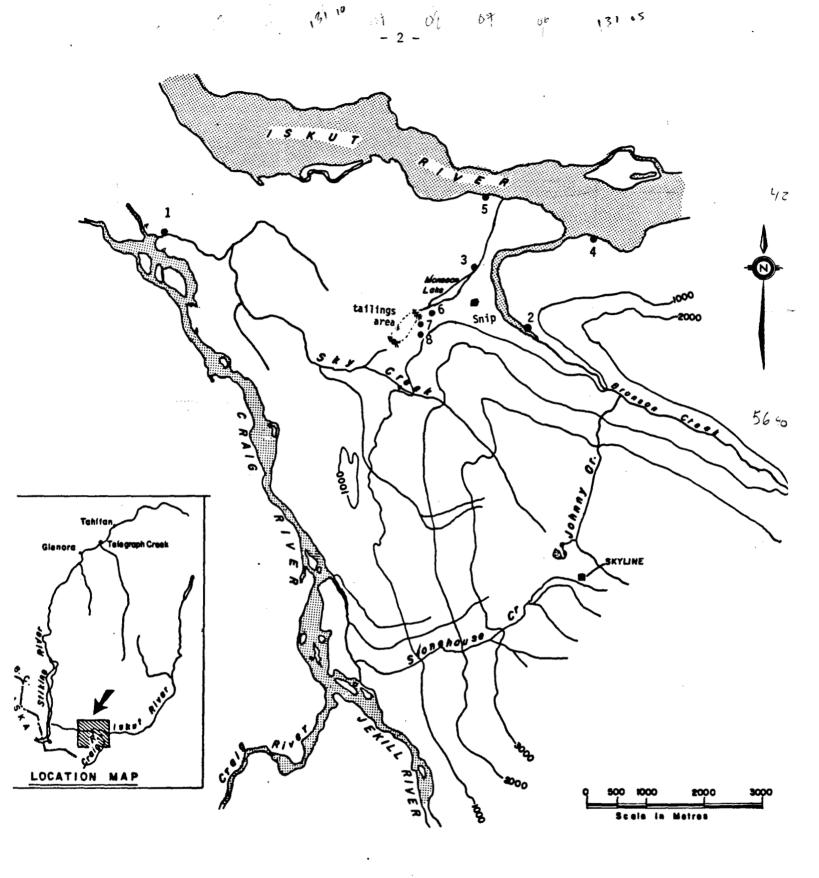


FIGURE 1 Snip Project - Sampling Sites

### MATERIAL AND METHODS

The site was visited on July 30, 1990. No flow measurements were taken at the sites. Water chemistry and sediment samples were collected at the six receiving water stations but only water at the mine adit. The following chemical parameters were analysed: alkalinity, pH, filterable residue, non-filterable residue, and sulphate. These samples were kept cool with ice until analysed. Dissolved metals were filtered the same day through a 0.45 micron cellulose nitrate membrane filter. Total and dissolved metals were preserved with nitric acid (0.5 ml/100 ml of sample). All samples were collected with clean polyethylene bottles. The bottles for metal samples were previously acid washed. The hardness was determined from the dissolved metal sample.

Inductively Coupled Argon Plasma (ICAP) was used for the total and dissolved metal analysis and gave a reading of twenty-eight metals. For copper, the samples were reanalysed with the graphite furnace when the values were below two times the detection limit on the ICAP procedure. For analytical method details, refer to the Environment Canada Pacific Region Laboratory Manual (Anon, 1979).

Sediment samples were collected from the streambed, below the water level, with a clean acrylic corer. Four replicates were taken at each sites, except for stations 6, 7 and 8. The samples were transferred into kraft bags and kept cool until analysed. The samples were air dried, sieved to <150 um, digested with aqua regia, and analysed for heavy metals using ICAP. A portion of the sediments were also ignited at 550° C in a muffle furnace. The loss of weight was reported as volatile residue and the remaining residue was reported as fixed residue. Statistical analysis consisted of averages and standard deviation for the water quality data and one way analysis of variance was performed on selected sediment data. The ANOVA was performed on a Hewlett Packward Model 9826. Multiple comparison procedures using the Tukey's harmonic significant differences were used to produce the various plots. Contaminants with values below the detection limit were used as equal to the detection limit. However stations with standard deviations equal to zero were given some lower value in order to introduce variability. A standard deviation equal to zero introduced an error in the Tukey's separation procedure. Such modification of the sediment data was necessary for cadmium at station 4 and mercury at station 3. Figure 2 shows the multiple comparison plots for sediment quality stations. the metal analysed are Al, Ca, Cd, Cu, Hg, Fe, Mn, Pb and Zn.

### RESULTS

The water metal results can be found in Table 1, while the other water quality results are found in Table 2. The sediment data are reported in Table 3. Metal Water Guality - Snip Project July 21, 1990

HG/L 4.005 4.005 003 <u>500</u> <u>. 005</u> <....< ..... DISICP .005.005.005 0.310 \$00.5 <..005 . ¢.005 0.095 0.104 0.111 0.103 0.103 0.036 0.042 0.038 0.038 0.038 500.3 500.3 0.045 0.045 0.047 0.046 0.046 \* TOTICP CO NG/L MG/L 1000.2 1000.2 0.0002 0.0003 0.001 ¢.0001 0.001 1000.3 1000. > 1000.3 DISGF CD 200° v \$00'' \$00.5 • 003 200. ) 200. ) 200. ) 200 200 200 200 200. 2005 2005 DISICP CD MG/L ; TOTGF CD MG/L .0001 .0001 .0001 1000.2 0.0017 0.0016 0.0020 0.0020 0.0013 **, 0001** 0.0002 0.0002 (.0001 1000. 10 1000. 10 T0TICP CD MG/L .005 (.005 (.005 .005.005 **200**. ^ 2003 2005 2005 0.006 50,50, ; ; 16.2 16.4 15.9 16.2 0.3 16.1 16.2 16.0 16.1 52.3 17.0 17.0 16.7 16.9 0.2 54.6 16.9 16.5 16.4 16.6 16.6 59.7 ... DISICP CA NG/L TOTICP CA NG/L 24.1 24.1 24.1 24.0 0.1 15.8 15.6 15.9 15.8 0.2 55.7 56.0 55.9 55.9 53.4 40.1 47.1 59.1 48.8 9.6 22.3 22.3 22.0 22.0 110.0 59.8 :; DISICP BA MG/L 0.044 0.037 0.037 0.037 0.037 0.034 0.035 0.035 0.035 0.035 0.044 0.024 0.024 0.024 0.024 0.024 0.095 0.095 0.098 0.096 0.096 0.035 0.034 0.035 0.035 0.035 0.048 ¢.001 T071CP BA NG/L 0.041 0.042 0.042 0.042 0.042 0.052 0.047 د,001 0.598 0.676 0.762 0.679 0.082 0.101 0.103 0.102 0.102 0.102 0.228 0.258 0.228 0.228 0.019 0.265 0.254 0.257 0.259 0.006 0.752 \$0, \$ 50, \$ 1, 03 8 5.05 5 5 5 i i 8 8 8 8 1 8 1 1 **8**. ^ DIGICP 5 5 5 i i 888 **8** AS MG/L TOTICP AS NG/L \$0.0 \$0.0 1 **8**.9 **8** 0.16 8.0 0.03 0.03 0.05 0.05 0.05 <u>8</u>88 20.0 20.0 20.0 1 80.0 80.0 80.1 8 8 8 8 1 1 • .05 0 .06 0 .08 0 .09 4.05 0.06 0.07 0.07 **8** 8 **8**.5 ¢.05 **50.** ^ DISICP 88811 -----AL NG/L 0.23 0.20 0.32 0.05 <.05 < 31.90 37.10 39.60 36.20 3.93 16.10 17.50 15.90 16.50 0.87 17.80 16.80 17.40 17.33 0.50 22.10 60.0 0.14 5555 i i TOTICP AL MG/L **..01** 555; | | 10,7 **10. 10.** 5551 10.2 DISICP AG NG/L 10.2 5,5,5, | | TOTICP AG HG/L 222 <u>8</u>88 5 5 5 I I 10'> 10,5 ¢.01 10.2 **ć.**01 2.01 Repl.1 Repl.2 Repl.3 Average S.D. Repl.1 Repl.2 Repl.3 Averege S.D. Station Number Blenk N 9 5 •

