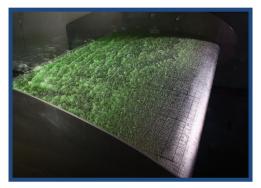
TP 15273E

WIND TUNNEL TRIALS TO SUPPORT FURTHER DEVELOPMENT OF ICE PELLET ALLOWANCE TIMES: WINTER 2013-14







Prepared for Transportation Development Centre

In cooperation with

Civil Aviation Transport Canada

and

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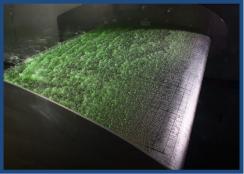
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WIND TUNNEL TRIALS TO SUPPORT FURTHER DEVELOPMENT OF ICE PELLET ALLOWANCE TIMES: WINTER 2013-14







by

Marco Ruggi



February 2015 Final Version 1.0 The contents of this report reflect the views of APS Aviation Inc. and not necessarily the official view or opinions of the Transportation Development Centre of Transport Canada.

The Transportation Development Centre does not endorse products or manufacturers. Trade or manufacturers' names appear in this report only because they are essential to its objectives.

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PREFACE

Under contract to the Transportation Development Centre of Transport Canada with support from the Federal Aviation Administration, APS Aviation Inc. has undertaken a research program to advance aircraft ground de/anti-icing technology. The specific objectives of the APS Aviation Inc. test program are the following:

- To develop holdover time data for all newly-qualified de/anti-icing fluids and update and maintain the website for the holdover time guidelines;
- To evaluate weather data from previous winters that can have an impact on the format of the holdover time guidelines;
- To conduct general and exploratory de/anti-icing research;
- To conduct tests to evaluate the effect of deployed flaps and slats prior to anti-icing;
- To conduct tests and research on surfaces treated with ice phobic products;
- To conduct tests with the snow machine to support ARP5485 changes;
- To conduct tests to evaluate holdover times in heavy snow conditions;
- To develop an SAE AIR for the evaluation of aircraft coatings;
- To support the evaluation of the National Research Council Canada propulsion icing wind tunnel to determine its flow characteristics;
- To develop holdover time guidance for operation in ice crystal conditions;
- To continue research for development of ice detection capabilities for pre-deicing, engine deicing and departing aircraft at the runway threshold;
- To develop a performance specification for electronic holdover time applications;
- To investigate pre-takeoff contamination check 5-minute allowance;
- To conduct full-scale general aviation aircraft windshield washer fluid deicing testing to substantiate and support flat plate testing results;
- To develop training and fluid failure photos/videos for global archive;
- To update the regression coefficient report with the newly-qualified de/anti-icing fluids; and
- To develop guidelines on radiation cooling during taxi.

The research activities of the program conducted on behalf of Transport Canada during the winter of 2013-14 are documented in eight reports. The titles of the reports are as follows:

- TP 15268E Winter Weather Impact on Holdover Time Table Format (1995-2014);
- TP 15269E Aircraft Ground Icing General Research Activities During the 2013-14 Winter;
- TP 15270E Regression Coefficients and Equations Used to Develop the Winter 2014-15 Aircraft Ground Deicing Holdover Time Tables;

- TP 15271E Aircraft Ground De/Anti-Icing Fluid Holdover Time Development Program for the 2013-14 Winter;
- TP 15272E Cold Climate Technologies Investigation of Sensor Technologies as an Alternative Means of Detecting Aircraft Icing (Year 3 of 3);
- TP 15273E Wind Tunnel Trials to Support Further Development of Ice Pellet Allowance Times: Winter 2013-14;
- TP 15274E Exploratory Wind Tunnel Aerodynamic Research Examination of Contaminated Anti-Icing Fluid Flow-Off Characteristics Winter 2013-14; and
- TP 15275E Investigation of Ice Phobic Technologies to Reduce Aircraft Icing in Northern and Cold Climates.

In addition, the following interim report is being prepared:

This report, TP 15273E has the following objective:

• To conduct research in the Circuit Propulsion Icing Wind Tunnel with a thin-high performance wing section to further support and develop the anti-icing fluid ice pellet allowance times.

This objective was met by conducting a series of full-scale tests using a thin high-performance wing model in the National Research Council Canada Propulsion Icing Wind Tunnel with the cooperation of Transport Canada and the Federal Aviation Administration.

PROGRAM ACKNOWLEDGEMENTS

This multi-year research program has been funded by Transport Canada with support from the Federal Aviation Administration, William J. Hughes Technical Center, Atlantic City, NJ. This program could not have been accomplished without the participation of many organizations. APS Aviation Inc. would therefore like to thank the Transportation Development Centre of Transport Canada, the Federal Aviation Administration, National Research Council Canada, and several fluid manufacturers.

APS Aviation Inc. would also like to acknowledge the dedication of the research team, whose performance was crucial to the acquisition of hard data. This includes the following people: Yelyzaveta Asnytska, Brandon Auclair; Steven Baker, Stephanie Bendickson, John D'Avirro, Jesse Dybka, Ben Falvo, Benjamin Guthrie, Michael Hawdur, Eric Perocchio, Dany Posteraro, Marco Ruggi, Gordon Smith, James Smyth, David Youssef, Nondas Zoitakis and Victoria Zoitakis.

Special thanks are extended to Howard Posluns, Yvan Chabot, Doug Ingold, Warren Underwood and Charles J. Enders, who on behalf of the Transportation Development Centre and the Federal Aviation Administration, have participated, contributed and provided guidance in the preparation of these documents.

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| 16. Abstract | , | | , | | |
| As part of a larger research program examining de/anti-icing fluid flow-off during simulated aircraft takeoff, APS Aviation Inc. conducted a series of full-scale tests in the National Research Council Canada 3 m x 6 m Open-Circuit Propulsion and Icing Wind Tunnel using a super critical wing model to determine the flow-off characteristics of anti-icing fluid with and without mixed precipitation conditions with ice pellets. A wind tunnel testing program was developed for the winter of 2013-14 with the primary objectives of conducting aerodynamic testing with a thin high performance airfoil ensure the repeatability of the dry wing performance, expand the ice pellet allowance times for light ice pellets mixed with light or moderate snow conditions, substantiate the current ice pellet allowance times with new fluids, fluids previously tested but with limited data, and temperatures close to the lowest operational use temperature (LOUT), and support the development of a Type III ice pellet allowance time table. | | | | | |
| The data collected in 2013-14 supported the development of a comprehensive Type III un-heated fluid allowance time table for use with high speed aircraft. Preliminary data was also collected with heated Type III fluid applications, however the tests showed risks of adhered contamination during take-off and therefore guidance could not be issued without further investigating the possible risks associated. | | | | | |
| Testing was conducted during the winter of 2013-14 to validate and expand the existing Type IV allowance times. The data collected in 2013-14 supported the following changes to the guidance material: 10-minute allowance time for moderate ice pellets at 115 knots rotation speed should be limited to -16°C due to the higher lift losses observed and 7-minute allowance time for Light Ice Pellets mixed with Moderate Snow below -5° to -10°C | | | | | |
| Possible future areas of research for the winter of 2014-15 may include allowance time testing to expand the guidance for mixed conditions including light ice pellets with light or moderate snow conditions, investigation of the higher lift losses observed at lower temperatures close to the fluid LOUT to determine the aerodynamic effects of ice pellet contamination at these colder temperatures, further substantiation of the ice pellet allowance times with new fluids, or fluids previously tested but with limited data, and lift loss scaling with NASA LS-0417 and NACA 23012 wing sections. | | | | | |
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| 17. Key Words Ice Pellet, Allowance Time, High Speed Rotation, Type II, Type III, Type IV, F Flow-Off, Wind Tunnel, Propulsion Icing Aerodynamics | luid Adherence, Fluid g Wind Tunnel, Wing | Transportat | mber of copi on Developmer | nt Centre | |
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| 15. | Remarques additionnelles (programmes de financement, titre | s de publications connexes, etc.) | | | | |
| | Plusieurs rapports de recherche sur des essais de technologies de dégivrage et d'antigivrage ont été produits au cours des hivers précédents pour le compte de Transports Canada. Ils sont disponibles auprès du Centre de développement des transports. Plusieurs rapports ont été rédigés dans le cadre du programme de recherche de cet hiver. Leur objet apparaît à l'avant-propos. Les travaux décrits dans ce rapport ont été en partie coparrainés par la Federal Aviation Administration. | | | | du programme de | |
| 16. | Résumé | | | | | |
| | Le présent rapport documente la série d'essais pleine grandeur réalisés dans la soufflerie de givrage à propulsion et à circuit ouvert de 3 m sur 6 m du Conseil national de recherches Canada, au moyen d'un modèle d'aile supercritique, afin de déterminer les caractéristiques de ruissellement du liquide d'antigivrage avec et sans conditions de précipitations mixtes comprenant des granules de glace. | | | | | |
| | Un programme d'essais en soufflerie a été élaboré pour l'hiver 2013-2014 avec comme principaux objectifs de réaliser des tests aérodynamiques au moyen d'une surface portante haute performance à profil mince afin d'assurer la répétabilité de la performance de l'aile sèche, d'élargir les marges de tolérance pour les granules de glace de façon à inclure les conditions mixtes de granules de glace légers avec de la neige légère ou modérée, de corroborer les marges de tolérance actuelles dans des conditions de granules de glace avec de nouveaux liquides et des liquides déjà testés, mais pour lesquels les données sont limitées, de même qu'à des températures se rapprochant de la température minimale d'utilisation opérationnelle (LOUT), et d'appuyer l'élaboration d'un tableau des marges de tolérance pour les liquides de type III dans des conditions de granules de glace. | | | | | |
| | Les données recueillies en 2013-2014 ont appuyé l'élaboration d'un tableau complet des marges de tolérance pour les liquides de type III non chauffés à utiliser avec les aéronefs à haute vitesse. Des données préliminaires ont aussi été recueillies pour l'application de liquides de type III chauffés, mais les essais ont démontré un risque que la contamination adhère aux surfaces durant le décollage ; il est donc impossible de formuler des lignes directrices à ce sujet avant d'avoir analysé les possibles risques associés. | | | | | |
| | Des essais ont été réalisés au cours de l'hiver 2013-2014 afin de valider et d'élargir les marges de tolérance existantes pour les liquides de type IV. Les données recueillies en 2013-2014 ont corroboré les changements suivants apportés aux lignes directrices : la marge de tolérance de 10 minutes dans des conditions de granules de glace modérés à une vitesse de rotation de 115 nœuds devrait être limitée à une température de -16 °C en raison des pertes de portance accrues observées, et la marge de tolérance de 7 minutes pour les granules de glace légers avec neige modérée à des températures inférieures à -10 °C. | | | | | |
| | Certains éléments qui pourraient être étudiés à l'hiver 2014-2015 peuvent inclure des essais sur les marges de tolérance visant à élargir les lignes directrices dans des conditions mixtes de façon à inclure les conditions de granules de glace légers avec de la neige légère ou modérée, l'analyse des pertes de portance supérieures observées à basse température se rapprochant de la température minimale d'utilisation opérationnelle du liquide (LOUT) afin de déterminer les effets aérodynamiques de la contamination par des granules de glace à ces températures plus froides, la corroboration supplémentaire des marges de tolérance dans des conditions de granules de glace avec les nouveaux liquides, ou avec les liquides déjà testés, mais pour lesquels les données sont limitées, et l'échelle des pertes de portance sur les profils d'aile NASA LS-0417 et NACA 23012. | | | | | |
| 17 | Mots clés | | 18. Diffusion | | | |
| 17. | Granule de glace, marge de tolérance, rotation à à basse vitesse, Type II, Type III, Type IV, | | Le Centre d | le développeme | | oorts dispose |
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EXECUTIVE SUMMARY

Under contract to the Transportation Development Centre (TDC), with financial support from the Federal Aviation Administration (FAA), APS Aviation Inc. (APS) has undertaken research activities to further advance aircraft ground de/anti-icing technology.

As part of a larger research program examining de/anti-icing fluid flow-off during simulated aircraft takeoff, APS conducted a series of full-scale tests in the National Research Council Canada (NRC) 3 m x 6 m Open-Circuit Propulsion Icing Wind Tunnel (PIWT) using a supercritical wing model to determine the flow-off characteristics of anti-icing fluid with and without mixed precipitation conditions with ice pellets.

Background and Objective

A wind tunnel testing program was developed for the winter of 2013-14 with the primary objectives of conducting aerodynamic testing with a thin high-performance airfoil to:

- Ensure the repeatability of the dry wing performance;
- Expand the ice pellet allowance times for light ice pellets mixed with light or moderate snow conditions;
- Substantiate the current ice pellet allowance times with new fluids, fluids previously tested but with limited data, and temperatures close to the lowest operational use temperature (LOUT); and
- Support the development of a Type III ice pellet allowance time table.

Additional research objectives were also attempted and are described in a separate report.

Conclusions

The data collected in 2013-14 supported the development of a comprehensive Type III unheated fluid allowance time table for use with high speed aircraft. Preliminary data was also collected with heated Type III fluid applications; however, the tests showed risk of adhered contamination during takeoff and therefore guidance could not be issued without further investigating the possible risks associated.

Testing was conducted during the winter of 2013-14 to validate and expand the existing Type IV allowance times. The data collected in 2013-14 supported the following changes to the guidance material:

- 10-minute allowance time for moderate ice pellets at 115 knots rotation speed should be limited to -16°C for propylene glycol (PG) fluids due to the higher lift losses observed; and
- 7-minute allowance time for Light Ice Pellets mixed with Moderate Snow below -5° to -10°C.

Future Research

Possible future areas of research for the winter of 2014-15 may include:

- Allowance time testing to expand the guidance for mixed conditions, including light ice pellets with light or moderate snow conditions;
- Investigation of the higher lift losses observed at lower temperatures close to the fluid LOUT to determine the aerodynamic effects of ice pellet contamination at these colder temperatures;
- Further substantiation of the ice pellet allowance times with new fluids, or fluids previously tested but with limited data; and
- Lift loss scaling with National Aeronautics and Space Administration (NASA) LS-0417 and NACA 23012 wing sections.

SOMMAIRE

Dans le cadre d'un contrat avec le Centre de développement des transports (CDT) et avec l'appui financier de la Federal Aviation Administration (FAA), APS Aviation Inc. (APS) a entrepris des activités de recherche visant à faire progresser les technologies associées au dégivrage et à l'antigivrage d'aéronefs au sol.

Le présent rapport documente la série d'essais pleine grandeur réalisés dans la soufflerie de givrage à propulsion et à circuit ouvert de 3 m sur 6 m du Conseil national de recherches Canada (CNRC), au moyen d'un modèle d'aile supercritique, afin de déterminer les caractéristiques de ruissellement du liquide d'antigivrage avec et sans conditions de précipitations mixtes comprenant des granules de glace.

Contexte et objectif

Un programme d'essais en soufflerie a été élaboré pour l'hiver 2013-2014 avec comme principaux objectifs de réaliser des tests aérodynamiques au moyen d'une surface portante haute performance à profil mince afin :

- D'assurer la répétabilité de la performance de l'aile sèche ;
- D'élargir les marges de tolérance pour les granules de glace de façon à inclure les conditions mixtes de granules de glace légers avec de la neige légère ou modérée ;
- De corroborer les marges de tolérance actuelles dans des conditions de granules de glace avec de nouveaux liquides et des liquides déjà testés, mais pour lesquels les données sont limitées, de même qu'à des températures se rapprochant de la température minimale d'utilisation opérationnelle (LOUT) ; et
- D'appuyer l'élaboration d'un tableau des marges de tolérance pour les liquides de type III dans des conditions de granules de glace.

D'autres objectifs de recherche ont aussi été ciblés et sont décrits dans un rapport distinct.

<u>Conclusions</u>

Les données recueillies en 2013-2014 ont appuyé l'élaboration d'un tableau complet des marges de tolérance pour les liquides de type III non chauffés à utiliser avec les aéronefs à haute vitesse. Des données préliminaires ont aussi été recueillies pour l'application de liquides de type III chauffés, mais les essais ont démontré un risque que la contamination adhère aux surfaces durant le décollage ; il est donc impossible de formuler des lignes directrices à ce sujet avant d'avoir analysé les possibles risques associés.

Des essais ont été réalisés au cours de l'hiver 2013-2014 afin de valider et d'élargir les marges de tolérance existantes pour les liquides de type IV. Les données recueillies en 2013-2014 ont corroboré les changements suivants apportés aux lignes directrices :

- La marge de tolérance de 10 minutes dans des conditions de granules de glace modérés à une vitesse de rotation de 115 nœuds devrait être limitée à une température de -16 °C pour les liquides à base de propylène glycol en raison des pertes de portance accrues observées ; et
- La marge de tolérance de 7 minutes pour les granules de glace légers avec neige modérée à des températures inférieures à -5° à -10 °C.

Recherches à venir

Voici certains éléments qui pourraient être étudiés à l'hiver 2014-2015 :

- Essais sur les marges de tolérance visant à élargir les lignes directrices dans des conditions mixtes de façon à inclure les conditions de granules de glace légers avec de la neige légère ou modérée ;
- Analyse des pertes de portance supérieures observées à basse température se rapprochant de LOUT du liquide afin de déterminer les effets aérodynamiques de la contamination par des granules de glace à ces températures plus froides ;
- Corroboration supplémentaire des marges de tolérance dans des conditions de granules de glace avec les nouveaux liquides, ou avec les liquides déjà testés, mais pour lesquels les données sont limitées ; et
- Mise à l'échelle des pertes de portance sur les profils d'aile National Aeronautics and Space Administration (NASA) LS-0417 et NACA 23012.

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GLOSSARY

| APS | APS Aviation Inc. |
|------|---|
| AWG | G-12 Aerodynamics Working Group |
| FAA | Federal Aviation Administration |
| НОТ | Holdover Time |
| LOUT | Lowest Operational Use Temperature |
| MSC | Meteorological Service of Canada |
| NASA | National Aeronautics and Space Administration |
| NRC | National Research Council Canada |
| ΟΑΤ | Outside Air Temperature |
| PG | Propylene Glycol |
| PIWT | 3 m x 6 m Open-Circuit Propulsion Icing Wind Tunnel |
| RTD | Resistance Temperature Detector |
| тс | Transport Canada |
| TDC | Transportation Development Centre |

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1. INTRODUCTION

Under winter precipitation conditions, aircraft are cleaned with a freezing point depressant fluid and protected against further accumulation by an additional application of such a fluid, possibly thickened to extend the protection time. Aircraft ground deicing had, until recently, never been researched and there is still an incomplete understanding of the hazard and of what can be done to reduce the risks posed by the operation of aircraft in winter precipitation conditions. This "winter operations contaminated aircraft – ground" program of research is aimed at overcoming this lack of knowledge.

Since the early 1990s, the Transportation Development Centre (TDC) of Transport Canada (TC) has managed and conducted de/anti-icing related tests at various sites in Canada; it has also coordinated worldwide testing and evaluation of evolving technologies related to de/anti-icing operations with the co-operation of the United States Federal Aviation Administration (FAA), the National Research Council Canada (NRC), the Meteorological Service of Canada (MSC), several major airlines, and deicing fluid manufacturers. The TDC is continuing its research, development, testing and evaluation program.

Under contract to the TDC, with financial support from the FAA, APS Aviation Inc. (APS) has undertaken research activities to further advance aircraft ground de/anti-icing technology.

As part of a larger research program examining de/anti-icing fluid flow-off during simulated aircraft takeoff, APS conducted a series of full-scale tests in the NRC 3 m x 6 m Open-Circuit Propulsion Icing Wind Tunnel (PIWT) using a supercritical wing model to determine the flow-off characteristics of anti-icing fluid with and without mixed precipitation conditions with ice pellets.

1.1 Background

In 2005-06, the inability for operators to release aircraft in ice pellet conditions led TC and the FAA to begin a research campaign to develop allowance times. Developing holdover times (HOTs) was not feasible due to the properties of the ice pellets, as they remain embedded in the fluid and take longer to dissolve compared to snow, which is immediately absorbed and dissolved. Research was initiated through live aircraft testing with the NRC Falcon 20 in Ottawa, Canada, and later evolved to a more controlled environment with the NRC Propulsion Icing Wind Tunnel, also in Ottawa.

The early testing in 2005-06 with the Falcon 20 primarily used visual observations to evaluate fluid flow-off. During the Falcon 20 work, the wing was anti-iced and exposed to contamination, and aborted takeoff runs allowed researchers onboard to observe and evaluate the fluid flow-off. Testing in 2006-07 began in the Propulsion Icing Wind Tunnel (PIWT), allowing aerodynamic data to be used for evaluating fluid flow-off performance. The PIWT also allowed for a more controlled environment less susceptible to the elements.

The work continued each year, and the test methods and equipment improved, allowing for real-time data analysis, better repeatability, and an overall greater confidence in the results. The work conducted by the FAA and TC was presented by APS to the G-12 Aerodynamics Working Group (AWG) and the HOT Committee yearly since 2006. Additional presentations were also given to the AWG in May 2012 and May 2013 by National Aeronautics and Space Administration (NASA) and the NRC, which focused on the extensive calibration and characterization work performed with a generic thin high-performance airfoil. This work also helped increase confidence in how the data was used to help support and develop TC/FAA guidance material. A detailed account of the more recent work conducted is included in the report, TC report, TP 15232E, *Wind Tunnel Trials to Examine Anti-Icing Fluid Flow-Off Characteristics and to Support the Development of Ice Pellet Allowance Times, Winters 2009-10 to 2012-13 (1).*

The Ice Pellet Allowance Time research has helped further develop and improve the PIWT facility. As a result, a new medium is now available for aerodynamic testing of aircraft ground icing fluids with or without contamination in a full-scale format. Several other ground deicing projects have been ongoing as a result of industry requests and are expected to continue. The PIWT has evolved into a multidisciplinary facility; however, it continues to be the primary source for the development and further refinement of the ground deicing ice pellet allowance time guidance material.

1.2 Program Objectives

A wind tunnel testing program was developed for the winter of 2013-14 with the primary objectives of conducting aerodynamic testing with a thin high-performance airfoil to:

- Ensure the repeatability of the dry wing performance;
- Expand the ice pellet allowance times for light ice pellets mixed with light or moderate snow conditions;
- Substantiate the current ice pellet allowance times with new fluids, fluids previously tested but with limited data, and temperatures close to the lowest operational use temperature (LOUT);

- Support the development of a Type III ice pellet allowance time table;
- Evaluate the effect of coatings on aerodynamics with and without fluids;
- Evaluate the equivalency of the new ice pellet/snow dispenser systems; and
- Evaluate Type I fluid flow-off performance for low-speed rotation less than 80 knots.

As secondary objectives, preliminary testing was also conducted to:

- Evaluate an airfoil performance monitor (APM) system;
- Investigate aerodynamic effects of heavy contamination; and
- Evaluate the effect of a cooling system on testing repeatability.

The work statement for these tests is provided in Appendix A.

Table 1.1 demonstrates the groupings for the global set of tests conducted at the wind tunnel during the winter of 2013-14. Only tests pertaining to the baseline and ice pellet allowance time testing (Objectives #1, #2, #3, and #4) are described in this report.

| Objective # | Objective | # of Runs |
|-------------|--|--------------|
| 1 | Baseline | 26 |
| 2 | Type III Allowance Times | 28 |
| 3 | Ice Pellet Expansion | 11 |
| 4 | Ice Pellet Validation with New Temperatures & Fluids | 10 |
| 5 | Ice Phobic Coatings | 257 |
| 6 | Type I Very Low Speed | 31 |
| 7 | New Ice Pellet Dispenser System Validation | 11 |
| 8 | R&D (APM, Heavy Contamination, Cooling System) | 9 |
| | Total | 383 |

 Table 1.1: Summary of 2013-14 Wind Tunnel Tests by Objective

1.3 Previous Ice Pellet Allowance Time Tables

The Type IV allowance time tables have been available since the winter of 2007-08. Each year, the Type IV testing has built upon the latest version of the allowance time table published in the TC and FAA HOT Guidelines.

In the case of Type III fluid, early research was conducted during the winter of 2008-09 with the LS-0417 wing section, and a preliminary allowance time table was developed (see Table 1.2). However, this table was never published due to the limitations of the data. The data collected was for low-speed 80-knot tests conducted with fluid applied at air temperature. Concerns were raised by the regulators; more testing was proposed at higher speeds (100 knots) as well as with heated fluid application to investigate any risks of adherence.

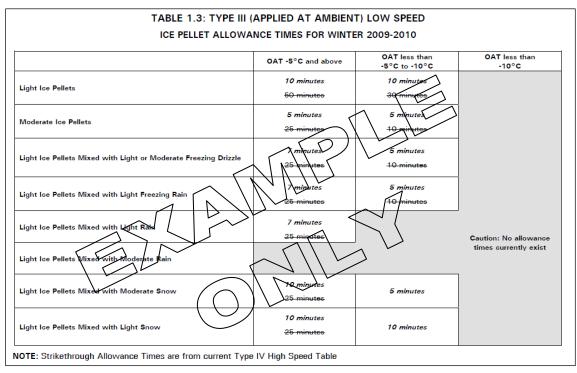


Table 1.2: Prototype Type III Allowance Time Table Developed in 2008-09

1.4 Report Format

The wind tunnel work has been conducted since the winter of 2006-07 and has been documented in yearly reports. A detailed account of the more recent work conducted is included in the report, TP 15232E (1). It contains more thorough details regarding the testing methodologies as well as links to previous historical reports. The current

report has been prepared in a more abbreviated format. The following list provides short descriptions of subsequent sections of this report:

- a) Section 2 describes the methodology used in testing, as well as equipment and personnel requirements necessary to carry out testing;
- b) Section 3 describes data collected during the full-scale testing conducted;
- c) Sections 4 to 9 describe the testing conducted to further develop the allowance time tables in each respective condition;
- d) Section 10 presents a summary of the conclusions and observations; and
- e) Section 11 lists the recommendations for future testing.

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2. METHODOLOGY

This section provides a brief description of the test methodology and equipment specific to the full-scale aerodynamic tests conducted at the NRC PIWT.

For more details, see TP 15232E (1), which contains more thorough details regarding the testing methodologies.

2.1 Test Schedule

Fifteen days of testing were conducted over a period of four weeks starting January 8, 2014, and ending January 29, 2014. Setup and teardown time was minimal and was done on the first and last day of testing. Testing days were selected based on weather. Table 2.1 presents the calendar of wind tunnel tests performed. It should be noted that the tests listed comprise all the tests conducted, which also include the tests pertaining to other objectives not discussed in this report. At the beginning of each test day, a plan was developed that included the list of tests (taken from the global test plan) to be completed based on the weather conditions and testing priorities. This daily plan was discussed, approved, and modified (if necessary) by TC, the FAA, and APS.

| Date (Start date in case of overnight) | # of Tests Run |
|--|----------------|
| 8 January 2014 | 6 |
| 9 January 2014 | 10 |
| 10 January 2014 | 9 |
| 13 January 2014 | 41 |
| 14 January 2014 | 68 |
| 15 January 2014 | 58 |
| 16 January 2014 | 52 |
| 17 January 2014 | 15 |
| 20 January 2014 | 36 |
| 21 January 2014 | 18 |
| 22 January 2014 | 21 |
| 23 January 2014 | 6 |
| 27 January 2014 | 13 |
| 28 January 2014 | 14 |
| 29 January 2014 | 16 |
| Total | 383 |

Table 2.1: Calendar of Tests

2.2 Wind Tunnel Procedure

To satisfy the fluid testing objective, simulated takeoff and climb-out tests were performed with the supercritical wing section. Different parameters including fluid thickness, wing temperature, and fluid freezing point were recorded at designated times during the tests. The supercritical wing section was constructed by the NRC specifically to conduct these tests following extensive consultations with an airframe manufacturer to ensure a representative supercritical design.

The procedure for each fluid test was as follows:

- a) The wing section was treated with anti-icing fluid, poured in a one-step operation (no Type I fluid was used during the tests);
- b) When applicable, contamination, in the form of simulated ice pellets, freezing rain, and/or snow, was applied to the wing section. Test parameters were measured at the beginning and end of the exposure to contamination;
- c) At the end of the contamination period, the tunnel was cleared of all equipment and scaffolding;
- d) The wind tunnel was subsequently operated through a simulated takeoff and climb-out test; and
- e) The behaviour of the fluid during takeoff and climb-out was recorded with digital high-speed still cameras. In addition, windows overlooking the wing section allowed observers to document the fluid elimination performance in real-time.

The procedure for the wind tunnel trials is included in Appendix B. The procedure includes details regarding the test objectives, test plan, procedure and methodology, and pertinent information and documentation.

2.2.1 Test Sequence

The length of each test (from start of setup to end of last measurement) varied largely due to the length of exposure to precipitation (if applicable). Time required for setup and teardown as well as preparing and configuring the wing section was relatively the same from test to test. Figure 2.1 demonstrates a sample timeline for a typical wind tunnel test. It should be noted that a precipitation exposure time of 30 minutes was used for illustration purposes; this time varied for each test depending on the objective.

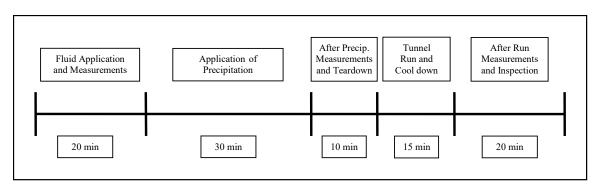


Figure 2.1: Typical Wind Tunnel Test Timeline

2.3 Wind Tunnel and Airfoil Model Technical Overview

The following sections describe the wind tunnel and major components.

2.3.1 Wind Tunnel Test Site

PIWT tests are performed at the NRC Aerospace Facilities, Building M-46, at the NRC Montreal Road campus, located in Ottawa, Canada. Figure 2.2 provides a schematic of the NRC Montreal Road campus showing the location of the NRC PIWT. Photo 2.1 shows an outside view of the wind tunnel test facility. Photo 2.2 shows an inside view of the wind tunnel test section. The open-circuit layout, with a fan at entry, permits contaminants associated with the test articles (such as heat or de/anti-icing fluid) to discharge directly, without recirculating or contacting the fan. The test section is 3 m (10 ft.) wide by 6 m (20 ft.) high by 12 m (40 ft.) long, with a maximum wind speed of 78 knots when using the electrical turbine drive and with a maximum wind speed of just over 115 knots when using the gas turbine drive. The fan is normally driven electrically, but high-speed operation can be accommodated by a gas turbine drive system. Due to the requirements of both high-speed and low-speed operations during the testing, the gas turbine was selected to allow for greater flexibility. The gas turbine drive can perform both low- and high-speed operations, whereas the electric drive is limited to low-speed operations. Scaffolding was constructed to allow access to the wing section, which facilitated the application of fluids and the subsequent inspection and cleaning of the airfoil.

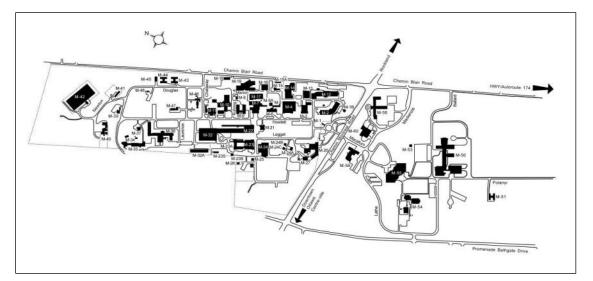


Figure 2.2: Schematic of NRC Montreal Road Campus

2.3.2 Generic High-Performance "Supercritical" Commuter Airfoil

The wing section used for testing was a generic high-performance commuter airfoil, also referred to as "supercritical." This wing section was constructed by the NRC in 2009 specifically to conduct these tests following extensive consultations with an airframe manufacturer to ensure a representative supercritical design. The original wing design was representative of an outboard section and did not include a flap; the flap was later added at the request of TC, the FAA, and APS. A computational fluid dynamics analysis of the modified wing section was conducted by the airframe manufacturer, and it was confirmed that the wing section provided a good representation of a flapped section of an operational thin high-performance wing. Photo 2.3 shows the wing section used for testing.

A cross sectional view of the supercritical wing section used for testing has been included in Figure 2.3; the dimensions indicated are in meters. Some of the pertinent dimensions of the wing section are:

- a) Chord length not including flap: 1.4 m (4.6 ft.); and
- b) Width: 2.4 m (8 ft.).

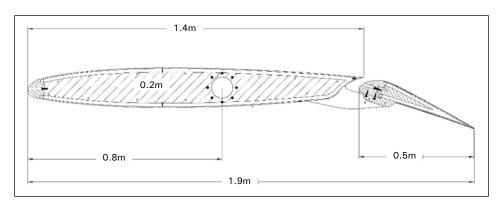


Figure 2.3: Generic "Supercritical " Wing Section

An analysis of the wing section model was conducted by the airframe manufacturer to determine the typical rest position of this type of wing section. It was determined that on a typical commuter aircraft, this section of wing would typically be pitched forward by 2° when sitting on the ground. As a result, the NRC ensured the rest position of the wing model was set to -2° for each test.

The wing section was fitted with a hinged flap. The flap position was fixed at 20° and was not intended to be changed during testing. The top surface of the flap wing section had a steeper angle; a flap setting of 20° created close to a 26° slope on the top surface of the flap (with the wing pitched forward by 2°). As testing progressed, the ability to change the flap setting from 0° to 20° was necessary; contrary to a nested flap, which is typically protected during precipitation, a hinged flap is always exposed, and results indicated earlier failures were due to the shallower angle of the hinged flap. Modifications were made by the NRC to allow the flap setting to alternate between 0° and 20° for the fluid application and contamination periods; however, all takeoff simulations were conducted with the flap set to 20°. No moveable devices were available on the wing section. Detailed coordinates for this airfoil are available.

End plates were installed on the wing section to eliminate the "wall effects" from the wind tunnel walls and to provide a better aerodynamic flow-off above the test area. Figure 2.4 demonstrates the end plates installed on the thin high-performance wing section (note: the wing section is depicted without the top wing skin).

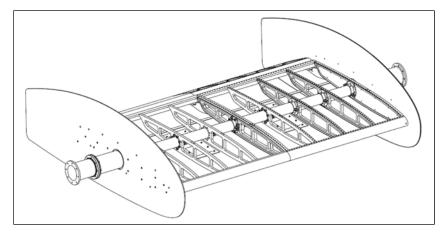


Figure 2.4: End Plates Installed on Supercritical Wing Section

2.3.3 Test Area Grid

APS personnel used markers to draw a grid on the wing's upper surface (excluding the flap). Each grid cell measured 5.1 cm x 5.1 cm (2 in. x 2 in.) with the cell axis positioned perpendicular and parallel to the leading edge (see Photo 2.4). The grid section was 2.4 m (8 ft.), which covered the entire wing section. The grid markings began approximately 10.1 cm (4 in.) aft of the leading edge stagnation point and continued along the length of the main chord; grid markings were not drawn on the flap section. The grid was used to facilitate observations of the fluid shearing off the wing and the movement of ice pellets during takeoff.

It should be noted that the grid was not re-drawn on the ice phobic skins installed over top of the wing section as the previous grid markings were still visible; however, this should be considered for future tests.

2.3.4 Wind Tunnel Measurement Capabilities

The supercritical wing section was supported on either side by 2-axis weigh scales capable of measuring drag and lift forces generated on the wing section. The wing section was attached to servo-systems capable of pitching the wing section to a static angle or generating dynamic movements. The servo-system was programmed to simulate pitch angles during takeoff and climb-out based on operational aircraft flight profiles.

The wing section was also equipped with eight Resistance Temperature Detectors (RTDs); these were installed by NRC personnel recording the skin temperature on the leading edge (LE), mid chord (MID), trailing edge (TE), and under-wing (UND). RTDs

were placed along a chord 0.5 m (1.5 ft.)in pairs to the left and to the right of the wing centreline. The following are the locations of the RTDs:

- RTD LE located approximately 25 cm from the leading edge (as measured along wing skin curvature);
- RTD MID located approximately 70 cm from the leading edge (as measured along wing skin curvature);
- RTD TE located approximately 30 cm from the trailing edge (as measured along wing skin curvature); and
- RTD UND located approximately 45 cm from the leading edge.

Figure 2.5 demonstrates the general location of the RTDs. These RTDs were primarily used to monitor the skin temperature in real-time through the NRC data display system and were recorded by APS personnel as described in Subsection 2.15.3.

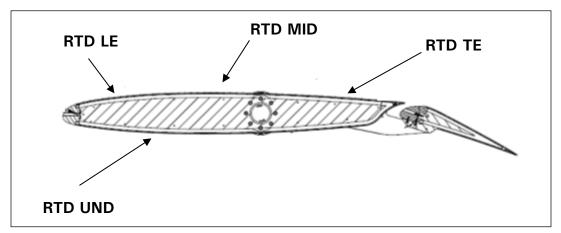


Figure 2.5: Location of RTDs Installed Inside Supercritical Wing

The wind tunnel was also equipped with sensors recording the following parameters:

- Air temperature inside the tunnel;
- Outside air temperature;
- Air pressure;
- Wind speed; and
- Relative humidity.

2.4 Simulated Precipitation

The following types of precipitation have been simulated for aerodynamic research in the PIWT:

- Ice Pellets;
- Snow;
- Freezing Rain/Rain; and
- Other conditions related to HOTs.

2.4.1 Ice Pellets

Simulated ice pellets were produced with diameters ranging from 1.4 mm to 4.0 mm to represent the most common ice pellet sizes observed during natural events. The ice pellets were manufactured inside a refrigerated truck (see Photo 2.5). Cubes of ice were crushed and passed through calibrated sieves (see Photo 2.6) to obtain the required ice pellet size range. Hand-held motorized dispensers were used to dispense the ice pellets. The ice pellets were applied to the leading and trailing edges of the wing at the same time.