- 5 -

Table 1

| (cont.) |  |
|---------|--|
| ble 1   |  |
| F       |  |

•

Metal Water Quality - Snip Project -July 21, 1990

| Station<br>Number    |         | TOTICP<br>CR<br>MG/L | DISICP<br>CR<br>MG/L | TOTICP<br>CU<br>NG/L | TOTGF<br>CU<br>MG/L | DISICP<br>CU<br>MG/L   | DISGF<br>CU<br>NG/L | TOTICP<br>FE<br>MG/L | DISICP<br>FE<br>NG/L | TOTICP<br>K<br>MG/L                     | DISICP<br>K<br>HG/L | TOTICP<br>MG<br>MG/L | DISICP<br>NG<br>NG/L  | TOTICP<br>MN<br>MG/L | DISICP<br>MN<br>NG/L | TOTICP<br>NO<br>NG/L  | DISICP<br>NO<br>NG/L |
|----------------------|---------|----------------------|----------------------|----------------------|---------------------|------------------------|---------------------|----------------------|----------------------|---|---------------------|----------------------|---|----------------------|----------------------|---|----------------------|
| )<br> <br> <br> <br> | Repl.1  | \$00.3               | ¢.005                | \$005                | •                   |                        | ¢.0005              | 1.400                | 0.494                | \$                                      | \$                  | 1.8                  | 1.8   | 0.233                | 0.232                | 10.2  | .01                  |
| T                    | Repl.2  | 500.5                | ¢.005                | <b>500</b> . •       |                     |                        | •                   | 1.340                | 0.515                | 9                                       | ĉ                   | 1.8                  | 1.8   | 0.229                | 0.235                |   | 10.>                 |
|                      | Repl.3  | \$000                | \$,005               | 0.007                |                     | × 00                   | <.0005              | 1.470                | 0.475                | ů<br>ů                                  | ů                   | 1.8                  | 1.7   | 0.234                | 0.228                | 10.2  | 10.>                 |
|                      | Average | ;                    |                      |                      | 0.0014              |                        | ;;                  | 1.403                | 0.495                | 1                                       | ļ                   | 1.8                  | 1.8   | 0.232                | 0.232                |   | :                    |
|                      | 3.D.    | ;                    | :                    |                      | 0.004               | :                      | !                   | 0.065                | 0.020                | ;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;; | :                   | 0.0                  | 0.1   | 0.003                | 0.004                | ;   | :                    |
|                      | Repl.1  | 0.032                | ¢.005                | 0.130                | ;                   | ¢.005                  | ¢,0005              | 35.700               | 0.034                | 12                                      | ç                   | 13.4                 | 1.3   | 1.610                | 0.088                |   | ۰.01                 |
| 2                    | Rep1.2  | 0.032                | <<br>005             | 0.102                | ;                   | ¢.005                  | <.0005              | 40.900               | 0.037                | 13                                      | 3                   | 15.1                 | 1.3   | 1.800                | 0,089                |   | 10.2                 |
|                      | Repl.3  | 0.041                | \$00.2               | 0.118                |                     | 00.<br>2               | €000°°              | 44.100               | 0.032                | 16                                      | ŝ                   | 16.4                 | 1.3   | 2.070                | 0.087                | <b>10.</b> 3  | 4.01                 |
|                      | Average | 0.035                |                      | 0.117                | ļ                   | !                      | 1                   | 40.233               | 0.034                | 14                                      | -                   | 15.0                 | 1.3   | 1.827                | 0.088                |   | :                    |
|                      | S.D.    | 0.005                |                      | 0.014                | :                   | ļ                      |                     | 4.239                | 0.003                | 8                                       | :                   | 1.5                  | 0.0   | 0.231                | 0.001                |   | í                    |
|                      | Repl.1  | <b>:</b> 00: •       | ¢.005                | <b>č</b> .005        | ¢.0006              | \$.00<br>\$            | <.0005              | 0.660                | 0.083                | N)                                      | ιń                  | 4.4                  | 4.3   | 0.373                | 0.372                | 10.5  | د.01                 |
| m                    | Repl.2  | \$,005               |                      | <b>500</b> .2        | ¢.0006              | •                      | <.0005              | 0.663                | 0.070                | <b>\$</b> D                             | <b>N</b>            | 4.4                  | 4.3   | 0.380                | 0.373                | ·   | ۰.01                 |
|                      | Repl.3  | <b>200</b> . •       | <b>\$</b> ,005       | 0.018                | 0.0173              | :00°°                  | <.0005              | 0.645                | 0.068                | Ð                                       | 9                   | 4.4                  | 4.4   | 0.375                | 0.389                |   | 10.2                 |
|                      | Average |                      |                      | ł                    | ;                   |                        | ;;                  | 0.656                | 0.080                | Ð                                       | ÷                   | 4.4                  | <b>6.4</b>  | 0.376                | 0.378                |   | ſ                    |
|                      | s.b.    | ;                    | :                    |                      | ;                   | !                      | ;                   | 0.010                | 600.0                | 0                                       | -                   | 0.0                  | 0.1   | 0.004                | 0.010                | •   | 1                    |
|                      | Repl.1  | 0.021                | <b>500.</b> >        | 0.036                | 1                   | <b>200</b> . )         | ¢.0005              | 15.600               | 0.018                | •                                       | û                   | 8.4                  | 2.5   | 0.367                | 0.013                | •   | 10.2                 |
| 4                    | Repl.2  | 0.024                | \$.005               | 0.049                | ;;;                 | <                      | <                   | 16.700               | 0.034                | *                                       | ŝ                   | 8.7                  | 2.5   | 0.376                | 0.013                | <b>۲,01</b>   | <b>.</b> .01         |
|                      | Repl.3  | 0.021                | <b>\$00</b>          | 0.039                | ;                   | <b>.</b> .005          | <pre>\$0002*</pre>  | 15.100               | 0.044                | 4                                       | ŝ                   | 8.1                  | 2.5   | 0.355                | 0.014                | •   | 10.2                 |
|                      | Average | 0.022                |                      | 0.041                | ;                   | 1                      | 1                   | 15,800               | 0.032                | 4                                       | !                   | 8.4                  | 2.5   | 0.366                | 0.013                | 1   | !                    |
|                      | S.D.    | 0.002                |                      | 0.007                | 1                   | ļ                      | 1<br>)<br>1         | 0.819                | 0.013                | 0                                       | !                   | 0.3                  | 0.0   | 0.011                | 0.001                | }   | 1                    |
|                      | Repl.1  | 0.019                | č. 005               | 0.027                | ;                   | <b>200</b> . >         | ¢.0005              | 17.200               | 0.029                | *                                       | ĝ                   | 8.7                  | 2.4   | 0.439                | 0.020                | ۰.01  | 10.01                |
| n                    | Repl.2  | 0.016                | £003.5               |                      | :                   | <pre>\$00.5</pre>      | <.0005              | 16.500               | 0,032                | *                                       | 3                   | 8.5                  | 2.4   | 0.431                | 0.019                |   | 10.2                 |
|                      | Repl.3  | 0.022                | ¢.005                |                      | ;;                  | <ul><li>.005</li></ul> | <.0005              | 17.500               | 0.060                | 1D                                      | 0                   | 8.7                  | 2.4   | 0.435                | 0.020                | 10.2  | د.01                 |
|                      | Average | 0.019                | :                    | 0.026                | ;                   |                        | ;                   | 17.067               | 0.040                | •                                       | 1                   | 8.6                  | 2.4   | 0.435                | 0.020                |   | !                    |
|                      | s.D.    | 0.003                | 1                    | 0.001                | ;                   | 1                      | ļ                   | 0.513                | 0.017                | -1                                      | :                   | 0.1                  | 0.0   | 0.004                | 0.001                | ;   |                      |
| 9                    | 19      | \$00°\$              | \$00°                | 1.330                | ļ                   | \$00.\$                | 0.0027              | 152.000              | 0.008                | 21                                      | ¢                   | 19.5                 | 6.2   | 3,930                | 0.704                | 0.1   | 0.0                  |
| 1                    | 17      | ¢.005                | ¢.005                | 0.016                | 0.0169              | ¢.005                  | <.0005              | 0.153                | 0.007                | s)                                      | Ŷ                   | 9.2                  | 9.2   | 0.052                | 0.049                | 0.0   | 0.0                  |
| Ø                    |         | <b>500</b> . >       |                      | <b>500</b> . >       | <b>, 0006</b>       | €00.>                  | <                   | 0.216                | 500°°                | Ð                                       | U)                  | 6.9                  | 6.9   | 0.014                | 0.008                | 0.0   | 0.0                  |
| Blenk                | 1       | <b>600</b>           | 500.2                | 80                   | 0.0010              | 200°. >                | <.0005              | \$.005               | 500° Y               | 5                                       | 2                   |                      |   | , 001                | 100. x               | 10. >   | 10.3                 |
|                      | 1       |                      |                      |                      | •                   |                        |                     |                      |                      |   |                     |                      | 1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 |                      |                      | <br> | ***                  |

•

.

,

:

| ~    |
|------|
|      |
| - 44 |
|      |
| - 5  |
| 9    |
| 0    |
| Ĵ.   |
| -    |
|      |
| -    |
|      |
|      |
|      |
| 7    |
|      |
|      |
| -    |
| -    |

,

Matal Water Quality - Snip Projet -

| Station    |         | TOTICP<br>NA | DISICP<br>NA | TOTICP<br>NI | DISICP<br>NI | TOTICP<br>P | DISICP      | TOTICP<br>PB | TOTGF<br>PB | DISICP<br>PB        | DISGF<br>PB    | TOTICP               | DISICP<br>SB | TOTICP<br>SI | DISICP<br>SI | TOTICP<br>SE | DISICP                |
|------------|---------|--------------|--------------|--------------|--------------|-------------|-------------|--------------|-------------|---------------------|----------------|----------------------|--------------|--------------|--------------|--------------|-----------------------|
| Number     |         | MG/L         | MG/L         | NG/L         | MG/L         | MG/L        | MG/L        | NG/L         | HG/L        | HG/L                | NG/L           | NG/L                 | NG/L         | NG/L         | NG/L         | NG/L         | NG/L                  |
|            | Repl.1  | 1.4          | 1.5          | د.02         | ¢.02         | د.1         |             | \$0.2        | 0.0006      | 50.2                | 5000.          | 50.3                 | 50.2         | 3.19         | CA. C        | 1            |                       |
|            | Repl.2  | 1.4          | 1.5          | ¢.02         |              |             | 1.1         | 50.5         |             | 50.5                | 5000.2         | č                    |              |              |              |              |                       |
|            | Repl.3  | 1.4          | 1.5          |              |              |             | 1.2         |              |             | 1                   |                |                      |              |              |              |              |                       |
|            | Average | 1.4          | 1.5          |              |              | 1           |             |              | 0.000       |                     |                |                      |              | 50°0         | 8/ • N       | <b>60.</b>   | 5.0                   |
| 5          | 2       | Ċ            |              |              |              |             | 1           |              |             |                     | 1              | )<br>)<br>)          |              | 57.5         | 79.7         | 8            |                       |
|            |         |              |              |              |              |             | •           | :            | 0,0002      |                     | 1              | Į                    | !            | 0.14         | 0.04         |              |                       |
|            | Repl.1  | 4.2          | 0.4          | 0.03         | ¢.02         | 1.6         | (.1         | 0.08         | 0.1060      | 20°2                | \$.000 \$      | Ę                    | Ę            | 40.00        |              |              | •                     |
| 2          | Repl.2  | 4.5          | 0.5          | 0.03         |              | 2.1         | 1.2         | 90-00        | -           | 55                  |                |                      |              |              |              |              |                       |
|            | Repl.3  | 4.5          | 4.0          | 0.03         | ¢.02         |             |             | 60.0         | -           | 50.5                | .0005          |                      |              |              |              | 38           |                       |
| 7          | Average | 4.4          | 0.4          | 0.03         |              |             | '           | 0.08         | -           |                     |                |                      | };;          |              |              |              |                       |
|            | s.b.    | 0.2          | 0.1          | 0.0          | ;            | 0.5         | •           | 0.02         | 0.0089      | 1                   | 1              | 1                    | :            | 14.03        |              |              |                       |
|            | Repl.1  | 2.1          | 2.4          |              |              | ۲.1         | <b>ć.1</b>  | ¢.05         | 6000.0      | ¢.05                | £000°, >       | 50°. >               | \$0°\$       | 2.96         | 2.91         | 50°.3        | 50.5                  |
| <b>m</b>   | Repl.2  | 2.1          | 2.3          |              |              |             | <b>1</b>    | <.05         | -           | •                   |                | <b>SO</b>            |              |              |              |              |                       |
|            | Repl.3  | 2.1          | 2.4          | ¢.02         | ¢.02         |             | <b>1</b>    | <.05         | _           | •                   | \$0000.2       | \$°. \$              | 50°°         | 2.98         |              | 50.3         | 50.2                  |
|            | Average | 2.1          | 2.4          | ;            | :            | ;           |             | 1            | 0.0012      | -                   | 1              | !                    |              |              | •            | •            |                       |
|            | s.D.    | 0.0          | 0.1          | -            | ł            | ;           | i           | !            | 0.0006      | 2<br>1<br>1         | •              |                      | •            | 0.01         | 0.06         | •            | ł                     |
| -          | Repl.1  | 3.0          | 1.1          | د.02         |              | <b>9.6</b>  |             | £0.2         | 0.0060      | <b>8</b> . <b>3</b> | ¢.0005         | <b>20.</b> 2         | (°.05        | 27.90        | 1.25         | 50.3         | 50°.2                 |
| -          | Repl.2  | 3.2          | 1.1          | ¢.02         |              | 0.4         | <b>1.</b> 7 | \$.05        | -           | \$0.5               | <              | 50.5                 | -            |              | 1.24         | -            |                       |
|            | Repl.3  | 3.1          | 1.1          | ¢.02         | -            | 0.4         | <b></b> 1   | <b>50.</b> 2 | -           |                     | -              | ¢.05                 |              |              | 1.26         |              | 20.2                  |
| -          | Average | 3.1          | 1.1          |              | ļ            |             | ļ           | :            | 0.0063      |                     |                | ļ                    | -            | 28.67        |              | -            |                       |
|            | 3.D.    | 0.1          | 0.0          | ;            |              | 0.0         | !           | }<br>1<br>1  | 0.0003      | •                   | 1              | :                    | :            | 1.16         |              | 1            | ł                     |
|            | Repl.1  | 3.4          |              |              | د.02         |             | ۲.1         | <b>20.</b> 2 | 0.0085      | •                   | <              | <b>20.</b> >         | -            | 33,00        | 1.21         | 20. v        | 50°2                  |
| <b>1</b> 0 | Repl.2  | 3.2          |              |              |              | 0.3         | د.1         | \$.05        | 0.0096      | •                   | ·              | \$0.5                | -            |              |              |              |                       |
|            | Repl.3  | 3.3          | 1.1          | ¢.02         |              | 4.0         | د.1         | <b>č.</b> 05 | £600°0      | •                   |                | <b>50</b> . <b>2</b> | ¢.05         |              | 1.21         | 50.5         | 50.2                  |
|            | Average | 3.3          |              | 1            | 1            |             |             | ]            | 0.0091      | 1                   | :              | 1                    |              |              |              |              |                       |
|            | s.b.    | 0.1          | 0.1          | l<br>I<br>T  | ;            | 0.1         | !           | !            | 0.0006      | 1                   | 1              | ļ                    | 1            | 1.72         | 0.01         | !            | !                     |
| 9          | 19      | 2.2          | 1.6          | 0.02         | د.02         | 2.7         | ۰.1         | 0.13         | 0.0016      | ÷.0                 | <b>\$000</b> * | <b>č.</b> , 05       | ¢.05         | 38.00        | 2.86         | ¢.05         | <.05                  |
| 2          | 17      | <b>8. 4</b>  | 6.1          | ¢.02         | <b>ć.02</b>  | ۲.1         | د.1         | \$°°?        | 0.0021      | <. 05               | 0.0005         | ÷.05                 | <b>30.</b> 3 | 4.54         | 4.53         | <b>č.</b> 05 | <5                    |
| •0         | 19      | 2.7          | 2.9          | ¢.02         | د.02         | (.)         |             | \$0.2        | 0.0012      | <b>50.</b> >        | 0.006          | <b>*.0</b>           | č0.>         | -            | 4.03         | ¢05          | <ul><li>.05</li></ul> |
| Blenk      |         |              | د.1          |              | · ·          | (.1         | ۲.۱         | <b>8</b>     | ¢.0006      |                     | <.000 A        | 50.0                 | <pre></pre>  | 0.07         | 50. V        | \$0.5        | 50° V                 |