2.4.2 Snow

Snow was produced using the same method for producing ice pellets. The snow used consisted of small ice crystals measuring less than 1.4 mm in diameter. Previous testing conducted by APS investigated the dissolving properties of the simulated snow versus natural snow. The simulated snow was selected as an appropriate substitute for natural snow.

The snow was manufactured inside a refrigerated truck. Cubes of ice were crushed and passed through calibrated sieves to obtain the required snow size range. Hand-held motorized dispensers were used to dispense the snow. The snow was applied to the leading and trailing edges of the wing at the same time.

2.4.3 Freezing Rain/Rain

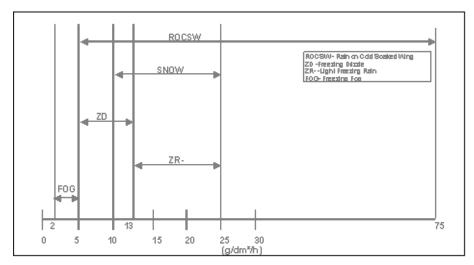
The same sprayer head and scanner used for HOT testing at the NRC Climatic Engineering Facility was employed for testing. The sprayer system uses compressed air and distilled water to produce freezing rain. The temperature of the water is controlled and is kept just above freezing temperature in order to produce freezing rain. To produce rain, the temperature of the water is raised until the precipitation no longer freezes on the test surfaces.

2.4.4 Definition of Precipitation Rates

When simulating precipitation rates for full-scale and plate testing, the rate limits defined for standard HOT testing were referenced. Figure 2.6 demonstrates the HOT testing rate precipitation breakdown.

HOT testing protocol for ice pellets does not currently exist. As a result, ice pellet precipitation rate limits were based on the freezing rain rate breakdown. The following precipitation rates were used for the full-scale and flat plate testing conducted during the winter of 2008-09:

| Light Ice Pellets: | 13-25 g/dm²/h; |
|----------------------------|--------------------------------|
| Moderate Ice Pellets: | 25-75 g/dm²/h; |
| Light Freezing Rain: | 13-25 g/dm²/h; |
| Moderate Freezing Drizzle: | 5-13 g/dm²/h; |
| Light Rain: | 13-25 g/dm²/h; |
| Moderate Rain: | 25-75 g/dm²/h; |
| Light Snow: | 4-10 g/dm ² /h; and |
| Moderate Snow | 10-25 g/dm²/h. |





2.5 Test Equipment

A considerable amount of test equipment was used to perform these tests. Key items are described in the following subsections; a full list of equipment is provided in the test procedure, which is included in Appendix B.

2.5.1 Video and Photo Equipment

APS used the observation windows on the sides of the test section to install Canon EOS XTi DSLR cameras and Profoto Compact 600 flashes capable of second-by-second photography with an intervalometer. In addition, GoPro cameras were used for wide-angle filming of fluid flow-off during the test runs. Photos 2.9 and 2.10 demonstrate the camera setup used for the testing period.

2.5.2 Refractometer/Brixometer

Fluid freezing points were measured using a hand-held Misco 10431VP refractometer with a Brix scale (shown in Figure 2.7). The freezing points of the various fluid samples were determined using the conversion curve or table provided to APS by the fluid manufacturer.

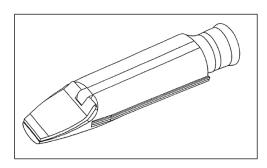


Figure 2.7: Hand-Held Refractometer/Brixometer

2.5.3 Wet Film Thickness Gauges

Wet film thickness gauges, shown in Figure 2.8, were used to measure fluid film thickness. These gauges were selected because they provide an adequate range of thicknesses (0.1 mm to 10.2 mm) for Type I/II/III/IV fluids. The rectangular gauge has a finer scale and was used in some cases when the fluid film was thinner (toward the end of a test). The observer recorded a thickness value (in mils), as read directly from the thickness gauge. The recorded value was the last wetted tooth of the

thickness gauge; however, the true thickness lies between the last wetted tooth and the next un-wetted tooth. A thickness conversion table was used to convert the recorded thickness values into the corrected thickness values.

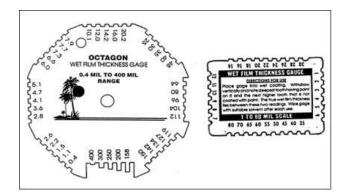


Figure 2.8: Wet Film Thickness Gauges

2.5.4 Temperature Sensor

When required, wing skin temperature and fluid temperature were measured using a Wahl digital heat-probe thermometer Model 392Vxc. A surface temperature probe was used for wing skin temperature measurements (generally, wing-mounted RTDs were used), and an immersion probe was used for measuring and monitoring fluid temperatures.

2.6 Personnel

During the fluid testing and exploratory research testing, four APS staff members were required to conduct the tests, and four additional persons from Ottawa were tasked to manufacture and dispense ice pellets as well as to help with general setup tasks. A professional photographer was retained to record digital images of the test setup and test runs. Representatives from NASA, the TDC, and the FAA provided direction in testing and participated as observers. Photo 2.12 shows a portion of the research team (due to scheduling, not all participants were available for the photo).

2.7 Data Forms

Several different forms were used to facilitate the documentation of the various data collected in the wind tunnel tests. These forms include:

a) General Form;

- b) Wing Temperature, Fluid Thickness and Fluid Brix Form;
- c) Ice Pellet and Snow Dispensing Forms;
- d) Sprayer Calibration Form;
- e) Visual Evaluation Rating Form;
- f) Condition of Wing and Plate Form;
- g) Fluid Receipt Form; and
- h) Log of Fluid Sample Bottles.

Copies of these forms are provided in the test procedure, which is included in Appendix B. Completed wing temperature, fluid thickness, and fluid Brix data forms have been included in Appendix C.

2.8 Data Collection

Fluid thickness, fluid Brix, and skin temperature measurements were collected by APS personnel. The measurements were collected before and after fluid application, after the application of contamination, and at the end of the test. The completed data forms have been scanned and included in Appendix C for referencing purposes.

High-speed digital photographs of each test were taken. In addition, videos were also taken during a greater portion of the tests. Due to the large amount of data available, photos of the individual tests have not been included in this report; rather, the high-resolution photos are in electronic format and have been made available to the TDC and can be seen upon request.

2.9 De/Anti-Icing Fluids

Seven fluids were used during the wind tunnel tests conducted during the winter of 2013-14. The seven fluids were leftover inventory acquired during the 2012-13 winter season that were verified for viscosity and overall integrity prior to the 2013-14 testing. The viscosity of the fluids received was measured using the Stony Brook PDVdi-120 Falling Ball Viscometer and the Brookfield Digital Viscometer Model DV-1 + to ensure the fluid was within the fluid manufacturer production specifications and comparable to previous samples received. The pertinent characteristics of these fluids are given in Table 2.2.

2.9.1 Viscometer

Historically, viscosity measurements were carried out using a Brookfield viscometer (Model DV-1 +, shown in Photo 2.13) fitted with a recirculating fluid bath and small sample adapter.

In recent years, on-site measurements are done with the Stony Brook PDVdi-120 Falling Ball Viscometer (Photo 2.14) to obtain a verification of the fluid integrity; falling ball tests are much faster and more convenient to perform as compared to tests with the Brookfield viscometer.

2.9.2 Type II/III/IV Fluid Application Equipment

The Type II/III/IV fluids were stored outside the wind tunnel and were kept at air temperature. The fluids were poured rather than sprayed so that application would not change the fluid viscosity. This methodology was appropriate given the relatively small test area of the wing section and the goal of minimizing the amount of fluid flowing off the wing.

Type II/III/IV fluids are generally received in 20 L containers; however, some fluids are received in large 200 L barrels and larger 1000 L totes. The fluid is applied to the wing section by using smaller 2 L containers (Photo 2.11). Approximately 16 L to 20 L of fluid were applied to the wing section for each test; less fluid was required for the less viscous Type III fluid. Due to the flat top surface of the supercritical wing, the thickened fluid did not easily settle and flow on the top surface. The wing was therefore tilted forward (by approximately 10 degrees) for 1 minute following the end of fluid application to allow for the fluid to spread out evenly over the top surface of the wing.

2.9.3 Waste Fluid Collection

Using a relatively small test area and applying the fluids by pouring minimized the amount of fluid falling off the wing. APS personnel used a vacuum to collect the fluid that would drip onto the tunnel floor prior to each test. The NRC also fitted the wind tunnel with appropriate drainage tubes to collect spent fluid during the takeoff test runs. At the end of the testing period, the services of Lacombe Waste Services were employed to safely dispose of the waste glycol fluid.

2.10 Analysis Methodology

The following provides a brief description of the analysis methodology. More details on the analysis methodology can be found in TP 15232E (1).

Each ice pellet test was analysed in detail using the following objectives:

- a) Test parameters;
- b) Visual ratings at the start of the test;
- c) Visual ratings at rotation;
- d) 8° lift loss; and
- e) Overall test status.

The evaluation grades for each criterion were "good," "review," or "bad." These grades were determined based on whether the criteria satisfied each test objective requirement. Figure 2.9 shows a summary of each test objective and criteria.

Several test parameters were evaluated, such as tunnel temperature before the start of the test, rate of precipitation, and exposure time of precipitation. These parameters were compared against the target parameters described in the test plan. The ramp-up time was also evaluated and compared to the target ramp-up time determined; this became less of an issue after 2011-12 with the use of the automated ramp-up system instead of the previous manual system.

2.10.1 Visual Ratings at the Start of the Test

During each of the tests conducted, visual contamination ratings were determined by three observers: one observer from the FAA and two observers from APS. The level of contamination present on the leading edge and trailing edge of the wing, as well as on the flap, was quantified using a scale of one-to-five with five being the worst case scenario. Partial numbers were sometimes assigned when cases were also marginally above or below a specific rating.

The visual contamination rating criteria at the start of the test on both the leading and trailing edge must be equal to 3 or less in order to pass. The flap must have a rating of 4 or less. For a review grade to be given, the leading and trailing edge must have a rating between 3 and 3.5, and the flap must have a rating between 4 and 4.5. Any rating greater than 3.5 on the leading and trailing edge is considered a fail, while anything greater than 4.5 on the flap is a fail.

2.10.2 Visual Ratings at Rotation

The visual contamination rating criteria at the time of rotation on the leading edge must be equal to 1 or less in order to pass. For a review grade to be given, the leading edge must have a rating between 1 and 1.5. Any rating on the leading edge greater than 1.5 is considered a fail.

2.10.3 Eight Degree Lift Loss

For a pass, the 8° lift loss must be less than 5.4 percent. A review grade was given should the lift loss be between 5.4 percent and 9.2 percent. Any lift loss greater than 9.2 is considered a fail.

2.10.4 Overall Test Status

After all objectives were analysed, an overall status was given a "good," "review," or "bad." This provided an overall summary for each test. The overall status was determined by the worst case scenario from any of the test objectives; if any of the criteria were given a "bad" grade, the overall status would be "bad" and the test is considered a fail.

2.10.5 Dry Wing Calibration

To ensure the accuracy of the testing results, a dry wing calibration test was conducted at the start of each day. The dry wing test allowed the research team to ensure that the model aerodynamics did not change due to mechanical, communication, or analytical errors. Dry wing tests were also conducted following any mechanical modification to the airfoil (i.e., after applying the ice phobic wing skins). During the winter of 2013-14, the dry wing results demonstrated that the changes in dry wing performance were within the range of experimental error and did not indicate any repeatability issues with the model.

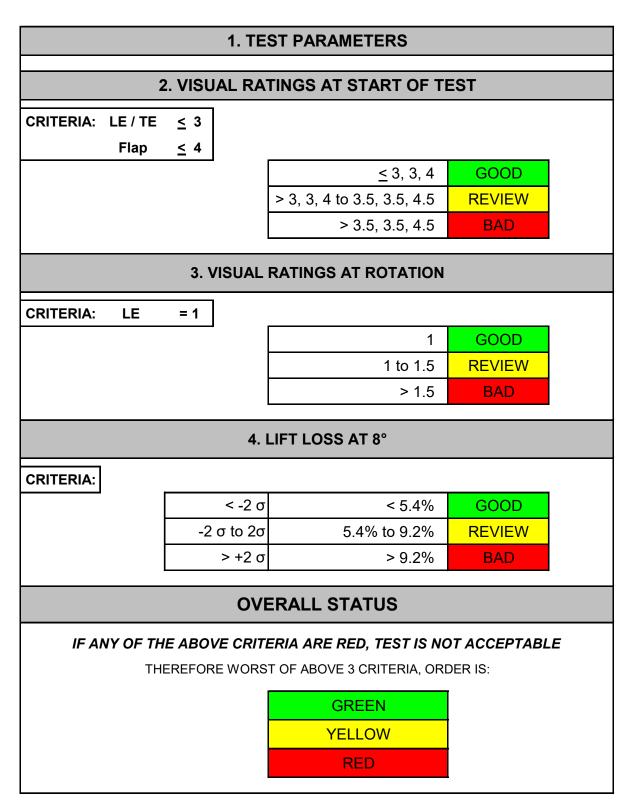


Figure 2.9: Ice Pellet Test Analysis Criteria

| Test # | Sample Name | Dilution | MID OR LOW VISCOSITY | Receiving Quantity | Method Type | Method | Spindle | Fluid Volume | Fluid Temp | Speed | Time (mins) | Can-Am Result (cP) 2012-13 | Can-Am Result (cP) 2013-14 | TAKE SAMPLE FROM | Without Guardleg |
|-----------|---------------------------------|----------|----------------------------|-----------------------|----------------|--------|---------|-----------------|---------------|-------|----------------|-------------------------------------|-------------------------------------|--------------------------------|---------------------|
| 1 | Kilfrost ABC-S Plus | 100/0 | MID | 500 | AIR/MAN | С | LV2 | 150 | 20 | 0.3 | 10 | 19,996 | 25,200 | From unopened containers | 19,800 |
| 2 | Dow FlightGuard AD-49 | 100/0 | MID | 700 | MAN. | k | 31 | 10 | 20 | 0.3 | 10 | 14,397 | 14,100 | From unopened containers | - |
| 3 | DOW EG 106 | 100/0 | MID | 800 | AIR | g | LV1 | 500 mL | 20 | 0.3 | 10 | 3,979 | 3,420 | From unopened drum | - |
| 4 | CLARIANT 2031 | 100/0 | MID | 200 | MAN. | h | LV0 | 16 | 20 | 0.3 | 10 | 554 | 322 | From opened drum | - |
| 5 | Clariant MPIV Launch | 100/0 | MID | 400 | AIR/MAN | g | LV1 | 500 | 20 | 0.3 | 10 | 13,997 | 13,320 | From unopened drum | - |
| 6 | Clariant MaxFlight 04 | 100/0 | MID | 700 | MAN. | d | LV1 | 500 | 20 | 0.3 | 33.33 | 11,658 | 11,780 | From unopened containers | - |
| 7 | Cryotech Polar Guard Advance | 100/0 | MID | 600 | MAN. | n | 34 | 10 | 20 | 0.3 | 10 | 15,200 | 15,400 | From unopened containers | - |

Table 2.2: 2013-14 Re-Testing of Existing 2012-13 Leftover Fluid Inventory

NOTES:

- Test #1: the fluid was completely de-bubbled in an ultrasonic bath

- Tests #1, #3, #5, #6 were performed with the Guard Leg - Test #1 was repeated without Guard Leg (19800 cP)

> APS/Library/Projects/PM2265.003 (TC Deicing 13-14)/Reports/Ice Pellet/Final Version 1.0/TP 15273E Final Version 1.0.docx Final Version 1.0, October 20

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Photo 2.1: Outside View of NRC Wind Tunnel Facility

Photo 2.2: Inside View of NRC Wind Tunnel Test Section





Photo 2.3: Thin High-Performance Wing Section Used for Testing

Photo 2.4: Grid Markings on Thin High-Performance Wing Section

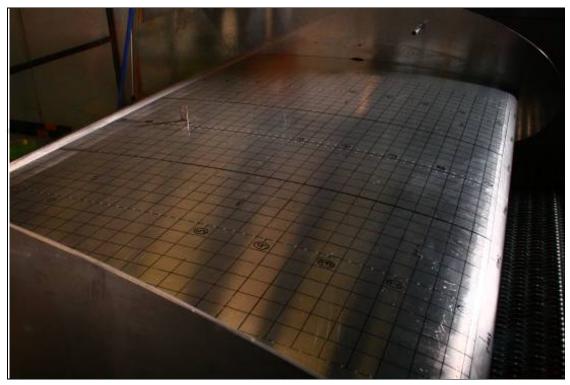




Photo 2.5: Refrigerated Truck Used for Manufacturing Ice Pellets

Photo 2.6: Calibrated Sieves Used to Obtain Desired Size Distribution





Photo 2.7: Ice Pellet Dispensers Operated by APS Personnel

Photo 2.8: Ceiling-Mounted Freezing Rain Sprayer





Photo 2.9: Wind Tunnel Setup for Flashes

Photo 2.10: Wind Tunnel Setup for Digital Cameras

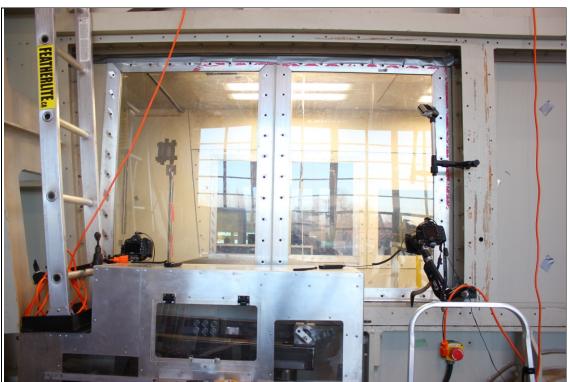




Photo 2.11: Fluid Pour Containers

Photo 2.12: 2012-13 Research Team





Photo 2.13: Brookfield Digital Viscometer Model DV-1+

Photo 2.14: Stony Brook PDVdi-120 Falling Ball Viscometer



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3. FULL-SCALE DATA COLLECTED

3.1 Test Log

A calendar of the tests conducted during the winter of 2013-14 can be found in Table 2.1. A detailed log of the tests conducted in the NRC PIWT is shown in Table 3.1. Data pertaining to all test objectives (exploratory research objectives as well) is included in the log. Table 3.1 provides relevant information for each of the tests, as well as final values used for the data analysis. Each column contains data specific to one test. The following is a brief description of the column headings for Table 3.1:

| Run #: | Exclusive number identifying each test run. |
|-------------------------|--|
| Test Plan #: | Exclusive number used for planning purposes and identified in the test procedure. |
| Year: | The year in which the test was conducted. |
| Objective: | Main objective of the test. |
| Test Condition: | Description of the simulated conditions for the test. |
| Fluid: | Aircraft anti-icing fluid used during the test. |
| Rotation Angle: | Maximum angle of rotation obtained during simulated takeoff run; began testing with a max 8° rotation angle and increased to 20° as testing progressed. |
| Flap Angle: | Positioning of the flap during the precipitation period; either 0° (retracted) or 20° (extended). <i>Note: Flap was always extended at 20° during</i> <i>the takeoff run.</i> |
| Date: | Date when the test was conducted. |
| Precipitation End Time: | End time of the application of precipitation, recorded in local time. |
| Tunnel Start Time: | Start of the simulated takeoff run, recorded in local time. |
| OAT Before Test (°C): | Outside air temperature recorded just before the start of the simulated takeoff test, measured in degrees Celsius. |

| | <i>Note: Not an important parameter as "Tunnel Temp. Before Test" was used as actual test temperature for analysis.</i> |
|---------------------------------------|---|
| Tunnel Temp. Before Test (°C): | Static tunnel air temperature recorded just before the start of the simulated takeoff test, measured in degrees Celsius. <i>Note: This parameter was used as the actual</i> <i>test temperature for analysis.</i> |
| Avg. Wing Temp. Before Test (°C): | Average of the wing skin temperature measurements just before the start of the simulated takeoff test, recorded in degrees Celsius. |
| Precipitation Rate (Type: [g/dm²/h]): | Simulated freezing precipitation rate (or combination of different precipitation rates). "N/A" indicates that no precipitation was applied. |
| Exposure Time: | Simulated precipitation period, recorded in minutes. |

The visual contamination ratings are described below. Visual contamination ratings were typically reported as the average of the three observer ratings and rounded to the nearest decimal. The visual contamination ratings system is further described in Subsection 4.1.

Visual Contamination Rating Before Takeoff (LE, TE, Flap):

Visual contamination rating determined before the start of the simulated takeoff:

- 1 Contamination not very visible, fluid still clean.
- 2 Contamination is visible, but lots of fluid still present.
- 3 Contamination visible, spots of bridging contamination.
- 4 Contamination visible, lots of dry bridging present.
- 5 Contamination visible, adherence of contamination.

Visual Contamination Rating at Rotation (LE, TE, Flap):

Visual contamination rating determined at the time of rotation:

| | Contamination not very visible, fluid still clean. Contamination is visible, but lots of fluid still present. Contamination visible, spots of bridging contamination. Contamination visible, lots of dry bridging present. Contamination visible, adherence of contamination. |
|--|---|
| <i>Visual Contamination Rating</i> <i>After Takeoff (LE, TE, Flap):</i> | Visual contamination rating determined at the end of the test: 1 - Contamination not very visible, fluid still clean. 2 - Contamination is visible, but lots of fluid still present. 3 - Contamination visible, spots of bridging contamination. 4 - Contamination visible, lots of dry bridging present. 5 - Contamination visible, adherence of contamination. |
| CL at 0° Before Rotation: | Calculated lift coefficient at the 0° wing angle position just prior to the start of the rotation; data provided by NRC. |
| CL at 8° During Rotation: | Calculated lift coefficient at the 8° wing rotation angle position; data provided by the NRC. |
| CL at 4° Following End of Rotation: | Calculated lift coefficient at the 4° wing rotation angle position attained at the end of the rotation cycle; data provided by the NRC. |
| % Lift Loss: | Percentage lift loss calculated based on the comparison of the 8° lift coefficient during the test run versus the dry wing average lift coefficient. |
| Speed (kts): | Maximum speed obtained during simulated takeoff run, recorded in knots. |