.

1

Table 1 (cont.)

Metal Weter Quality - Snip Project -July 21, 1990

| :                 |                            | TOTICP                 | DISICP         | TOTICP     | DISICP     | TOTICP                                  | DISICP          | TOTICP                        | DISICP      | TOTICP                 | DISICP           |
|-------------------|----------------------------|------------------------|----------------|------------|------------|---|-----------------|-------------------------------|-------------|------------------------|------------------|
| Station<br>Number | -                          | SN<br>NG/L             | SN<br>MG/L     | SR<br>NG/L | SR<br>NG/L | TI<br>NG/L                              | TI<br>NG/L      | V<br>MG/L                     | V<br>MG/L   | ZN<br>NG/L             | ZN<br>NG/L       |
| 1                 |                            |                        |                |            | 1          |   |                 |                               |             |                        |                  |
| -                 | C   und                    |                        |                | 0/010      |            |   |                 |                               |             |                        | 200              |
| 4                 | Renlag                     |                        |                | 0.077      |            |   |                 |                               |             |                        | 2001             |
|                   | Averege                    |                        |                | 0.076      | 0.074      |   |                 |                               |             |                        |                  |
|                   | S.D.                       |                        | 1              | 0.001      | 0.001      | 1                                       | !               | 1                             | i           | 1<br>1<br>1            | !                |
|                   | Repl.1                     | 50.3                   | -              | 0.270      |            | 1 .840                                  | <.002           | 0.10                          | 10.3        | 0.560                  | C00. 2           |
| 2                 | Repl.2                     | 50.2                   | <b>50.</b>     | 0.301      |            | 2.010                                   | .002            | 0.11                          | 10.2        | 0.260                  | <<               |
| r                 | Repl.3                     | 50.5                   | -              | 0.342      | 0.082      | 2.110                                   | ¢.002           | 0.13                          | .01         | 0.282                  | . 002            |
|                   | Average                    |                        |                | 0.304      | 0.082      | 1.987                                   |                 | 0.11                          |             | 0.367                  | 1                |
|                   | S.D.                       | !                      |                | 0.036      | 0.000      | 0.137                                   | 1               | 0.02                          | 1           | 0.167                  | 1                |
|                   | Repl.1                     | <ul><li>*.05</li></ul> |                | 0.396      | 0.386      | ¢.002                                   | ¢.002           | 10.2                          | ۰.01        | ¢.002                  | ¢.002            |
| m                 | Repl.2                     | 50.2                   |                | 0.397      |            | ¢.002                                   | ¢.002           | 10.3                          | 10.3        | ¢.002                  | <b>&lt;.002</b>  |
|                   | Repl.3                     | <b>5</b> , 05          | ¢.05           | 0.396      | 0.394      | ¢.002                                   | ¢.002           | 10.2                          | 10.3        | ¢.002                  | <b>&lt;.</b> 002 |
|                   | Average                    |                        |                | 0.396      |            | 1                                       | i               | i                             | 1           | ;                      | ;                |
|                   | S.D.                       | ;                      | 1              | 0.001      | 0.005      |   |                 | ł                             | 1           | 1<br>}<br>1            | ]                |
|                   | Repl.1                     | <b>8</b> .9            | -              | 0.145      |            | 0.477                                   | د.002           |                               | 10.2        | 0.034                  |                  |
| 4                 | Repl.2                     | <b>20.</b> 0           | ¢.05           | 0.147      | 0.098      | 0.548                                   | ¢.002           |                               | 10.01       | 0.037                  |                  |
|                   | Repl.3                     | <b>5</b> .5            | -              | 0.145      |            | 0.450                                   | د.002           | 0.04                          | 10.2        | 0.034                  | <.002            |
|                   | Average                    |                        | 1              | 0.146      |            | 0.492                                   | 1               |                               | :           | 0.035                  |                  |
|                   | S.D.                       | ļ                      | ļ              | 0.001      |            | 0.051                                   | :               | 10.01                         | ł           | 0.002                  | ;                |
|                   | Repl.1                     | <b>8</b> .3            | \$0. <b>\$</b> | 0.155      | 860.0      | 0.655                                   | ¢.002           | 0.05                          | 10.3        | 0.075                  | د.002            |
| eî)               | Repl.2                     | <b>8</b> .9            | •              | 0.154      |            | 0.543                                   | ¢.002           | 0.04                          | 10.5        | 0.048                  | ¢.002            |
|                   | Repl.3                     | \$0 <b>.</b> \$        |                | 0.155      | -          | 0.581                                   | ¢.002           | 0.05                          | <b>4.01</b> | 0.049                  |                  |
|                   | Average                    | !                      | 1              | 0.155      | -          | 0.593                                   | ł               | <u>0</u> .05                  | ł           | 0.057                  | ;                |
|                   | s.D.                       | 3                      | !              | 0.001      | 0.001      | 0.057                                   |                 | 0.01                          | !           | 0.015                  | ;                |
| y                 |                            | <b>6</b> , 9           | ¢.05           | 0.682      | 0.362      | 1.390                                   | د.002           | 0.13                          | 10.>        | 0.386                  | د.002            |
| ٢                 |                            | 8.                     | <b>6.</b> 0    | 1.110      | 1.100      | د.002                                   | ¢.002           | د.01                          | 10.>        | 0.035                  | د.002            |
| 40                |                            | <b>\$0</b> **          | 5.9            | 0.576      | •          | د.002                                   | <b>&lt;.002</b> | 10.5                          | ۰.01        | 0.022                  | 0.003            |
| Blenk             | 1<br>4<br>5<br>6<br>6<br>8 | 50°,                   | 50.,           | ¢.001      | , 001      | ¢.002                                   | ¢.002           | 10.2                          | 10.2        | <ul><li>.002</li></ul> | د.002            |
|                   |                            |                        |                | * * * * *  |            | 1 |                 | /<br>  <br>  <br>  <br>  <br> |             |                        |                  |

.

.

•

- 8 -

,

.

| HG/L HC/L HC/L HC/L HC/L HC/L HG/L HG/L HG/L HG/L HG/L HG/L HG/L HG   | REL.U. MG/L<br>6<br>7.8<br>7.6<br>6.1<br>8.0<br>8.1<br>8.0<br>8.1<br>8.1<br>6.25<br>8.1<br>7.8<br>8.1<br>6.25<br>8.1<br>7.8<br>8.0<br>530<br>530<br>530<br>530<br>530<br>530<br>530<br>53 |   | MG/L<br><br>6.6<br>6.4<br>19.3<br>19.3<br>19.3<br>19.3<br>19.3<br>19.3<br>19.3<br>19.3 |
|---|---|---|--|
| Repl.1 51 47.8 49.2   Repl.2  48.4 49.2   Repl.3 45 47.0 48.4   Average 48 47.7 49.2   S.D. 4 47.7 49.2   S.D. 4 43 45.6 46.3   Repl.2 41 45.9 46.6   Repl.3 41 45.4 46.4   Repl.3 41 45.4 46.4   Repl.3 41 45.4 46.2   Repl.3 41 45.4 46.2   Repl.1 124 153.0 155.0   Repl.3 127 160.0 155.0   Repl.3 127 160.0 155.0   Repl.4 125 155.3 157.0   Repl.4 125 155.3 157.0   Repl.4 125 155.3 157.0   Repl.4 2 4.0 3.5  | اه مدر مرموم همه  | 0 00 C 00000  | 10 000 0000 0000 0000 0000 0000 0000 0   |
| Repl.1 51 47.8<br>Repl.2 48.4<br>Average 48 47.0<br>Average 48 47.7<br>5.0. 4 0.7<br>8.0.1 43 45.6<br>Repl.3 41 45.4<br>Average 43 45.6<br>8.0. 2 0.3<br>8.0.1 124 153.0<br>Repl.1 124 153.0<br>Repl.2 125 155.3<br>Average 125 155.3<br>Average 125 155.3  | 8 974 04004 888<br>1  | 7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7 | 6, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,  |
| Repl.2 46.4<br>Repl.3 45.4<br>Averace 48 47.7<br>S.D. 4 47.7<br>S.D. 4 47.7<br>Repl.1 43 45.6<br>Averace 43 45.6<br>S.D. 2 0.3<br>Repl.1 124 153.0<br>Repl.1 124 153.0<br>Repl.1 125 155.3<br>S.D. 2 4.0  | ,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,<br>,   | 80<br>75<br>74<br>810<br>810<br>800<br>800<br>800<br>800<br>800<br>800<br>800               |  |
| Repl.3 45 47.0<br>Average 48 47.7<br>S.D. 4 0.7<br>Repl.1 43 45.6<br>Repl.2 44 45.9<br>Repl.3 41 45.4<br>Average 2 0.3<br>Repl.2 125 153.0<br>Repl.3 127 160.0<br>Repl.3 127 160.0<br>Repl.3 125 155.3<br>S.D. 2 4.0  |   | 80<br>810<br>810<br>810<br>810<br>810<br>810<br>810<br>810<br>810<br>8                      |  |
| Average 48 47.7<br>3.D. 4 0.7<br>Repl.1 43 45.6<br>Repl.2 44 45.9<br>Repl.3 41 45.4<br>Average 43 45.6<br>S.D. 2 0.3<br>Repl.1 124 153.0<br>Repl.3 127 160.0<br>Repl.3 127 160.0<br>Repl.3 125 155.3<br>S.D. 2 4.0  |   | 75<br>740<br>810<br>850<br>800<br>850   | 44 46 66 66 69 69 69 69 69 69 69 69 69 69 69   |
| S.D. 4 0.7   Repl.1 43 45.6   Repl.2 44 45.9   Repl.3 41 45.4   Average 43 45.6   S.D. 2 0.3   S.D. 2 0.3   Repl.1 124 153.0   Repl.3 127 160.0   Repl.4 125 155.3   S.D. 2 125   Repl.4 47 52.5   S.D. 2 4.0   |   | 7<br>740<br>810<br>850<br>800<br>800<br>800   | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  |
| Repl.1 43 45.6<br>Repl.2 44 45.9<br>Repl.3 41 45.4<br>Averege 43 45.6<br>S.D. 2 0.3<br>Repl.1 124 153.0<br>Repl.2 125 153.0<br>Repl.3 127 160.0<br>Averege 125 155.3<br>S.D. 2 4.0  |   | 740<br>810<br>850<br>800<br>36  | 90 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5   |
| Repl.2 44 45.9   Repl.3 41 45.4   Average 43 45.4   Average 43 45.4   S.D. 2 0.3   S.D. 2 0.3   Repl.1 124 153.0   Repl.3 125 153.0   Repl.3 127 160.0   Average 125 155.3   S.D. 2 4.0   |   | 810<br>800<br>96<br>96  | 5 0 1 0  |
| Repl.3 41 45.4   Average 43 45.4   S.D. 2 0.3   S.D. 2 0.3   Repl.1 124 153.0   Repl.2 125 153.0   Repl.3 127 160.0   Average 125 155.3   S.D. 2 4.0   Repl.1 47 52.5   |   | 5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5 | 500  |
| Average 43 45.6<br>S.D. 2 0.3<br>Repl.1 124 153.0<br>Repl.2 125 153.0<br>Repl.3 127 160.0<br>Average 125 155.3<br>S.D. 2 4.0  |   | 8<br>8<br>8   | 0.0  |
| S.D. 2 0.3<br>Repl.1 124 153.0<br>Repl.2 125 153.0<br>Repl.3 127 160.0<br>Average 125 155.3<br>S.D. 2 4.0<br>Repl.1 47 52.5   |   | ¥   | 0  |
| Repl.1 124 153.0<br>Repl.2 125 153.0<br>Repl.3 127 160.0<br>Average 125 155.3<br>5.D. 2 4.0<br>Repl.1 47 52.5   |   |   | <b>2</b>   |
| Repl.2 125 153.0<br>Repl.3 127 160.0<br>Average 125 155.3<br>5.D. 2 4.0<br>Repl.1 47 52.5   |   | 230   | -  |
| 127 160.0<br>125 155.3<br>2 4.0<br>47 52.5  |   | 220   | 45.1   |
| 125 155.3 1<br>2 4.0<br>47 52.5   |   | 210   | 45.3   |
| 2 4.0<br>47 52.5  | 8.0   | 220   | 45.4   |
| 47 52.5   | 0.3   | 10  | 0.3  |
|   | 7.9 255   | 330   | 14.9   |
| 46 51.5   |   | 360   | 14.9   |
| 47 51.3   | 7.9 261   | 360   | 14.8   |
| age 47 51.8 52  | 2   | 350   | 14.  |
| S.D. 1 0.6 0.5  | 0.1 5   | 17  | 0  |
| Repl.1 46 52.3  | 7.9 292   | 390   | 14.7   |
| 47 52.2   |   | 380   | 15.3   |
| 46 51.7   |   | 380   | 15.6   |
| verage 46 52.1 52   | Ņ   | 383   | 15.2   |
|   | 0.0 17  | 9   | 50   |
| 6 106 162.0 164.0   | 7.7 2370  | 3150  | 72.4   |
| 7 126 187.0 188.0   | 8.1 (5  | 230   | 63.4   |
| 8 121 159.0 160.0   | 8.3 <5  | 220   |  |
| <ul><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><li>4.4</li><l< td=""><td>5.4 (5</td><td>&lt;10<br/>&lt;10</td><td>0.5</td></l<></ul> | 5.4 (5  | <10<br><10  | 0.5  |

•

.