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° Cl vs Dry Cl | Speed Kts |
|-----------|--------------|-----------------|--------------------------------|---------------|-------------------|-------------------------------|----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|---|--------------|
| 1 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 8-Jan-14 | -9.9 | -9.3 | - | - | - | - | - | 1.460 | 0.38% | 80 |
| 2 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 8-Jan-14 | -9.9 | -9.3 | - | - | - | - | - | 1.473 | -0.56% | 100 |
| 3 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 8-Jan-14 | -10.1 | -10.1 | - | - | - | - | - | 1.460 | 0.34% | 80 |
| 4 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 8-Jan-14 | -10.1 | -10.1 | - | - | - | - | - | 1.474 | -0.60% | 100 |
| 5 | 2013-14 | R&D | EFFECT OF COOLING SYSTEM | | 8 | 20 | 8-Jan-14 | -9.2 | -5.2 | - | - | - | - | - | 1.439 | 1.78% | 100 |
| 6 | 2013-14 | R&D | EFFECT OF COOLING SYSTEM | EG106 | 8 | 20 | 8-Jan-14 | n/a | n/a | - | - | - | - | - | n/a | - | 100 |
| 7 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 9-Jan-14 | -11.5 | -9.9 | - | - | - | - | - | 1.462 | 0.24% | 80 |
| 8 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 9-Jan-14 | -10.1 | -7.3 | - | - | - | - | - | 1.471 | -0.41% | 100 |
| 9 | 2013-14 | IP Expansion | IP- / SN- | ABC-S Plus | 8 | 20 | 9-Jan-14 | -10.1 | -7.3 | IP = 25 SN = 10 | 10 | 2, 2, 2.5 | 1, 1.5, 1.75 | 1, 1, 1.1 | 1.370 | 6.47% | 100 |
| 10 | 2013-14 | IP Expansion | IP- / SN | ABC-S Plus | 8 | 20 | 9-Jan-14 | -9.6 | -6.7 | IP = 25 SN = 25 | 10 | 2, 2, 3 | 1, 1.5, 2.25 | 1, 1, 1.2 | 1.372 | 6.38% | 100 |
| 11 | 2013-14 | IP Expansion | IP- / SN | Launch | 8 | 20 | 9-Jan-14 | -9 | -5.2 | IP = 25 SN = 25 | 10 | 2, 1.75, 3.25 | 1, 1.35, 2.25 | 1, 1, 1.2 | 1.367 | 6.70% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--------------------------------|-------------------|----------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 12 | 2013-14 | IP Expansion | IP- / SN | AD-49 | 8 | 20 | 9-Jan-14 | -7.4 | -3.3 | IP = 25 SN = 25 | 10 | 2, 2, 3.5 | 1, 1.6, 2.25 | 1, 1.2, 1.4 | 1.381 | 5.75% | 100 |
| 13 | 2013-14 | Type III Allowance Times | IP- / SN | 2031 - Cold | 8 | 20 | 9-Jan-14 | -7.4 | -3.1 | IP = 25 SN = 25 | 10 | 2.25, 1.9, 3.5 | 1, 1.5, 1.95 | 1, 1.15, 1.2 | 1.431 | 2.32% | 100 |
| 14 | 2013-14 | Type III Allowance Times | IP- / SN- | 2031 - Cold | 8 | 20 | 9-Jan-14 | -7.2 | -4.2 | IP = 25 SN = 10 | 10 | 2, 2, 2.1 | 1, 1.05, 1.25 | 1, 1, 1 | 1.441 | 1.64% | 100 |
| 15 | 2013-14 | Type III Allowance Times | IP- | 2031 - Cold | 8 | 20 | 9-Jan-14 | -7.1 | -4.7 | IP=25 | 10 | 2, 2, 2 | 1, 1, 1.15 | 1, 1, 1 | 1.434 | 2.14% | 100 |
| 16 | 2013-14 | Type III Allowance Times | IP Mod | 2031 - Cold | 8 | 20 | 9-Jan-14 | -7.3 | -4.8 | IP=75 | 5 | 2, 2, 2.15 | 1, 1.1, 1.4 | 1, 1, 1 | 1.441 | 1.63% | 100 |
| 17 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 10-Jan-14 | -11.2 | -4.8 | - | - | - | - | - | 1.465 | 0.00% | 80 |
| 18 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 10-Jan-14 | -11.2 | -4.8 | - | - | - | - | - | 1.462 | 0.22% | 100 |
| 19 | 2013-14 | Type III Allowance Times | IP- / ZR- | 2031 - Cold | 8 | 20 | 10-Jan-14 | -9.2 | -3.8 | IP = 25 ZR = 25 | 7 | 2, 2, 2.15 | 1, 1, 1.5 | 1, 1, 1.35 | 1.442 | 1.57% | 100 |
| 20 | 2013-14 | Type III Allowance Times | IP- / ZR- | 2031 - Hot | 8 | 20 | 10-Jan-14 | -8.5 | -3.3 | IP = 25 ZR = 25 | 7 | 1.25, 1.5, 1.45 | 1, 1, 1 | 1, 1, 1 | 1.439 | 1.77% | 100 |
| 21 | 2013-14 | Type III Allowance Times | IP- | 2031 - Hot | 8 | 20 | 10-Jan-14 | -7.7 | -5.2 | IP = 25 | 10 | 2, 2, 2.1 | 1, 5, 1 | 1, 5, 1 | 1.437 | 1.90% | 100 |
| 22 | 2013-14 | Type III Allowance Times | IP- | 2031 - Hot | 8 | 20 | 10-Jan-14 | -7.2 | -2.8 | IP=25 | 7 | 1.9, 1.75, 1.25 | 1, 3, 1 | 1, 3, 1 | 1.441 | 1.64% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--------------------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 23 | 2013-14 | Type III Allowance Times | IP- | 2031 - Hot | 8 | 20 | 10-Jan-14 | -6.9 | -2.9 | IP=25 | 5 | 1.5, 1.25, 1.15 | 1, 1, 1 | 1, 1, 1 | 1.436 | 2.00% | 100 |
| 24 | 2013-14 | Type III Allowance Times | IP Mod | 2031 - Hot | 8 | 20 | 10-Jan-14 | -6.7 | -3 | IP = 75 | 5 | 2.25, 2, 2.25 | 1, 5, 1 | 1, 5, 1 | 1.444 | 1.46% | 100 |
| 25 | 2013-14 | Type III Allowance Times | IP- / SN | 2031 - Hot | 8 | 20 | 10-Jan-14 | -6.1 | -2.3 | IP = 25 SN = 25 | 10 | 2.5, 2, 3.75 | 1, 3.25, 3.75 | 1, 5, 3.75 | 1.439 | 1.76% | 100 |
| 26 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 13-Jan-14 | 4.8 | 8.1 | - | - | - | - | - | 1.460 | 0.35% | 80 |
| 27 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 13-Jan-14 | 4.8 | 8.1 | - | - | - | - | - | 1.477 | -0.81% | 100 |
| 28 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.470 | -0.29% | 100 |
| 29 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.471 | -0.37% | 100 |
| 30 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.473 | -0.56% | 100 |
| 31 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.481 | -1.10% | 100 |
| 32 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.482 | -1.14% | 100 |
| 33 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.482 | -1.11% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 34 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 80 |
| 35 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 80 |
| 36 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 80 |
| 37 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 100 |
| 38 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 100 |
| 39 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 100 |
| 40 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 115 |
| 41 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 115 |
| 42 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | n/a | - | 115 |
| 43 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 22 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.461 | 0.26% | 80 |
| 44 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 22 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.466 | -0.03% | 80 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 45 | 2013-14 | lce Phobic R&D | Dry Wing | none | 22 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.466 | -0.03% | 80 |
| 46 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.474 | -0.63% | 100 |
| 47 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.469 | -0.27% | 100 |
| 48 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 13-Jan-14 | 5.5 | 5.7 | - | - | - | - | - | 1.469 | -0.26% | 100 |
| 49 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 40 |
| 50 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 40 |
| 51 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 40 |
| 52 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 60 |
| 53 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 60 |
| 54 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 60 |
| 55 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 80 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 56 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 80 |
| 57 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 80 |
| 58 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 100 |
| 59 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 100 |
| 60 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | 100 |
| 61 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | max (120) |
| 62 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | max (120) |
| 63 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | n/a | - | max (120) |
| 64 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | 1.448 | 1.21% | 80 |
| 65 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | 1.464 | 0.09% | 80 |
| 66 | 2013-14 | lce Phobic R&D | Dry Wing | none | 23 | 20 | 13-Jan-14 | 6.1 | 6.4 | - | - | - | - | - | 1.464 | 0.09% | 80 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 67 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.466 | -0.08% | 100 |
| 68 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.459 | 0.44% | 100 |
| 69 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.460 | 0.33% | 100 |
| 70 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.471 | -0.38% | 100 |
| 71 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.470 | -0.32% | 100 |
| 72 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.470 | -0.32% | 100 |
| 73 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 80 |
| 74 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 80 |
| 75 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 80 |
| 76 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 100 |
| 77 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 78 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 100 |
| 79 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 115 |
| 80 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 115 |
| 81 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 115 |
| 82 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 20 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.449 | 1.11% | 80 |
| 83 | 2013-14 | lce Phobic R&D | Dry Wing | none | 20 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.449 | 1.14% | 80 |
| 84 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 20 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.447 | 1.24% | 80 |
| 85 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.458 | 0.46% | 100 |
| 86 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.461 | 0.27% | 100 |
| 87 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.462 | 0.20% | 100 |
| 88 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.464 | 0.11% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 89 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.465 | 0.04% | 100 |
| 90 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.461 | 0.30% | 100 |
| 91 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.470 | -0.31% | 100 |
| 92 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.472 | -0.44% | 100 |
| 93 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.470 | -0.33% | 100 |
| 94 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 80 |
| 95 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 80 |
| 96 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 80 |
| 97 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 100 |
| 98 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 100 |
| 99 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 100 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 115 |
| 101 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 115 |
| 102 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | n/a | - | 115 |
| 103 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 20 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.445 | 1.37% | 80 |
| 104 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 20 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.444 | 1.44% | 80 |
| 105 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 20 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.451 | 0.97% | 80 |
| 106 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.463 | 0.17% | 100 |
| 107 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.460 | 0.36% | 100 |
| 108 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.4 | 4.3 | - | - | - | - | - | 1.461 | 0.31% | 100 |
| 109 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.460 | 0.33% | 100 |
| 110 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.458 | 0.50% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 111 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.462 | 0.25% | 100 |
| 112 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.466 | -0.02% | 100 |
| 113 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.464 | 0.06% | 100 |
| 114 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.466 | -0.07% | 100 |
| 115 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 80 |
| 116 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 80 |
| 117 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 80 |
| 118 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 100 |
| 119 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 100 |
| 120 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 100 |
| 121 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 115 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 122 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 115 |
| 123 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | n/a | - | 115 |
| 124 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.444 | 1.43% | 80 |
| 125 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.443 | 1.53% | 80 |
| 126 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.446 | 1.30% | 80 |
| 127 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.458 | 0.50% | 100 |
| 128 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.454 | 0.76% | 100 |
| 129 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | 4.3 | 4.4 | - | - | - | - | - | 1.453 | 0.85% | 100 |
| 130 | 2013-14 | lce Phobic R&D | Fluid Only | EG106 | 8 | 20 | 14-Jan-14 | -0.4 | 1.2 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.426 | 2.65% | 100 |
| 131 | 2013-14 | lce Phobic R&D | Fluid Only | EG106 | 8 | 20 | 14-Jan-14 | -0.5 | 1.2 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.427 | 2.62% | 100 |
| 132 | 2013-14 | lce Phobic R&D | Fluid Only | EG106 | 8 | 20 | 14-Jan-14 | -1.3 | 1.1 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.424 | 2.83% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 133 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | -1.2 | -0.3 | - | - | - | - | - | 1.444 | 1.45% | 100 |
| 134 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 14-Jan-14 | -1.2 | -0.3 | - | - | - | - | - | 1.445 | 1.36% | 100 |
| 135 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -1.1 | 1.4 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.426 | 2.71% | 100 |
| 136 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -1.5 | -0.5 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.425 | 2.74% | 100 |
| 137 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -1.7 | 0.9 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.430 | 2.42% | 100 |
| 138 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.5 | 0.4 | - | - | - | - | - | 1.456 | 0.65% | 100 |
| 139 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.5 | 0.4 | - | - | - | - | - | 1.457 | 0.55% | 100 |
| 140 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.454 | 0.76% | 100 |
| 141 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.452 | 0.93% | 100 |
| 142 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.462 | 0.20% | 100 |
| 143 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.462 | 0.25% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|---------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 144 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.461 | 0.29% | 100 |
| 145 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 100 |
| 146 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 80 |
| 147 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 80 |
| 148 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 80 |
| 149 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 100 |
| 150 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 100 |
| 151 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 100 |
| 152 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 115 |
| 153 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 115 |
| 154 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | n/a | - | 115 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 155 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.442 | 1.59% | 80 |
| 156 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.443 | 1.49% | 80 |
| 157 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.435 | 2.05% | 80 |
| 158 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.453 | 0.82% | 100 |
| 159 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.455 | 0.69% | 100 |
| 160 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -2.3 | -1.5 | - | - | - | - | - | 1.454 | 0.80% | 100 |
| 161 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -2.9 | -1.2 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.426 | 2.70% | 100 |
| 162 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -3 | -1.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.426 | 2.68% | 100 |
| 163 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -3.3 | -1.8 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.426 | 2.66% | 100 |
| 164 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -4.3 | 0.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.436 | 1.99% | 100 |
| 165 | 2013-14 | lce Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -4.1 | -2.9 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.437 | 1.95% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 166 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -4.3 | 0.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.436 | 2.00% | 100 |
| 167 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 15-Jan-14 | -0.3 | 0.3 | - | - | - | - | - | 1.479 | -0.96% | 100 |
| 168 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 15-Jan-14 | -0.3 | 0.3 | - | - | - | - | - | 1.456 | 0.64% | 80 |
| 169 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.459 | 0.45% | 100 |
| 170 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.1 | -1 | ŀ | - | - | ŀ | - | 1.459 | 0.44% | 100 |
| 171 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.457 | 0.56% | 100 |
| 172 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.468 | -0.20% | 100 |
| 173 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.466 | -0.07% | 100 |
| 174 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.468 | -0.20% | 100 |
| 175 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 80 |
| 176 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 80 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 177 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 80 |
| 178 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 100 |
| 179 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 100 |
| 180 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 100 |
| 181 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 115 |
| 182 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 115 |
| 183 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | n/a | - | 115 |
| 184 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.435 | 2.04% | 80 |
| 185 | 2013-14 | lce Phobic R&D | Dry Wing | none | 23 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.445 | 1.35% | 80 |
| 186 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.435 | 2.09% | 80 |
| 187 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.453 | 0.81% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 188 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.455 | 0.68% | 100 |
| 189 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 15-Jan-14 | -1.1 | -1 | - | - | - | - | - | 1.457 | 0.54% | 100 |
| 190 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -0.9 | -0.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.429 | 2.46% | 100 |
| 191 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -0.8 | -0.5 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.424 | 2.80% | 100 |
| 192 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 15-Jan-14 | -0.9 | -0.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.430 | 2.40% | 100 |
| 193 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.1 | -0.3 | - | - | - | - | - | 1.462 | 0.25% | 100 |
| 194 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.1 | -0.3 | - | - | - | - | - | 1.456 | 0.62% | 100 |
| 195 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.460 | 0.39% | 100 |
| 196 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.456 | 0.66% | 100 |
| 197 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.453 | 0.86% | 100 |
| 198 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.461 | 0.32% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 199 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.462 | 0.25% | 100 |
| 200 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.463 | 0.13% | 100 |
| 201 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 100 |
| 202 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 100 |
| 203 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 100 |
| 204 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 80 |
| 205 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 80 |
| 206 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 80 |
| 207 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 115 |
| 208 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 115 |
| 209 | 2013-14 | lce Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | n/a | - | 115 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 210 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.439 | 1.78% | 80 |
| 211 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.439 | 1.81% | 80 |
| 212 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.442 | 1.60% | 80 |
| 213 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.458 | 0.49% | 100 |
| 214 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.455 | 0.70% | 100 |
| 215 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -1.9 | -2.3 | - | - | - | - | - | 1.456 | 0.66% | 100 |
| 216 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 16-Jan-14 | -2 | -0.8 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.426 | 2.68% | 100 |
| 217 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 16-Jan-14 | -2.2 | -1.1 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.424 | 2.84% | 100 |
| 218 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 16-Jan-14 | -2.5 | -2.2 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.426 | 2.65% | 100 |
| 219 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -2.6 | -1.8 | - | - | - | - | - | 1.448 | 1.21% | 100 |
| 220 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -2.6 | -1.8 | - | - | - | - | - | 1.450 | 1.01% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 221 | 2013-14 | lce Phobic R&D | ZR | none | 8 | 20 | 16-Jan-14 | -2.8 | -1.8 | ZR = 100 | 2 | - | - | - | 1.427 | 2.59% | 100 |
| 222 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.458 | 0.50% | 100 |
| 223 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.455 | 0.71% | 100 |
| 224 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.449 | 1.14% | 100 |
| 225 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.461 | 0.29% | 100 |
| 226 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.458 | 0.50% | 100 |
| 227 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | 100 |
| 228 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 229 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 230 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 231 | 2013-14 | lce Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 232 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 233 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 234 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 235 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 236 | 2013-14 | Ice Phobic R&D | Dry Wing | none | n/a* | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | n/a | - | n/a* |
| 237 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.435 | 2.09% | 100 |
| 238 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.439 | 1.80% | 100 |
| 239 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.434 | 2.10% | 100 |
| 240 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.450 | 1.03% | 100 |
| 241 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.443 | 1.50% | 100 |
| 242 | 2013-14 | lce Phobic R&D | Dry Wing | none | 8 | 20 | 16-Jan-14 | -3 | -3.4 | - | - | - | - | - | 1.449 | 1.12% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|------------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 243 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 16-Jan-14 | -3.5 | -1.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.422 | 2.96% | 100 |
| 244 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 16-Jan-14 | -3.7 | -3.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.422 | 2.94% | 100 |
| 245 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 17-Jan-14 | -3.8 | -1.8 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.414 | 3.47% | 100 |
| 246 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 17-Jan-14 | -4.1 | -1.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.420 | 3.07% | 100 |
| 247 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 17-Jan-14 | -4.2 | -2.6 | - | - | - | - | - | 1.449 | 1.13% | 100 |
| 248 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 17-Jan-14 | -4.2 | -2.6 | - | - | - | - | - | n/a | - | 100 |
| 249 | 2013-14 | Ice Phobic R&D | ZR | none | 8 | 20 | 17-Jan-14 | -4.1 | -1.5 | - | 5 | - | - | - | 1.446 | 1.34% | 100 |
| 250 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 17-Jan-14 | -4.3 | 0 | - | - | - | - | - | 1.447 | 1.26% | 80 |
| 251 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 17-Jan-14 | -4.3 | 0 | - | - | - | - | - | 1.463 | 0.17% | 100 |
| 252 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 17-Jan-14 | -4.3 | -0.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.463 | 0.16% | 100 |
| 253 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 17-Jan-14 | -4.4 | -1.4 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.434 | 2.11% | 60 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|------------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 254 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 17-Jan-14 | -4.5 | -1.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.437 | 1.91% | 55 |
| 255 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 17-Jan-14 | -4.5 | -0.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.440 | 1.71% | 45 |
| 256 | 2013-14 | Type I Low Speed | Baseline | none | 8 | 20 | 17-Jan-14 | -4.4 | -0.2 | - | - | - | - | - | 1.466 | -0.04% | 45 |
| 257 | 2013-14 | Type I Low Speed | Baseline | none | 8 | 20 | 17-Jan-14 | -4.4 | -0.2 | - | - | - | - | - | 1.459 | 0.41% | 55 |
| 258 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 17-Jan-14 | -4.4 | -0.7 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.422 | 2.95% | 45 |
| 259 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 17-Jan-14 | -4.5 | -1 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.430 | 2.44% | 55 |
| 260 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.463 | 0.18% | 100 |
| 261 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.455 | 0.68% | 100 |
| 262 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.461 | 0.27% | 100 |
| 263 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.468 | -0.16% | 100 |
| 264 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.468 | -0.17% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 265 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.469 | -0.27% | 100 |
| 266 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 80 |
| 267 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 80 |
| 268 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 80 |
| 269 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 100 |
| 270 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 100 |
| 271 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 100 |
| 272 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0, +2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 115 |
| 273 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 115 |
| 274 | 2013-14 | Ice Phobic R&D | Dry Wing | none | -2,0,+2 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | n/a | - | 115 |
| 275 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.438 | 1.83% | 80 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|-------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 276 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.442 | 1.59% | 80 |
| 277 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 23 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.439 | 1.77% | 80 |
| 278 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.456 | 0.63% | 100 |
| 279 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.456 | 0.62% | 100 |
| 280 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -8.1 | -8.3 | - | - | - | - | - | 1.456 | 0.66% | 100 |
| 281 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 20-Jan-14 | -9 | -8.7 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.425 | 2.75% | 100 |
| 282 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 20-Jan-14 | -9.4 | -8.7 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.423 | 2.91% | 100 |
| 283 | 2013-14 | Ice Phobic R&D | Fluid Only | EG106 | 8 | 20 | 20-Jan-14 | -10 | -9.8 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.423 | 2.88% | 100 |
| 284 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -10.4 | -10.1 | - | - | - | - | - | 1.461 | 0.26% | 100 |
| 285 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 | 20 | 20-Jan-14 | -10.4 | -10.1 | - | - | - | - | - | 1.458 | 0.52% | 100 |
| 286 | 2013-14 | Ice Phobic R&D | ZR | none | 8 | 20 | 20-Jan-14 | -10.7 | -10.3 | - | 6 | - | - | - | 1.429 | 2.47% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--------------------------------|-------------------|-------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 287 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -11.8 | -11.6 | - | - | - | - | - | 1.466 | -0.08% | 100 |
| 288 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -11.8 | -11.6 | - | - | - | - | - | 1.463 | 0.13% | 100 |
| 289 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -11.8 | -11.6 | - | - | - | - | - | 1.464 | 0.10% | 100 |
| 290 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -13 | -13 | - | - | - | - | - | 1.467 | -0.10% | 100 |
| 291 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -13 | -13 | - | - | - | - | - | 1.465 | 0.03% | 100 |
| 292 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 20-Jan-14 | -13 | -13 | - | - | - | - | - | 1.465 | -0.01% | 100 |
| 293 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 20-Jan-14 | -20 | -17.9 | - | - | - | - | - | 1.458 | 0.52% | 80 |
| 294 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 20-Jan-14 | -20 | -17.9 | - | - | - | - | - | 1.465 | 0.03% | 100 |
| 295 | 2013-14 | Type III Allowance Times | IP- | 2031 - Cold | 8 | 20 | 20-Jan-14 | -20.4 | -18.7 | IP=25 | 10 | 2.2, 2.2, 2.7 | 1, 1.8, 2.1 | 1, 1, 1.2 | 1.384 | 5.55% | 100 |
| 296 | 2013-14 | Type III Allowance Times | IP Mod | 2031 - Cold | 8 | 20 | 21-Jan-14 | -20.6 | -17.7 | IP = 75 | 5 | 2.3, 2.3, 2.8 | 1, 1.8, 2.1 | 1, 1.1, 1.3 | 1.393 | 4.90% | 100 |
| 297 | 2013-14 | Type III Allowance Times | IP- | 2031 - Hot | 8 | 20 | 21-Jan-14 | -21.1 | -18.1 | IP=25 | 10 | 2.2, 2.1, 2.7 | 2.3, 3.8, 1.6 | 2.3, 5, 1.2 | 1.395 | 4.79% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--|-------------------|------------------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 298 | 2013-14 | Type III Allowance Times | IP Mod | 2031 - Hot | 8 | 20 | 21-Jan-14 | -21.3 | -19 | IP = 75 | 5 | 2.2, 2.5, 3.2 | 2.4, 5, 2 | 2.3, 5, 1.2 | 1.396 | 4.73% | 100 |
| 299 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 21-Jan-14 | -21.7 | -18.5 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.436 | 2.01% | 100 |
| 300 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 21-Jan-14 | -22 | -20.5 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.398 | 4.57% | 60 |
| 301 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 21-Jan-14 | -22.4 | -20.2 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.401 | 4.41% | 60 |
| 302 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 21-Jan-14 | -22.4 | -20.2 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.409 | 3.83% | 55 |
| 303 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 21-Jan-14 | -22.5 | -17.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.404 | 4.21% | 45 |
| 304 | 2013-14 | IP Expansion | IP- / SN- | Polar Guard Advance | 8 | 20 | 21-Jan-14 | -23.5 | -14.6 | IP = 25 SN = 10 | 15 | 2.5, 2.7, 3.83 | 1.2, 1.9, 3.2 | 1.1, 1.1, 2.8 | 1.348 | 8.01% | 115 |
| 305 | 2013-14 | New Ice Pellet Dispenser Validation | IP- / SN- | Polar Guard Advance | 8 | 20 | 21-Jan-14 | -23.8 | -11.4 | IP = 25 SN = 10 | 15 | 2.5, 2.6, 3.8 | 1.2, 2, 3 | 1, 1.4, 2.9 | 1.351 | 7.80% | 115 |
| 306 | 2013-14 | New Ice Pellet DispensrV alidation | IP- / SN- | Polar Guard Advance | 8 | 20 | 21-Jan-14 | -24 | -14.4 | IP = 25 SN = 10 | 15 | 2.3, 2.3, 3.6 | 1.2, 1.8, 3 | 1, 1.5, 2.7 | 1.348 | 7.97% | 115 |
| 307 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 21-Jan-14 | -22.6 | -14 | - | - | - | - | - | 1.456 | 0.62% | 80 |
| 308 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 21-Jan-14 | -22.6 | -14 | - | - | - | - | - | 1.465 | 0.00% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--|-------------------|------------------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 309 | 2013-14 | New Ice Pellet Dispenser Validation | IP- / SN- | Polar Guard Advance | 8 | 20 | 21-Jan-14 | -22.6 | -9.6 | IP = 25 SN = 10 | 15 | 2.8, 2.8, 4 | 1.1, 2, 3.3 | 1.1, 1.5, 3.2 | 1.349 | 7.94% | 115 |
| 310 | 2013-14 | IP Expansion | IP- / SN- | EG106 | 8 | 20 | 21-Jan-14 | -23.1 | -17.4 | IP = 25 SN = 10 | 15 | 1.7, 1.7, 2.3 | 1, 1.3, 1.5 | 1, 1.1, 1.3 | 1.436 | 2.00% | 115 |
| 311 | 2013-14 | IP Expansion | IP- / SN- | EG106 | 8 | 20 | 21-Jan-14 | -23.9 | -18.1 | IP = 25 SN = 10 | 15 | 1.9, 1.9, 2.3 | 1.1, 1.5, 1.7 | 1, 1.1, 1.2 | 1.406 | 4.06% | 100 |
| 312 | 2013-14 | IP Expansion | IP- / SN- | Launch | 8 | 20 | 21-Jan-14 | -24.3 | -17.4 | IP = 25 SN = 10 | 15 | 2.8, 2.7, 3.7 | 1.1, 1.9, 2.4 | 1, 1.6, 2.1 | 1.332 | 9.11% | 115 |
| 313 | 2013-14 | IP Expansion | IP- / SN- | Max-Flight | 8 | 20 | 21-Jan-14 | -24.5 | -15.3 | IP = 25 SN = 10 | 15 | 2.6, 2.5, 3.5 | 1.1, 1.8, 2.4 | 1, 1.1, 1.4 | 1.340 | 8.54% | 115 |
| 314 | 2013-14 | IP Expansion | IP- / SN- | AD-49 | 8 | 20 | 22-Jan-14 | -24.8 | -19.8 | IP = 25 SN = 10 | 15 | 3, 2.4, 4 | 1.3, 2, 3.7 | 1.1, 1.8, 3.7 | 1.342 | 8.39% | 115 |
| 315 | 2013-14 | IP Expansion | IP- / SN- | AD-49 | 8 | 20 | 22-Jan-14 | -25.1 | -19.4 | IP = 25 SN = 10 | 10 | 2.9, 2.8, 3.8 | 1.2, 1.9, 3 | 1.1, 1.9, 3 | 1.361 | 7.14% | 115 |
| 316 | 2013-14 | Type I Low Speed | Fluid Only | Dow ADF | 8 | 20 | 22-Jan-14 | -25.5 | -23.4 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.449 | 1.11% | 100 |
| 317 | 2013-14 | Type I Low Speed | Fluid Only | Dow ADF | 8 | 20 | 22-Jan-14 | -25.6 | -23.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.438 | 1.83% | 60 |
| 318 | 2013-14 | Type I Low Speed | Fluid Only | Dow ADF | 8 | 20 | 22-Jan-14 | -25.6 | -24.1 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.434 | 2.11% | 55 |
| 319 | 2013-14 | Type I Low Speed | Fluid Only | Dow ADF | 8 | 20 | 22-Jan-14 | -25.7 | -24.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.421 | 3.05% | 45 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 320 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -25.8 | -24.3 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.409 | 3.84% | 100 |
| 321 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -25.9 | -25 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.375 | 6.15% | 60 |
| 322 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -26 | -25.4 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.353 | 7.65% | 55 |
| 323 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -26 | -25.1 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.342 | 8.40% | 45 |
| 324 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -26.2 | -24.8 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.406 | 4.06% | 100 |
| 325 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -26.3 | -25.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.370 | 6.50% | 60 |
| 326 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -26.4 | -25.1 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.346 | 8.14% | 55 |
| 327 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 22-Jan-14 | -26.5 | -25.5 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.340 | 8.55% | 45 |
| 328 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 22-Jan-14 | -19.8 | -16.1 | - | - | - | - | - | 1.465 | 0.00% | 80 |
| 329 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 22-Jan-14 | -19.8 | -16.1 | - | - | - | - | - | 1.472 | -0.43% | 100 |
| 330 | 2013-14 | New Ice Pellet Dispenser Validation | IP Mod | Launch | 8 | 20 | 22-Jan-14 | -20 | -18.1 | IP = 75 | 10 | 2.5, 3, 3.6 | 1, 1.9, 2.4 | 1, 1, 1.6 | 1.353 | 7.67% | 115 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|---|-------------------|------------------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 331 | 2013-14 | New Ice Pellet Dispenser Validation | IP Mod | Launch | 8 | 20 | 22-Jan-14 | -20.2 | -16.3 | IP = 75 | 10 | 2.7, 2.8, 3.6 | 1.1, 2.1, 2.5 | 1, 1.4, 2 | 1.334 | 8.95% | 115 |
| 332 | 2013-14 | New Ice Pellet Dispenser Validation | IP Mod | Launch | 8 | 20 | 22-Jan-14 | -20.6 | -17 | IP = 75 | 10 | 2.9, 2.8, 3.8 | 1.1, 1.7, 2.5 | 1, 1.2, 1.5 | 1.330 | 9.25% | 115 |
| 333 | 2013-14 | New Ice Pellet Dispenser Validation | IP Mod | Launch | 8 | 20 | 22-Jan-14 | -20.6 | -16.4 | IP = 75 | 10 | 3, 2.8, 3.8 | 1.1, 1.9, 2.4 | 1, 1.2, 1.5 | 1.327 | 9.42% | 115 |
| 334 | 2013-14 | New Ice Pellet Dispenser Validation | IP Mod | Launch | 8 | 20 | 23-Jan-14 | -20.9 | -18.8 | IP = 75 | 10 | 2.9, 2.8, 3.8 | 1.1, 1.9, 2.3 | 1, 1.1, 1.4 | 1.307 | 10.82% | 115 |
| 335 | 2013-14 | New Ice Pellet Dispenser Validation | IP Mod | Launch | 8 | 20 | 22-Jan-14 | -21 | -20 | IP = 75 | 10 | 2.8, 2.8, 3.8 | 1.1, 1.9, 2.2 | 1, 1.3, 1.5 | 1.325 | 9.55% | 115 |
| 336 | 2013-14 | New Ice Pellet Dispensr Validation | IP Mod | Launch | 8 | 20 | 23-Jan-14 | -21.4 | -19.6 | IP = 75 | 10 | 3, 2.8, 3.8 | 1.1, 1.6, 2.2 | 1, 1.3, 1.5 | 1.328 | 9.35% | 115 |
| 337 | 2013-14 | New Ice Pellet Dispensr Validation | IP Mod | Launch | 8 | 20 | 23-Jan-14 | -21.9 | -20.6 | IP = 75 | 5 | 2.6, 2.5, 3.7 | 1.1, 1.8, 2.2 | 1, 1.1, 1.4 | 1.338 | 8.66% | 115 |
| 338 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | ABC-S Plus | 8 | 20 | 23-Jan-14 | -22.3 | -20.6 | IP = 75 | 7 | 2.8, 2.7, 3.8 | 1, 1.7, 2.1 | 1, 1.1, 1.3 | 1.368 | 6.61% | 115 |
| 339 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Max-Flight | 8 | 20 | 23-Jan-14 | -22.6 | -21.5 | IP = 75 | 7 | 2.6, 2.6, 3.9 | 1, 1.7, 2.2 | 1, 1, 1.2 | 1.358 | 7.35% | 115 |
| 340 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Polar Guard Advance | 8 | 20 | 23-Jan-14 | -22.8 | -21.4 | IP = 75 | 10 | 2.7, 2.4, 3.8 | 1, 1.6, 2.2 | 1, 1, 1.2 | 1.372 | 6.37% | 115 |
| 341 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 27-Jan-14 | -13.3 | -9.3 | - | - | - | - | - | 1.468 | -0.16% | 80 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--------------------------------|-------------------|---------------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 342 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 27-Jan-14 | -13.3 | -9.3 | - | - | - | - | - | 1.459 | 0.45% | 100 |
| 343 | 2013-14 | Type III Allowance Times | IP- | 2031 - Cold | 8 | 20 | 27-Jan-14 | -11.6 | -11.4 | IP=25 | 10 | 2.5, 2.7, 2.8 | 1, 1, 1.3 | 1, 1, 1.1 | 1.439 | 1.76% | 100 |
| 344 | 2013-14 | Type III Allowance Times | IP- | 2031 - Hot | 8 | 20 | 27-Jan-14 | -9.2 | -9.1 | IP=25 | 10 | 2.3, 2.4, 2.2 | 3, 5, 5 | 3, 5, 5 | 1.432 | 2.30% | 100 |
| 345 | 2013-14 | Type III Allowance Times | IP Mod | 2031 - Cold | 8 | 20 | 27-Jan-14 | -7.8 | -6.9 | IP = 75 | 5 | 2.5, 2.7, 2.8 | 1, 1.1, 1.2 | 1, 1, 1 | 1.435 | 2.04% | 100 |
| 346 | 2013-14 | Type III Allowance Times | IP Mod | 2031 - Hot | 8 | 20 | 27-Jan-14 | -7.9 | -6.4 | IP = 75 | 5 | 2.8, 2.4, 2.2 | 2.3, 4.7, 2.5 | 2.3, 4.8, 4.5 | 1.439 | 1.77% | 100 |
| 347 | 2013-14 | Type III Allowance Times | IP Mod | ABC-S Plus - Hot | 8 | 20 | 27-Jan-14 | -11.3 | -9.4 | IP = 75 | 10 | 2.1, 2.4, 2.8 | 3, 5, 5 | 3, 5, 5 | 1.390 | 5.13% | 100 |
| 348 | 2013-14 | Type III Allowance Times | IP Mod | EG106 - Hot | 8 | 20 | 27-Jan-14 | -11.7 | -10.6 | IP = 75 | 10 | 2.5, 2.3, 3 | 3, 5, 5 | 3, 5, 5 | 1.445 | 1.40% | 100 |
| 349 | 2013-14 | Type III Allowance Times | IP Mod | 2031 - Hot | 8 | 20 | 27-Jan-14 | -12.4 | -9.5 | IP = 75 | 5 | 2.7, 2.7, 2.5 | 3, 5, 5 | 3, 5, 5 | 1.412 | 3.61% | 100 |
| 350 | 2013-14 | Type III Allowance Times | IP- / ZR- | 2031 - Cold | 8 | 20 | 27-Jan-14 | -12.2 | -11.1 | IP = 25 ZR = 25 | 5 | 2.5, 2.7, 2.9 | 1, 1.1, 1.5 | 1, 1, 1.1 | 1.426 | 2.68% | 100 |
| 351 | 2013-14 | Type III Allowance Times | IP- / ZR- | 2031 - Hot | 8 | 20 | 27-Jan-14 | -12.9 | -9.6 | IP = 25 ZR = 25 | 5 | 2, 2, 2.3 | 5, 5, 5 | 5, 5, 5 | 1.434 | 2.15% | 100 |
| 352 | 2013-14 | Type III Allowance Times | IP- / SN- | 2031 - Cold | 8 | 20 | 27-Jan-14 | -12.8 | -11 | IP = 25 SN = 10 | 10 | 2.5, 2.8, 3.3 | 1.1, 1.4, 1.8 | 1, 1.1, 1.3 | 1.410 | 3.75% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|---|-------------------|------------------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 353 | 2013-14 | Type III Allowance Times | IP- / SN | 2031 - Cold | 8 | 20 | 27-Jan-14 | -13 | -10.2 | IP = 25 SN = 25 | 5 | 2.5, 2.7, 3.5 | 1.1, 1.4, 2 | 1, 1.1, 1.3 | 1.409 | 3.83% | 100 |
| 354 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 28-Jan-14 | -19 | -11.4 | - | - | - | - | - | 1.459 | 0.46% | 80 |
| 355 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 28-Jan-14 | -19 | -11.4 | - | - | - | - | - | 1.469 | -0.26% | 100 |
| 356 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | AD-49 | 8 | 20 | 28-Jan-14 | -18.7 | -11.6 | IP = 75 | 7 | 2.7, 2.4, 3.5 | 1.2, 1.6, 2 | 1, 1.3, 1.5 | 1.368 | 6.66% | 115 |
| 357 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | AD-49 | 8 | 20 | 28-Jan-14 | -17.9 | -14 | IP = 75 | 10 | 3, 2.8, 3.8 | 1.2, 1.6, 2.2 | 1, 1.2, 1.6 | 1.360 | 7.16% | 115 |
| 358 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | ABC-S Plus | 8 | 20 | 28-Jan-14 | -16.9 | -12.2 | IP = 75 | 10 | 2.5, 2.3, 3.8 | 1, 1.5, - | -, -, - | n/a | - | 115 |
| 359 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | ABC-S Plus | 8 | 20 | 28-Jan-14 | -14.1 | -10.9 | IP = 75 | 10 | 2.4, 2.4, 3.8 | 1.1, 1.5, 1.9 | 1, 1.1, 1.2 | 1.358 | 7.31% | 115 |
| 360 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Launch | 8 | 20 | 28-Jan-14 | -12.3 | -12.1 | IP = 75 | 10 | 2.3, 2.3, 3.7 | 1.1, 1.3, 1.9 | 1, 1, 1.2 | 1.363 | 6.95% | 115 |
| 361 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Max-Flight | 8 | 20 | 28-Jan-14 | -11 | -10.9 | IP = 75 | 10 | 2.2, 2.3, 3.3 | 1, 1.2, 1.7 | 1, 1, 1.2 | 1.391 | 5.08% | 115 |
| 362 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Polar Guard Advance | 8 | 20 | 28-Jan-14 | -10.9 | -11 | IP = 75 | 10 | 2.3, 2.3, 3.3 | 1, 1.3, 1.7 | 1, 1, 1.2 | 1.377 | 6.01% | 115 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|---|-------------------|------------------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 363 | 2013-14 | Type III Allowance Times | IP Mod | ABC-S Plus | 8 | 20 | 28-Jan-14 | -10.6 | -7.4 | IP = 75 | 10 | 2, 2, 2.8 | 1, 1.3, 1.7 | 1, 1, 1.2 | 1.337 | 8.72% | 100 |
| 364 | 2013-14 | Type III Allowance Times | IP Mod | EG106 | 8 | 20 | 28-Jan-14 | -10.2 | -7.1 | IP = 75 | 10 | 2.3, 2.3, 2.8 | 3, 5, 5 | 3, 5, 5 | 1.442 | 1.56% | 100 |
| 365 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 28-Jan-14 | -10.7 | -10.4 | - | - | - | - | - | 1.463 | 0.13% | 100 |
| 366 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 28-Jan-14 | -10.7 | -10.4 | - | - | - | - | - | 1.455 | 0.67% | 100 |
| 358 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | ABC-S Plus | 8 | 20 | 28-Jan-14 | -16.9 | -12.2 | IP = 75 | 10 | 2.5, 2.3, 3.8 | 1, 1.5, - | -, -, - | n/a | - | 115 |
| 359 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | ABC-S Plus | 8 | 20 | 28-Jan-14 | -14.1 | -10.9 | IP = 75 | 10 | 2.4, 2.4, 3.8 | 1.1, 1.5, 1.9 | 1, 1.1, 1.2 | 1.358 | 7.31% | 115 |
| 360 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Launch | 8 | 20 | 28-Jan-14 | -12.3 | -12.1 | IP = 75 | 10 | 2.3, 2.3, 3.7 | 1.1, 1.3, 1.9 | 1, 1, 1.2 | 1.363 | 6.95% | 115 |
| 361 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Max-Flight | 8 | 20 | 28-Jan-14 | -11 | -10.9 | IP = 75 | 10 | 2.2, 2.3, 3.3 | 1, 1.2, 1.7 | 1, 1, 1.2 | 1.391 | 5.08% | 115 |
| 362 | 2013-14 | IP Validation with New Temps & Fluids | IP Mod | Polar Guard Advance | 8 | 20 | 28-Jan-14 | -10.9 | -11 | IP = 75 | 10 | 2.3, 2.3, 3.3 | 1, 1.3, 1.7 | 1, 1, 1.2 | 1.377 | 6.01% | 115 |
| 363 | 2013-14 | Type III Allowance Times | IP Mod | ABC-S Plus | 8 | 20 | 28-Jan-14 | -10.6 | -7.4 | IP = 75 | 10 | 2, 2, 2.8 | 1, 1.3, 1.7 | 1, 1, 1.2 | 1.337 | 8.72% | 100 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|--------------------------------|-------------------|------------|-------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 364 | 2013-14 | Type III Allowance Times | IP Mod | EG106 | 8 | 20 | 28-Jan-14 | -10.2 | -7.1 | IP = 75 | 10 | 2.3, 2.3, 2.8 | 3, 5, 5 | 3, 5, 5 | 1.442 | 1.56% | 100 |
| 365 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 28-Jan-14 | -10.7 | -10.4 | - | - | - | - | - | 1.463 | 0.13% | 100 |
| 366 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 28-Jan-14 | -10.7 | -10.4 | - | - | - | - | - | 1.455 | 0.67% | 100 |
| 367 | 2013-14 | Ice Phobic R&D | Dry Wing | none | 8 pitch pause | 20 | 28-Jan-14 | -10.7 | -10.4 | - | - | - | - | - | 1.458 | 0.52% | 100 |
| 368 | 2013-14 | Baseline | Dry Wing | none | 22 | 20 | 29-Jan-14 | -14.1 | -8.2 | - | - | - | - | - | 1.471 | -0.41% | 80 |
| 369 | 2013-14 | Baseline | Dry Wing | none | 8 | 20 | 29-Jan-14 | -14.1 | -8.2 | - | - | - | - | - | 1.465 | -0.01% | 100 |
| 370 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 29-Jan-14 | -13.6 | -13.8 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.442 | 1.57% | 100 |
| 371 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 29-Jan-14 | -13.3 | -13.4 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.414 | 3.52% | 60 |
| 372 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 29-Jan-14 | -12.6 | -13.1 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.400 | 4.47% | 55 |
| 373 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 29-Jan-14 | -12.5 | -13 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.386 | 5.41% | 45 |
| 374 | 2013-14 | Type I Low Speed | Fluid Only | Polar Plus | 8 | 20 | 29-Jan-14 | -12.3 | -12.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.366 | 6.79% | 30 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

| Test # | Test Year | Objective | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | Date | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Visual Contamination Rating After Takeoff (LE,TE,Flap) | Corrected for 3D Effects CL at 8° | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|-----------|--------------|------------------------|---------------------------------------|---------------------------------|------------------------|-------------------------------|-----------|-------------------------------|--|------------------------------------|---------------------------|---|--|--|--|--|--------------|
| 375 | 2013-14 | Type I Low Speed | Fluid Only w/ Squeegee Lines | Polar Plus | 8 | 20 | 29-Jan-14 | -12.2 | -12.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | 1.420 | 3.06% | 45 |
| 376 | 2013-14 | Ice Phobic R&D | Fluid Only | 2031 | fixed angle 4deg | 20 | 29-Jan-14 | -12.3 | -12.6 | - | - | 1, 1, 1 | 1, 1, 1 | 1, 1, 1 | n/a | - | 100 |
| 377 | 2013-14 | R&D | HEAVY CONTAMI NATION | ABC-S+ | 22 | 20 | 29-Jan-14 | -11.2 | -4.1 | IP = 375 ZR = 50 | 26 | - | - | - | 1.279 | 12.73% | 80 |
| 378 | 2013-14 | R&D | APM Unit | None | 23 | 20 | 29-Jan-14 | -11.2 | -1.8 | - | - | - | - | - | 1.442 | 1.57% | 80 |
| 379 | 2013-14 | R&D | APM Unit | None | 23 PITCH PAUSE | 20 | 29-Jan-14 | -11.2 | -11.3 | - | - | - | - | - | 1.459 | 0.41% | 80 |
| 380 | 2013-14 | R&D | APM Unit | ABC-S Plus | 23 | 20 | 29-Jan-14 | -11.1 | -11.3 | - | - | - | - | - | 1.355 | 7.56% | 80 |
| 381 | 2013-14 | R&D | APM Unit | ABC-S Plus | 23 PITCH PAUSE | 20 | 29-Jan-14 | -11.1 | -11.6 | - | - | - | - | - | 1.431 | 2.33% | 80 |
| 382 | 2013-14 | R&D | APM Unit | ABC-S Plus (unit covered) | 23 | 20 | 29-Jan-14 | -11 | -11.3 | - | - | - | - | - | 1.422 | 2.96% | 80 |
| 383 | 2013-14 | R&D | APM Unit | ABC-S Plus (unit covered) | 23 PITCH PAUSE | 20 | 29-Jan-14 | -11 | -11.3 | - | - | - | - | - | 1.436 | 2.02% | 80 |

Table 3.1: Wind Tunnel Test Log 2013-14 (cont'd)

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4. LIGHT ICE PELLET ALLOWANCE TIMES

A summary of the Light Ice Pellet tests conducted with Type III fluids in the wind tunnel is shown in Table 4.1. The table provides relevant information for each of the tests, as well as final values used for the data analysis. Each row contains data specific to one test. A more detailed test log of all conditions tested using the wind tunnel is provided in Subsection 3.1.

It should be noted that Type IV testing was not conducted in Light Ice Pellet conditions, as this was not an area of high priority for the 2013-14 research program.

4.1 Analysis of Data Collected

The data collected has been sorted according to test parameters and included in the respective cells of the ice pellet allowance time table format for ease of reference; this is shown in Table 4.2. A more detailed analysis separating the data according to the allowance time cell and rotation speed has been conducted and is shown in Table 4.3. In addition, a conclusion regarding the test results has also been included for each condition in Table 4.3.

4.2 Overall Summary of Results

The testing results indicated that an allowance time of 10 minutes was acceptable for Type III fluid down to below -10°C when applied cold (air temperature). The data collected with heated fluid applications indicated risks of adhered contamination, especially at colder temperatures; therefore, providing allowance times was not feasible without more extensive testing to understand the potential effects.

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|----------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 15 | IP- | 2031 - Cold | 8 | 20 | -7.1 | -4.7 | IP=25 | 10 | 2, 2, 2 | 1, 1, 1.15 | 2.14% | 100 |
| 21 | IP- | 2031 - Hot | 8 | 20 | -7.7 | -5.2 | IP=25 | 10 | 2, 2, 2.1 | 1, 5, 1 | 1.90% | 100 |
| 22 | IP- | 2031 - Hot | 8 | 20 | -7.2 | -2.8 | IP=25 | 7 | 1.9, 1.75, 1.25 | 1, 3, 1 | 1.64% | 100 |
| 23 | IP- | 2031 - Hot | 8 | 20 | -6.9 | -2.9 | IP = 25 | 5 | 1.5, 1.25, 1.15 | 1, 1, 1 | 2.00% | 100 |
| 295 | IP- | 2031 - Cold | 8 | 20 | -20.4 | -18.7 | IP = 25 | 10 | 2.2, 2.2, 2.7 | 1, 1.8, 2.1 | 5.55% | 100 |
| 297 | IP- | 2031 - Hot | 8 | 20 | -21.1 | -18.1 | IP = 25 | 10 | 2.2, 2.1, 2.7 | 2.3, 3.8, 1.6 | 4.79% | 100 |
| 343 | IP- | 2031 - Cold | 8 | 20 | -11.6 | -11.4 | IP = 25 | 10 | 2.5, 2.7, 2.8 | 1, 1, 1.3 | 1.76% | 100 |
| 344 | IP- | 2031 - Hot | 8 | 20 | -9.2 | -9.1 | IP=25 | 10 | 2.3, 2.4, 2.2 | 3, 5, 5 | 2.30% | 100 |

Table 4.1: Summary of 2013-14 Type III Light Ice Pellet Testing

| Light Ice Pellets | OAT -5°C and Above | OAT Less than -5°C to -10°C | OAT Less than -10°C |
|-------------------|----------------------------|--------------------------------------|--|
| | 10 Minutes Test # 15 | | |
| 100 kts Runs | 7 Minutes Test # 22 (h) | 10 Minutes Test # 21 (h), 344 (h) | 10 Minutes Test # 295, 297 (h), 343 |
| | 5 Minutes Test # 23 (h) | | |

Table 4.2: Type III Light Ice Pellets Allowance Time Tests Winter 2013-14

Note: (h) = Hot Application of Fluid

| Table 4.3: Summary of Type III Light Ice Pellets Allowance Time Test Resul | ts |
|--|----|
|--|----|

| | | | | OAT -5°(| C AND ABOVE 1 | 00 Kts (1 | 0 MINUTES) | | | | |
|----------|----------------|---|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status |
| 15 | 2031 - Cold | -4.7 | IP = 25 | 10 | 2, 2, 2 | Good | 1, 1, 1.15 | Good | 2.14% | Good | Good |

| | | | | 0AT -5 | °C AND ABOVE 1 | 100 Kts (1 | 7 MINUTES) | | | | | | | |
|-------|--|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|--|--|--|
| 22 | 2031 - Hot | -2.8 | IP = 25 | 7 | 1.9, 1.75, 1.25 | Good | 1, 3, 1 | Good | 1.64% | Good | Good | | | |
| | | | | 0AT -5 | °C AND ABOVE 1 | 100 Kts (! | 5 MINUTES) | | | | | | | |
| 23 | 2031 - Hot | -2.9 | IP = 25 | 5 | 1.5, 1.25, 1.15 | Good | 1, 1, 1 | Good | 2.00% | Good | Good | | | |
| | | | | | | | | | | | | | | |
| | 5 MINUTES IS GOOD FOR HOT FLUID, 7 MINUTES MAY ALSO BE ACCEPTABLE. | | | | | | | | | | | | | |
| | OAT LESS THAN -5°C TO -10°C 100 Kts (10 MINUTES) | | | | | | | | | | | | | |
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | | | |
| 21 | 2031 - Hot | -5.2 | IP = 25 | 10 | 2, 2, 2.1 | Good | 1, 5, 1 | Good | 1.90% | Good | Good | | | |
| 344 | 2031 - Hot | -9.1 | IP = 25 | 10 | 2.3, 2.4, 2.2 | Good | 3, 5, 5 | Bad | 2.30% | Good | Bad | | | |
| | 1 | CONCLUS | SION: ALLOWAN | ICE TIMES N | IAY NOT BE POS | SIBLE FO | R HOT FLUID DUE | TO RISK C | OF ADHE | SION | | | | |

Table 4.3: Summary of Type III Light Ice Pellets Allowance Time Test Results (cont'd)

APS/Library/Projects/PM2265.003 (TC Deicing 13-14)/Reports/Ice Pellet/Final Version 1.0/TP 15273E Final Version 1.0.docx Final Version 1.0, October 20

| | OAT LESS THAN -10°C 100 Kts (10 MINUTES) | | | | | | | | | | | | | | |
|----------|--|--|---------------------------------|------------------------|---|-----------------------------|--|-----------------------|----------------|---------------------|-------------------|--|--|--|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | | | | |
| 295 | 2031 - Cold | -18.7 | IP = 25 | 10 | 2.2, 2.2, 2.7 | Good | 1, 1.8, 2.1 | Good | 5.55% | Review | Review | | | | |
| 297 | 2031 - Hot | -18.1 | IP = 25 | 10 | 2.2, 2.1, 2.7 | Good | 2.3, 3.8, 1.6 | Bad | 4.79% | Good | Bad | | | | |
| 343 | 2031 - Cold | -11.4 | IP = 25 | 10 | 2.5, 2.7, 2.8 | Good | 1, 1, 1.3 | Good | 1.76% | Good | Good | | | | |
| | CONCLUSION: 10 MINUTES IS GOOD FOR COLD FLUID. | | | | | | | | | | | | | | |
| | | А | LLOWANCE TIN | IES MAY NO | OT BE POSSIBLE F | OR HOT I | FLUID DUE TO RIS | SK OF ADHI | SION | | | | | | |

Table 4.3: Summary of Type III Light Ice Pellets Allowance Time Test Results (cont'd)

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5. MODERATE ICE PELLET ALLOWANCE TIMES

A summary of the Moderate Ice Pellet tests conducted with Type III and Type IV fluids in the wind tunnel is shown in Table 5.1 and Table 5.2. The tables provide relevant information for each of the tests, as well as final values used for the data analysis. Each row contains data specific to one test. A more detailed test log of all conditions tested using the wind tunnel is provided in Subsection 3.1.

5.1 Analysis of Data Collected

The data collected has been sorted according to test parameters and included in the respective cells of the ice pellet allowance time table format for ease of reference; this is shown in Table 5.3 and Table 5.4. A more detailed analysis separating the data according to the allowance time cell and rotation speed has been conducted and is shown in Table 5.5 and Table 5.6. In addition, a conclusion regarding the test results has also been included for each condition in Table 5.5 and Table 5.6.

5.2 Overall Summary of Results

5.2.1 Type III Testing

The testing results indicated that an allowance time of 5 minutes was acceptable for Type III fluid down to below -10°C when applied cold (air temperature). The data collected with heated fluid applications indicated risks of adhered contamination, especially at colder temperatures; therefore, providing allowance times was not feasible without more extensive testing to understand the potential effects.

Additional tests with heated Type IV fluids were conducted to confirm the results seen with Type III fluid. The results indicated that less adherence occurred with Type IV fluids (likely due to the thicker fluid); however, adherence did still occur, further supporting why allowance times have only existed for unheated fluid applications.

5.2.2 Type IV Testing

The testing results showed that, for Type IV propylene glycol (PG) fluids, the existing 10-minute allowance time at 115 knots rotation speed should be limited to -16°C due to the higher lift losses observed. The data collected this year, as well as in previous years with the same wing model, supports this change to the current guidance.

Preliminary testing has also indicated that a shorter allowance time could be explored as an alternative; however, shorter allowance times may not be as useful operationally.

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|----------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 16 | IP Mod | 2031 - Cold | 8 | 20 | -7.3 | -4.8 | IP = 75 | 5 | 2, 2, 2.15 | 1, 1.1, 1.4 | 1.63% | 100 |
| 24 | IP Mod | 2031 - Hot | 8 | 20 | -6.7 | -3 | IP = 75 | 5 | 2.25, 2, 2.25 | 1, 5, 1 | 1.46% | 100 |
| 296 | IP Mod | 2031 - Cold | 8 | 20 | -20.6 | -17.7 | IP = 75 | 5 | 2.3, 2.3, 2.8 | 1, 1.8, 2.1 | 4.90% | 100 |
| 298 | IP Mod | 2031 - Hot | 8 | 20 | -21.3 | -19 | IP=75 | 5 | 2.2, 2.5, 3.2 | 2.4, 5, 2 | 4.73% | 100 |
| 345 | IP Mod | 2031 - Cold | 8 | 20 | -7.8 | -6.9 | IP=75 | 5 | 2.5, 2.7, 2.8 | 1, 1.1, 1.2 | 2.04% | 100 |
| 346 | IP Mod | 2031 - Hot | 8 | 20 | -7.9 | -6.4 | IP=75 | 5 | 2.8, 2.4, 2.2 | 2.3, 4.7, 2.5 | 1.77% | 100 |
| 349 | IP Mod | 2031 - Hot | 8 | 20 | -12.4 | -9.5 | IP = 75 | 5 | 2.7, 2.7, 2.5 | 3, 5, 5 | 3.61% | 100 |

Table 5.1: Summary of 2013-14 Type III Moderate Ice Pellet Testing

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|---------------------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 330 | IP Mod | Launch | 8 | 20 | -20 | -18.1 | IP = 75 | 10 | 2.5, 3, 3.6 | 1, 1.9, 2.4 | 7.67% | 115 |
| 331 | IP Mod | Launch | 8 | 20 | -20.2 | -16.3 | IP = 75 | 10 | 2.7, 2.8, 3.6 | 1.1, 2.1, 2.5 | 8.95% | 115 |
| 332 | IP Mod | Launch | 8 | 20 | -20.6 | -17 | IP = 75 | 10 | 2.9, 2.8, 3.8 | 1.1, 1.7, 2.5 | 9.25% | 115 |
| 333 | IP Mod | Launch | 8 | 20 | -20.6 | -16.4 | IP = 75 | 10 | 3, 2.8, 3.8 | 1.1, 1.9, 2.4 | 9.42% | 115 |
| 334 | IP Mod | Launch | 8 | 20 | -20.9 | -18.8 | IP = 75 | 10 | 2.9, 2.8, 3.8 | 1.1, 1.9, 2.3 | 10.82% | 115 |
| 335 | IP Mod | Launch | 8 | 20 | -21 | -20 | IP = 75 | 10 | 2.8, 2.8, 3.8 | 1.1, 1.9, 2.2 | 9.55% | 115 |
| 336 | IP Mod | Launch | 8 | 20 | -21.4 | -19.6 | IP = 75 | 10 | 3, 2.8, 3.8 | 1.1, 1.6, 2.2 | 9.35% | 115 |
| 337 | IP Mod | Launch | 8 | 20 | -21.9 | -20.6 | IP = 75 | 5 | 2.6, 2.5, 3.7 | 1.1, 1.8, 2.2 | 8.66% | 115 |
| 338 | IP Mod | ABC-S Plus | 8 | 20 | -22.3 | -20.6 | IP = 75 | 7 | 2.8, 2.7, 3.8 | 1, 1.7, 2.1 | 6.61% | 115 |
| 339 | IP Mod | Max- Flight | 8 | 20 | -22.6 | -21.5 | IP = 75 | 7 | 2.6, 2.6, 3.9 | 1, 1.7, 2.2 | 7.35% | 115 |
| 340 | IP Mod | Polar Guard Advance | 8 | 20 | -22.8 | -21.4 | IP = 75 | 10 | 2.7, 2.4, 3.8 | 1, 1.6, 2.2 | 6.37% | 115 |

Table 5.2: Summary of 2013-14 Type IV Moderate Ice Pellet Testing

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|---------------------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 347 | IP Mod | ABC-S Plus - Hot | 8 | 20 | -11.3 | -9.4 | IP = 75 | 10 | 2.1, 2.4, 2.8 | 3, 5, 5 | 5.13% | 100 |
| 348 | IP Mod | EG106 - Hot | 8 | 20 | -11.7 | -10.6 | IP = 75 | 10 | 2.5, 2.3, 3 | 3, 5, 5 | 1.40% | 100 |
| 356 | IP Mod | AD-49 | 8 | 20 | -18.7 | -11.6 | IP = 75 | 7 | 2.7, 2.4, 3.5 | 1.2, 1.6, 2 | 6.66% | 115 |
| 357 | IP Mod | AD-49 | 8 | 20 | -17.9 | -14 | IP = 75 | 10 | 3, 2.8, 3.8 | 1.2, 1.6, 2.2 | 7.16% | 115 |
| 358 | IP Mod | ABC-S Plus | 8 | 20 | -16.9 | -12.2 | IP = 75 | 10 | 2.5, 2.3, 3.8 | 1, 1.5, - | #VALUE! | 115 |
| 359 | IP Mod | ABC-S Plus | 8 | 20 | -14.1 | -10.9 | IP=75 | 10 | 2.4, 2.4, 3.8 | 1.1, 1.5, 1.9 | 7.31% | 115 |
| 360 | IP Mod | Launch | 8 | 20 | -12.3 | -12.1 | IP = 75 | 10 | 2.3, 2.3, 3.7 | 1.1, 1.3, 1.9 | 6.95% | 115 |
| 361 | IP Mod | Max- Flight | 8 | 20 | -11 | -10.9 | IP = 75 | 10 | 2.2, 2.3, 3.3 | 1, 1.2, 1.7 | 5.08% | 115 |
| 362 | IP Mod | Polar Guard Advance | 8 | 20 | -10.9 | -11 | IP = 75 | 10 | 2.3, 2.3, 3.3 | 1, 1.3, 1.7 | 6.01% | 115 |
| 363 | IP Mod | ABC-S Plus | 8 | 20 | -10.6 | -7.4 | IP = 75 | 10 | 2, 2, 2.8 | 1, 1.3, 1.7 | 8.72% | 100 |
| 364 | IP Mod | EG106 | 8 | 20 | -10.2 | -7.1 | IP = 75 | 10 | 2.3, 2.3, 2.8 | 3, 5, 5 | 1.56% | 100 |

Table 5.2: Summary of 2013-14 Type IV Moderate Ice Pellet Testing (cont'd)

| Moderate Ice Pellets | OAT -5°C and | OAT Less than | OAT Less than |
|----------------------|----------------|------------------|--------------------------------------|
| | Above | -5°C to -10°C | -10°C |
| | 5 Minutes | 5 Minutes | 10 Minutes |
| | Tests # 16, 24 | Tests # 345, | Tests # 347, |
| | (h) | 346 (h), 349 (h) | 348, 363, 364 |
| 100 kts | | | 5 Minutes Tests # 296, 298 (h) |

Note: (h) = Hot Application of Fluid

| Table 5.4: Type IV Moderate Ice Pellets Allowance Time Tests W | Vinter 2013-14 |
|--|----------------|
|--|----------------|

| Moderate Ice Pellets | OAT -5°C and | OAT Less than | OAT Less than |
|----------------------|--------------|---------------|--|
| | Above | -5°C to -10°C | -10°C |
| 100 kts | 25 Minutes | 10 Minutes | 5 Minutes |
| | N/A | N/A | Tests # 337 |
| 115 kts | | <u>.</u> | 10 Minutes Tests # 330, 331, 332, 333, 334, 335, 336, 340, 357, 358, 359, 360, 361, 362 7 Minutes Tests # 338, 339, 356 |

| | OAT -5°C AND ABOVE 100 Kts (5 MINUTES) | | | | | | | | | | | | | | |
|----------|---|--|---------------------------------|------------------------|---|-----------------------------|--|-----------------------|----------------|---------------------|-------------------|--|--|--|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | | | | |
| 16 | 2031 - Cold | -4.8 | IP = 75 | 5 | 2, 2, 2.15 | Good | 1, 1.1, 1.4 | Good | 1.63% | Good | Good | | | | |
| 24 | 2031 - Hot | -3 | IP = 75 | 5 | 2.25, 2, 2.25 | Good | 1, 5, 1 | Good | 1.46% | Good | Good | | | | |
| | CONCLUSION: 5 MINUTES IS GOOD FOR COLD FLUID. 5 MINUTES MAY BE OK FOR HOT FLUID. | | | | | | | | | | | | | | |

| | OAT LESS THAN -5°C TO -10°C 100 Kts (5 MINUTES) | | | | | | | | | | | | | | |
|----------|---|--|---------------------------------|------------------------|---|-----------------------------|--|-----------------------|----------------|---------------------|-------------------|--|--|--|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | | | | |
| 345 | 2031 - Cold | -6.9 | IP = 75 | 5 | 2.5, 2.7, 2.8 | Good | 1, 1.1, 1.2 | Good | 2.04% | Good | Good | | | | |
| 346 | 2031 - Hot | -6.4 | IP = 75 | 5 | 2.8, 2.4, 2.2 | Good | 2.3, 4.7, 2.5 | Bad | 1.77% | Good | Bad | | | | |
| 349 | 2031 - Hot | -9.5 | IP = 75 | 5 | 2.7, 2.7, 2.5 | Good | 3, 5, 5 | Bad | 3.61% | Good | Bad | | | | |
| | | | | | | | | | | | | | | | |

CONCLUSION: 5 MINUTES IS GOOD FOR COLD FLUID.

ALLOWANCE TIMES MAY NOT BE POSSIBLE FOR HOT FLUID DUE TO RISK OF ADHERED ICE PELLETS.

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| | OAT LESS THAN -10°C 100 Kts (5 MINUTES) | | | | | | | | | | | | | | |
|----------|--|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|--|--|--|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | | | | |
| 296 | 2031 - Cold | -17.7 | IP = 75 | 5 | 2.3, 2.3, 2.8 | Good | 1, 1.8, 2.1 | Good | 4.90% | Good | Good | | | | |
| 298 | 2031 - Hot | -19 | IP = 75 | 5 | 2.2, 2.5, 3.2 | Good | 2.4, 5, 2 | Bad | 4.73% | Good | Bad | | | | |
| | CONCLUSION: 5 MINUTES IS GOOD FOR COLD FLUID. ALLOWANCE TIMES MAY NOT BE POSSIBLE FOR HOT FLUID DUE TO RISK OF ADHERED ICE PELLETS. | | | | | | | | | | | | | | |

| | ADDITIONAL TYPE IV TESTING TO CONFIRM ADHERENCE ISSUES OBSERVED WITH TYPE III OAT Less than -10°C (10 MINUTES) | | | | | | | | | | |
|-----|---|-------|---------|----|---------------|------|-------------|------|-------|--------|--------|
| 347 | ABC-S Plus - Hot | -9.4 | IP = 75 | 10 | 2.1, 2.4, 2.8 | Good | 3, 5, 5 | Bad | 5.13% | Good | Bad |
| 348 | EG106 - Hot | -10.6 | IP = 75 | 10 | 2.5, 2.3, 3 | Good | 3, 5, 5 | Bad | 1.40% | Good | Bad |
| 363 | ABC-S Plus | -7.4 | IP = 75 | 10 | 2, 2, 2.8 | Good | 1, 1.3, 1.7 | Good | 8.72% | Review | Review |
| 364 | EG106 | -7.1 | IP=75 | 10 | 2.3, 2.3, 2.8 | Good | 3, 5, 5 | Bad | 1.56% | Good | Bad |
| CON | CONCLUSION: SIMILAR TO TYPE III FLUID, ALLOWANCE TIMES MAY NOT BE POSSIBLE FOR HOT FLUID DUE TO RISK OF ADHERED ICE PELLETS. | | | | | | | | | | |

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| | OAT Less than -10°C 100 Kts (5 MINUTES) | | | | | | | | | | |
|----------|---|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status |
| 337 | Launch | -20.6 | IP = 75 | 5 | 2.6, 2.5, 3.7 | Good | 1.1, 1.8, 2.2 | Review | 8.66% | Review | Review |
| | 115 Kts (10 MINUTES) | | | | | | | | | | |
| 330 | Launch | -18.1 | IP = 75 | 10 | 2.5, 3, 3.6 | Good | 1, 1.9, 2.4 | Good | 7.67% | Review | Review |
| 331 | Launch | -16.3 | IP = 75 | 10 | 2.7, 2.8, 3.6 | Good | 1.1, 2.1, 2.5 | Review | 8.95% | Review | Review |
| 332 | Launch | -17 | IP = 75 | 10 | 2.9, 2.8, 3.8 | Good | 1.1, 1.7, 2.5 | Review | 9.25% | Bad | Bad |
| 333 | Launch | -16.4 | IP = 75 | 10 | 3, 2.8, 3.8 | Good | 1.1, 1.9, 2.4 | Review | 9.42% | Bad | Bad |
| 334 | Launch | -18.8 | IP = 75 | 10 | 2.9, 2.8, 3.8 | Good | 1.1, 1.9, 2.3 | Review | 10.82% | Bad | Bad |
| 335 | Launch | -20 | IP = 75 | 10 | 2.8, 2.8, 3.8 | Good | 1.1, 1.9, 2.2 | Review | 9.55% | Bad | Bad |
| 336 | Launch | -19.6 | IP = 75 | 10 | 3, 2.8, 3.8 | Good | 1.1, 1.6, 2.2 | Review | 9.35% | Bad | Bad |
| 340 | Polar Guard Advance | -21.4 | IP = 75 | 10 | 2.7, 2.4, 3.8 | Good | 1, 1.6, 2.2 | Good | 6.37% | Review | Review |
| 357 | AD-49 | -14 | IP = 75 | 10 | 3, 2.8, 3.8 | Good | 1.2, 1.6, 2.2 | Review | 7.16% | Review | Review |
| 358 | ABC-S Plus | -12.2 | IP = 75 | 10 | 2.5, 2.3, 3.8 | Good | 1, 1.5, - | Good | | | |
| 359 | ABC-S Plus | -10.9 | IP = 75 | 10 | 2.4, 2.4, 3.8 | Good | 1.1, 1.5, 1.9 | Review | 7.31% | Review | Review |
| 360 | Launch | -12.1 | IP = 75 | 10 | 2.3, 2.3, 3.7 | Good | 1.1, 1.3, 1.9 | Review | 6.95% | Review | Review |

Table 5.6: Summary of Type IV Moderate Ice Pellets Allowance Time Test Results

| | 115 Kts (10 MINUTES) Cont'd | | | | | | | | | | |
|-----|--|-------|---------|----|---------------|------|-------------|--------|-------|--------|--------|
| 361 | Max-Flight | -10.9 | IP = 75 | 10 | 2.2, 2.3, 3.3 | Good | 1, 1.2, 1.7 | Good | 5.08% | Good | Good |
| 362 | Polar Guard Advance | -11 | IP = 75 | 10 | 2.3, 2.3, 3.3 | Good | 1, 1.3, 1.7 | Good | 6.01% | Review | Review |
| | 115 Kts (7 MINUTES) | | | | | | | | | | |
| 338 | ABC-S Plus | -20.6 | IP = 75 | 7 | 2.8, 2.7, 3.8 | Good | 1, 1.7, 2.1 | Good | 6.61% | Review | Review |
| 339 | Max-Flight | -21.5 | IP = 75 | 7 | 2.6, 2.6, 3.9 | Good | 1, 1.7, 2.2 | Good | 7.35% | Review | Review |
| 356 | AD-49 | -11.6 | IP = 75 | 7 | 2.7, 2.4, 3.5 | Good | 1.2, 1.6, 2 | Review | 6.66% | Review | Review |
| | CONCLUSION: 10-MINUTE ALLOWANCE TIMES @ 115 KTS SHOULD BE LIMITED TO -16°C FOR PG FLUIDS. ALTERNATIVELY, SHORTER ALLOWANCE TIMES COULD BE EXPLORED. | | | | | | | | | | |

| Table 5.6: Summar | v of Type IV Moderate | ice Pellets Allowance Ti | ime Test Results (cont'd) |
|-------------------|-----------------------|--------------------------|---------------------------|
| | | | |

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6. LIGHT ICE PELLETS MIXED WITH LIGHT FREEZING RAIN ALLOWANCE TIMES

A summary of the Light Ice Pellets mixed with Light Freezing Rain tests conducted with Type III fluid in the wind tunnel is shown in Table 6.1. The table provides relevant information for each of the tests, as well as final values used for the data analysis. Each row contains data specific to one test. A more detailed test log of all conditions tested using the wind tunnel is provided in Subsection 3.1.

It should be noted that Type IV testing was not conducted in Light Ice Pellet Mixed with Light Freezing Rain conditions, as this was not an area of high priority for the 2013-14 research program. Also, allowance times developed for Light Ice Pellets Mixed with Light Freezing Rain are also applied to Light Ice Pellets Mixed with Light or Moderate Freezing Drizzle as well as Light Ice Pellets Mixed with Light Rain, as this was determined to be a conservative approach based on the rate of precipitation and risk of adherence.

6.1 Analysis of Data Collected

The data collected has been sorted according to test parameters and included in the respective cells of the ice pellet allowance time table format for ease of reference; this is shown in Table 6.2. A more detailed analysis separating the data according to the allowance time cell and rotation speed has been conducted and is shown in Table 6.3. In addition, a conclusion regarding the test results has also been included for each condition in Table 6.3.

6.2 Overall Summary of Results

6.2.1 Type III Testing

The testing results indicated that allowance times of 7 minutes at -5°C and above and 5 minutes below -5°C were acceptable for Type III fluid when applied cold (air temperature). The data collected with heated fluid applications indicated risks of adhered contamination, especially at colder temperatures; therefore, providing allowance times was not feasible without more extensive testing to understand the potential effects.

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|----------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 19 | IP- / ZR- | 2031 - Cold | 8 | 20 | -9.2 | -3.8 | IP = 25 ZR = 25 | 7 | 2, 2, 2.15 | 1, 1, 1.5 | 1.57% | 100 |
| 20 | IP- / ZR- | 2031 - Hot | 8 | 20 | -8.5 | -3.3 | IP = 25 ZR = 25 | 7 | 1.25, 1.5, 1.45 | 1, 1, 1 | 1.77% | 100 |
| 350 | IP- / ZR- | 2031 - Cold | 8 | 20 | -12.2 | -11.1 | IP = 25 ZR = 25 | 5 | 2.5, 2.7, 2.9 | 1, 1.1, 1.5 | 2.68% | 100 |
| 351 | IP- / ZR- | 2031 - Hot | 8 | 20 | -12.9 | -9.6 | IP = 25 ZR = 25 | 5 | 2, 2, 2.3 | 5, 5, 5 | 2.15% | 100 |

Table 6.1: Summary of 2013-14 Type III Light Ice Pellets and Light Freezing Rain Testing

Table 6.2: Type III Light Ice Pellets and Light Freezing Rain Allowance Time Tests Winter 2013-14

| Light Ice Pellets Mixed with Moderate Rain | OAT -5°C and Above | OAT Less than -5°C to -10°C | OAT Less than -10°C |
|--|--------------------|--------------------------------|------------------------|
| 100 kts | 7 Minutes | 5 Minutes | 5 Minutes |
| | Test # 19, 20 (h) | Test # 351 (h) | Test # 350 |

Note: (h) = Hot Application of Fluid

| | OAT -5°C AND ABOVE 100 Kts (7 MINUTES) | | | | | | | | | | | |
|----------|---|------|-----------------|---|------------|------|-----------|------|-------|------|------|--|
| Run # | Fluid ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' | | | | | | | | | | | |
| 19 | 2031 - Cold | -3.8 | IP = 25 ZR = 25 | 7 | 2, 2, 2.15 | Good | 1, 1, 1.5 | Good | 1.57% | Good | Good | |
| 20 | 2021 | | | | | | | | | | | |
| | CONCLUSION: 7 MINUTES IS GOOD FOR COLD FLUID. | | | | | | | | | | | |
| | 7 MINUTES MAY ALSO BE OK FOR HOT FLUID. | | | | | | | | | | | |

| | OAT LESS THAN -5°C TO -10°C 100 Kts (5 MINUTES) | | | | | | | | | | | |
|----------|---|--|---------------------------------|------------------------|--|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | |
| 351 | 2031 - Hot | -9.6 | IP = 25 ZR = 25 | 5 | 2, 2, 2.3 | Good | 5, 5, 5 | Bad | 2.15% | Good | Bad | |
| | CONCLUSION: | | | | | | | | | | | |
| | ALLOWANCE TIMES MAY NOT BE POSSIBLE FOR HOT FLUID DUE TO RISK OF ADHERED ICE PELLETS. | | | | | | | | | | | |

| | OAT LESS THAN -10°C 100 Kts (5 MINUTES) | | | | | | | | | | | |
|----------|---|--|---------------------------------|------------------------|--|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | |
| 350 | 2031 - Cold | -11.1 | IP=25 ZR=25 | 5 | 2.5, 2.7, 2.9 | Good | 1, 1.1, 1.5 | Good | 2.68% | Good | Good | |
| | CONCLUSION: 5 MINUTES IS GOOD FOR COLD FLUID. | | | | | | | | | | | |

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7. LIGHT ICE PELLETS MIXED WITH MODERATE RAIN ALLOWANCE TIMES

Testing in Light Ice Pellets mixed with Moderate Rain was not conducted with either Type III or Type IV fluids during the winter of 2013-14. As a result, no changes were made to the existing Type IV allowance times, and no new allowance times were issued for Type III fluid.

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8. LIGHT ICE PELLETS MIXED WITH LIGHT SNOW ALLOWANCE TIMES

A summary of the Light Ice Pellets Mixed with Light Snow tests conducted with Type III and Type IV fluids in the wind tunnel is shown in Table 8.1 and Table 8.2. The tables provide relevant information for each of the tests, as well as final values used for the data analysis. Each row contains data specific to one test. A more detailed test log of all conditions tested using the wind tunnel is provided in Subsection 3.1.

8.1 Analysis of Data Collected

The data collected has been sorted according to test parameters and included in the respective cells of the ice pellet allowance time table format for ease of reference; this is shown in Table 8.3 and Table 8.4. A more detailed analysis separating the data according to the allowance time cell and rotation speed has been conducted and is shown in Table 8.5 and Table 8.6. In addition, a conclusion regarding the test results has also been included for each condition in Table 8.5 and Table 8.6.

8.2 Overall Summary of Results

8.2.1 Type III Testing

The testing results indicated that an allowance time of 10 minutes was acceptable for Type III fluid when applied cold (air temperature). No testing was conducted with heated fluids as early indications with ice pellets showed that this was not feasible without more extensive testing to understand the potential effects.

8.2.2 Type IV Testing

The testing results showed that for OAT less than -10°C, a 10-minute allowance time at 100 knots or 15-minute allowance time at 115 knots could be feasible. Higher lift losses at the colder temperatures raised some concern, and therefore some additional tests and analysis are recommended to further substantiate these results.

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|----------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 14 | IP- / SN- | 2031 - Cold | 8 | 20 | -7.2 | -4.2 | IP = 25 SN = 10 | 10 | 2, 2, 2.1 | 1, 1.05, 1.25 | 1.64% | 100 |
| 352 | IP- / SN- | 2031 - Cold | 8 | 20 | -12.8 | -11 | IP = 25 SN = 10 | 10 | 2.5, 2.8, 3.3 | 1.1, 1.4, 1.8 | 3.75% | 100 |

Table 8.1: Summary of 2013-14 Type III Light Ice Pellets and Light Snow Testing

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|---------------------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 9 | IP- / SN- | ABC-S Plus | 8 | 20 | -10.1 | -7.3 | IP = 25 SN = 10 | 10 | 2, 2, 2.5 | 1, 1.5, 1.75 | 6.47% | 100 |
| 304 | IP- / SN- | Polar Guard Advance | 8 | 20 | -23.5 | -14.6 | IP = 25 SN = 10 | 15 | 2.5, 2.7, 3.83 | 1.2, 1.9, 3.2 | 8.01% | 115 |
| 305 | IP- / SN- | Polar Guard Advance | 8 | 20 | -23.8 | -11.4 | IP = 25 SN = 10 | 15 | 2.5, 2.6, 3.8 | 1.2, 2, 3 | 7.80% | 115 |
| 306 | IP- / SN- | Polar Guard Advance | 8 | 20 | -24 | -14.4 | IP = 25 SN = 10 | 15 | 2.3, 2.3, 3.6 | 1.2, 1.8, 3 | 7.97% | 115 |
| 309 | IP- / SN- | Polar Guard Advance | 8 | 20 | -22.6 | -9.6 | IP = 25 SN = 10 | 15 | 2.8, 2.8, 4 | 1.1, 2, 3.3 | 7.94% | 115 |
| 310 | IP- / SN- | EG106 | 8 | 20 | -23.1 | -17.4 | IP = 25 SN = 10 | 15 | 1.7, 1.7, 2.3 | 1, 1.3, 1.5 | 2.00% | 115 |
| 311 | IP- / SN- | EG106 | 8 | 20 | -23.9 | -18.1 | IP = 25 SN = 10 | 15 | 1.9, 1.9, 2.3 | 1.1, 1.5, 1.7 | 4.06% | 100 |
| 312 | IP- / SN- | Launch | 8 | 20 | -24.3 | -17.4 | IP = 25 SN = 10 | 15 | 2.8, 2.7, 3.7 | 1.1, 1.9, 2.4 | 9.11% | 115 |
| 313 | IP- / SN- | Max- Flight | 8 | 20 | -24.5 | -15.3 | IP = 25 SN = 10 | 15 | 2.6, 2.5, 3.5 | 1.1, 1.8, 2.4 | 8.54% | 115 |
| 314 | IP- / SN- | AD-49 | 8 | 20 | -24.8 | -19.8 | IP = 25 SN = 10 | 15 | 3, 2.4, 4 | 1.3, 2, 3.7 | 8.39% | 115 |
| 315 | IP- / SN- | AD-49 | 8 | 20 | -25.1 | -19.4 | IP = 25 SN = 10 | 10 | 2.9, 2.8, 3.8 | 4.1, 2.1, 3.2 | 7.14% | 115 |

Table 8.2: Summary of 2013-14 Type IV Light Ice Pellets and Light Snow Testing

APS/Library/Projects/PM2265.003 (TC Deicing 13-14)/Reports/Ice Pellet/Final Version 1.0/TP 15273E Final Version 1.0.docx Final Version 1.0, October 20

| Light Ice Pellets Mixed with Light Snow | OAT -5°C and Above | OAT Less than -5°C to -10°C | OAT Less than -10°C |
|---|-----------------------|--------------------------------|------------------------|
| 100 Kts | 10 Minutes | 10 Minutes | 10 Minutes |
| | Test # 14 | | Test # 352 |

Table 8.3: Type III Light Ice Pellets and Light Snow Allowance Time Tests Winter2013-14

Note: (h) = Hot Application of Fluid

Table 8.4: Type IV Light Ice Pellets and Light Snow Allowance Time Tests Winter2013-14

| Light Ice Pellets Mixed with Light Snow | OAT -5°C and Above | OAT Less than -5°C to -10°C | OAT Less than -10°C |
|---|-----------------------|--------------------------------|--|
| 100 Kts | 25 Minutes | 15 Minutes Test # 9 | 15 Minutes Test # 311 |
| | | 10 Minutes | 10 Minutes |
| | | 15 Minutes Test # 309 | 10 Minutes Tests # 315 |
| 115 Kts | | | 15 Minutes |
| | | | Test # 304, 310, 312, 313, 314, 305, 306 |

| | OAT -5°C AND ABOVE 100 Kts (10 MINUTES) | | | | | | | | | | | | |
|----------|--|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|--|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | | |
| 14 | 2031 - Cold | -4.2 | IP = 25 SN = 10 | 10 | 2, 2, 2.1 | Good | 1, 1.05, 1.25 | Good | 1.64% | Good | Good | | |
| | CONCLUSION: 10 MINUTES IS GOOD FOR COLD FLUID. | | | | | | | | | | | | |

Table 8.5: Summary of Type III Light Ice Pellets and Light Snow Allowance Time Test Results

OAT LESS THAN -10°C (10 MINUTES) Visual Visual Tunnel Contamination Contamination Before At % Lift Temp. Precipitation Exposure Lift Loss Overall Run # Fluid Rating Takeoff Rating Rotation Before Rate (g/dm²/h) Time (min) Status Loss Status Before Takeoff Status at Rotation (LE, Status Test (°C) (LE, TE, Flap) TE, Flap) 2031 -352 -11 IP = 25 SN = 1010 2.5, 2.8, 3.3 Good 1.1, 1.4, 1.8 Review 3.75% Good Review Cold CONCLUSION: 10 MINUTES IS GOOD FOR COLD FLUID.

Table 8.6: Summary of Type IV Light Ice Pellets and Light Snow Allowance Time Test Results

| | OAT LESS THAN -10°C | | | | | | | | | | | |
|----------|----------------------|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|--|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status | |
| | 100 Kts (10 MINUTES) | | | | | | | | | | | |
| 9 | ABC-S Plus | -7.3 | IP = 25 SN = 10 | 10 | 2, 2, 2.5 | Good | 1, 1.5, 1.75 | Good | 6.47% | Review | Review | |

APS/Library/Projects/PM2265.003 (TC Deicing 13-14)/Reports/Ice Pellet/Final Version 1.0/TP 15273E Final Version 1.0.docx Final Version 1.0, October 20

| | | | | | 100 Kts (15 M | /INUTES | 5) | | | | |
|-----|---------------------------|-------|-----------------|-----------|----------------|---------|---------------|----------|---------|--------|--------|
| 311 | EG106 | -18.1 | IP = 25 SN = 10 | 15 | 1.9, 1.9, 2.3 | Good | 1.1, 1.5, 1.7 | Review | 4.06% | Good | Review |
| | | | | | 115 Kts (10 | Minutes |) | | | | |
| 315 | AD-49 | -19.4 | IP=25 SN=10 | 10 | 2.9, 2.8, 3.8 | Good | 1.2, 1.9, 3.0 | Review | 7.14% | Review | Review |
| | | | | | 115 Kts (15 | Minutes |) | | | | |
| 304 | Polar Guard Advance | -14.6 | IP = 25 SN = 10 | 15 | 2.5, 2.7, 3.83 | Good | 1.2, 1.9, 3.2 | Review | 8.01% | Review | Review |
| 309 | Polar Guard Advance | -9.6 | IP = 25 SN = 10 | 15 | 2.8, 2.8, 4 | Good | 1.1, 2, 3.3 | Review | 7.94% | Review | Review |
| 310 | EG106 | -17.4 | IP = 25 SN = 10 | 15 | 1.7, 1.7, 2.3 | Good | 1, 1.3, 1.5 | Good | 2.00% | Review | Review |
| 312 | Launch | -17.4 | IP = 25 SN = 10 | 15 | 2.8, 2.7, 3.7 | Good | 1.1, 1.9, 2.4 | Review | 9.11% | Review | Review |
| 113 | Max-Flight | -15.3 | IP = 25 SN = 10 | 15 | 2.6, 2.5, 3.5 | Good | 1.1, 1.8, 2.4 | Review | 8.54% | Review | Review |
| 314 | AD-49 | -19.8 | IP = 25 SN = 10 | 15 | 3, 2.4, 4 | Good | 1.3*, 2, 3.7 | Review | 8.39% | Review | Review |
| 305 | Polar Guard Advance | -11.4 | IP = 25 SN = 10 | 15 | 2.5, 2.6, 3.8 | Good | 1.2, 2, 3 | Review | 7.80% | Review | Review |
| 306 | Polar Guard Advance | -14.4 | IP = 25 SN = 10 | 15 | 2.3, 2.3, 3.6 | Good | 1.2, 1.8, 3 | Review | 7.97% | Review | Review |
| | | CONCL | USION: 10-N | IINUTE TO |) 15-MINUTE A | LLOWA | NCE TIMES M | AY BE PO | OSSIBLE | | |

Table 8.6: Summary of Type IV Light Ice Pellets and Light Snow Allowance Time Test Results (cont'd)

Note: Runs #9 and #309 were run in cold conditions; however, significant warming in the tunnel caused the test temperature to rise above -10°C prior to the start.

9. LIGHT ICE PELLETS MIXED WITH MODERATE SNOW ALLOWANCE TIMES

A summary of the Light Ice Pellets Mixed with Moderate Snow tests conducted with Type III and Type IV fluids in the wind tunnel is shown in Table 9.1 and Table 9.2. The tables provide relevant information for each of the tests, as well as final values used for the data analysis. Each row contains data specific to one test. A more detailed test log of all conditions tested using the wind tunnel is provided in Subsection 3.1.

9.1 Analysis of Data Collected

The data collected has been sorted according to test parameters and included in the respective cells of the ice pellet allowance time table format for ease of reference; this is shown in Table 9.3 and Table 9.4. A more detailed analysis separating the data according to the allowance time cell and rotation speed has been conducted and is shown in Table 9.5 and Table 9.6. In addition, a conclusion regarding the test results has also been included for each condition in Table 9.5 and Table 9.6.

9.2 Overall Summary of Results

9.2.1 Type III Testing

The testing results indicated that an allowance time of 10 minutes was acceptable for Type III fluid when applied cold (air temperature). Although only 5-minute data was collected with this airfoil, historical low-speed data from 2008-09 conducted with the LS-0417 wing section indicated that a 10-minute allowance time could be possible for the below -5 °C to -10°C range. If future testing is planned, it is suggested that testing be conducted to further validate this allowance time.

No testing was conducted with heated fluids as early indications with ice pellets showed that this was not feasible without more extensive testing to understand the potential effects.

9.2.2 Type IV Testing

The results indicated that the 10-minute allowance time above -5°C is valid and has potential to be expanded.

Data also helped support the expansion of the Light Ice Pellets Mixed with Moderate Snow allowance times in the below -5° to -10°C range. The data indicated that 10 minutes would be feasible; however, the allowance was limited to 7 minutes to be conservative based on the data collected from 2009-10 to 2012-13.