- · · ·

Sediment Quelity - Snip Project July 21, 1990

14200 2440 2450 15900 8748 7311 917 893 882 2430 1230 3730 4930 3080 1601 836 882 34 243 275 269 689 684 719 687 695 16 770 864 772 802 802 SEDICP NN UG/G 8420 8910 9350 6630 5900 4690 5460 5460 812 SEDICP NG UG/G 6460 6200 6580 6580 6345 209 7190 6600 8200 8630 8630 7655 927 11000 10800 11200 111200 11100 171 10800 11500 11100 11100 10600 11000 11000 2700 2400 1800 2100 2250 387 2000 11000 11800 11450 526 2300 2500 2500 2575 2575 2575 4500 4400 5200 5600 4925 574 5300 5400 6200 5100 5300 5300 5000 5000 245 SEDICP K 0/00 0.040 0.010 0.010 0.033 0.028 0.072 0.069 0.071 0.010 0.010 0.010 0.010 0.010 0.009 0.010 0.020 0.010 0.012 0.005 0.030 0.020 0.038 0.038 0.038 0.046 0.052 0.052 0.046 SEDHG HG 0/90 87600 54100 74100 72400 72050 13764 27600 29100 30400 93300 82300 67600 72600 78950 11347 64500 69100 61800 6210 60600 60300 54000 60000 58725 3160 43300 38200 38500 40200 40050 2339 **58400** 55200 SEDICP FE ..... NG/G 16.0 16.9 17.6 221.0 183.0 147.0 169.0 180.0 51.3 45.7 34.6 45.5 44.3 7.0 98.9 130.0 82.0 116.0 116.7 20.8 191.0 175.0 232.0 275.0 275.0 218.3 44.8 6.4 SEDICP CU UG/G 58.55 57.6 49.4 45.9 48.5 47.0 47.7 1.6 49.2 50.0 34.2 24.4 27.9 25.0 25.0 4.5 20.0 19.8 19.4 18.2 19.4 0.8 51.6 50.1 56.3 56.3 3.0 SEDICP CR UG/G 88881 8888 | | 8888 | | SEDICP CO UG/G 8888;; <u>888</u> 888811 SEDICP CD UG/G 3.1 0.3 • • 2.1 ¢.8 1.0 8.08.0 0.2 2.9 2.8 3.0 \$. 8 ÷.8 4300 4520 1750 7530 6900 6740 7020 7048 342 17200 16600 16100 14400 16075 1204 8180 7290 9490 8765 8765 1268 13600 13800 14400 14500 14075 443 SEDICP CA UG/G 11000 11500 9820 12200 11130 1002 1 1 1 1 1 1 2.00°4.00 4.00°5.00 0.6 0.3 4.00.0 SEDICP BE UG/G 0.3 0.7 0.7 SEDICP BA UG/G 304 304 273 14 273 556 492 629 598 598 95 **389** 344 332 332 360 360 26 461 501 498 499 499 499 499 222 970 2559 960 424 424 SEDICP AS UG/G 8 <u>8</u> 8 23 482 <del>6</del> <del>6</del> 8.5 ŝ **8 8 8** -14800 13500 11100 13125 1533 SEDICP AL UG/G 14900 14300 15200 14650 14650 480 23000 23200 26500 16900 17400 21300 22300 19975 2232 20200 20000 21400 19400 20250 839 21500 23100 22900 22900 22100 22100 22400 333 Ĝ 33 Ĝ Q ů Ç ů g 333 SEDICP AG UG/G -1 1 1 -; 1 i Repl.1 Repl.2 Repl.3 Repl.4 Average S.D. Repl.1 Repl.2 Repl.3 Repl.4 Average S.D. Repl.1 Repl.2 Repl.3 Repl.4 Averege S.D. Average S.D. Average S.D. Repl.1 Repl.2 Repl.3 Repl.4 Repl.1 Repl.2 Repl.3 Repl.4 NBS 1646 NBS 1646 Station Number NBS 1646 ŝ

.......

fable 3

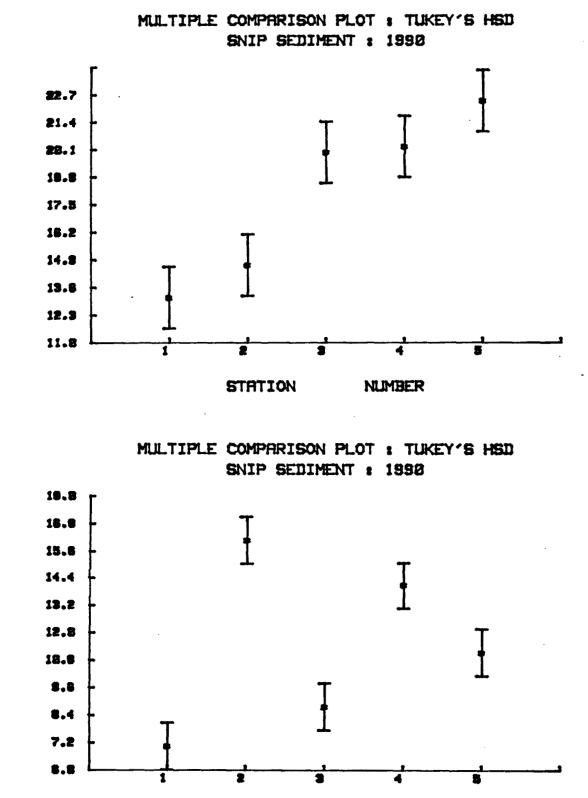
Table 3 (cont.)