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|----------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 13 | IP- / SN | 2031 - Cold | 8 | 20 | -7.4 | -3.1 | IP = 25 SN = 25 | 10 | 2.25, 1.9, 3.5 | 1, 1.5, 1.95 | 2.32% | 100 |
| 25 | IP- / SN | 2031 - Hot | 8 | 20 | -6.1 | -2.3 | IP = 25 SN = 25 | 10 | 2.5, 2, 3.75 | 1, 3.25, 3.75 | 1.76% | 100 |
| 353 | IP- / SN | 2031 - Cold | 8 | 20 | -13 | -10.2 | IP = 25 SN = 25 | 5 | 2.5, 2.7, 3.5 | 1.1, 1.4, 2 | 3.83% | 100 |

Table 9.1: Summary of 2013-14 Type III Light Ice Pellets Mixed with Moderate Snow Testing

Table 9.2: Summary of 2013-14 Type IV Light Ice Pellets Mixed with Moderate Snow Testing

| Test # | Test Condition | Fluid Name | Rotation Angle | Flap Angle (0°, 20°) | OAT Before Test (°C) | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE,TE,Flap) | Visual Contamination Rating at Rotation (LE,TE,Flap) | Corrected for 3D Effects % Lift Loss on 8° CL vs. Dry CL | Speed Kts |
|--------|-------------------|---------------|-------------------|-------------------------------|-------------------------------|---|------------------------------------|---------------------------|---|--|---|--------------|
| 10 | IP- / SN | ABC-S Plus | 8 | 20 | -9.6 | -6.7 | IP = 25 SN = 25 | 10 | 2, 2, 3 | 1, 1.5, 2.25 | 6.38% | 100 |
| 11 | IP- / SN | Launch | 8 | 20 | -9 | -5.2 | IP = 25 SN = 25 | 10 | 2, 1.75, 3.25 | 1, 1.35, 2.25 | 6.70% | 100 |
| 12 | IP- / SN | AD-49 | 8 | 20 | -7.4 | -3.3 | IP = 25 SN = 25 | 10 | 2, 2, 3.5 | 1, 1.6, 2.25 | 5.75% | 100 |

| Table 9.3: Type III Light Ice Pellets Mixed with Moderate Snow Allowance Time |
|---|
| Tests Winter 2013-14 |

| Light Ice Pellets Mixed with Moderate Snow | OAT -5°C and Above | OAT Less than -5°C to -10°C | OAT Less than -10°C |
|---|-----------------------|--------------------------------|------------------------|
| 100 kts | 10 minutes | 10 Minutes | 5 Minutes |
| | Test # 13, 25(h) | N/A | Test # 353 |

Note: (h) = Hot Application of Fluid

Table 9.4: Type IV Light Ice Pellets Mixed with Moderate Snow Allowance TimeTests Winter 2013-14

| Light Ice Pellets Mixed with Moderate Snow | OAT -5°C and Above | OAT Less than -5°C to -10°C | OAT Less than -10°C |
|---|-----------------------|--------------------------------|------------------------|
| 100 kts | 10 minutes | 10 Minutes | |
| 100 Kts | Test # 12 | Test # 10, 11 | |

| | | | | OAT -5° | C AND ABOVI | E 100 Kt | ts (10 MINUTE | ES) | | | |
|----------|---------------|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status |
| 13 | 2031- Cold | -3.1 | IP=25 SN=25 | 10 | 2.25, 1.9, 3.5 | Good | 1, 1.15, 1.2 | Good | 2.32% | Good | Review |
| 25 | 2031 - Hot | -2.3 | IP = 25 SN = 25 | 10 | 2.5, 2, 3.75 | Good | 1, 3.25, 3.75 | Good | 1.76% | Good | Good |
| | | 1 | COI | NCLUSION | : 10 MINUTES | S IS GOO | DD FOR COLD | FLUID. | 1 | I. | |

| | | | | OAT LESS | THAN -10°C | 100 Kts | (5 MINUTES) | | | | |
|----------|----------------|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|-------------|------------------------|-------------------|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status |
| 353 | 2031 - Cold | -10.2 | IP = 25 SN = 25 | 5 | 2.5, 2.7, 3.5 | Good | 1.1, 1.4, 2 | Review | 3.83% | Good | Review |
| | CONC | LUSION | 5 MINUTES | | FOR COLD FL | | | Y BE FEA | SIBLE BA | SED ON | l |

| | | | | OAT -5° | C AND ABOVI | E 100 K | ts (10 MINUTE | ES) | | | |
|----------|-------|--|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status |
| 12 | AD-49 | -3.3 | IP = 25 SN = 25 | 10 | 2, 2, 3.5 | Good | 1, 1.6, 2.25 | Good | 5.75% | Review | Review |
| | | CONC | LUSION: 10 | -MINUTE / | ALLOWANCE | TIME IS | VALID AND C | OULD BE | EXPAN | IDED. | |

Table 9.6: Summary of Type IV Light Ice Pellets Mixed with Moderate Snow Allowance Time Test Results

| | | | 0A1 | LESS TH | AN-5°C TO -1 | 10°C 10 | 00 Kts (10 MIN | UTES) | | | |
|----------|---------------|---|---------------------------------|------------------------|---|-----------------------------|--|--------------------------|----------------|---------------------|-------------------|
| Run # | Fluid | Tunnel Temp. Before Test (°C) | Precipitation Rate (g/dm²/h) | Exposure Time (min) | Visual Contamination Rating Before Takeoff (LE, TE, Flap) | Before Takeoff Status | Visual Contamination Rating at Rotation (LE, TE, Flap) | At Rotation Status | % Lift Loss | Lift Loss Status | Overall Status |
| 10 | ABC-S Plus | -6.7 | IP = 25 SN = 25 | 10 | 2, 2, 3 | Good | 1, 1.5, 2.25 | Good | 6.38% | Review | Review |
| 11 | Launch | -5.2 | IP = 25 SN = 25 | 10 | 2, 1.75, 3.25 | Good | 1, 1.35, 2.25 | Good | 6.70% | Review | Review |
| | | 1 | | | : 10-MINUTE A ISTORICAL DA | | | - | 1 | | |

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10. CONCLUSIONS AND OBSERVATIONS

These observations and conclusions were derived from the testing conducted during the winter of 2013-14.

10.1 Type III High-Speed Allowance Times

Testing was conducted during the winter of 2013-14 with the objective of substantiating the low-speed Type III allowance time table previously developed (but not published) in 2008-09 for use with high-speed performance aircraft. This approach was conservative, however, to minimize the costs associated with developing a brand new table and to help accelerate the development process.

The data collected in 2013-14 supported the development of a comprehensive Type III unheated fluid allowance time table for use with high-speed rotation aircraft. Preliminary data was also collected with heated Type III fluid applications; however, the tests showed risks of adhered contamination during takeoff, and therefore guidance could not be issued without further investigating the possible risks associated.

10.2 Type IV High-Speed Allowance Times

Testing was conducted during the winter of 2013-14 to validate and expand the existing allowance times. The data collected in 2013-14 supported the following changes:

- 10-minute allowance time for Moderate Ice Pellets at 115 knots rotation speed should be limited to -16°C for PG fluids due to the higher lift losses observed; and
- 7-minute allowance time for Light Ice Pellets Mixed with Moderate Snow below -5° to -10°C.

Some preliminary data also indicated the following; however, no guidance changes were made until further testing can be conducted:

- 10-minute allowance time at 100 knots or 15-minute allowance time at 115 knots could be feasible for Light Ice Pellets Mixed with Light Snow below -10°C; and
- 10-minute allowance time above -5°C for Light Ice Pellets Mixed with Moderate Snow has margin to be expanded.

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11. RECOMMENDATIONS

The following recommendations were compiled based on the work conducted during the winter of 2013-14.

11.1 Changes to Ice Pellet Allowance Time Guidance

The following changes were made to the Ice Pellet Allowance Time guidance material based on the 2013-14 wind tunnel test results.

- Research was conducted to provide additional guidance for aircraft operations during ice pellet conditions when operating with undiluted (100/0) Type III fluid applied unheated. A separate ice pellet allowance time table has been developed for Type III fluids and is included in this document (Table 11.1 and Table 11.2).
- Small hail has been added to the allowance time tables as it has been determined to be meteorologically equivalent to moderate ice pellets (see previous section). It has also been added to the titles of the allowance time guidance section and allowance time tables (Table 11.1, Table 11.2, Table 11.3, and Table 11.4).
- Research has indicated that Type IV PG fluids are removed less effectively during takeoff when contaminated with moderate ice pellets at temperatures below -16°C. Therefore, operations in these conditions are not recommended, and no allowance times exist for PG fluids in conditions of moderate ice pellets at temperatures below -16°C, irrespective of aircraft rotation speed.
- Research has provided data to support a new Type IV allowance time of 7 minutes for light ice pellets mixed with moderate snow at temperatures below -5 to -10°C.

The brand new Type III allowance time table is shown in Table 11.1 and Table 11.2, and the updated Type IV allowance time table is shown in Table 11.3 and Table 11.4.

11.2 Future Testing Using the PIWT and Thin High-Performance Wing Model

The testing results have demonstrated the PIWT and thin high-performance wing model are appropriate for the testing and comparative evaluation of de/anti-icing fluid flow-off with and without contamination. It is recommended that testing continue

using the existing methodologies with an outlook to continue improving on testing protocols and procedures.

| ansport Canada Holdover Time G | ulaelines | V | Vinter 2014-20 |
|---|------------------------|----------------------|---------------------------------|
| | TABLE 11 | | |
| SAE TYPE III ICE PELLE | T AND SMALL HAIL | ALLOWANCE TIM | ES |
| This table is for use with SAE Type | | | |
| THE RESPONSIBILITY FOR THE APPLIC | | | |
| Precipitation Type | Ou -5°C and above | Itside Air Temperati | ure Below -10°C ¹ |
| Light Ice Pellets | 10 minutes | 10 minutes | |
| Moderate Ice Pellets or Small Hail | 5 minutes | 5 minutes | |
| Light Ice Pellets Mixed with Light or Moderate Freezing Drizzle | 7 minutes | 5 minutes | |
| Light Ice Pellets Mixed with Light Freezing Rain | 7 minutes | 5 minutes | |
| Light Ice Pellets Mixed with Light Rain | 7 minutes ² | | Caution: No allowance times |
| Light Ice Pellets Mixed with Moderate Rain | | | currently exist |
| Light Ice Pellets Mixed with Light Snow | 10 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Moderate Snow | 10 minutes | 10 minutes | |
| IOTES Ensure that the lowest operational use temperature No allowance times exist in this condition for ten freezing rain. CAUTIONS Fluids used during ground de/anti-icing do not | nperatures below 0°C; | - | ce pellets mixed with |
| | | | |

Table 11.1: 2014-15 TC Type III Ice Pellet Allowance Time Table

Table 11.2: 2014-15 FAA Type III Ice Pellet Allowance Time Table

2014-2015 Holdover Times Tables

08/01/14

TABLE 9. FAA ICE PELLET AND SMALL HAIL ALLOWANCE TIMES FOR SAE TYPE III FLUIDS (2014-2015)

This table is for use with SAE Type III undiluted (100/0) fluids applied unheated only

| Precipitation Type | Outside Air Temperature | | |
|--|-------------------------|-------------------|--------------------------------|
| | -5°C and above | Below -5 to -10°C | Below -10°C ¹ |
| Light Ice Pellets | 10 minutes | 10 minutes | |
| Moderate Ice Pellets or Small Hail | 5 minutes | 5 minutes | |
| Light Ice Pellets Mixed with Light or Moderate Freezing Drizzle | 7 minutes | 5 minutes | |
| Light Ice Pellets Mixed with Light Freezing Rain | 7 minutes | 5 minutes | |
| Light Ice Pellets Mixed with Light Rain | 7 minutes ² | | Caution: No allowance times |
| Light Ice Pellets Mixed with Moderate Rain | | - - | currently exist |
| Light Ice Pellets Mixed with Light Snow | 10 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Moderate Snow | 10 minutes | 10 minutes | |

THE RESPONSIBILITY FOR THE APPLICATION OF THESE DATA REMAINS WITH THE USER

NOTES

- 1 Ensure that the lowest operational use temperature (LOUT) is respected.
- 2 No allowance times exist in this condition for temperatures below 0°C; consider use of light ice pellets mixed with light freezing rain.

CAUTIONS:

- FLUIDS USED DURING GROUND DE/ANTI-ICING DO NOT PROVIDE IN-FLIGHT ICING PROTECTION.
- THIS TABLE IS FOR DEPARTURE PLANNING ONLY AND SHOULD BE USED IN CONJUNCTION WITH
 PRETAKEOFF CHECK PROCEDURES.

Table 11.3: 2014-15 TC Type IV Ice Pellet Allowance Time Table

Transport Canada Holdover Time Guidelines

Winter 2014-2015

TABLE 12

SAE TYPE IV ICE PELLET AND SMALL HAIL ALLOWANCE TIMES

This table is for use with SAE Type IV undiluted (100/0) fluids only. All Type IV fluids are propylene glycol based with the exception of Dow EG106 and LNT Solutions E450 which are ethylene glycol based.

THE RESPONSIBILITY FOR THE APPLICATION OF THESE DATA REMAINS WITH THE USER

| Precipitation Type | Outside Air Temperature | | |
|--|-------------------------|-------------------|--------------------------------|
| | -5°C and above | Below -5 to -10°C | Below -10°C ¹ |
| Light Ice Pellets | 50 minutes | 30 minutes | 30 minutes ² |
| Moderate Ice Pellets or Small Hail | 25 minutes ³ | 10 minutes | 10 minutes ^{2,4} |
| Light Ice Pellets Mixed with Light or Moderate Freezing Drizzle | 25 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Light Freezing Rain | 25 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Light Rain | 25 minutes⁵ | | Caution: No allowance times |
| Light Ice Pellets Mixed with Moderate Rain | 25 minutes ⁶ | | currently exist |
| Light Ice Pellets Mixed with Light Snow | 25 minutes | 15 minutes | |
| Light Ice Pellets Mixed with Moderate Snow | 10 minutes | 7 minutes | |

NOTES

Ensure that the lowest operational use temperature (LOUT) is respected.

- No allowance times exist for propylene glycol (PG) fluids, when used on aircraft with rotation speeds less than 115 knots. (For these aircraft, if the fluid type is not known, assume zero allowance time). Allowance times exist for propylene glycol (PG) fluids or when the fluid type is unknown. No allowance times exist for propylene glycol (PG) fluids in this condition for temperatures below -16°C. 2
- 3
- 4
- 5 No allowance times exist in this condition for temperatures below 0°C; consider use of light ice pellets mixed with light freezing rain.
- 6 No allowance times exist in this condition for temperatures below 0°C.

CAUTIONS

Fluids used during ground de/anti-icing do not provide in-flight icing protection.

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Table 11.4: 2014-15 FAA Type IV Ice Pellet Allowance Time Table

2014-2015 Holdover Times Tables

08/01/14

TABLE 10. FAA ICE PELLET AND SMALL HAIL ALLOWANCE TIMES FOR SAE TYPE IV FLUIDS (2014-2015)

This table is for use with SAE Type IV undiluted (100/0) fluids only. All Type IV fluids are propylene glycol based with the exception of Dow EG106 and LNT E450 which are ethylene glycol based.

| Precipitation Type | Outside Air Temperature | | |
|--|-------------------------|-------------------|--------------------------------|
| | -5°C and above | Below -5 to -10°C | Below -10°C ¹ |
| Light Ice Pellets | 50 minutes | 30 minutes | 30 minutes ² |
| Moderate Ice Pellets or Small Hail | 25 minutes ³ | 10 minutes | 10 minutes ^{2,4} |
| Light Ice Pellets Mixed with Light or Moderate Freezing Drizzle | 25 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Light Freezing Rain | 25 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Light Rain | 25 minutes⁵ | | Caution: No allowance times |
| Light Ice Pellets Mixed with Moderate Rain | 25 minutes ⁶ | | currently exist |
| Light Ice Pellets Mixed with Light Snow | 25 minutes | 15 minutes | |
| Light Ice Pellets Mixed with Moderate Snow | 10 minutes | 7 minutes | |

THE RESPONSIBILITY FOR THE APPLICATION OF THESE DATA REMAINS WITH THE USER

NOTES

- 1 Ensure that the lowest operational use temperature (LOUT) is respected.
- 2 No allowance times exist for propylene glycol (PG) fluids when used on aircraft with rotation speeds less than 115 knots. (For these aircraft, if the fluid type is not known, assume zero allowance time).
- 3 Allowance time is 15 minutes for propylene glycol (PG) fluids, or when the fluid type is unknown.
- 4 No allowance times exist for propylene glycol (PG) fluids in this condition for temperatures below -16°C.
- 5 No allowance times exist for this condition for temperatures below 0 °C; consider use of light ice pellets mixed with light freezing rain.

6 $\,$ No allowance times exist in this condition for temperatures below 0 $^{\circ}\text{C}$

CAUTIONS:

- FLUIDS USED DURING GROUND DE/ANTI-ICING DO NOT PROVIDE IN-FLIGHT ICING PROTECTION.
- THIS TABLE IS FOR DEPARTURE PLANNING ONLY AND SHOULD BE USED IN CONJUNCTION WITH PRETAKEOFF CHECK PROCEDURES.

11.3 Future Research

The following sections describe higher priority areas of possible future wind tunnel testing and research. These areas of future research have been determined based on consultations with TC, the FAA, and NASA and through industry discussions, and as such they may not be directly linked to the research described in this report. These areas of research have been listed below for ease of reference and to maintain continuity in the year-to-year reporting.

11.3.1 Allowance Time Expansion of Mixed Light Ice Pellets and Light and Moderate Snow Conditions

Historical winter weather data has indicated that a significant portion of ice pellet occurrences are mixed with light or moderate snow conditions. The data collected to date has indicated a potential to further expand the allowance times to include colder temperatures as well as to provide longer allowance times at the warmer temperatures. A more detailed multi-year analysis of the data collected in these conditions should be performed to determine future testing targets.

11.3.2 Lift Losses at LOUT

Previous testing has shown that lift losses in general significantly increase at the lower temperatures. Limited data is available at (or very near) the fluid LOUT. Additional testing is recommended to obtain data close to the fluid LOUT to determine the aerodynamic effects of ice pellet contamination at these colder temperatures.

11.3.3 Substantiation of Ice Pellet Allowance Times with New Fluids

Testing should continue to investigate different Type III and IV fluids to further substantiate the ice pellet allowance times. Testing should consider new fluids or fluids previously tested but with limited data.

11.3.4 Lift Loss Scaling with NASA LS-0417 and NACA 23012 Wing Sections

The extensive work conducted with the thin high-performance wing section has led to the development of a methodology for evaluating aerodynamic performance based on a lift loss scaling between the model results and the AS5900 aerodynamic acceptance test. If research capacities are available, it is recommended that limited testing be conducted with the wing sections previously tested in 2006-07 and 2008-09 to better understand the sensitivity of these models used in the development of the ice pellet allowance time tables.

REFERENCES

1. Ruggi, M., Wind Tunnel Trials to Examine Anti-Icing Fluid Flow-Off Characteristics and to Support the Development of Ice Pellet Allowance Times, Winters 2009-10 to 2012-13, APS Aviation Inc., Transportation Development Centre, Montreal, November 2013, TP 15232E, XX (to be published). This page intentionally left blank.

APPENDIX A

TRANSPORTATION DEVELOPMENT CENTRE WORK STATEMENT EXCERPT – AIRCRAFT & ANTI-ICING FLUID WINTER TESTING 2013-14

TRANSPORTATION DEVLOPMENT CENTRE WORK STATEMENT EXCERPT – AIRCRAFT & ANTI-ICING FLUID WINTER TESTING 2013-14

5.39 Wind Tunnel Testing

5.39.1 Testing to Further Refine Ice Pellet Allowance Times (1 Week)

NOTE: This task is scheduled for 3 total weeks of testing: 1 week related to ice pellet allowance time development, 1 week to support the development of aircraft ground deicing related procedures and technologies. The 3rd week will consist of 2 days to evaluate Type I LOUT for very low speed aircraft, and 3 days to conduct Type III allowance time testing. As such, the costing has been split accordingly.

a) Meet and discuss with NRC personnel to arrange for access to the Propulsion Wind Tunnel (PWT) in M46 at the NRC Montreal Road facility in Ottawa;

NOTE: The NRC facility costs associated with testing at M46 are not included in this task and are dealt with directly with TC through a M.O.U. agreement with NRC.

- b) Develop a procedure and test plan with the NRC staff who operates the PIWT. It is anticipated that much of the testing will be conducted during overnight hours; The procedure will specify the collection of the following data during the tests:
 - i. Type and amount of fluid applied;
 - ii. Type and rate of contamination applied;
 - iii. Extent of fluid contamination prior to the test run;
 - iv. Fluid Brix, thickness, and temperature measurements; and
 - v. High speed photography and videography.
- c) Conduct pre-testing setup and calibration work;
- d) Perform wind tunnel tests over a period of five (5) days to further refine ice pellet allowance times with ethylene glycol and propylene glycol anti-icing fluids, to validate and possibly expand current allowance times published by TC and FAA for super-critical airfoils; and
 - i. A portion of the testing will be to perform correlation testing to calibrate the TC model and to demonstrate repeatability with dry wing, fluid, and fluid and contamination. Changes or upgrades to equipment (such as ice pellet dispensers) will need to be evaluated to demonstrate repeatability through comparative testing;

- ii. Testing will attempt to expand the ice pellet allowance times in cells where allowance times are restrictive, or not currently available;
- iii. Testing will attempt to validate the ice pellet allowance times cells for use with new fluids; and
- iv. Testing will attempt to collect additional data in ice pellet allowance times cells where data with specific fluids previously tested may be limited, typically at colder temperatures.
- e) Analyze the data collected, Report the findings, and prepare presentation material for the SAE G-12 meetings.

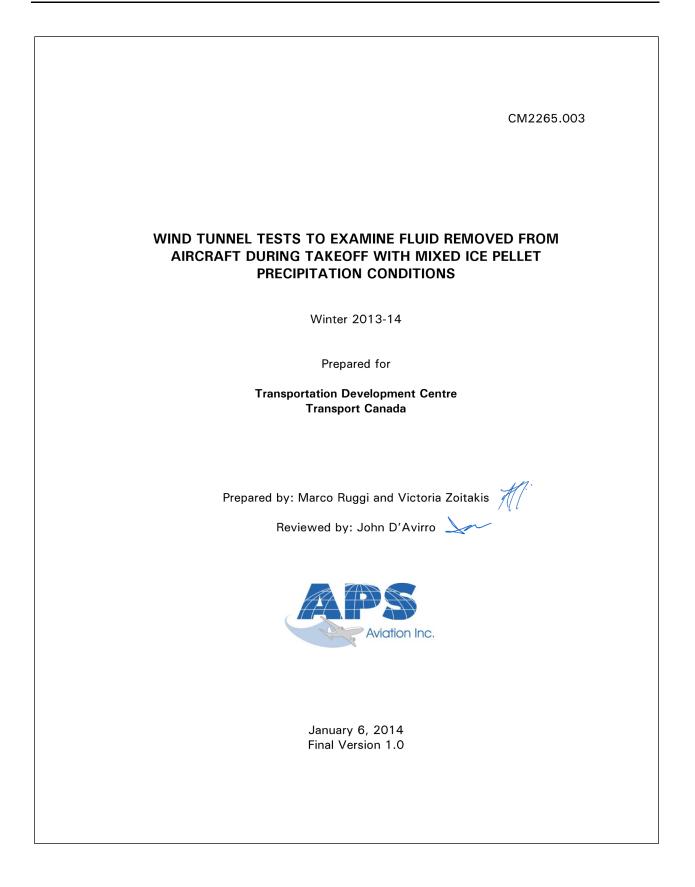
5.39.4 Type III Ice Pellet Allowance Timed Testing - Phase 1 (3 Days)

Testing will be done according to the procedures and methodologies used for "Testing to Further Refine Ice Pellet Allowance Times".

- a) Identify other aircraft types that may be affected by lack of current operational guidance. Identify current operational performance limitations associated with dispatching during ice pellet conditions in affected aircraft types;
- b) Conduct a thorough review of Type III data collected in previous years of ice pellet testing to determine information gaps;
- c) Develop procedure for conducting wind tunnel testing in accordance with the existing ice pellet allowance time testing methodology;
- d) Conduct testing over a period of three (3) days at the NRC PIWT. Testing will target obtaining data to fill the information gaps from previous years, and to provide guidance that could be useful for the operation at Toronto Island Airport;
- e) Analyze the data and develop preliminary Type III allowance time guidance;
- f) Report the findings, and prepare presentation material for the SAE G-12 meetings; and
- g) If appropriate publish limited Type III allowance times in the Transport Canada 2014-2015 HOT Guidelines.

APPENDIX B

PROCEDURE: WIND TUNNEL TESTS TO EXAMINE FLUID REMOVED FROM AIRCRAFT DURING TAKEOFF WITH MIXED ICE PELLET PRECIPITATION CONDITIONS



WIND TUNNEL TESTS TO EXAMINE FLUID REMOVED FROM AIRCRAFT DURING TAKEOFF WITH MIXED ICE PELLET PRECIPITATION CONDITIONS

WIND TUNNEL TESTS TO EXAMINE FLUID REMOVED FROM AIRCRAFT DURING TAKEOFF WITH MIXED ICE PELLET **PRECIPITATION CONDITIONS**

1. BACKGROUND

Prior to the winter of 2006-07, Holdover Time (HOT) guidance material did not exist for ice pellet conditions, however aircraft could still depart during ice pellet conditions following aircraft deicing and a pre take off contamination check. This protocol was feasible for common air carrier aircraft that provided access to emergency exit windows overlooking the leading edge of the aircraft wings; however, it posed a significant problem for cargo aircraft that have limited visibility of the wings from the cabin.

On December 22, 2004, United Parcel Service (UPS) aircraft in Louisville were grounded for several hours due to extended ice pellet conditions. Due to cargo aircraft configuration, pre-take off contamination checks by the on-board crew were not possible. FedEx had been faced with similar problems in Memphis. Following this event, in October 2005, the FAA issued two notices restricting take offs in ice pellet conditions.

As a result of this costly incident, UPS set out to obtain experimental data to provide guidance and allow operations to continue in ice pellet conditions. During the winter of 2004-05, aerodynamic and endurance time testing were conducted in simulated ice pellet conditions. APS also conducted some preliminary flat plate research (see TP 14718E). Based on the preliminary data, an allowance of 20 minutes in light ice pellet conditions was proposed, however no changes to the HOT guidelines were made.

During the following winter of 2006-07, the FAA provided a 25 minute allowance as a preliminary guideline; TC issued a note indicating that no changes would be made to the HOT guidelines. This allowance was based on the previous research conducted during the winter of 2005-06, primarily as a result of Falcon 20 aerodynamic research (see TP 14716E); these results were presented at the Society of Automotive Engineers (SAE) meeting in Lisbon in May 2006. To address the option of a pre-take off contamination check, the 20 minute targeted allowance was extended to 25 minutes; pre-take off contamination checks would no longer apply. This allowance was followed by a list of conditions; one restriction was that operations would be limited to ice pellets alone (no mixed conditions).

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Due to the high occurrence of ice pellets combined with freezing rain or snow, the industry requested additional guidance material for operations in mixed ice pellet conditions. Additional endurance time testing and aerodynamic research were conducted in simulated ice pellet conditions during the winter of 2006-07.

During the winter of 2007-08, the TC and FAA provided allowance time guidance material for operations in mixed conditions with ice pellets guideline. These allowance times were based on the research conducted during the winter of 2006-07 (see TP 14779E). The recommended allowance times were based on aerodynamic research conducted using the $3 \text{ m} \times 6 \text{ m}$ Open Circuit Propulsion and Icing Wind Tunnel (PIWT) and the NRC Falcon 20 aircraft; these results were presented at the SAE meeting in San Diego in May 2007. These allowance time guidelines were followed by a list of restrictions based on the results obtained through the research conducted, and the lack of data in specific conditions.

During the winter of 2008-09, additional endurance time testing and aerodynamic research was conducted to support and further expand the ice pellet allowance times (see TP 14935E). Full-scale testing with the NRC PIWT was conducted in mixed conditions with ice pellets and in non precipitation conditions. Testing was geared towards validating the current ice pellet allowance times, and potentially expanding the guidance material to include different conditions, fluids, and acceleration profiles. A revised version of the ice pellet allowance times was published for the winter of 2009-10; changes were made to the high speed table allowance times only.

During the winter of 2009-10, additional aerodynamic research using a generic super-critical wing model was conducted at the NRC PIWT to support and further expand the ice pellet allowance times for use with newer generation aircraft. During the testing, fluid flow-off issues with the supercritical wing were observed with PG fluids at the lower temperatures; more specifically during light ice pellets and moderate ice pellet conditions below -10°C. In addition fluid failure issues with the supercritical wing were observed with PG fluids during moderate ice pellets above -5°C; the relatively flat surface of the wing had less fluid flow off during contamination and resulted in an earlier fluid failure for PG fluids. In general, higher lift losses were observed with the supercritical wing as compared to previous wings tested. A revised version of the ice pellet allowance times was published for the winter of 2009-10. Additional analysis paired with wind tunnel testing was recommended for the winter of 2010-11 to develop a correlation between the lift losses observed in the wind tunnel and those used as the basis of the aerodynamic acceptance tests for fluid certification.

Results from the 2010-11 testing demonstrated similar results to the 2009-10 testing in that the results indicated fluid flow-off issues with the supercritical

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wing when using PG fluids at the lower temperatures. The results indicated that the changes to the guidance material made the previous winter were still relevant and should remain in the allowance time table for the winter of 2011-12. However, a large part of the 2010-11 work was focused on developing a correlation between the PIWT and the aerodynamic acceptance test. Based on the work that was conducted by NASA and APS, it was determined that a maximum lift loss of 5.24% on the B737-200ADV airplane is equivalent to a lift loss of 7.29% on the PIWT model. Due to the scatter in the data, the standard error of the estimate resulted in a range of values which determined an upper limit of lift loss on the PIWT model of 9.2% and a lower limit of 5.4%. Currently the scatter in the "review" range is still large and causes complications when analyzing the data collected. It is anticipated that as future testing progresses, and as more data is collected, a single-value pass/fail cutoff maybe developed similar to the AAT and B737-200ADV airplane tests.

Due to industry concern with the validity of the results obtained, and the relevance of the test methods to operational aircraft, it was recommended that testing during the winter of 2011-12 focus on surveying and calibrating the wind tunnel to obtain a better sense of the repeatability of the results. With the support of NRC and under direction of NASA, a large series of test runs were conducted to better understand the performance characteristics of the wind tunnel and airfoil. The results indicated that the year-to-year equipment and facility upgrades have increased the integrity of the aerodynamic data produced, and the wind tunnel can closely simulate aircraft take-off profiles. The characterization of the current dry wing model with original endplates demonstrated appropriate aerodynamic behavior. The back-to-back fluid-only runs demonstrated excellent repeatability of test methods and this was reflected in the aerodynamic data collected. The repeatability of the testing was considered acceptable for this type of aerodynamic testing work and was not indicative of systematic errors in procedures or equipment.

FAA and TC were satisfied with calibration technical evaluation results, and therefore it was recommended that testing during the winter of 2012-13 revert back to the initial research and development objectives of further refining and substantiating the ice pellet allowance times. During the winter of 2012-13, the clean, dry wing aerodynamic repeatability was confirmed in comparison with previous data and the additional data collected in 2012-13 helped in substantiating these findings. The stalling characteristics of the wing with fluid (or fluid with contamination) appeared to be driven by secondary wave effects near the leading edge; these effects were difficult to interpret on the two-dimensional model relative to a fully three-dimensional wing and therefore should not be used in developing allowance times. Additional lift-loss scaling correlation data with different fluids at colder temperatures confirmed that previous lift loss limits were still valid. Forty ice pellet allowance time tests were

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conducted to validate and possibly expand the current guidance material. The data validated the current allowance times with new fluids and also indicated a potential to expand the allowance times for light ice pellets mixed with light snow and moderate snow.

For the Winter 2013-14, the primary focus of testing will be on the ice pellet allowance time validation and development and other R&D activities.

2. **OBJECTIVES**

The objective of this testing is to conduct aerodynamic testing with a super critical airfoil to:

- Ensure the repeatability of the dry wing performance;
- Expand the ice pellet allowance times for light ice pellets mixed with light or moderate snow conditions;
- Substantiate the current ice pellet allowance times with new fluids, fluids previously tested but with limited data, and temperatures close to the lowest operational use temperature (LOUT);
- Evaluate the equivalency of the new ice pellet/snow dispenser systems;
- Evaluate the effect of coatings on aerodynamics with and without fluids;
- Support the development of a Type III ice pellet allowance time table; and
- Evaluate Type I fluid flow-off performance for low speed rotation less than 80 knots.

Attachments I to VII provide additional information for performing some of these activities which may not use the typical wind tunnel testing methodology.

As lower priority objectives, testing may be conducted to investigate other objectives of high importance to industry which may include (and is described further in Section 6.11):

- Evaluation of an airfoil performance monitor (APM) system;
- Heavy snow;
- Heavy contamination;
- Effect of cooling system on testing repeatability;
- Effect of fluid viscosity;
- Fluid and contamination at LOUT;
- Small hail;

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WIND TUNNEL TESTS TO EXAMINE FLUID REMOVED FROM AIRCRAFT DURING TAKEOFF WITH MIXED ICE PELLET PRECIPITATION CONDITIONS • Frost simulation in the wind tunnel; Flaps/Slats testing to support YMX tests; Mixed HOT conditions; o Snow on an un-protected wing; • Feasibility of IP testing at higher speed (130-150kts); o Windshield washer used as a Type I deicer; o Effect of fluid seepage on dry wing performance; and Second wave of fluid at rotation. To satisfy these objectives, a super-critical wing section (Figure 2.1) will be subjected to a series of tests in the NRC PIWT. The dimensions indicated are in inches. This wing section was constructed by NRC in 2009 specifically for the conduct of these tests following extensive consultations with an airframe manufacturer to ensure a representative super-critical design. Fifteen days of testing have been scheduled for the conduct of these tests. The available testing days will be from January 8^{th} to the 31^{st} (see Figure 2.2). Testing will likely be conducted during overnight periods (i.e. 10 pm - 6 am), unless temperatures are suitable for day/evening testing. The weekends will be considered only if deemed necessary. 17 Figure 2.1: Super-Critical Wing Section

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| | | | DAR JANUAI | | | |
|----------------|--|--|---|---|--|--|
| Sunday | Monday | Tuesday | Wednesday | Thursday I 2 NRC back from holidays | Friday check forecast and ensure wx is good for the daytime testing (1st | Saturday |
| | 5 6 | 7 | TEST DAY 1 | 3 TEST DAY 2 | daytime testing (1st 10 TEST DAY 3 | 1 |
| | | | -Set-up calibration, training, briefing TES TING | TESTING | TESTING | |
| | ice Pelet Manufacturing Start | Pack Truck and leave for YOW ice Peter Manufacturing Continue | ACTIVITY TBD* day shift (Ram-Apro) | ACTIVITY TBD day sNift (Sam-Apre) | ACTIVITY TBD day shift (8xm-4pm) | |
| | 12 13 | 14 | WT Task: TBD | WT Tesk: TBD | WT Tesk: TBD | 18 |
| | TEST DAY 4 | TEST DAY 5 | TEST DAY 6 | TEST DAY 7 | TEST DAY 8 | |
| | ACTIMITY TBD | TESTING ACTIVITY TBD | TESTING ACTIVITY TBD | TESTING ACTIVITY TBD | TESTING ACTIVITY TBD | |
| | WT Task: TBD | WT Task: TBD | WT Task: TBD | WT Task: TBD | WT Task: TBD | |
| | 19 20 TEST DAY 9 | 21 TEST DAY 10 | 2 TEST DAY 11 | 2 23 TEST DAY 12 | 24 TEST DAY 13 | 25 |
| | TESTING | TESTING ACTIVITY | TESTING ACTIVITY | TESTING | TESTING | |
| | TBD | TBD | TBD | TBD | TBD | |
| | WT Task: TBD 26 27 | WT Task: TBD 28 | WT Task: TBD 2 | WT Task: TBD 30 | WT Task: TBD 31 | FEB |
| | TEST DAY 14 | TEST DAY 15 | BACKUP DAY | BACKUP DAY | BACKUP DAY | |
| | TESTING ACTIVITY TBD | TESTING ACTIVITY TBD | TESTING ACTIVITY TBD | TESTING ACTIMITY TBD | TESTING ACTIVITY TBD | |
| NOTES | WT Task: TBD | WT Task: TBD | WT Task: TBD | WT Task: TBD | WT Task: TBD | |
| | effect of cooling system tests | | TING ACTIVI | TIES | | |
| | | | | | | n/a TYPE III |
| Above 0°C | | | | | | ALLOWANCE TIMES (also some at above 0°C) |
| | | | | | | WT Task: TIII |
| | #1 TYPE III | | | | | |
| 0°C to -5°C | ALLOWANCE TIMES (also some at above 0°C) WT Task; Till | | | | | |
| | #2 | #3 | #4 SNC (skin no coating), | #5 | #6 | #7 R&D ACTIVITIES |
| Below -5°C | NEW ICE PELLET DISPENSER CALIBRATION | Coatings: B14, B15 -M ethodology Validation -Orag and Fuel Efficiency -Effect on Fluid Flow Off -Effect with Contamination | SNC (skin no coating), OW (Original Wing) -trethodology Validation -Orag and Fuel Efficiency -Effect on Fluid Flow Off Effect with Coating Index | Coatings: E1, C3 -M ethodology Validation -Drag and Fuel Efficiency -Effect on Fluid FlowOff -Effect with Contamination | Coatings: B12, B13, SNC -M ethodology Validation -Drag and Fuel Efficiency -Effect with Contamination -Instalation Recentability | - APM UNIT - EFFECT OF COOLING - HEAVY SNOW - ETC |
| | WT Task: IP #8 | WT TASK: R&D | WT TASK: R&D | WT TASK: R&D | WT TASK: R&D | WT TASK: R&D / IP |
| -5°C to -10°C | IP EXPANSION (IP/SN, IP/SN-) | TYPE III ALLOWANCE TIMES | | | | TYPE I FOR VERY LOW SPEED T/O |
| | (also some at -10 to -30°C) WT Task: IP | WT Task: Till | | | | (also some at -5 to -10°) WT Task: TI <60kts |
| | #10 | #11 | | | | n/a |
| -10°C to -20°C | TYPE III ALLOWANCE TIMES | TYPE I FOR VERY LOW SPEED T/O (also some at -5 to -10°) | | | | IP EXPANSION (IP/SN, IP/SN-) (also some at -10 to -30°C) |
| | WT Task: TIII #12 | WT Task: TI <60kts #13 | #14 | W15 | | WT Task: IP n/a |
| -20°C to -30°C | IP VALIDATION (NEW TEMPS & FLUIDS) | IP VALIDATION (NEW TEMPS & FLUIDS) | TYPE I FOR VERY LOW SPEED T/O (also some <30°C) | | | IP EXPANSION (IP/SN, IP/SN-) (also some at -10 to -30°C) |
| | WT Task: IP | WT Task: IP | WT Task: TI <60kts | WT Task: IP / R&D | | WT Task: IP |
| | | | | | | n/a |
| Below -30°C | | | | | | TYPE I FOR VERY LOW SPEED T/O (also some <-30°C) |
| | | | | | | WT Task: TI <60kts |
| | | Figure 10 |).1: Test | Calenda | r | |

TEST PLAN 3.