Sediment Quality - Snip Project -July 21, 1990

|                          |         |            |        |                  |        |            |             | -      |            |            |        |           |             |        |            |  |
|--------------------------|---------|------------|--------|------------------|--------|------------|-------------|--------|------------|------------|--------|-----------|-------------|--------|------------|--|
| 04.44                    |         | SEDICP     | SEDICP | SEDICP           | SEDICP | SEDICP     | SEDICP      | SEDICP | SEDICP     | SEDICP     | SEDICP | SEDICP    | SEDICP      | SEDICP | SEDICP     |  |
| Number                   |         | 9/9A       | 0C/6   | 0C/G             | 0C/G   | NG/G       | 0C/G        | 00/00  | 0C/G       | 06/G       | 0C/G   | UG/G      | 0/9/        | MG/KG  | MG/KG      |  |
| <br> <br> <br> <br> <br> | Repl.1  | 10         | 470    | 4<br>9<br>9<br>1 | 1400   | 6)         | 8)          | 1380   | <b>8</b>   | 52.8       | 1460   | 171       | 314         | 975000 | 24600      |  |
|                          | Repl.2  | â          | 470    | 23               |        | 10         | <b>8</b> >  | 1030   | <b>8</b> > | 46.6       | 1430   | 120       | 166         | 968000 | 32300      |  |
|                          | Repl.3  | 0          | 350    |                  | •      | 10         | <b>8</b> ×  | 1060   | <b>8</b> ) | 42.7       | 1280   | 181       | 141         | 974000 | 26000      |  |
|                          | Repl.4  | •          | 860    |                  | -      | <b>8</b> > | <b>8</b> ×  | 1310   | <b>8</b> > | 56.0       | 1300   | 120       | 378         | 978000 | 21800      |  |
|                          | Average | 1          | 538    |                  | -      |            | ;;;         | 1195   | 1 1 1      | 49.5       | 1368   | 148       | 250         | 973750 | 26175      |  |
|                          | 3.D.    | [          | 193    |                  |        | 1          | ;           | 152    | 1<br>]<br> | 5.2        | 79     | 28        | 66          | 3631   | 3846       |  |
|                          | •       | •          |        | _                |        |            |             |        | •          |            |        |           | Į           |        |            |  |
|                          | Kepi.1  | <b>e</b> 1 | 194    | <b>1</b>         | 1670   | 267        | 8           | 1250   | 8          | 87.2       | 1240   |           | 24          | 000/96 | 32800      |  |
| 1                        | Repl.2  | in (       | 150    | -                |        | 244        | 8           | 1190   | 8          | 82.4       | 1150   |           | 478         | 968000 | 32100      |  |
| 2                        | Repl.3  | 9          | 440    | 34               | -      | 150        | 69          | 1070   | 8)         | 81.4       | 1160   | 83        | 458         | 973000 | 26800      |  |
|                          | Repl.4  | 17         | 430    |                  | 1400   | 130        | 8>          | 1230   | <b>8</b>   | 72.1       | 1100   | 83        | 481         | 966000 | 33700      |  |
|                          | Average | 2          | 445    |                  | -      | 203        | :           | 1185   | ;;;        | 80.8       | 1163   | 68        | 473         | 968500 | 31350      |  |
|                          | S.D.    | 9          | 11     | *                | 120    | 53         | ;           | 70     |            | 5,5        | ያ      | 7         | 6           | 2693   | 2687       |  |
|                          | Repl.1  | 10         | 570    |                  |        | 61         | 8>          | 1530   | <b>8</b> > | 83.2       | 1290   | 88        | 292         | 976000 | 24400      |  |
|                          | Repl.2  | •0         | -      |                  |        | 4          | 8           | 1250   | 8)         | 72.2       | 1200   | 78        | 293         | 989000 | 11300      |  |
| m                        | Repl.3  | 20         | -      | т.<br>Т          | 1920   | 61         | <b>8</b> ×  | 1480   | <b>8</b> > | 94.9       | 1440   |           | 334         | 972000 | 27800      |  |
|                          | Repl.4  | 8          |        |                  |        | 61         | 8           | 1550   | <b>8</b> > | 104.0      | 1520   | 8         | <b>86</b> 8 | 964000 | 35900      |  |
|                          | Average | 15         | 9      |                  | 1823   | 8          | 1           | 1453   |            | 88.6       | 1363   | 68        | 328         | 975250 | 24850      |  |
|                          | S.D.    | 9          | 2      | *                | 161    | 9          | ļ           | 120    | 1          | 12.0       | 125    | 2         | 41          | 9038   | 8869       |  |
|                          | Repl.1  | ů          | 310    |                  |        | 10         | 8>          | 1370   | 6          | 57.7       | 1150   | 110       | 111         | 987000 | 13400      |  |
|                          | Repl.2  | 0          |        |                  |        |            | 8>          | 1470   | 8>         | 54.5       | 1030   |           | 107         | 986000 | 14400      |  |
| 4                        | Repl.3  | 0          |        | 53               | 940    |            | <b>8</b> >  | 1410   | 8>         | 56.8       | 1070   |           | 107         | 985000 | 14800      |  |
|                          | Repl.4  | 3          |        |                  | •••    |            | 8)          | 1540   | <b>8</b> > | 56.3       | 1120   | <u>18</u> | 109         | 987000 | 12800      |  |
|                          | Average | •          | 363    |                  |        | 20         | ļ           | 1448   | :          | 56.3       | 1093   | 100       | 109         | 986250 | 13850      |  |
| •                        | S.D.    | ļ          | 43     | -                | 27     | -          | ;           | 64     | ;          | 1.2        | 46     | 9         | 7           | 829    | 792        |  |
|                          | Repl.1  | 4          | 430    |                  | 1200   | 32         | 85          | 1460   | 8>         | 61.1       | 1320   |           | 180         | 986000 | 13900      |  |
|                          | Repl.2  | •          | 610    |                  | -      | 27         | đ           | 1550   | 8          | 64.8       | 1430   | 130       | 231         | 983000 | 16600      |  |
| Ð                        | Repl.3  | 8          | 580    |                  |        | 20         | 8>          | 1350   | 8)         | <b>36.</b> | 1240   |           | 178         | 985000 | 15100      |  |
|                          | Repl.4  | 9          |        | 53               | -      | 4          | <b>6</b> 8> | 1250   | <b>8</b> > | 67.3       | 1380   |           | 225         | 985000 | 14900      |  |
|                          | Average | Ð          | 513    |                  |        | 8          | 1           | 1403   |            | 62.4       | 1343   | 133       | 204         | 984750 | 15125      |  |
|                          | 3.D.    | 2          | 69     |                  |        | 2          | ;           | 113    | }          | 4.1        | 11     | -         | 23          | 1090   | <b>363</b> |  |
|                          |         |            |        |                  |        |            |             |        |            |            |        |           |             |        |            |  |
| <b>NBS 1646</b>          | 9       | 2          | 11300  |                  |        | 23         | 8>          | 1780   | 8>         | 30.8       | 758    | 53        | 123         |        | 1          |  |
| NBS 1646                 | 9       | \$         |        |                  |        | 25         | 8>          | 2030   | 8          | 32.9       | 786    | 52        | 127         | 1      | 1          |  |
| NBS 1646                 | 9       | 0          |        | 27               | 580    | 27         | 8>          | 1760   | 8)         | 35.0       | 851    | 62        | 134         | i      | :          |  |
|                          |         |            |        |                  |        |            |             |        |            |            |        |           |             |        |            |  |

.

;