The NRC wind tunnel is an open circuit tunnel. The temperature inside the wind tunnel is dependent on the outside ambient temperature. Prior to testing, the weather should be monitored to ensure proper temperatures for testing.

Representative Type I/III/IV propylene and ethylene fluids in Neat form (standard mix for Type I) shall be evaluated against their uncontaminated performance; Attachments VIII to XIV present the generic holdover time guidelines for Type I and III as well as the fluid-specific holdover time guidelines for the representative Type IV fluids that will be tested. The current Ice Pellet Allowance Time table has been included in Attachment XV.

A preliminary list of test objectives is shown in Table 3.1. It should be noted that the order in which the tests will be carried out will be depend on weather conditions and TC/FAA directive. A detailed preliminary test matrix is shown in Table 3.2.

NOTE: The numbering of the test runs will be done in a sequential order starting with number 1.

A rating system has been developed for fluid and contamination tests, and will be filled out by the onsite experts when applicable. The overall rating will provide insight into the severity of the conditions observed. A test failure (failure to shed the fluid at time of rotation) shall be determined by the on-site experts based on residual contamination.

PRE-TESTING SETUP ACTIVITIES 4.

The activities to be performed for planning and preparation, on the first day of testing, and prior to each testing day thereafter, have been detailed in a list included in Attachment XVI.

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| | Table 4.1: Preliminary | | Festing Objectives for Winter 2012-13 Funnel Testing | |
|-----------|--|----------|---|--------------|
| ltem # | Objective | Priority | Description | # of Days |
| 1 | Dry Wing Baseline Repeatability | 1 | Baseline test at beginning of each day. Ensure repeatability | - |
| 2 | IP Expansion (IP-/SN and IP-/SN-) | 1 | Expand IP Allowance Time Table for IP-/SN and IP-/SN- | 1 |
| 3 | IP Validation (New Temps & Fluids) | 1 | Substantiate current times with new fluids, fluids previously tested but with limited data, and temperatures close to LOUT | 2 |
| 4 | New Ice Pellet Dispenser Calibration | 1 | Evaluate the equivalency of the new ice pellet/snow dispenser systems | 1 |
| 5 | Ice Phobic Coating R&D | 1 | Evaluate the effect of coatings on aerodynamics with and without fluids | 4 |
| 6 | Type III IP Allowance Times | 1 | Support the development of a Type III high speed ice pellet allowance time table | 4 |
| 7 | Type I for Very Low Speed T/O | 1 | Evaluate Type I fluid flow-off performance for low speed rotation less than 80 knots | 2 |
| 8 | Other R&D Activites | 1 | To be selected from item # 8.1 to 8.16 | 1 |
| 8.1 | Evaluation of an APM Sensor | 2 | Testing an airfoil performance monitor (APM) to evaluate potential for use in ground icing operations with and without fluids | - |
| 8.2 | Heavy Snow | 2 | Continue Heavy Snow Research comparing lift losses with Light/Moderate Snow vs. heavy Snow | - |
| 8.3 | Heavy Contamination (Aero vs. Visual Failure) | 2 | Continue work looking at aerodynamic failure vs. HOT defined failure, and effect of surface roughness on lift degredation | - |
| 8.4 | Tunnel Test Section Cooling System Evaluation | 2 | Evaluate effectiveness of new wind tunnel colling system and potential effects on data results | - |
| 8.5 | Effect of Viscosity on Fluid Aerodynamics | 3 | Evaluate effect of viscosity on aero flow-off to better understand year to year differences with same fluid (test high and low visc) | - |
| 8.6 | Fluid + Cont @ LOUT | 3 | Effect of contamination on fluid performance at LOUT with IP, SN, ZF, Frost etc. | - |
| 8.7 | Small Hail | 3 | Develop HOT Guidance for small hail. Requires consult with meteorologist for specific conditions | - |
| 8.8 | Simulate Frost in Wind Tunnel | 3 | Attempt to simulate frost conditions in wind tunnel. | - |
| 8.9 | Flaps/Slats to Support YMX | 3 | Conduct flaps failure research to support UPS/SWA trials, comparative fluid/cont. and possibly sandpaper tests | - |
| 8.10 | Mixed HOT Conditions | 3 | Develop HOT Guidance for mixed conditions i.e. ZR/SN, R/SN, ZD/SN | - |
| 8.11 | Snow on Un-protected Wing | 3 | Continue previous research | - |
| 8.12 | 130-150 Knots IP Testing | 3 | Conduct IP testing at 130-150 knots or validate feasibility MAY NEED TO MODIFY TUNNEL | - |
| 8.13 | Windshield Washer Fluid Testing | 3 | Conduct aero testing to support full testing conducted at Rockliffe Flying Club in Ottawa | - |
| 8.14 | Effect of Fluid Seepage | 3 | Evaluate the effect of fluid seepage on dry wing performance and repeatability | - |
| 8.15 | 2nd Wave of Fluid During Rotation | 3 | Investigate the aero effects of the 2nd wave of fluid created from fluid at the stagnation point which flows over the LE during rotation | - |
| 8.16 | Other | 3 | Any potential suggestions from industry | - |

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| | | | | | Tabl | e 3.1: Pro | oposed Te | est Pla | n | | | | | | |
|-------------------|------------------|-----------------------|----------------|-------------------|-----------------|-----------------------|------------|----------------------|----------------------|----------------------|---------------------|------------------|---------|----------|--|
| Test Plan # | Objective | Objective Priority | Test Condition | Rotation Angle | Ramp (s/kts) | Target OAT (°C) | Fluid | IP Rate (g/dm²/h) | SN Rate (g/dm²/h) | ZR Rate (g/dm²/h) | R Rate (g/dm²/h) | Exposure Time | Coating | Priority | COMMENT |
| P001 | Baseline | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | | - | 1 | to be conducted d before start ot tes |
| P002 | Baseline | 1 | Dry Wing | stall | 100 | any (target <-5°C) | none | | - | | - | | - | 1 | to be conducted d before start of tes |
| P003 | Type I Low Speed | 1 | Fluid Only | 8 | 100 | below -30 | Polar Plus | - | - | - | - | - | - | 1 | |
| P004 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | below -30 | Polar Plus | - | - | - | - | - | - | 1 | |
| P005 | Type I Low Speed | 1 | Fluid Only | 8 | 55 | below -30 | Polar Plus | | - | | - | - | | 1 | |
| P006 | Type I Low Speed | 1 | Fluid Only | 8 | 55+3 sec | below -30 | Polar Plus | - | - | - | - | - | - | 1 | |
| P007 | Type I Low Speed | 1 | Fluid Only | 8 | 100 | -20 to -30 | Polar Plus | - | | | | - | - | 1 | |
| P008 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -20 to -30 | Polar Plus | - | - | - | - | - | - | 1 | |
| P009 | Type I Low Speed | 1 | Fluid Only | 8 | 55 | -20 to -30 | Polar Plus | - | - | - | - | - | - | 1 | |
| P010 | Type I Low Speed | 1 | Fluid Only | 8 | 55+3 sec | -20 to -30 | Polar Plus | - | - | - | - | - | | 1 | |
| P011 | Type I Low Speed | 1 | Fluid Only | 8 | 100 | -20 to -30 | Polar Plus | - | - | - | - | - | - | 2 | |
| P012 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -20 to -30 | Polar Plus | - | - | - | - | - | - | 2 | |
| P013 | Type I Low Speed | 1 | Fluid Only | 8 | 55 | -20 to -30 | Polar Plus | - | - | - | - | - | - | 2 | |
| P014 | Type I Low Speed | 1 | Fluid Only | 8 | 55+3 sec | -20 to -30 | Polar Plus | - | - | | - | - | - | 2 | |
| P015 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -20 to -30 | Polar Plus | - | - | - | - | - | - | 3 | |
| P016 | Type I Low Speed | 1 | Fluid Only | 8 | 100 | -20 to -30 | Dow ADF | - | | | - | - | | 1 | |
| P017 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -20 to -30 | Dow ADF | - | - | - | - | | - | 1 | |
| P018 | Type I Low Speed | 1 | Fluid Only | 8 | 55 | -20 to -30 | Dow ADF | - | - | - | - | - | - | 1 | |
| P019 | Type I Low Speed | 1 | Fluid Only | 8 | 55+3 sec | -20 to -30 | Dow ADF | - | | | - | | - | 1 | |
| P020 | Type I Low Speed | 1 | Fluid Only | 8 | 100 | -10 to -20 | Polar Plus | - | - | - | - | - | - | 1 | |
| P021 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -10 to -20 | Polar Plus | - | - | | - | | - | 1 | |
| P022 | Type I Low Speed | 1 | Fluid Only | 8 | 55 | -10 to -20 | Polar Plus | - | - | - | - | - | - | 1 | |
| P023 | Type I Low Speed | 1 | Fluid Only | 8 | 55+3 sec | -10 to -20 | Polar Plus | - | - | - | - | - | - | 1 | |
| P024 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -10 to -20 | Polar Plus | - | - | - | - | - | - | 2 | |
| P025 | Type I Low Speed | 1 | Fluid Only | 8 | 100 | -5 to -10 | Polar Plus | - | - | - | - | - | - | 1 | |
| | | | | | | | | | | | | | | | |

| | | | | Tab | ole 3. | .1: Propos | sed Test I | Plan (c | ont.) | | | | | | |
|------|--------------------------|---|------------|-----|-------------|--------------|-------------|---------|-------|----|----|----|---|---|--|
| P026 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -5 to -10 | Polar Plus | - | - | - | - | - | - | 1 | |
| P027 | Type I Low Speed | 1 | Fluid Only | 8 | 60 | -5 to -10 | Polar Plus | - | - | - | - | - | - | 2 | |
| P028 | Type I Low Speed | 1 | Fluid Only | 8 | 55 | -5 to -10 | Polar Plus | - | | - | - | | | 1 | |
| P029 | Type I Low Speed | 1 | Fluid Only | 8 | 55+3 sec | -5 to -10 | Polar Plus | - | | | - | | | 1 | |
| P030 | Type III Allowance Times | 1 | IP- | 8 | 100 | -5 and above | 2031 - Hot | 25 | - | - | - | 10 | | 1 | |
| P031 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -5 and above | 2031 - Hot | 75 | - | - | - | 5 | - | 1 | |
| P032 | Type III Allowance Times | 1 | IP- / ZR- | 8 | 100 | -5 and above | 2031 - Hot | 25 | - | 25 | - | 7 | | 1 | |
| P033 | Type III Allowance Times | 1 | IP-/R | 8 | 100 | -5 and above | 2031 - Hot | 25 | - | - | 75 | 7 | - | 1 | |
| P034 | Type III Allowance Times | 1 | IP- / SN- | 8 | 100 | -5 and above | 2031 - Hot | 25 | 10 | | | 10 | - | 1 | |
| P035 | Type III Allowance Times | 1 | IP- / SN | 8 | 100 | -5 and above | 2031 - Hot | 25 | 25 | - | - | 10 | - | 1 | |
| P036 | Type III Allowance Times | 1 | IP- | 8 | 100 | -5 to -10 | 2031 - Hot | 25 | | - | | 10 | | 1 | |
| P037 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -5 to -10 | 2031 - Hot | 75 | - | - | - | 5 | - | 1 | |
| P038 | Type III Allowance Times | 1 | IP-/ZR- | 8 | 100 | -5 to -10 | 2031 - Hot | 25 | - | 25 | - | 5 | - | 1 | |
| P039 | Type III Allowance Times | 1 | IP-/SN- | 8 | 100 | -5 to -10 | 2031 - Hot | 25 | 10 | - | - | 10 | - | 1 | |
| P040 | Type III Allowance Times | 1 | IP- / SN | 8 | 100 | -5 to -10 | 2031 - Hot | 25 | 25 | - | - | 5 | - | 1 | |
| P041 | Type III Allowance Times | 1 | IP- | 8 | 100 | -10 to -20 | 2031 - Hot | 25 | - | - | - | 10 | - | 1 | |
| P042 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -10 to -20 | 2031 - Hot | 75 | - | - | - | 5 | - | 1 | |
| P043 | Type III Allowance Times | 1 | IP- | 8 | 100 | -20 to -30 | 2031 - Hot | 25 | - | - | - | 10 | - | 1 | |
| P044 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -20 to -30 | 2031 - Hot | 75 | - | - | - | 5 | - | 1 | |
| P045 | Type III Allowance Times | 1 | IP- | 8 | 100 | -5 and above | 2031 - Cold | 25 | - | - | - | 10 | - | 1 | |
| P046 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -5 and above | 2031 - Cold | 75 | - | - | - | 5 | - | 1 | |
| P047 | Type III Allowance Times | 1 | IP-/ZR- | 8 | 100 | -5 and above | 2031 - Cold | 25 | - | 25 | - | 7 | - | 1 | |
| P048 | Type III Allowance Times | 1 | IP- / SN- | 8 | 100 | -5 and above | 2031 - Cold | 25 | 10 | - | - | 10 | - | 1 | |
| P049 | Type III Allowance Times | 1 | IP- / SN | 8 | 100 | -5 and above | 2031 - Cold | 25 | 25 | - | - | 10 | - | 1 | |
| P050 | Type III Allowance Times | 1 | IP- | 8 | 100 | -5 and above | 2031 - Cold | 25 | - | - | - | 10 | - | 1 | |
| P051 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -5 to -10 | 2031 - Cold | 75 | - | - | - | 5 | - | 1 | |
| P052 | Type III Allowance Times | 1 | IP- / ZR- | 8 | 100 | -5 to -10 | 2031 - Cold | 25 | - | 25 | - | 5 | - | 1 | |
| | | | | | | | | | | | | | | | |

| | | | | T - 1 | | 1. D | | | | | | | | | |
|------|---------------------------------------|---|-----------|--------------|--------|------------|------------------------|--------|-------|---|----|----|---|---|----------------------|
| | 1 | | | lat | ble 3. | 1: Propo | sed Test I | lan (c | ont.) | | | | | | |
| P053 | Type III Allowance Times | 1 | IP-/R | 8 | 100 | -5 to -10 | 2031 - Cold | 25 | - | - | 75 | 7 | - | 1 | |
| P054 | Type III Allowance Times | 1 | IP- / SN- | 8 | 100 | -5 to -10 | 2031 - Cold | 25 | 10 | - | - | 10 | - | 1 | |
| P055 | Type III Allowance Times | 1 | IP- / SN | 8 | 100 | -5 to -10 | 2031 - Cold | 25 | 25 | - | - | 5 | - | 1 | |
| P056 | Type III Allowance Times | 1 | IP- | 8 | 100 | -10 to -20 | 2031 - Cold | 25 | - | - | - | 10 | - | 1 | |
| P057 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -10 to -20 | 2031 - Cold | 75 | - | - | - | 5 | - | 1 | |
| P058 | Type III Allowance Times | 1 | IP- | 8 | 100 | -20 to -30 | 2031 - Cold | 25 | - | - | - | 10 | - | 1 | |
| P059 | Type III Allowance Times | 1 | IP Mod | 8 | 100 | -20 to -30 | 2031 - Cold | 75 | - | - | - | 5 | - | 1 | |
| P060 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -10 to -20 | ABC-S Plus | 25 | 10 | - | - | 15 | | 2 | |
| P061 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -10 to -20 | Launch | 25 | 10 | - | | 15 | | 2 | |
| P062 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -10 to -20 | Max-Flight | 25 | 10 | - | - | 15 | | 2 | |
| P063 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -10 to -20 | AD-49 | 25 | 10 | - | - | 15 | | 2 | |
| P064 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -10 to -20 | Polar Guard Advance | 25 | 10 | - | - | 15 | | 2 | |
| P065 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -20 to -30 | EG106 | 25 | 10 | - | - | 15 | | 1 | |
| P066 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -20 to -30 | ABC-S Plus | 25 | 10 | - | - | 15 | | 1 | |
| P067 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -20 to -30 | Launch | 25 | 10 | | - | 15 | | 1 | |
| P068 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -20 to -30 | Max-Flight | 25 | 10 | - | - | 15 | | 1 | |
| P069 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -20 to -30 | AD-49 | 25 | 10 | - | - | 15 | | 1 | |
| P070 | IP Expansion | 1 | IP- / SN- | 8 | 100 | -20 to -30 | Polar Guard Advance | 25 | 10 | | | 15 | | 1 | |
| P071 | IP Expansion | 1 | IP-/SN | 8 | 100 | -5 to -10 | ABC-S Plus | 25 | 10 | - | - | 10 | | 1 | |
| P072 | IP Expansion | 1 | IP- / SN | 8 | 100 | -5 to -10 | Launch | 25 | 10 | | | 10 | | 1 | |
| P073 | IP Expansion | 1 | IP-/SN | 8 | 100 | -5 to -10 | AD-49 | 25 | 10 | - | - | 10 | | 1 | |
| P074 | IP Expansion | 1 | IP-/SN | 8 | 100 | -5 to -10 | Polar Guard Advance | 25 | 10 | - | - | 10 | | 1 | failed in 2012-13 te |
| P075 | IP Validation with New Temps & Fluids | 1 | IP- | 8 | 115 | -20 to -30 | ABC-S Plus | 25 | | | | 50 | - | 1 | run @ LOUT |
| P076 | IP Validation with New Temps & Fluids | 1 | IP- | 8 | 115 | -20 to -30 | EG106 | 25 | - | - | - | 50 | - | 1 | run @ LOUT |
| P077 | IP Validation with New Temps & Fluids | 1 | IP- | 8 | 115 | -20 to -30 | Launch | 25 | | - | - | 50 | - | 1 | run @ LOUT |
| P078 | IP Validation with New Temps & Fluids | 1 | IP- | 8 | 115 | -20 to -30 | Max-Flight | 25 | | - | - | 50 | - | 1 | run @ LOUT |
| P079 | IP Validation with New Temps & Fluids | 1 | IP- | 8 | 115 | -20 to -30 | AD-49 | 25 | - | - | | 50 | - | 1 | run @ LOUT |
| | | | 1 | | | 1 | 1 | | | | 1 | 1 | | 1 | |

| | | | | Tab | ole 3. | 1: Propo | sed Test F | Plan (c | ont.) | | | | | | |
|------|---------------------------------------|---|------------|------------------|--------|-----------------------|------------------------|---------|-------|---|---|----|-----|---|------------------|
| P080 | IP Validation with New Temps & Fluids | 1 | IP- | 8 | 115 | -20 to -30 | Polar Guard Advance | 25 | - | - | - | 50 | - | 1 | run @ LOUT |
| P081 | IP Validation with New Temps & Fluids | 1 | IP Mod | 8 | 115 | -20 to -30 | ABC-S Plus | 75 | | - | | 10 | - | 1 | run @ LOUT |
| P082 | IP Validation with New Temps & Fluids | 1 | IP Mod | 8 | 115 | -20 to -30 | EG106 | 75 | | - | | 10 | - | 1 | run @ LOUT |
| P083 | IP Validation with New Temps & Fluids | 1 | IP Mod | 8 | 115 | -20 to -30 | Launch | 75 | | | | 10 | - | 1 | run @ LOUT |
| P084 | IP Validation with New Temps & Fluids | 1 | IP Mod | 8 | 115 | -20 to -30 | Max-Flight | 75 | - | - | - | 10 | - | 1 | run @ LOUT |
| P085 | IP Validation with New Temps & Fluids | 1 | IP Mod | 8 | 115 | -20 to -30 | AD-49 | 75 | - | - | - | 10 | - | 1 | run @ LOUT |
| P086 | IP Validation with New Temps & Fluids | 1 | IP Mod | 8 | 115 | -20 to -30 | Polar Guard Advance | 75 | - | - | - | 10 | - | 1 | run @ LOUT |
| P087 | IP Validation with New Temps & Fluids | 1 | Fluid Only | 8 | 115 | -20 to -30 | ABC-S Plus | - | - | - | - | - | - | 1 | run @ LOUT |
| P088 | IP Validation with New Temps & Fluids | 1 | Fluid Only | 8 | 115 | -20 to -30 | EG106 | - | - | - | | | - | 1 | run @ LOUT |
| P089 | IP Validation with New Temps & Fluids | 1 | Fluid Only | 8 | 115 | -20 to -30 | Launch | - | - | - | - | - | - | 1 | run @ LOUT |
| P090 | IP Validation with New Temps & Fluids | 1 | Fluid Only | 8 | 115 | -20 to -30 | Max-Flight | - | - | - | - | - | - | 1 | run @ LOUT |
| P091 | IP Validation with New Temps & Fluids | 1 | Fluid Only | 8 | 115 | -20 to -30 | AD-49 | - | - | - | - | - | - | 1 | run @ LOUT |
| P092 | IP Validation with New Temps & Fluids | 1 | Fluid Only | 8 | 115 | -20 to -30 | Polar Guard Advance | - | - | - | - | - | - | 1 | run @ LOUT |
| P093 | New Ice Pellet Dispenser Validation | 1 | IP Mod | 8 | 100 | below -5 | Launch | 75 | - | - | - | 10 | - | 1 | new dispense |
| P094 | New Ice Pellet Dispenser Validation | 1 | IP Mod | 8 | 100 | below -5 | Launch | 75 | - | - | - | 10 | - | 1 | new dispense |
| P095 | New Ice Pellet Dispenser Validation | 1 | IP Mod | 8 | 100 | below -5 | Launch | 75 | - | - | - | 10 | - | 2 | new dispense |
| P096 | New Ice Pellet Dispenser Validation | 1 | IP Mod | 8 | 100 | below -5 | Launch | 75 | - | - | - | 10 | - | 1 | old dispenser |
| P097 | New Ice Pellet Dispenser Validation | 1 | IP Mod | 8 | 100 | below -5 | Launch | 75 | | | | 10 | - | 1 | old dispenser |
| P098 | New Ice Pellet Dispenser Validation | 1 | IP Mod | 8 | 100 | below -5 | Launch | 75 | - | - | - | 10 | - | 2 | old dispense |
| P099 | New Ice Pellet Dispenser Validation | 1 | IP-/SN- | 8 | 100 | below -5 | Polar Guard Advance | 25 | 25 | - | - | 15 | - | 1 | new dispense |
| P100 | New Ice Pellet Dispenser Validation | 1 | IP-/SN- | 8 | 100 | below -5 | Polar Guard Advance | 25 | 25 | - | - | 15 | - | 1 | new dispense |
| P101 | New Ice Pellet Dispenser Validation | 1 | IP-/SN- | 8 | 100 | below -5 | Polar Guard Advance | 25 | 25 | - | - | 15 | - | 1 | old dispense |
| P102 | New Ice Pellet Dispenser Validation | 1 | IP-/SN- | 8 | 100 | below -5 | Polar Guard Advance | 25 | 25 | - | - | 15 | - | 1 | old dispense |
| P103 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B14 | 1 | objective: basel |
| P104 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B14 | 1 | objective: basel |
| P105 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B14 | 2 | objective: basel |
| P106 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | | - | B14 | 1 | objective: basel |
| | | | | | | | | | | | | | | | |

| | | | | Tab | ole 3. | 1: Propos | ed Test | Plan (c | ont.) | | | | | | |
|------|----------------|---|------------|------------------|--------|-----------------------|---------|---------|-------|----|---|----|-----|---|--|
| P107 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | | B14 | 1 | objective: baselin |
| P108 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B14 | 2 | objective: baselin |
| P109 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B14 | 1 | objective: drag ar fuel efficiency * SCENARIO 1: cli or cruise to be simulated, i.e: 0 ° 30 sec |
| P110 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B14 | 2 | objective: drag an fuel efficiency * SCENARIO 2: clii or cruise to be simulated, i.e: +2 ° 15 sec |
| P111 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B14 | 3 | objective: drag ar fuel efficiency * SCENARIO 3: cli or cruise to be simulated, i.e:-2 ° 10 sec |
| P112 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B14 | 1 | objective: effect of coatings on fluid flo off |
| P113 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B14 | 1 | objective: effect of coatings on fluid flo off |
| P114 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | | | - | | - | B14 | 2 | objective: effect of coatings on fluid flo |
| P115 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | - | - | 25 | - | 20 | B14 | 1 | objective: effect of coatings with pred |
| P116 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B14 | 1 | objective: baselin fluid seepage |
| P117 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B14 | 2 | objective: baselin fluid seepage |
| P118 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B15 | 1 | objective: baselin |
| P119 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B15 | 1 | objective: baselin |
| P120 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B15 | 2 | objective: baselin |
| P121 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B15 | 1 | objective: baselin |
| P122 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B15 | 1 | objective: baselin |
| P123 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | | B15 | 2 | objective: baselin |
| P124 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | | | - | B15 | 1 | objective: drag ar fuel efficiency * SCENARIO 1: cli or cruise to be simulated, i.e: 0 ° 30 sec |
| P125 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B15 | 2 | objective: drag an fuel efficiency * SCENARIO 2: cli or cruise to be simulated, i.e: +2 ° 15 sec |

| | | | | Tab | ole 3. | 1: Propos | sed Test | Plan (c | ont.) | | | | | | |
|------|----------------|---|------------|------------------|--------|-----------------------|----------|---------|-------|----|---|----|--------------------|---|---|
| P126 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B15 | 3 | objective: drag am fuel efficiency * SCENARIO 3: clin or cruise to be simulated, i.e2 ° fr 10 sec |
| P127 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B15 | 1 | objective: effect o coatings on fluid flor off |
| P128 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B15 | 1 | objective: effect o coatings on fluid flor off |
| P129 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B15 | 2 | objective: effect o coatings on fluid flo |
| P130 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | | - | 25 | - | 20 | B15 | 1 | objective: effect o coatings with preci |
| P131 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B15 | 1 | objective: baseline fluid seepage |
| P132 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B15 | 2 | objective: baseline fluid seepage |
| P133 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | skin no coating | 1 | objective: baseline |
| P134 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | | - | - | - | skin no coating | 1 | objective: baseline |
| P135 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | skin no coating | 2 | objective: baseline |
| P136 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | skin no coating | 1 | objective: baseline |
| P137 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | | - | - | - | skin no coating | 1 | objective: baseline |
| P138 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | | - | - | - | skin no coating | 2 | objective: baseline |
| P139 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | skin no coating | 1 | objective: drag an fuel efficiency * SCENARIO 1: clin or cruise to be simulated, i.e: 0 ° f 30 sec |
| P140 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | skin no coating | 2 | objective: drag an fuel efficiency * SCENARIO 2: clin or cruise to be simulated, i.e: +2 ° 15 sec |
| P141 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | | - | - | - | skin no coating | 3 | objective: drag an fuel efficiency * SCENARIO 3: clin or cruise to be simulated, i.e:-2 ° 1 10 sec |
| P142 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | | | - | - | skin no coating | 1 | objective: effect of coatings on fluid flo off |
| P143 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | skin no coating | 1 | objective: effect of coatings on fluid flo |
| P144 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | skin no coating | 2 | off objective: effect of coatings on fluid flo off |
| P145 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | - | - | 25 | - | 20 | skin no coating | 1 | off objective: effect o coatings with preci |
| P146 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | skin no coating | 1 | objective: baseline fluid seepage |
| | | · | | | · | | | _ | | | | - | | - | |

| | | | | Tab | ole 3. | 1: Propos | sed Test | Plan (c | ont.) | | | | | | |
|------|----------------|---|------------|------------------|--------|-----------------------|----------|---------|-------|----|---|----|--------------------|---|--|
| P147 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | skin no coating | 2 | objective: baseline fluid seepage |
| P148 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 1 | objective: baselin |
| P149 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 1 | objective: baselin |
| P150 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 2 | objective: baselin |
| P151 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 1 | objective: baselin |
| P152 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 1 | objective: baselin |
| P153 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 2 | objective: baselin |
| P154 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | original wing | 1 | objective: drag an fuel efficiency * SCENARIO 1: cli or cruise to be simulated, i.e: 0 ° 1 30 sec |
| P155 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | original wing | 2 | objective: drag an fuel efficiency * SCENARIO 2: cli or cruise to be simulated, i.e: +2 ° 15 sec |
| P156 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | original wing | 3 | objective: drag ar fuel efficiency * SCENARIO 3: cli or cruise to be simulated, i.e:-2 ° 10 sec |
| P157 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | original wing | 1 | objective: effect of coatings on fluid flo off |
| P158 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | original wing | 1 | objective: effect of coatings on fluid flo off |
| P159 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | original wing | 2 | objective: effect of coatings on fluid flo off |
| P160 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | - | - | 25 | - | 20 | original wing | 1 | objective: effect of coatings with prec |
| P161 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 1 | objective: baselin fluid seepage |
| P162 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | original wing | 2 | objective: baselin fluid seepage |
| P163 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | E1 | 1 | objective: baselin |
| P164 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | E1 | 1 | objective: baselin |
| P165 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | E1 | 2 | objective: baselin |
| P166 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | E1 | 1 | objective: baselin |
| P167 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | E1 | 1 | objective: baselin |
| | | | | | | | | | | | | | | | |

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|------|----------------|---|------------|------------------|-------|-----------------------|----------|---------|-------|----|---|----|----|---|--|
| P168 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | | - | | | E1 | 2 | objective: baselin |
| P169 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | E1 | 1 | objective: drag at fuel efficiency * SCENARIO 1: cl or cruise to be simulated, i.e: 0 ° 30 sec |
| P170 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | E1 | 2 | objective: drag al fuel efficiency * SCENARIO 2: cl or cruise to be simulated, i.e: +2 ° 15 sec |
| P171 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | E1 | 3 | objective: drag au fuel efficiency * SCENARIO 3: cl or cruise to be simulated, i.e:-2 ° 10 sec |
| P172 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | E1 | 1 | objective: effect coatings on fluid fl off |
| P173 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | E1 | 1 | objective: effect coatings on fluid fl |
| P174 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | E1 | 2 | off objective: effect coatings on fluid fl |
| P175 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | | | 25 | | 20 | E1 | 1 | off objective: effect coatings with pre |
| P176 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | E1 | 1 | objective: baselin fluid seepage |
| P177 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | | - | | - | E1 | 2 | objective: baselir fluid seepage |
| P178 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | | - | | - | C3 | 1 | objective: baseli |
| P179 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | C3 | 1 | objective: baseli |
| P180 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | C3 | 2 | objective: baseli |
| P181 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | | - | | - | C3 | 1 | objective: baseli |
| P182 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | C3 | 1 | objective: baseli |
| P183 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | C3 | 2 | objective: baseli |
| P184 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | C3 | 1 | objective: drag a fuel efficiency * SCENARIO 1: cl or cruise to be simulated, i.e: 0 ° 30 sec |
| P185 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | C3 | 2 | objective: drag a fuel efficiency * SCENARIO 2: cl or cruise to be simulated, i.e: +2 ' 15 sec |

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|------|----------------|---|------------|------------------|--------|-----------------------|----------|---------|-------|----|---|----|-----|---|---|
| P186 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | СЗ | 3 | objective: drag an fuel efficiency * SCENARIO 3: cli or cruise to be simulated, i.e2 ° 10 sec |
| P187 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | C3 | 1 | objective: effect of coatings on fluid flo off |
| P188 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | C3 | 1 | objective: effect of coatings on fluid flo off |
| P189 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | C3 | 2 | objective: effect of coatings on fluid flo off |
| P190 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | - | - | 25 | - | 20 | C3 | 1 | objective: effect of coatings with pred |
| P191 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | C3 | 1 | objective: baselin fluid seepage |
| P192 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | C3 | 2 | objective: baselin fluid seepage |
| P193 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B12 | 1 | objective: baselin |
| P194 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B12 | 1 | objective: baselin |
| P195 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B12 | 2 | objective: baselin |
| P196 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | | B12 | 1 | objective: baselin |
| P197 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B12 | 1 | objective: baselin |
| P198 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B12 | 2 | objective: baselin |
| P199 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B12 | 1 | objective: drag an fuel efficiency * SCENARIO 1: cli or cruise to be simulated, i.e: 0 ° 1 30 sec |
| P200 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B12 | 2 | objective: drag an fuel efficiency * SCENARIO 2: clii or cruise to be simulated, i.e: +2 ° 15 sec |
| P201 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | | - | - | - | B12 | 3 | objective: drag an fuel efficiency * SCENARIO 3: clii or cruise to be simulated, i.e:-2 ° 1 10 sec |
| P202 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B12 | 1 | objective: effect of coatings on fluid flo off |
| P203 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B12 | 1 | off objective: effect of coatings on fluid flo off |
| P204 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B12 | 2 | off objective: effect of coatings on fluid flo |
| P205 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | - | - | 25 | - | 20 | B12 | 1 | objective: effect of coatings with prec |
| P206 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B12 | 1 | objective: baselin fluid seepage |
| | | 1 | | 1 | | | | - | | | | | | | |

| | | | | τ | | 1. D | | DI | | | | | | | |
|------|----------------|---|----------------------------|------------------|------|-----------------------|----------|---------|-------|-----|-----|-----|--------------------|---|---|
| | | | T | | 1 | | sed Test | Plan (c | ont.) | | | | 1 | | - March |
| P207 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B12 | 2 | objective: baseline fluid seepage |
| P208 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B13 | 1 | objective: baselin |
| P209 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B13 | 1 | objective: baselin |
| P210 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | - | - | - | - | B13 | 2 | objective: baselin |
| P211 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B13 | 1 | objective: baselin |
| P212 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B13 | 1 | objective: baselin |
| P213 | Ice Phobic R&D | 1 | Dry Wing | 8 pitch pause | 100 | any (target <-5°C) | none | - | - | - | - | - | B13 | 2 | objective: baselin |
| P214 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | | - | | - | B13 | 1 | objective: drag an fuel efficiency * SCENARIO 1: clin or cruise to be simulated, i.e: 0 ° f 30 sec |
| P215 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B13 | 2 | objective: drag an fuel efficiency * SCENARIO 2: cli or cruise to be simulated, i.e: +2 ° 15 sec |
| P216 | Ice Phobic R&D | 1 | Dry Wing | n/a* | n/a* | any (target <-5°C) | none | - | - | - | - | - | B13 | 3 | objective: drag an fuel efficiency * SCENARIO 3: clii or cruise to be simulated, i.e:-2 ° 10 sec |
| P217 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | - | - | - | - | - | B13 | 1 | objective: effect of coatings on fluid flo off |
| P218 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | _ | | - | | - | B13 | 1 | objective: effect of coatings on fluid flo |
| P219 | Ice Phobic R&D | 1 | Fluid Only | 8 | 100 | below -5 | EG106 | | - | - | - | - | B13 | 2 | off objective: effect of coatings on fluid flo |
| P220 | Ice Phobic R&D | 1 | ZR | 8 | 100 | below -5 | none | | | 25 | | 20 | B13 | 1 | off objective: effect of |
| P221 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | any (target <-5°C) | none | - | | - | | | B13 | 1 | coatings with prec objective: baselin |
| P222 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | anv | none | - | - | - | | | B13 | 2 | fluid seepage objective: baselin |
| P223 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | (target <-5°C) any | none | | - | - | | | skin no | 1 | fluid seepage objective: baseline/installatio |
| P224 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | (target <-5°C) any | none | - | - | - | | - | coating skin no | 1 | repeatability objective: baseline/installatio |
| P225 | Ice Phobic R&D | 1 | Dry Wing | 8 | 100 | (target <-5°C) any | none | | | | | | coating skin no | 2 | repeatability objective: baseline/installatio |
| | | | | - | | (target <-5°C) | | | | | | | coating | | repeatability |
| P226 | R&D | 1 | APM Unit | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 1 | |
| P227 | R&D | 1 | S+++ HEAVY | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 1 | + |
| P228 | R&D | 1 | CONTAMINATION EFFECT OF | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 1 | - |
| P229 | R&D | 1 | COOLING | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 1 | |

| | | | Tab | ole 3. | 1: Propo | sed Test F | lan (c | ont.) | | | | | | |
|-----|---|---|---|--|--|--|---|---|---|---|---|---|--|--|
| R&D | 1 | Effect of Viscosity | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | | 2 | |
| | | | | | | | | | | | | | | |
| R&D | 1 | LOUT | IBD | IBD | IBD | IBD | IBD | IBD | IBD | IBD | IBD | - | 2 | |
| R&D | 1 | SMALL HAIL | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 2 | |
| R&D | 1 | FROST | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 2 | |
| R&D | 1 | FLAPS/SLATS | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 2 | |
| R&D | 1 | MIXED CONDITIONS | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | | 2 | |
| R&D | 1 | SNOW NO FLUID | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 2 | |
| R&D | 1 | IP TESTs @ 130- 150 KTS | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 2 | |
| R&D | 1 | WINDSHIELD WASHER FLUID | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 2 | |
| R&D | 1 | FLUID SEEPAGE | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | TBD | - | 2 | |
| | R&D R&D R&D R&D R&D R&D R&D | R&D 1 R&D 1 | RåD 1 FLUID & CONT @ LOUT RåD 1 SMALL HAIL RåD 1 FROST RåD 1 FROST RåD 1 FLAPS/SLATS RåD 1 CONDITIONS RåD 1 SNOW NO FLUID RåD 1 SNOW NO FLUID RåD 1 IP TESTs @ 130- 150 KTS RåD 1 WINSSHELD WASHER FLUID | R&D 1 Effect of Viscosity TBD R&D 1 FLUID & CONT @ LOUT TBD R&D 1 SMALL HAIL TBD R&D 1 SMALL HAIL TBD R&D 1 FROST TBD R&D 1 FROST TBD R&D 1 FLAPS/SLATS TBD R&D 1 CONDITIONS TBD R&D 1 SNOW NO FLUID TBD R&D 1 IP TEST® @130- 150 KTS TBD R&D 1 WINDSHEED TBD R&D 1 WINSHEED TBD | R&D 1 Effect of Viscosity LOUT TBD TBD R&D 1 FLUID & CONT @ LOUT TBD TBD R&D 1 FLUID & CONT @ LOUT TBD TBD R&D 1 SMALL HAIL TBD TBD R&D 1 FROST TBD TBD R&D 1 FROST TBD TBD R&D 1 FLAPS/SLATS TBD TBD R&D 1 CONDITIONS TBD TBD R&D 1 SNOW NO FUID TBD TBD R&D 1 IPTESTS @ 130- 150 KTS TBD TBD R&D 1 WINDSHELD WASHER FLUID TBD TBD | R&D 1 Effect of Viscosity LOUT TBD TBD TBD R&D 1 FLUID & CONT @ LOUT TBD TBD TBD TBD R&D 1 SMALL HAIL TBD TBD TBD TBD R&D 1 SMALL HAIL TBD TBD TBD TBD R&D 1 FROST TBD TBD TBD TBD R&D 1 FLAPS/SLATS TBD TBD TBD TBD R&D 1 SNOW NO FLUID TBD TBD TBD TBD R&D 1 SNOW NO FLUID TBD TBD TBD TBD R&D 1 IPETEST @ 130- 150 KTS TBD TBD TBD TBD R&D 1 WINSHELD TBD TBD TBD TBD R&D 1 WINSHELD TBD TBD TBD TBD | R&D 1 Effect of Viscosity LOUT TBD TBD | R&D 1 Effect of Viscosity TBD TBD | R&D1FLUID & CONT @ LOUTTBD | R&D 1 Effect of Viscosity LOUT TBD TBD | R&D 1 Effect of Viscosity TBD TBD | R&D 1 Effect of Viscosity LOUT TBD TBD | R&D1Effect of ViscosityTBD | R&D1Effect of ViscosityTBD |

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DATA FORMS 5.