STATION NUMBER

FIGURE 2: SEDIMENT MULTIPLE COMPARISON PLOT - SNIP 1990 - A1, Ca

Ca mg/g

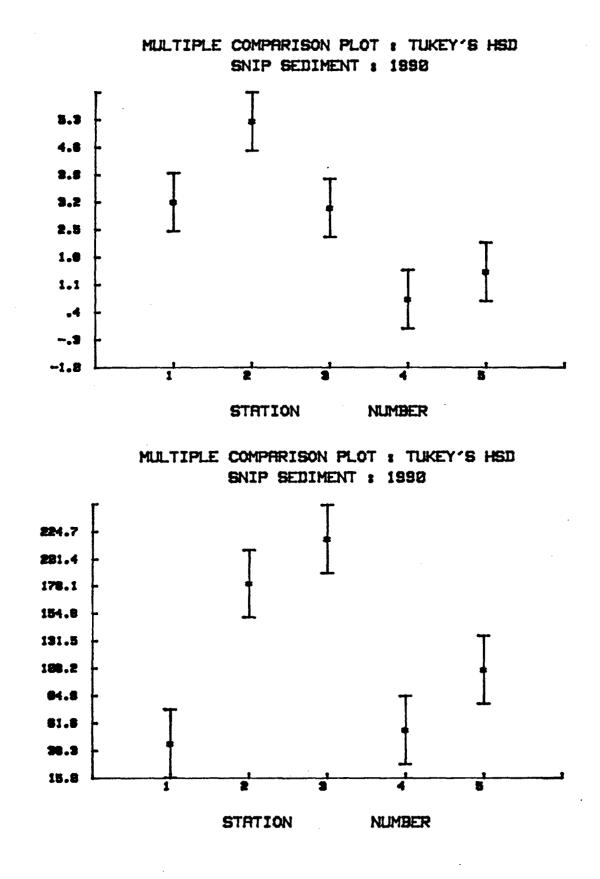


FIGURE 2: SEDIMENT MULTIPLE COMPARISON PLOT - SNIP 1990 - Cd, Cu

cd ug/g

Cu ug/g

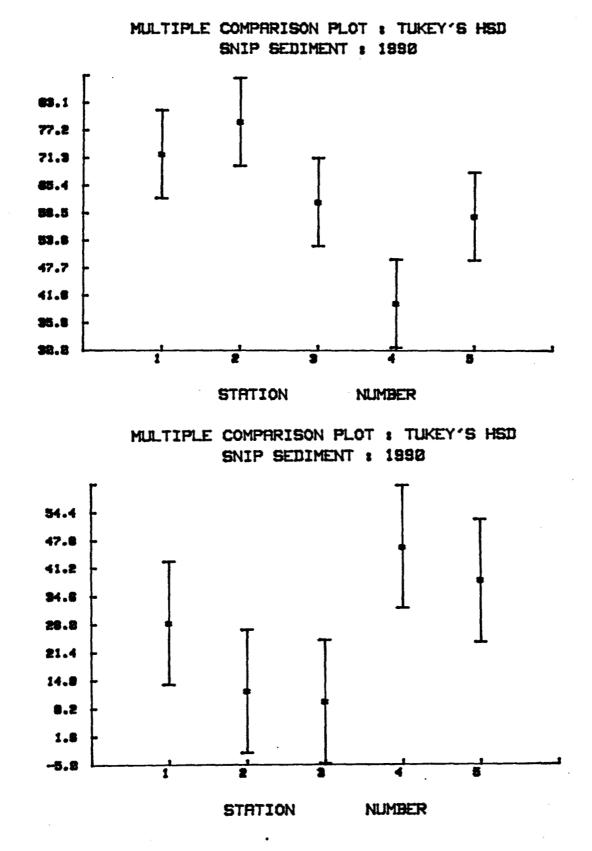
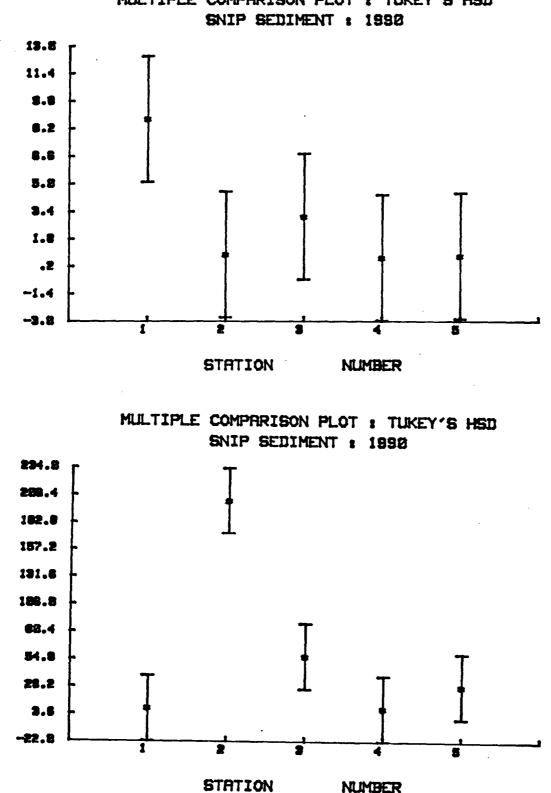


FIGURE 2: SEDIMENT MULTIPLE COMPARISON PLOT - SNIP 1990 - Fe, Hg

Fe mg/g

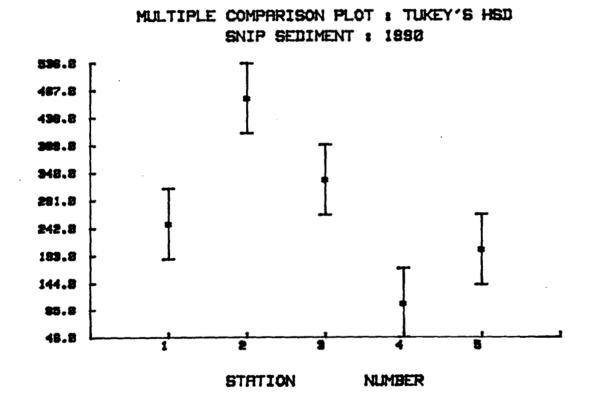
B/Bu BH



MULTIPLE COMPARISON PLOT : TUKEY'S HSD

- 15 -

FIGURE 2: SEDIMENT MULTIPLE COMPARISON PLOT - SNIP 1990 - Mn, Pb



₿∕₿n uZ

Sky Creek site (station 1) is characterised by relatively low aluminum, calcium, copper, lead, and zinc sediment concentrations in comparison with the other sites in this survey. This is a reflection of good water quality with low metal content, adequate buffering capacity and low hardness.

The Bronson Creek site (station 2) upstream of the Cominco camp is located about 3 km from the mouth of the creek. The area is influenced by the Bronson Glacier, Johnny Creek (receiving Skyline mine discharge) and natural acid rock drainage generated from the canyon walls in the lower part of the system. Sediment content showed detectable values for arsenic with an average of 108 ug/g. Except for mercury, high sediment values were found for most metals with the following averages: Cd 5.3 ug/g; Cu 180.0 ug/g; Pb 203 ug/g; Zn 473 ug/g. Water quality showed detectable total cadmium levels of 1.8 ug/l, and high total copper values with 117 ug/l. No detectable dissolved cadmium or copper could be found with the graphite furnace.

The Monsoon Creek site (station 3) sediment content showed only significantly higher aluminum, and copper values than station 1 for these fairly humic creeks. No significant difference could be detected between the two stations with any other metals. Station 3 showed higher alkalinity (125 mg/l) and hardness (157 mg/l) levels than any other stations in the survey. Sulphate levels were the highest of the receiving water stations surveyed with 45 mg/l.

The Iskut River site upstream of the Bronson Creek (station 4) and Iskut River site downstream of Monsoon Creek (station 5) did not show significant differences in the sediment metal analysis. These two sites had also the lower cadmium contentration in the sediments. The water quality at these two stations was dominated by the high suspended solids content which was in average 268 mg/l. Total metals were generally high for many contaminants such as aluminum, copper, and zinc however the dissolved fraction was close to or below the detection limit. - 18 -

Mine water collected at the level 130 (station 6) showed very high level of non-filterable residue (2370 mg/l) as compared to the two other levels 180 (station 7) and 300 (station 8) where the NFR levels were <5 mg/l. The levels 180, and 300 were not active at the time of the sampling, while active drilling was occurring at level 130. This explains the high total metal content for Al, Ca, Co, Cu, Fe, Mn, Si, and Zn, as compared to the other two levels. The metal contaminants (Al, As, Cd, Cu, Pb, Zn) were however close or below the detection limit for all levels in the dissolved fraction, except for station 6, Diss. Cu where the level was 0.0027 mg/l.

# REFERENCES

Anonymous. 1979. Laboratory Manual. Department of the Environmental Protection Service. Department of Fisheries and Oceans (Pacific Region).

.