The following data forms are required for the January 2014 wind tunnel tests:

- Attachment XVII General Form;
- Attachment XVIII Wing Temperature, Fluid Thickness and Fluid Brix Measurements and Condition of Wing and Plate Form;
- Attachment XIX, XX and XXI Ice Pellet, Snow and Sifted Snow Dispensing Forms;
- Attachment XXII Visual Evaluation Rating Form
- Attachment XXIII Fluid Receipt Form (Generic form used by APS; will be used for this project as appropriate);
- Attachment XXIV Log of Fluid Sample Bottles.

When and how the data forms will be used is described throughout Section 6.

PROCEDURE 6.

The following sections describe the tasks to be performed during each test conducted. It should be noted that some sections (i.e. fluid application and contamination application) will be omitted depending on the objective of the test.

6.1 **Initial Test Conditions Survey**

- · Record ambient conditions of the test (Attachment XVII); and
- Record wing temperature (Attachment XVIII).

6.2 Fluid Application (Pour)

- Hand pour 20L of anti-icing fluid over the test area (fluid can be poured directly out of pales or transferred into smaller 3L jugs);
- Record fluid application times (Attachment XVII);
- Record fluid application quantities (Attachment XVII);
- Let fluid settle for 5 minutes (as the wing section is relatively flat, last winter it required tilting the wing for 1-minute to enable fluid to be uniform);
- Measure fluid thickness at pre-determined locations on the wing (Attachment XVIII);
- Record wing temperature (Attachment XVIII).

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- Measure fluid Brix value (Attachment XVIII); and
- Photograph and videotape the appearance of the fluid on the wing;
- Begin the time-lapse camera to gather photos of the precipitation application phase.

Note: At the request of TC/FAA, a standard aluminum test plate can be positioned on the wing in order to run a simultaneous endurance time test.

6.3 **Application of Contamination**

6.3.1 Ice Pellet/Snow Dispenser Calibration and Set-Up

Calibration work was performed during the winter of 2007-08 on the modified ice pellet/snow dispensers prior to testing with the Falcon 20. The purpose of this calibration work was to attain the dispenser's distribution footprint for both ice pellets and snow. A series of tests were performed in various conditions:

- 1. Ice Pellets, Low Winds (0 to 5 km/h);
- 2. Ice Pellets, Moderate Winds (10 km/h);
- 3. Snow, Low Wind (0 to 5 km/h); and
- 4. Snow, Moderate Wind (10 km/h).

These tests were conducted using 121 collection pans, each measuring 6 x 6 inches, over an area 11 x 11 feet. Pre-measured amounts of ice pellets/snow were dispersed over this area and the amount collected by each pan was recorded. A distribution footprint of the dispenser was attained and efficiency for the dispenser was computed.

6.3.2 Dispensing Ice Pellets/Snow for Wind Tunnel Tests

Using the results from these calibration tests, a decision was made to use two dispensers on each of the leading and trailing edges of wing; each of the four dispensers are moved to four different positions along each edge during the dispensing process. Attachments XIX and XX display the data sheets that will be used during testing in the wind tunnel. These data sheets will provide all the necessary information related to the amount of ice pellets/snow needed, effective rates and dispenser positions. During the winter of 2009-10, snow was also dispensed manually using sieves. This technique was used when higher rates of precipitation were required (for heavy snow) or when winds in the tunnel made dispensing difficult. The efficiency of this technique was

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estimated at 90% and a form to be used for this dispensing process along with dispensing instructions is included in Attachment XXI.

Note: Dispensing forms should be filled out and saved for each run and included and pertinent information shall be included in the general form (Attachment XVII). Any comments regarding dispensing activities should be documented directly on the form.

6.3.3 New Ice Pellets/Snow Dispensing Systems for 2014 Onwards

Yardworks seed spreaders were modified and used for applying ice pellets and snow during wind tunnel and flat plate testing. The spreaders are no longer available as the manufacturer has stopped production. A new replacement seed spreader system, Wolf Garten, was found which is similar (but not identical), and may be a suitable replacement (with necessary modifications). Some calibration work was required to demonstrate an equivalency in the two systems: the historical system versus the new replacement system. TC requested to evaluate the new system while at NRC Cold Chamber in September 2013.

The data collected demonstrates that the new system is very similar to old system. Some small variation is present in distribution within the footprint, but equivalent efficiency on the overall footprint. Based on this it was concluded that for ice pellets, the use of the new system can be made as a direct replacement. For snow, the new system is more efficient, therefore a reduction of 10% shall be used for the snow mass requested. The details of this calibration are described in TC report, TP 15230E, Aircraft Ground Icing General Research Activities During the 2012-13 Winter.

6.4 Prior to Engines-On Wind Tunnel Test

- Measure fluid thickness at the pre-determined locations on the wing (Attachment XVIII);
- Measure fluid Brix value (Attachment XVIII);
- Record wing temperatures (Attachment XVIII);
- Record start time of test (Attachment XVII); and
- Fill out visual evaluation rating form (Attachment XXII).

Note: In order to minimize the measurement time post precipitation, temperature should be measured 5 minutes before the end of precipitation, thickness measured 3 minutes before the end of precipitation, and Brix measured when

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the precipitation ends. Also consideration as been given to reducing the number of measures that are taken for this phase (i.e. locations 2 and 5 only).

6.5 **During Wind Tunnel Test:**

- Take still pictures and video the behavior of the fluid on the wing during the takeoff run, capturing any movement of fluid/contamination;
- Fill out visual evaluation rating form at the time of rotation (Attachment XXII); and
- Record wind tunnel operation start and stop times.

6.6 After the Wind Tunnel Test:

- · Measure fluid thickness at the pre-determined locations on the wing (Attachment XVIII);
- Measure fluid Brix value (Attachment XVIII);
- Record wing temperatures (Attachment XVIII);
- Observe and record the status of the fluid/contamination (Attachment XVIII);
- Fill out visual evaluation rating form (Attachment XXII);
- Obtain lift data (excel file) from NRC; and
- Update APS test log with pertinent information.

6.7 Fluid Sample Collection for Viscosity Testing

Two litres of each fluid to be tested are to be collected on the first day of testing. The fluid receipt form (Attachment XXIII) should be completed indicating quantity of fluid and date received. Any samples extracted for viscosity purposes should be documented in the log of fluid samples data form (Attachment XXIV). A falling ball viscosity test should be performed on site to confirm that fluid viscosity is appropriate before testing.

6.8 At the End of Each Test Session

If required, APS personnel will collect the waste solution. At the end of the testing period, the glycol recovery service provider will be employed to safely dispose of the waste glycol fluid.

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6.9 Camera Setup

It is anticipated that the camera setup will be similar to the setup used during the winter of 2011-12. Modifications may be necessary to account for the different airfoil. The flashes will be positioned on the control-room side of the tunnel, and the cameras will be positioned on the opposite side. The final positioning of the cameras and flashes should be documented to identify any deviation from the previous year's setup.

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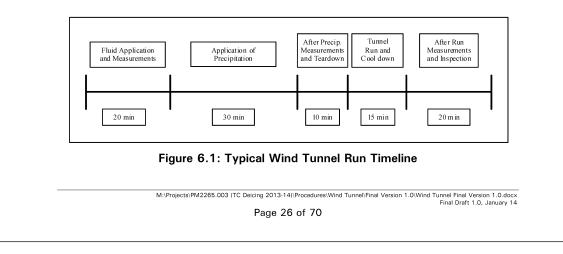
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6.10 Demonstration of a Typical Wind Tunnel Test Sequence

Table 6.1 demonstrates a typical Wind Tunnel test sequence of activities, assuming the test starts at 08:00:00. Figure 6.1 demonstrates a typical wind tunnel run timeline.

| TIME | ТАЅК |
|----------|--|
| 8:30:00 | START OF TEST. ALL EQUIPMENT READY. |
| 8:30:00 | - Record test conditions. |
| 8:35:00 | - Prepare wing for fluid application (clean wing, etc). |
| 8:45:00 | Measure wing temperature. Ensure clean wing for fluid application |
| 8:50:00 | - Pour fluid over test area. |
| 9:00:00 | - Measure Brix, thickness, wing temperature. |
| 9:00:00 | - Photograph test area. |
| 9:05:00 | - Apply contamination over test area. (i.e. 30 min) |
| 0.25.00 | - Measure Brix, thickness, wing temperature. |
| 9:35:00 | - Photograph test area. |
| 9:40:00 | - Clear area and start wind tunnel |
| 9:55:00 | - Wind tunnel stopped |
| | - Measure Brix, thickness, wing temperature. |
| 10:05:00 | - Photograph test area. |
| | - Record test observations. |
| 10:35:00 | END OF TEST |

Table 6.1: Typical Wind Tunnel Test



WIND TUNNEL TESTS TO EXAMINE FLUID REMOVED FROM AIRCRAFT DURING TAKEOFF WITH MIXED ICE PELLET PRECIPITATION CONDITIONS 6.11 Procedures for R&D Activities It is anticipated that testing will be conducted to support several research and development (R&D) activities. The objectives of these lower priority activities are as follows: • Evaluation of an airfoil performance monitor (APM) system; Heavy snow; o Heavy contamination; o Effect of cooling system on testing repeatability; o Effect of fluid viscosity; Fluid and contamination at LOUT; Small hail; Frost simulation in the wind tunnel; Flaps/Slats testing to support YMX tests; Mixed HOT conditions; o Snow on an un-protected wing; • Feasibility of IP testing at higher speed (130-150kts); • Windshield washer used as a Type I deicer; o Effect of fluid seepage on dry wing performance; and Second wave of fluid at rotation. As these full-scale R&D activities have in general not been previously attempted, therefore brief summaries of the anticipated procedures have been prepared to provide guidance at the time of testing. These procedures are attached to this document as Attachments XXV to XXXIX. The procedures are preliminary and may change based on the quality of the results obtained in the wind tunnel. 7. EQUIPMENT Equipment to be employed is shown in Table 7.1.

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| Table 7.1: | Test Equ | uipment Checklist | |
|---|----------|---|------------|
| EQUIPMENT | STATUS | EQUIPMENT | STATU |
| General Support and Testing Equipment | | Camera Equipment | |
| 20L containers x 12 | | AA Batteries x48 | |
| Adherence Probes Kit | | C2032 Batteries x 4 | |
| Barrel Opener (steel) | | Digital still cameras x3 (two suitcases) | |
| Black Shelving Unit (or plastic) | | Flashes and tripods (in APS storage) | |
| Blow Horns x 4 | | GoPro Camera | |
| Electrical tape x 5 | | | |
| Envelopes and labels | | | |
| Exacto Knives x 2 | | Ice Pellets Fabrication Equipment | |
| Extension cords (power bars x6 + reels x4) | | Blenders x 12 in good condition | |
| Falling Ball Viscometer | | Folding tables (2 large, 1small) | |
| Fluid pouring jugs x 60 | | Ice bags | |
| Fluids (ORDER and SHIP to Ottawa) | | Ice bags storage freezer x 3 | |
| Funnels(1big+1small) | | Ice pellets sieves (base, 1.4 mm, 4 mm) | 1set in YC |
| Gloves - black and yellow | | Ice pellets Styrofoam containers x20 | |
| Gloves - cotton (1box) | | Measuring cups (1L and smaller ones for dispensing) | |
| Gloves - latex (2 boxes) | | NCAR Scale x1 | |
| Grid Section +Location docs | | Refrigerated Truck | |
| Hard water chemicals x 3 premixes | | Rubber Mats xall | |
| Horse and tap for fluid barrel x all | | Wooden Spoons | |
| Hot Plate x 3 and Large Pots with rubber handles for Type III | | | |
| Ice pellet box supports for railing x4 | | Freezing Rain Equipment | |
| Ice Pellet control wires and boxes (all for new and old) | | APSPC equipped with rate station software | |
| Ice pellets dispersers x 12 (6 new and 6 old) | | NRC Freezing rain sprayer (NRC will provide) | |
| Inclino meter (yellow level) x 2 | | Rubber suction cup feet for wooden boards | |
| lsopropyl x 24 | | White plastic rate pans (1to 8 x 2) | |
| Large and small tape measure | | Wooden boards for rate pans (x8) | |
| Large Sharpies for Grid Section | | | |
| Long Ruler for marking wing x 2 | | | |
| Marker for waste x 2 | | Office Equipment | |
| Paper to wel x 48 | | Accordian Folder | |
| Protective clothing (all) and personel clothing | | APS Laptops x 6 | |
| Protective clothing (all) and personel clothing | | Calculators x 3 | |
| Sample bottles for viscosity measurement x 8 | | Clip boards x8 | |
| Sartorius Weigh Scale x 1 | | Dry eraser markers | |
| Scrapers x 5 | | Envelopes (9x12) x box | |
| Shop Vac | | Hard drive with all TC Deicing Projects | |
| Speed tape x 1small | | Hard Drive x 2 | _ |
| Squeegees (5 small +3 large floor) | | Mouse for Rate Station and keypad | |
| Stands for ice pellets dispensing devices x 6 | | Pencils +wing markers for sample locations | |
| Stop Watches x 4 | | Projector for laptop | |
| Temperature probes: immersion x 3 | | Scissors | |
| Temperature probes: surface x 3 | | Small 90° aluminum ruler for wing | |
| Temperature readers x2 +spare batteries | | Test Procedures x 8, data forms, printer paper | |
| Test Plate x 1 | | YOWemployee contracts | |
| Thermometer for Reefer Truck | | | _ |
| Thickness Gauges (5 small, 5 big) | | | |
| Vise grip (large) +rubber opener for containers | | | _ |
| Walkie Talkies x 12 | | | _ |
| Water (2 x 18L) for hard water | | | |
| Watmans Paper and conversion charts | | | _ |
| | | | |

FLUIDS 8.

Mid-viscosity samples of ethylene glycol and propylene glycol IV fluid will be used in the wind tunnel tests. Although the number of tests conducted will be determined based on the results obtained, the fluid quantities available are shown in Table 8.1 (quantities to be confirmed once fluid is received). Fluid application will be performed by pouring the fluid (rather than spraying) to reduce any shearing to the fluid.

| FLUID | QUANTITY ORDERED | QUANTITY ALREADY IN STOCK | COMBINED TOTAL OF FLUID AVAILABLE | TOTAL QUANTITY RQ'D |
|------------------------------|---------------------|---------------------------------|--|---------------------------|
| Kilfrost ABC-S Plus | 400 | 250 | 650 | 120 |
| Dow FlightGuard AD-49 | 0 | 440 | 440 | 120 |
| Dow EG106 | 0 | 600 | 600 | 560 |
| Clariant MP III 2031 ECO | 200 | 150 | 350 | 300 |
| Clariant MP IV Launch | 0 | 200 | 200 | 240 |
| Clariant Max-Flight | 0 | 160 | 160 | 100 |
| Cryotech Polar Guard Advance | 400 | 120 | 520 | 200 |
| Cryotech Polar Plus | 240 | 0 | 240 | 230 |
| Dow Type I ADF | 60 | 0 | 60 | 40 |

Table 8.1: Fluid Available for Wind Tunnel Tests

3600 L Ordered For 2009-10 Testing (18 Days)

3200 L Ordered For 2010-11 Testing (15 Days) 1800 L Ordered For 2011-12 Testing (7 of 15 days will be fluid testing)

4200 L Ordered for 2012-13 Testing (15 Days)

9. PERSONNEL

Four APS staff members are required for the tests at the NRC wind tunnel. Four additional persons (with one back-up) will be required from Ottawa for making and dispensing the ice pellets and snow. One additional person from

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Ottawa will be required to photograph the testing. Table 9.1 demonstrates the personnel required and their associated tasks.

Fluid and ice pellets applications will be performed by APS/YOW personnel at the NRC wind tunnel. NRC personnel will operate the NRC wind tunnel and operate the freezing rain/drizzle sprayer (if requested).

| Wind Tunnel 11-12- Tentative | | | | | | |
|------------------------------|--|--|--|--|--|--|
| Person | Responsibility | | | | | |
| John | Overall Co-ordinator | | | | | |
| Marco | Co-ordinator / General | | | | | |
| Victoria | Forms & Data Collection Manager / IP Manager / YOW Pers. Manager / Camera Documentation | | | | | |
| Dave | Data Collection / IP Support / Fluid Application / Fluid Manager | | | | | |
| YOW Personnel | | | | | | |
| Ben/Jesse | Photography | | | | | |
| James | Fluids / IP / Dispensing / General Support | | | | | |
| YOW 1 | Fluids / IP / Dispensing | | | | | |
| YOW 2 | Fluids / IP / Dispensing | | | | | |
| YOW 3 | Fluids / IP / Dispensing | | | | | |
| YOW 4 | Back-up | | | | | |

| Table 9.1: Personnel | List |
|----------------------|------|
|----------------------|------|

NRC Institute of Aerospace Research Contacts

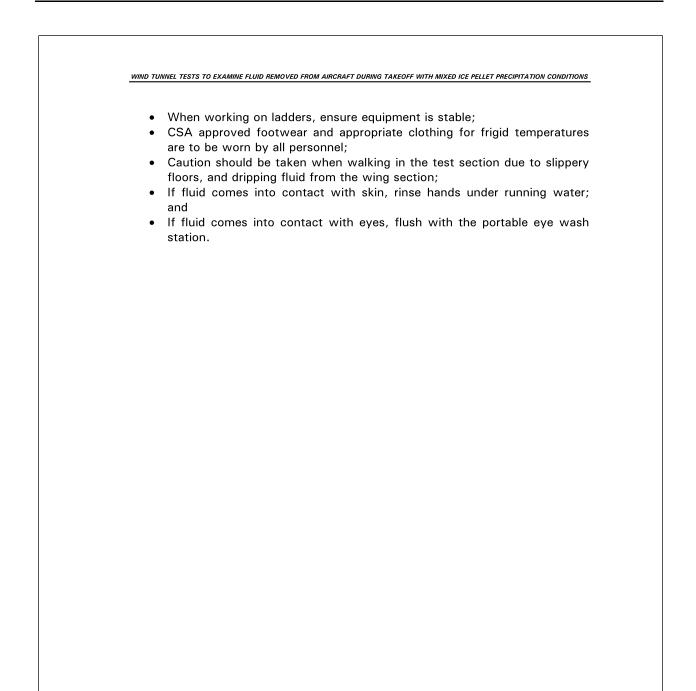
- Lucio Del Ciotto: (613) 913-9720
- Catherine Clark: (613) 998-6932

10. SAFETY

- A safety briefing will be done on the first day of testing;
- · Personnel should be familiar with NRC emergency procedures i.e. DO NOT CALL 9-1-1, instead call the NRC Emergency Center as they will contact and direct the necessary services;
- All personnel must be familiar with the Material Safety Data Sheets (MSDS) for fluids;
- · Prior to operating the wind tunnel, loose objects should be removed from the vicinity;
- When wind tunnel is operating, ensure that ear plugs are worn if necessary and personnel keep safe distances;

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ATTACHMENT I – Procedure: Dry Wing Performance

Background

A significant amount of work has been done in conjunction with NASA and NRC in order to calibrate and characterize the wind tunnel and airfoil model during the last two winter seasons. This work has further increased the confidence in the data produced, however ongoing verification is necessary in order to identify potential changes in the system performance.

Objective

Verify that clean model aerodynamic data agree with the data acquired in previous years with the same model. Given the various issues with repeatability and angle of attack offsets in the past, this is an important step prior to fluids testing.

Methodology

- Ensure the wing is clean and dry;
- Conduct a dry wing test using the regular take-off profile;
- · Conduct a dry wing test using a take-off profile with rotation to stall;
- Compare lift performance to historical data; and
- Address potential discrepancies accordingly. •

Test Plan

This testing should be conducted at the start of each testing day.

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ATTACHMENT II - Procedure: Allowance Times in Light Ice Pellets Mixed with Light or Moderate Snow Conditions

Background

Historical winter weather data has indicated that a significant portion of "light ice pellets mixed with light snow" precipitation occurs below -10°C and "light ice pellets mixed with moderate snow" precipitation occurs below -5 to -10°C where no allowance times currently exist. Some additional data has been collected in 2012-13 which supports a potential for guidance in these conditions, however testing is still required in order to substantiate any proposed changes to the allowance times.

Objective

To conduct testing in conditions of "light ice pellets mixed with light snow" below -10°C and "light ice pellets mixed with moderate snow" below -5 to -10°C to support potential changes to the allowance times table.

Methodology

- Analyze existing data;
- Identify data gaps (fluids, temperatures, etc);
- Conduct testing with appropriate conditions to address data gaps;
- Adjust testing plan accordingly based on aerodynamic data collected.

Test Plan

One day of testing is planned, however testing could be expanded to 3 days.

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ATTACHMENT III - Procedure: Ice Pellet Allowance Time Substantiation with New Fluids, Fluids Previously Tested with Limited Data, and **Temperatures Close to the LOUT**

Background

Previous testing has shown that typically lift losses will significantly increase at the lower temperatures. Limited data is available at (or very near) the fluid Lowest Operational Use Temperature (LOUT). Additional testing is recommended to obtain data close to the fluid LOUT to determine the aerodynamic effects of ice pellet contamination at these colder temperatures.

Objective

To determine the aerodynamic effects of ice pellet contamination close to the fluid LOUT.

Methodology

- Analyze existing data;
- Identify data gaps (fluids, temperatures, etc);
- ٠ Conduct testing close to the fluid LOUT (-20 to -30°C) with appropriate conditions to address data gaps;
- Adjust testing plan accordingly based on aerodynamic data collected.

Test Plan

Two days of testing are planned, however this testing is temperature critical and requires very low temperatures below -20°C.

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ATTACHMENT IV – Procedure: Equivalency of New IP/SN Dispenser Systems

Background

In the winter of 2012-13, seed spreaders historically modified and used for applying ice pellets during wind tunnel and flat plate testing, were no longer available as the manufacturer has stopped production of the model. A new replacement seed spreader system was found which is similar (but not identical). Some calibration work was required to demonstrate an equivalency in the two systems: testing was conducted to verify the distribution of the historical system versus the new replacement system. The data collected demonstrates that the new system is very similar to old system with some small variations. It is recommended comparative wind tunnel testing be conducted to validate the equivalency of the systems.

Objective

To evaluate the equivalency of the new and old generation dispenser systems through comparative wind tunnel testing.

Methodology

- Conduct 2-3 tests with the same fluid in an existing ice pellet only condition with the old dispenser systems;
- Conduct the same 2-3 tests with the new dispenser system;
- Compare the results and address discrepancies accordingly; and
- Repeat for snow conditions (consider doing 1-2 tests for each dispenser instead).

Test Plan

One day of testing is anticipated.

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ATTACHMENT V – Procedure: Effect of Ice Phobic Coating on Aerodynamics With or Without Fluids

Background

In recent years, there has been significant industry interest in the use of coatings to protect aircraft critical surfaces. These coatings can sometimes designed and marketed as ice phobic coatings, but the behavior and performance of these coatings during ground icing operations has yet to be fully investigated Previous flat plate and wind tunnel work has been conducted since 2009-10 and has helped identify both strengths and weaknesses associated with these technologies. Additional aerodynamic testing was recommended to further develop the evaluation methodology and to investigate new product formulations.

Objective

To investigate the aerodynamic performance of ice phobic coatings with and without de/anti-icing fluids.

Methodology

Testing will be conducted using wing skins specifically manufactured to fit onto the existing thin high performance wing section and be secured by bolts. To cover the entire test wing, two individual wing skin halves are required.

Testing will consist of comparative test sets done with different sets of wing skins. The test set will consist of the following:

- Dry wing tests to 8degrees and to stall to understand effects of coatings and to evaluate the repeatability of the tests;
- Simulated climb-out or cruise runs to evaluate drag and fuel efficiency;
- Fluid only testing with a known fluid;
- Freezing rain with no fluid test to evaluate how contamination forms on the surface and the aerodynamic effects (beads of ice vs. smooth ice);
- Repeat dry wing tests to investigate fluid seepage issues associated with the wing skins and effect on repeatability;
- Un-install and re-install a wing skin to evaluate the repeatability of the installation process; and
- Compare the results with the coated wing skins to the un-coated wing skins. An additional comparison to the original wing is also useful.

Test Plan

Four days of testing are planned.

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ATTACHMENT VI – Procedure: Development of a Type III Ice Pellet Allowance Time Table

Background

Several Canadian regional air operators (Porter & Skyregional) operating out of the Toronto Island airport, use Type III fluid for deicing and anti-icing of their turbo-prop aircraft. These operators were driven to use Type III fluids instead of Type IV fluids, due to aircraft performance penalties when using Type IV fluids. As this airport (and several other Canadian airports) is subject to ice pellet conditions, Porter has requested guidance from TC on the use of Type III fluids in ice pellet conditions. It is likely that other air operators will be requesting similar guidance in the near future, since both Skyregional and WestJet Encore also operate Dash 8-400 aircraft. Additional operational research is required by TC prior to providing operational guidance in this area due to the limited knowledge in using Type III fluids during ice pellet events.

Objective

To develop preliminary ice pellet allowance times for use with Type III fluids.

Methodology

- Conduct a thorough review of Type III data collected in previous years of ice pellet testing to determine information availability and requirements;
- Identify data requirements (fluids, temperatures, etc);
- Conduct testing with appropriate conditions to address data requirements. Both hot and cold fluid application data should be collected; and
- Adjust testing plan accordingly based on aerodynamic data collected to support the development of a Type III allowance time table.

Test Plan

Four days of testing are anticipated.

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ATTACHMENT VII – Procedure: Evaluation of Type I Fluid Flow-off for Low Speed Rotation Less than 80 Knots

Background

The lowest operational use temperature (LOUT) for a fluid is determined based on the higher of the fluid freeze point plus a buffer, or the lowest temperature which passes the aerodynamic test (AS5900) for either the low speed or high speed ramp. Currently the high speed ramp is representative of aircraft rotating at 100 knots or higher, whereas the low speed ramp is representative of aircraft rotating between 67 knots and 100 knots.

There currently does not exist any fluid qualification for aircraft rotating below 67 knots, however several operators have aircraft that rotate below 67 knots that encounter ground icing conditions during winter months. Aerodynamic testing in the NRC wind tunnel, and possibly according to AS5900, can provide insight into alternatives for operating in such conditions; i.e. limit LOUT for lower rotation speeds, use diluted fluid, delay rotation when at Vr, increase the rotation speed etc. These operators have requested that TC provide operational guidance when using Type I fluids on these aircraft. Additional operational research is required by TC prior to providing operational guidance in this area.

Objective

To evaluate the aerodynamic impact of using Type I fluid on aircraft with rotation speeds below 67 knots and resulting effect on the LOUT.

Methodology

- Comparative test sets should be done at all temperatures below -5°C, but specifically data at or near the Polar Plus LOUT is especially useful;
- Conduct a high speed (100kts) test with Polar Plus Type I fluid to identify acceptable lift losses;
- Conduct comparative test runs with the same fluid at 60 kts, 55kts, and at 55kts with a 3 second delayed rotation to determine likely increases in lift losses:
- When testing close to the Polar Plus LOUT, conduct an additional set of test with a Type I EG fluid with a lower LOUT (i.e. Dow ADF).
- Analyze results and modify test plan accordingly.

Test Plan

Two days of testing are anticipated.

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| Type I Fluid / Vater Mixture must be selected so that the freezing point of the mixture is at least 10°C (18°F) below outside air temperature. Ensure that the lowest operational use temperature (LOUT) is respected. Use light freezing rain holdover times in conditions of very light or light snow mixed with light rain. Use light recent grain holdover times in conditions of very light or light snow mixed with light rain. Use light recent grain holdover times in conditions of very light or light snow mixed with light rain. Use light recent grain holdover times with of this condition for OC (32°F) and below. No holdover time guidelines exist for this condition for OC (32°F) and below. Heavy snow, ice pellets, moderate and heavy freezing rain, and hail. CAUTIONS The only acceptable decision-making criterion, for takeoff without a pre-takeoff contamination inspection, is the shorter time within the applicable ho time table cell. The time of protection will be shortened in heavy weather conditions, heavy precipitation rates, or high moisture content. High wind velocity or jet blast may reduce holdover time. Holdover time may be reduced when aircraft skin temperature is lower than outside air temperature. | Transport | Canada H | oldover Tir | ne Guideli | ines | | | | Winter | 2013-2 |
|---|--|--|---|---|---|---|--|-------------------------------|----------------------|--------------------|
| This table applies to aircraft with critical surfaces constructed predominantly or entirely of aluminum materials that have demonstrated satisfactory use of these holdover times. THE RESPONSIBILITY FOR THE APPLICATION OF THESE DATA REMAINS WITH THE USER Outside Air Temperature ² Approximate Holdover Times Under Various Weather Conditions (minutes) Degrees Feezing Fog Or Tee APPLICATION OF THESE DATA REMAINS WITH THE USER Degrees Freezing Fog Or Tee Crystals Freezing For Yery Light ² Light Freezing Rain on Cold Soaked Wing ⁶ Outside Air Temperature ² Count of the Crystals Freezing Fog Tee Crystals The result of the Crystals Freezing Fog Tee Crystals Count of the Crystals They Light ² Hight Freezing Rain on Cold Soaked Wing ⁶ Other ⁴ - 3 and 27 and 11 - 17 18 11 - 18 6 - 11 9 - 13 4 - 6 2 - 5 Below -3 below 27 8 - 13 14 8 - 14 5 - 8 5 - 9 4 - 6 CAUTION: No holdover Notes Notes 1 CAUTION: No holdover t | | | | | | | | | 1 | |
| Temperature ² (minutes) Degrees Celsius Degrees Fahrenheit Freezing or toe Crystals Snow, Snow Grains or Snow Pellets Very Light ² Freezing Light Moderate Light Freezing Drizzle ⁴ Rain on Cold Soaked Wing ⁶ Other ⁶ -3 and above 27 and above 11 – 17 18 11 – 18 6 – 11 9 – 13 4 – 6 2 – 5 below -3 to -6 below 27 to -6 8 – 13 14 8 – 14 5 – 8 5 – 9 4 – 6 CAUTION: No holdover time guidelines exist below -6 to -10 below 21 to -10 6 – 10 11 6 – 11 4 – 6 4 – 7 2 – 5 CAUTION: No holdover time guidelines exist NOTES 1 Type I Fluid / Water Mixture must be selected so that the freezing point of the mixture is at least 10°C (18°F) below outside air temperature. 2 2 2 Ensure that the lowest operational use temperature (VOTT) is respected. 3 3 3 4 – 6 4 – 7 2 – 5 4 6 3 Use light freezing rain holdover times in conditions of very light or light snow mixed with light rain. 4 3 3 4 6 6 6 6 6 6 6 6 | | SAETT | This table a aluminun | applies to aircrafi n materials that h | t with critical sur have demonstrat | faces constructed ted satisfactory u | d predominantly se of these holde | or entirely of over times. | ER 2013-2014 | |
| Degrees Degrees Fahrenheit Too of a solution of a soluti solution of a solution a solution of a solution a sol | | | | Ap | proximate Hold | | | ather Conditior | IS | |
| Image: Constraint of the constr | | | or | | 1 | now Pellets | | Freezing | | Other ⁶ |
| above <th< td=""><td>-3 and</td><td>27 and</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<> | -3 and | 27 and | | | | | | | | |
| Ite-0 Ite 21 CAUTION: No holdover time guidelines below -6 below 21 6 - 10 11 6 - 11 4 - 6 4 - 7 2 - 5 CAUTION: No holdover time guidelines below -10 below 14 5 - 9 7 4 - 7 2 - 4 Caution OPTES Type I Fluid / Water Mixture must be selected so that the freezing point of the mixture is at least 10°C (18°F) below outside air temperature. Ensure that the lowest operational use temperature (LQUP) is respected. Use light freezing rain holdover times in conditions of Very light or light snow mixed with light rain. Use light freezing rain holdover times in conditions of 0°C (32°F) and below. No holdover time guidelines exist for this condition for 0°C (32°F) and below. Heavy snow, ice pellets, moderate and heavy freezing rain, and hail. CAUTIONS The only acceptable decision-making criterion, for takeoff without a pre-takeoff contamination inspection, is the shorter time within the applicable head time of protection will be shortened in heavy weather conditions, heavy precipitation rates, or high moisture content. High wind velocity or jet blast may reduce holdover time. Holdover time any be reduced when aircraft skin temperature is lower than outside air temperature. | below -3 | below 27 | | | | | | | 2.0 | |
| below 10 below 14 5 - 9 7 4 - 7 2 - 4 exist | below -6 | below 21 | 6-10 | 11 | 6-11 | 4-6 | 4 - 7 | 2-5 | No holdo | ver |
| Type I Fluid / Water Mixture must be selected so that the freezing point of the mixture is at least 10°C (18°F) below outside air temperature. Ensure that the lowest operational use temperature (LOUT) is respected. Use light freezing rain holdover times in conditions of very light or light snow mixed with light rain. Use light reezing rain holdover times in conditions of very light or light snow mixed with light rain. Use light reezing rain holdover times in conditions of very light or light snow mixed with light reach No holdover time guidelines exist for this condition for O°C (32°F) and below. Heavy snow, ice pellets, moderate and heavy freezing rain, and hail. CAUTIONS The only acceptable decision-making criterion, for takeoff without a pre-takeoff contamination inspection, is the shorter time within the applicable here. The time of protection will be shortened in heavy weather conditions, heavy precipitation rates, or high moisture content. High wind velocity or jet blast may reduce holdover time. Holdover time may be reduced when an aircraft skin temperature is lower than outside air temperature. | - | | 5 – 9 | 7 | 4 - 7 | 2-4 | | | | |
| | Ensure that ti Use light free Use light free No holdover Heavy snow, CAUTIONS The only acc time table or The time of j High wind vi Holdover tim | the lowest opera azing rain holdov zing rain holdov time guidelines i ce pellets, moc ceptable decisi ell. protection will elocity or jet bl ne may be redu | tional use tempera ere times in conditii er times if positive exist for this conditi lerate and heavy fi on-making criteri be shortened in h ast may reduce h ced when aircraft | ture (LOUT) is ru ons of very light i identification of tion for 0°C (32°F reezing rain, and on, for takeoff v neavy weather c oldover time. t skin temperatu | espected. or light snow mb freezing drizzle F) and below. I hail. without a pre-ta conditions, heav | ked with light rain is not possible. Akeoff contamination wy precipitation | n. ation inspectior rates, or high m | n, is the shorte | r time within the ap | plicable h |

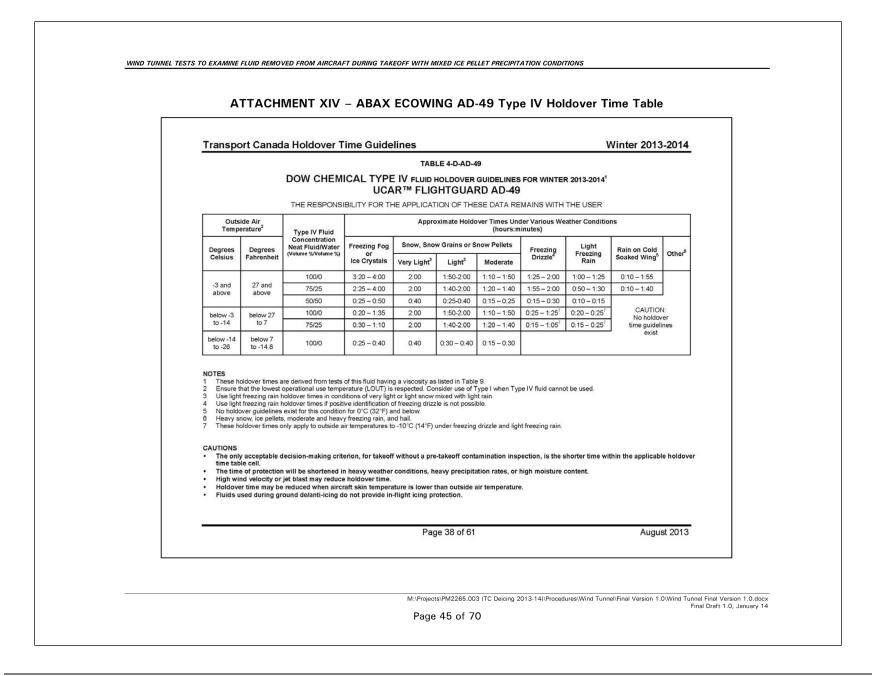
| | | ATTACHN | IENT IX - | - Generi | с Туре | III Holdo | over Tin | ne Tab | le | |
|---|--|---|---|---|---|---|---|--------------------|--------------------------|--------------------|
| Transpo | ort Canad | la Holdover T | ime Guide | lines | | | | | Winter 201 | 3-201 |
| | | | | | ABLE 3 | | | | | |
| | | | TYPE III FLU | | | | | | | |
| | 1960 - 2461. | THE RESPONS | IBILITY FOR TH | | | | | | | |
| | ide Air erature ¹ | | | Appro | kimate Holdov | er Times Unde (minute) | | ather Condit | ions | |
| Degrees | Degrees Fahrenhe | Type III Fluid Concentration Neat Fluid/Water (Volume %/Volume %) | Freezing Fog | Snow, Sno | ow Grains or S | now Pellets | Freezing | Light Freezing | Rain on Cold | Other ⁵ |
| Celsius | it | , | Ice Crystals | Very Light ² | Light ² | Moderate | Drizzle ³ | Rain | Soaked Wing ⁴ | |
| | | 100/0 | 20 – 40 | 35 | 20 – 35 | 10 - 20 | 10 – 20 | 8 – 10 | 6 – 20 | |
| -3 and above | 27 and above | 75/25 | 15 – 30 | 25 | 15 – 25 | 8 – 15 | 8 – 15 | 6 – 10 | 2-10 | |
| | | 50/50 | 10-20 | 15 | 8 – 15 | 4 - 8 | 5-9 | 4 - 6 | CALIFIC . | |
| below -3 to -10 | below 27 to 14 | 100/0 | 20 - 40 | 30 | 15 - 30 | 9-15 | 10-20 | 8 - 10 | CAUTION No holdov | er |
| below -10 | below 14 | 75/25 | 15 - 30 ⁶ 20 - 40 | 25 ⁶ 30 | 10 - 25 ⁶ 15 - 30 | 7 - 10 ⁶ 8 - 15 | 9 – 12 ⁶ | 6 - 9 ⁶ | time guidel exist | |
| Use light No holdd Heavy s For aircr outside : manufac CAUTIONS The only time tab The time High wii Holdove | t freezing rain wer guidelines now, ice pellet aft with a take air temperature turer. y acceptable le cell. e of protectio nd velocity or r time may b | holdover times in com holdover times if posit exist for this conditions s, moderate and heav -off profile conforming es from below -3°C to decision-making critt n will be shortened i jet blast may reduce round de/anti-icing of | ive identification of n for 0°C (32°F) ai y freezing rain, an to the low speed o -9°C (below 27°F) errion, for takeoff n heavy weather e holdover time. raft skin tempera | of freezing drizz nd below. d hail. aerodynamic te to 15.8°F). If t without a pre conditions, he ture is lower t | le is not possit uncertain whet -takeoff conta eavy precipita han outside a | le. fer to Section 8 ner the aircraft mination inspo tion rates, or h | performance o ection, is the s igh moisture (| onforms to th | is criterion, consult | t the aircr |
| | | | | Pag | e 27 of 61 | | | | Aug | ust 201 |

| riansport o | Canada | a Holdover | Time Guid | elines | | | | | Winter 201 | 3-201 |
|--|---|--|---|---|--|---|---|------------------------|--------------------------|-----------|
| | | DOW CHEM | | | | | | ER 2013-2014 | ľ | |
| Outside Air | | THE RESPONS | SIBILITY FOR T | | | over Times Ur | der Various W | H THE USER | | |
| Temperature Degrees Degr | rees | Type IV Fluid Concentration Neat Fluid/Water (Volume %/Volume | Freezing Fog | Snow, Sno | w Grains or S | | ninutes) Freezing | Light Freezing | Rain on Cold | Other |
| Celsius Fahre | enheit | %) | Ice Crystals | Very Light ³ | Light ³ | Moderate | Drizzle ⁴ | Rain | Soaked Wing ⁶ | Other |
| -3 and 27 a | and | 100/0 | 2:05 - 3:10 | 2:00 | 1:20 - 2:00 | 0:40 - 1:20 | 1:10 - 2:00 | 0:50 - 1:15 | 0:20 - 2:00 | |
| | iove | 75/25 50/50 | | | | | | | - | |
| below -3 below | ow 27 | 100/0 | 1:50 - 3:20 | 2:00 | 1:05 - 2:00 | 0:30 - 1:05 | 0:55 - 1:507 | 0:45 - 1:107 | CAUTIC No holdo | |
| | o7 | 75/25 | | 10000 | | | | | time guide | lines |
| | ow 7 16.6 | 100/0 | 0:30 - 1:05 | 0:40 | 0:30 - 0:40 | 0:15 - 0:30 | | | exist | |
| Ensure that the Use light freezi Use light freezi Use light freezi No holdover gu Heavy snow, ic These holdover The only accetime table cell The time of pr High wind vei Holdover time | e lowest o ing rain he uidelines o ce pellets, er times or eptable de Il. rotection locity or j e may be | re derived from test operational use tem oldover times in cor oldover times in cor oldover times in poor exist for this conditive moderate and hea existion the source of the ecision-making cri will be shortened te blast may reduced reduced when airs pund de/anti-icing | perature (LOUT) i nditions of very lig itive identification on for 0°C (32°F) vy freezing rain, a air temperatures iterion, for takeo in heavy weathe ce holdover time craft skin tempei | is respected. C tht or light snow of freezing dri and below. and hail. to -10°C (14°F off without a p er conditions, b. | onsider use of v mixed with lig zzle is not poss) under freezin re-takeoff con heavy precipi r than outside | Type I when T Int rain. jible. g drizzle and li tamination in: tation rates, o | ght freezing rain spection, is the r high moistur | n. e shorter time ' | within the applica | able hold |
| | | | | Pa | age 36 of 6' | | | | Aug | ust 201 |

| Transpo | ort Cana | da Holdover [·] | Time Guid | elines | | | | | Winter 201 | 3-201 |
|--|---|---|---|---|---|--|--|---|--|----------|
| | | | | TAB | LE 4-K-ABC | -S+ | | | | |
| | | KILFRO | ST TYPE IN | | DOVER GU | | OR WINTER 2 | 013-2014 ¹ | | |
| | | THE RESPONS | SIBILITY FOR T | | | | EMAINS WIT | H THE USER | | |
| | ide Air erature ² | Turne Dif Florid | | Appr | oximate Holdo | ver Times Un (hours:n | | eather Conditio | ons | |
| | | Type IV Fluid Concentration Neat Fluid/Water | Freezing Fog | Snow, Sno | w Grains or S | | | Light | Dain an Calif | |
| Degrees Celsius | Degrees Fahrenheit | (Volume %/Volume %) | or Ice Crystals | Very Light ³ | Light ³ | Moderate | Freezing Drizzle ⁴ | Freezing Rain | Rain on Cold Soaked Wing ⁶ | Other |
| 2 and | 27 and | 100/0 | 2:10 - 4:00 | 2:00 | 2:00 - 2:00 | 1:15 - 2:00 | 1:50 - 2:00 | 1:05 - 2:00 | 0:25 - 2:00 | |
| -3 and above | 27 and above | 75/25 | 1:25 - 2:40 | 2:00 | 1:15 - 2:00 | 0:45 - 1:15 | 1:00 - 1:20 | 0:30 - 0:50 | 0:10 - 1:20 | |
| | 1 1 07 | 50/50 100/0 | 0:30 - 0:55 0:55 - 3:30 | 1:00 | 0:30 - 1:00 | 0:15 - 0:30 | 0:15 - 0:40 0:25 - 1:35 ⁷ | 0:15 - 0:20 0:20 - 0:30 ⁷ | CAUTIO | |
| below -3 to -14 | below 27 to 7 | 75/25 | 0:45 - 1:50 | 1:45 | 1:00 - 1:45 | 0:35 - 1:00 | $0.20 - 1.00^7$ | 0:15 - 0:257 | No holdov time guidel | |
| below -14 to -28 | below 7 to -18.4 | 100/0 | 0:40 - 1:00 | 0:40 | 0:30 - 0:40 | 0:15 - 0:30 | | | exist | |
| 2 Ensure 1 3 Use ligh 4 Use ligh 5 No hold 5 Heavy s 7 These h CAUTIONS • The onl time tat • Heigh wi • Holdow | that the lowes t freezing rain over guideline now, ice pelle oldover times y acceptable ole cell. e of protectid nd velocity o er time may b | are derived from test t operational use temp holdover times in cor holdover times in cor holdover times in cor holdover times if pose sexist for this condition ts, moderate and hea only apply to outside decision-making cri on will be shortened r jet blast may reduc round de/anti-icing | perature (LOUT) in iditions of very lig itive identification on for 0°C (32°F) vy freezing rain, a air temperatures iterion, for takec in heavy weathe ce holdover time craft skin tempe | is respected. C th to r light snow of freezing drix and below. and hail. to -10°C (14°F off without a pin er conditions, a. | onsider use of r mixed with lig zzle is not pose) under freezin re-takeoff con heavy precipil than outside | Type I when T ht rain. ible. g drizzle and lig tamination ins ation rates, or | ght freezing rain spection, is the r high moisture | n. e shorter time v | /ithin the applical | ble hold |
| | | | | Pa | ge 40 of 6' | | | | Augu | ust 201 |

| | da Holdover | Time Guid | elines | | | | 1 | Winter 2013 | 3-201 |
|---|---|--|--|--|---|---|------------------------------------|--|--------|
| | | | TABL | E 4-C-LAUNC | н | | | | |
| | CLARIA | NT TYPE I | | LDOVER GUI | | R WINTER 20 | 013-2014 ¹ | | |
| | THE RESPONS | | | | | EMAINS WITH | THE USER | | |
| Outside Air Temperature ² | | | App | roximate Holdo | | | eather Conditio | ins | |
| | Type IV Fluid Concentration Neat Fluid/Water | Freezing Fog | Snow, Sno | ow Grains or S | (hours:m | | Light | | |
| Degrees Degrees Celsius Fahrenheit | (Volume %/Volume %) | or Ice Crystals | Very Light ³ | Light ³ | Moderate | Freezing Drizzle ⁴ | Freezing Rain | Rain on Cold Soaked Wing ⁵ | Other |
| | 100/0 | 4:00 - 4:00 | 2:00 | 1:45 - 2:00 | 1:05 - 1:45 | 1:30 - 2:00 | 1:00 - 1:40 | 0:15 - 1:40 | |
| -3 and 27 and above above | 75/25 | 3:40 - 4:00 | 2:00 | 1:45 - 2:00 | 1:00 - 1:45 | 1:40 - 2:00 | 0:45 - 1:15 | 0:10 - 1:45 | |
| | 50/50 | 1:25 - 2:45 | 1:25 | 0:45 - 1:25 | 0:25 - 0:45 | 0:30 - 0:50 | 0:20 - 0:25 | | |
| below -3 below 27 to -14 to 7 | 100/0 | 1:00 - 1:55 0:40 - 1:20 | 2:00 | 1:20 - 2:00 1:25 - 2:00 | 0:50 - 1:20 | 0:35 - 1:40 ⁷ 0:25 - 1:10 ⁷ | $0:25 - 0:45^7$ $0:25 - 0:45^7$ | CAUTION No holdov | |
| below -14 below 7 to -28.5 to -19.3 | 100/0 | 0:30 - 0:50 | 0:40 | 0:30 - 0:40 | 0:45 - 1:25 | 0.25 - 1.10 | 0.25 - 0.45 | time guideli exist | ines |
| These holdover times Ensure that the lowes Use light freezing rain Use light freezing rain No holdover guideling Heavy snow, ice pelle These holdover times CAUTIONS The only acceptable time table cell. The time of protectif High wind velocity of Holdover time may Fluids used during f | It operational use tem holdover times in cos holdover times in cos es exist for this conditi ts, moderate and hea only apply to outside decision-making cr on will be shortened or jet blast may redu | perature (LOUT) nditions of very lig litve identification on for 0°C (32°F) vy freezing rain, a air temperatures iterion, for taked in heavy weathe ce holdover time craft skin tempe | is respected. C pith or light snow of freezing dri and below. and hail. to -10°C (14°F off without a p er conditions, a. rature is lower in-flight icing | onsider use of i winked with lig zzle is not possi) under freezing re-takeoff cont heavy precipit r than outside a protection. | Type I when Ty It rain. drizzle and ligi amination insp ation rates, or | ht freezing rain. pection, is the high moisture | shorter time w | | |
| | | | Pa | age 32 of 61 | | | | Augu | st 201 |

| Transport Can | ada Holdover | Time Guide | elines | | | | ١ | Winter 2013 | 3-201 |
|--|--|--|---|--|--|---|-----------------------|--------------------------|---------|
| | | | TABL | E 4-CR-PG-A | | | | | |
| | CRYOTE | CH TYPE I | | LDOVER GU | | OR WINTER 2 | 013-2014 ¹ | | |
| | THE RESPON | SIBILITY FOR T | HE APPLICA | TION OF THE | SE DATA RE | EMAINS WITH | I THE USER | | |
| Outside Air Temperature ² | Type IV Fluid | | Аррг | oximate Holdo | over Times Un (hours:r | ider Various W ninutes) | eather Conditio | ons | |
| Degrees Degree | Concentration Neat Fluid/Wate | Freezing Fog | Snow, Sno | ow Grains or S | now Pellets | Freezing | Light | Rain on Cold | 011 |
| Celsius Fahrenh | |) or Ice Crystals | Very Light ³ | Light ³ | Moderate | Drizzle ⁴ | Freezing Rain | Soaked Wing ⁶ | Other |
| -3 and 27 and | 100/0 | 2:50 - 4:00 | 2:00 | 1:50 - 2:00 | 1:20 - 1:50 | 1:35 - 2:00 | 1:15 - 1:30 | 0:15 - 2:00 | - |
| above above | 75/25 | 2:30 - 4:00 0:50 - 1:25 | 2:00 | 1:20 - 2:00 0:35 - 1:20 | 0:45 - 1:20 | 1:40 - 2:00 0:20 - 0:45 | 0:40 - 1:10 | 0:09 - 1:40 | 1 |
| below -3 below 2 | 100.0 | 0:55 - 2:30 | 1:45 | 1:15 - 1:45 | 0:55 - 1:15 | 0:35 - 1:357 | 0:35 - 0:457 | CAUTIO | N: |
| to -14 to 7 | 75/25 | 0:40 - 1:30 | 1:45 | 1:00 - 1:45 | 0:35 - 1:00 | 0:25 - 1:057 | 0:35 - 0:457 | No holdov time guidel | |
| below -14 below to -30.5 to -22.9 | 100/0 | 0:25 - 0:50 | 0:40 | 0:30 - 0:40 | 0:15 - 0:30 | | | exist | |
| Ensure that the low Use light freezing right freezing right No holdover guidel Heavy snow, lee pe These holdover tim CAUTIONS The only acceptat time table cell. The time of protect High wind velocitji Holdover time maintage | es are derived from tes est operational use ten in holdover times in co in holdover times in co nes exist for this condi liets, moderate and he es only apply to outside le decision-making c tion will be shortenee or jet blast may redu / be reduced when aii g ground de/anti-icing | perature (LOUT) is nditions of very ligi sitive identification ion for 0°C (32°F) a vy freezing rain, a air temperatures t riterion, for takeol l in heavy weathe ce holdover time. craft skin temper | Tespected Cc ht or light snow of freezing driz and below. Ind hail. to -10°C (14°F) ff without a pr r conditions, f ature is lower sflight icing p | nsider use of T mixed with ligh zle is not possi under freezing e-takeoff cont: neavy precipita than outside a rotection. | ype I when Ty t rain. ole. drizzle and lig amination ins tion rates, or | ht freezing rain. pection, is the high moisture | shorter time wi | | |
| | | | Pa | ge 35 of 61 | | | | Augu | st 2013 |

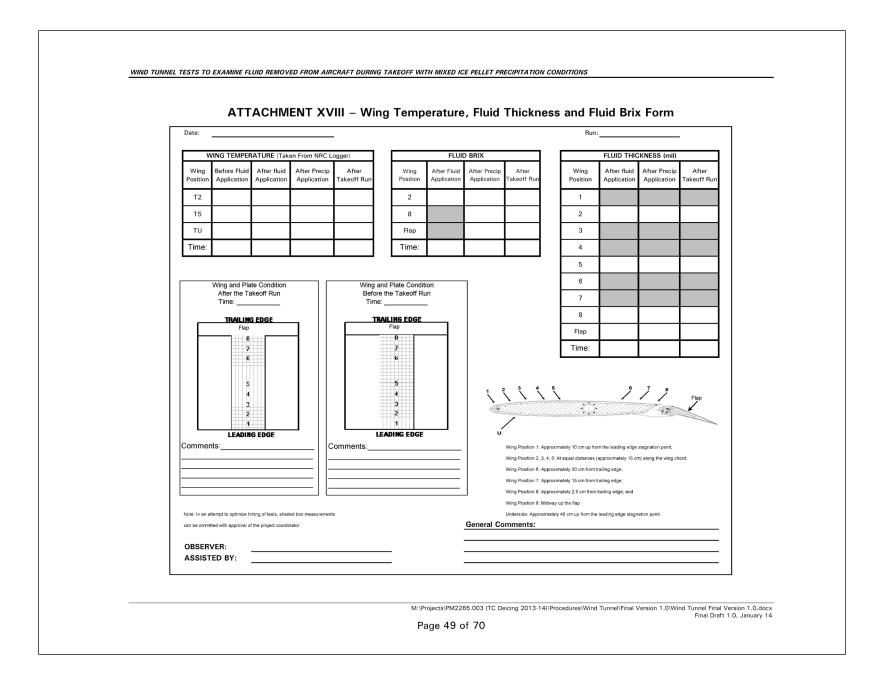


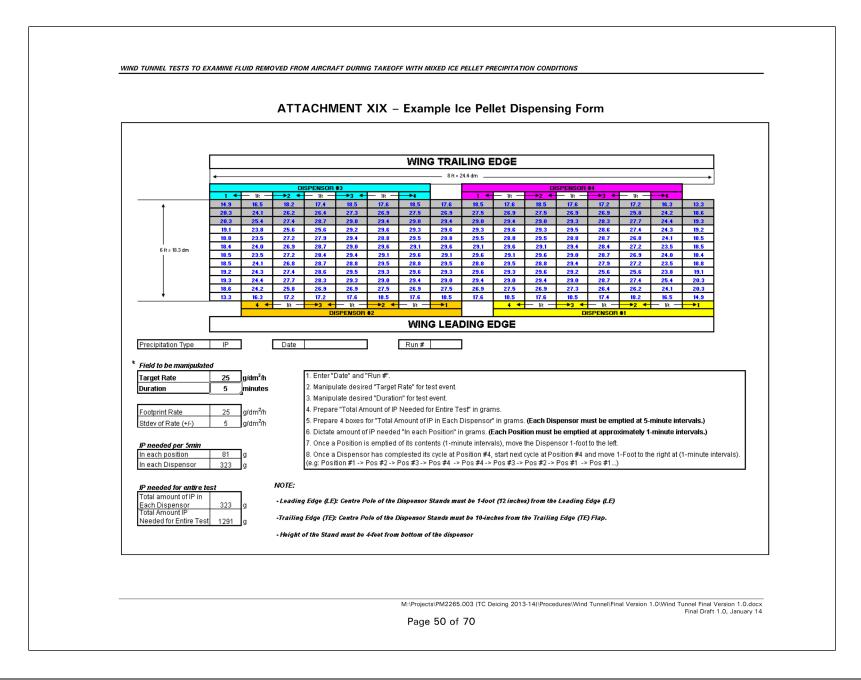
| ransport Canada Holdover Time (| | | Vinter 2013-20 |
|---|--|---|---|
| | TABLE 11 | | |
| | NCE TIMES FOR WI | | |
| All Type IV fluids are propylene glycol based with t THE RESPONSIBILITY FOR THE APPL | he exception of Dow Chen | nical EG106 which is eth | |
| | OAT -5°C and | OAT less than | OAT less than |
| Light Ice Pellets | above 50 minutes | -5°C to -10°C 30 minutes | -10°C ¹ 30 minutes ² |
| Moderate Ice Pellets | 25 minutes ³ | 10 minutes | 10 minutes ² |
| Light Ice Pellets Mixed with Light or Moderate Freezing Drizzle | 25 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Light Freezing Rain | 25 minutes | 10 minutes | |
| Light Ice Pellets Mixed with Light Rain | 25 minutes ⁴ | | Caution: No allowance times |
| Light Ice Pellets Mixed with Moderate Rain | 25 minutes⁵ | | currently exist |
| Light Ice Pellets Mixed with Light Snow | 25 minutes | 15 minutes |] |
| Light Ice Pellets Mixed with Moderate Snow | 10 minutes | | 1 |
| Ensure that the lowest operational use term No allowance times exist for propylene give 115 knots. (For these aircraft, if the fluid typ Allowance time is 15 minutes for propylene No allowance times exist in this condition for with light freezing rain. No allowance times exist in this condition for AUTIONS Fluids used during ground de/anti-icing | (PG) fluids, when u e is not known, assur glycol (PG) fluids or w or temperatures below r temperatures below | sed on aircraft with r e zero allowance tim hen the fluid type is to 0°C; consider use o 0°C. | e). unknown. |

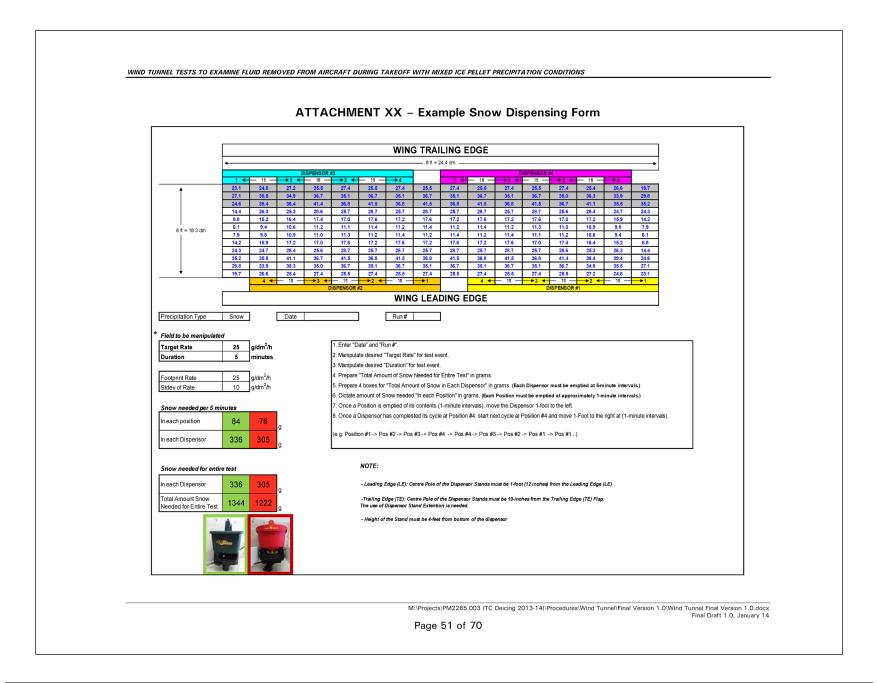
| | ATTACHMENT XVI – Task List for Setup | and Actual T | ests |
|----------|---|--------------|--------|
| o. | Task | Person | Status |
| 0. | Planning and Preparation | reison | Status |
| | Co-ordinate with NRC wind tunnel personnel | MR/JD | |
| 2 | Ensure fluid is received ny NRC and is stored outdoors | MR/JD | |
| } | Check with NRC the status of the testing site, tunnel etc | MR | |
| ł | Arrange for hotel accommodations for APS personnel | VZ | |
| 5 | Arrange truck rental | VZ | |
| 6 7 | Arrange for ice and freezer delivery Organize personnel travel to Ottawa; | DY VZ | |
| 3 | Hire YOW personnel | VZ | |
| ,) | Complete contract for YOW personnel | VZ | |
| 0 | Co-ordinate with APS photographer | MR | |
| 1 | Ensure availability of freezing rain sprayer equipment; | MR | |
| 2 | Prepare and Arrange Office Materials for YOW | VZ | |
| 3 | Prepare Data forms and procedure | VZ | |
| 4 | Back up hard drives with all TC projects | VZ | |
| 5 | Prepare Test Log and Merge Historical Logs for Reference | VZ | |
| 6 7 | Prepare weather forceast spreadsheet Prepare historical falling ball records spreadsheet | VZ VZ | |
| / 8 | Frepare historical failing ball records spreadsheet Finalize and complete list of equipment/materials required | MR | |
| 9 | Prepare and Arrange Site Equipment for YOW | DY | |
| 0 | Ensure proper functioning of ice pellet dispenser equipment; | MR | |
| 1 | Review IP/ZR/SN dispersal techniques and location | VZ/MR | |
| 2 | Update IP Rate File (if necessary) | VZ/MR | |
| 3 | Check weather prior to finalizing test dates and Day vs. Night Shift, | MR/JD | |
| 4 | Arrange for pallets to lift up 1000L totes (if applicable) | MR | |
| 5 | Purchase new 20 L containers (as necessary) | DY | |
| 6 7 | Complete purchase list and shopping Pack and leave YUL for YOW on Monday Jan 7th for AM start on Jan | VZ APS | |
| <i>,</i> | Wednesday Jan 8 | AFG | |
| 8 | Safety Briefing & Training (APS/YOW) | MR | |
| 9 | Unload Truck and organize equipement in lower, middle, or office area | APS | |
| 0 | Verify and Organize Fluid Recieved (labels and fluid receipt forms) | DY/JS | |
| 1 | Transfer Fluids from 1000 L Totes to 20 L containers | DY/JS | |
| 2 | Collect fluid samples for viscosity at APS office and for Falling Ball | DY/VZ | |
| 3 | Conduct falling ball verification | DY/VZ | |
| 4 | Confirm ice and freezer delivery | DY | |
| 5 6 | Setup general office and testing equipment | VZ VZ | |
| 7 | Setup Projector Setup Printer | VZ | |
| 8 | Setup rate station (if necessary) | DY | |
| 9 | Setup IP/SN manufacturing material in reefer truck | JS | |
| 0 | Test and prepare IP dispensing equipment | JS | |
| 1 | Train IP making personnel (ongoing) | JS/YOW | |
| 2 | Co-ordinate fabrication of ice pellets/snow | VZ/JS | |
| 3 | IP/SN/ZR Calibration (if necessary) | DY/VZ/MR | |
| 4 | Start IP manufacturing | JS | |
| 5 6 | Mark wing (only if requested); Setup Still and Video Cameras same as 2010-11 | VZ BG/JsD | |
| о 7 | Verify photo and video angles, resolution, etc, against 2010-11/11-12 | BG/JsD/MR | |
| 8 | Document new final camera and flash locations | VZ/BG/JsD | |
| 9 | General safety briefing and update on testing | APS/NRC/YOW | |
| 0 | Dry Run of tests with APS and NRC (if necessary) | APS/NRC | |
| 1 | Start Testing (Dry wing tests may be possible while setup occurs) | APS/NRC | |
| | Each Testing Day | | |
| 2 | Check with NRC the status of the testing site, tunnel, weather etc | MR | |
| 3 | Deicide personnel requirements for following day for 24hr notice | MR/WU | |
| 4 5 | Prepare equipment and fluid to be used for test Manufacture ice pellets | DY JS/YOW | |
| 5 6 | Prepare photography equipment | BG | |
| 7 | Prepare biotography equipment | VZ | |
| 8 | Conduct tests based on test plan | APS | |
| 9 | Modify test plan based on results obtained | WU/JD/MR | |
| 0 | Update ice pellet, snow, raw ice, and fluid Inventory (end of day) | VZ/JS | |
| 1 | Update Test Log and Test Plan (ongoing and end of day) | VZ | |

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| | Form 1 |
|--|--|
| | GENERAL FORM (EVERY TEST) |
| DATE: | FLUID APPLIED: RUN # (Plan #): |
| AIR TEMPERATURE (*C) BEFORE TEST: | AIR TEMPERATURE (*C) AFTER TEST: |
| | TUNNEL TEMPERATURE (*C) AFTER TEST: |
| WIND TUNNEL START TIME: | PROJECTED SPEED (S/KTS): |
| ROTATION ANGLE: | EXTRA RUN INFO: |
| FLAP SETTING (20°, 0°): | |
| | Check if additional notes provided on a separate sheet |
| | FLUID APPLICATION |
| Actual start time: | Actual End Time: |
| Fluid Brix: | Amount of Fluid (L): |
| Fluid Temperature (°C): | Fluid Application Method: POUR |
| | |
| | ICE PELLETS APPLICATION (if applicable) |
| ctual start time:ate of Ice Pellets Applied (g/dm²/h): | |
| xposure Time: | ice Pellete Size (nin). |
| Total IP Required per Dispenser: | |
| | REEZING RAIN/DRIZZLE APPLICATION (if applicable) |
| ctual start time: | Actual End Time: |
| ate of Precipitation Applied (g/dm²/h): | |
| Exposure Time: | Needle: |
| | Flow: |
| | Pressure |
| | SNOW APPLICATION (if applicable) |
| Actual start time: | Actual End Time: |
| Rate of Snow Applied (g/dm²/h): | Snow Size (mm): <1.4 mm |
| | Method: Dispenser Sieve |
| Exposure Time: | |
| | |
| Exposure Time: | |
| Total SN Required per Dispenser: | |





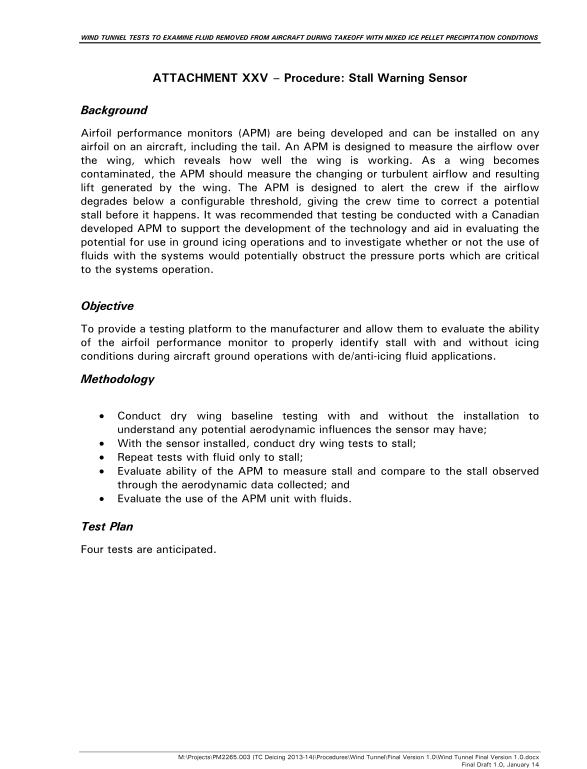


| | ATTACHMENT XXI – Example Snow Dispensing Form |
|---|---|
| Precipitation Type Sited Snow * Field to be manipulated Target Rate 25 Duration 5 minutes | ATACCHMENT XXI - Example Snow Dispensing Form □ text |
| | M:\Projects\PM2265.003 (TC Deicing 2013-14)\Procedures\Wind Tunnel\Final Version 1.0\Wind Tunnel Final Version 1.0. |

| Date: Ratings: 1 - Contamination not very visible, fluid still clean. 2 - Contamination visible, but lots of fluid still present 3 - Contamination visible, spots of bridging present 5 - Contamination visible, adherence of contamination Before Take-off Run <u>Area Visual Severity</u> <u>Leading Edge</u> Trailing Edge <u>Trailing Edge</u> <u>Trailing Edge</u> <u>Trailing Edge</u> <u>Flap</u> <u>Atea Take-off Run</u> <u>Expected</u> Lift Loss (%) <u>Context Severity</u> <u>Context Sev</u> | Ratings: 1 - Contamination not very visible, fluid still clean. 2 - Contamination is visible, but lots of fluid still present 3 - Contamination visible, spots of bridging contamination 4 - Contamination visible, lots of dry bridging present 5 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination 1 - Contamination <th>Ratings: 1 - Contamination not very visible, fluid still clean. 2 - Contamination is visible, but lots of fluid still present 3 - Contamination visible, spots of bridging contamination 4 - Contamination visible, lots of dry bridging present 5 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination 1 - Contamination 9 - Contamination 1 - Contamination <th>VIS</th><th>JAL EVALUATION I</th><th>RATING OF CONDI</th><th>TION OF WING</th></th> | Ratings: 1 - Contamination not very visible, fluid still clean. 2 - Contamination is visible, but lots of fluid still present 3 - Contamination visible, spots of bridging contamination 4 - Contamination visible, lots of dry bridging present 5 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 8 - Contamination visible, adherence of contamination 9 - Contamination 1 - Contamination 9 - Contamination 1 - Contamination <th>VIS</th> <th>JAL EVALUATION I</th> <th>RATING OF CONDI</th> <th>TION OF WING</th> | VIS | JAL EVALUATION I | RATING OF CONDI | TION OF WING |
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| | Additional Observations: | Additional Observations: | | | | |

| L. | ATTACHMEN | IT XXIII – Flui | d Receipt Form | | |
|--|---------------------|-----------------|--------------------|---------------------|--|
| [| Consider usi | ng electronic a | auto-fill format) | | |
| SECTION A - SITE | 0 | HOT SAMPLE | | I/OTHER SAMPLE | |
| Receiving Location: | | | Date of Receiving: | | |
| Manufacturer: | | Fluid Name: | | Fluid Type: | |
| Date of Production: | | | Batch #: | | |
| Fluid Dilution: | | | | | |
| | x L= | | x L= L | X L = L | |
| APS Measured BRIX: | | | | | |
| | | | | | |
| Note any additional information included o | n fluid containers: | | Received | l by: | |
| | | | | (PRINT NAME) on: | |
| | | | | (DATE) | |
| | | | | | |
| SECTION B - OFFICE | | | | | |
| Fluid Code Assigned: 10 | 0/0 | 75/25 | 50/50 | Туре I | |
| Viscosity Information Received:1 | | Visc | osity Measured:1 | | |
| WSET Sample Sent to AMIL: | | WSE | T Result Received: | | |
| FFP Curves Received: ² | | | | | |
| | | | | | |

| | ATTACHMENT XXIV – Log of Fluid Sample Bottles | | | | | | |
|-----------------------|---|---------|---------------------------------|------------------------------------|-------------------------------|----------|--|
| Date of Extraction | Fluid and Dilution | Batch # | Sample Source (i.e. drum) | Falling Ball Fluid Temp (°C) | Falling Ball Time (sec) | Comments | |
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ATTACHMENT XXVI – Procedure: Heavy Snow

Background

As a direct result of the ice pellet research conducted, the use of HOTs for determining the protection time provided by anti-icing fluids was questioned. The focus has turned towards "aerodynamic failure" which can be defined as a significant lift loss resulting from contaminated anti-icing fluid. Heavy snow conditions have been selected for this study for two reasons. First, snow conditions account for the most significant portion of de-icing operations globally. Secondly, there has been a recent industry interest for holdover time for heavy snow conditions. Preliminary aerodynamic testing was conducted during the winters of 2006-07 and 2008-2011.

Objective

To investigate the fluid aerodynamic flow-off characteristics of anti-icing fluid contaminated with simulated heavy snow versus moderate snow.

Methodology

The general methodology to be used during these tests is in accordance with the methodologies used for typical snow condition tests conducted in the wind tunnel.

- For a chosen fluid, conduct a test simulating moderate snow conditions (rate of 25 g/dm²/h) for an exposure time derived from the HOT table based on the tunnel temperature at the time of the test
- Record lift data, visual observations, and manually collected data;
- Conduct two comparative tests simulating heavy snow conditions (rate of 50 g/dm²/h or higher) for the same exposure time used during the moderate snow test.
 - NOTE: previous testing has indicated that using half, to ³⁄₄ of the moderate snow HOT generates similar end conditions, whereas using the full moderate HOT for heavy snow conditions generates a more sever fluid failure which behaves worse aerodynamically. ;
- Record lift data, visual observations, and manually collected data;
- Compare the heavy snow results to the moderate snow results. If the heavy snow results are worse, repeat the heavy snow test with a reduced exposure time, if the results are better, repeat the heavy snow test with an increased exposure time.
- Repeat until similar lift data, and visual observations are achieved for both heavy snow and moderate snow; and
- Document the percentage of the moderate snow HOT that is acceptable for heavy snow conditions.

Test Plan

Two to four comparative tests are anticipated. See previous reports for suggested test plan.

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ATTACHMENT XXVII – Procedure: Heavy Contamination

Background

Previous testing in the wind tunnel demonstrated that although very heavy ice pellet and/or snow contamination was applied to a fluid covered wing section, significant lift losses were not apparent. The initial testing indicated that after a certain level of contamination, the dry loose ice pellets or snow no longer absorb into the fluid and easily fly off during the acceleration. The protection is due to a thin layer of fluid present underneath the contamination that prevents adherence. Questions of which point the lift losses become detrimental have been raised.

Objective

To continue previous research investigating heavy contamination effects on fluid flow off.

Methodology

The general methodology to be used during these tests is in accordance with the methodologies used for typical ice pellet tests conducted in the wind tunnel.

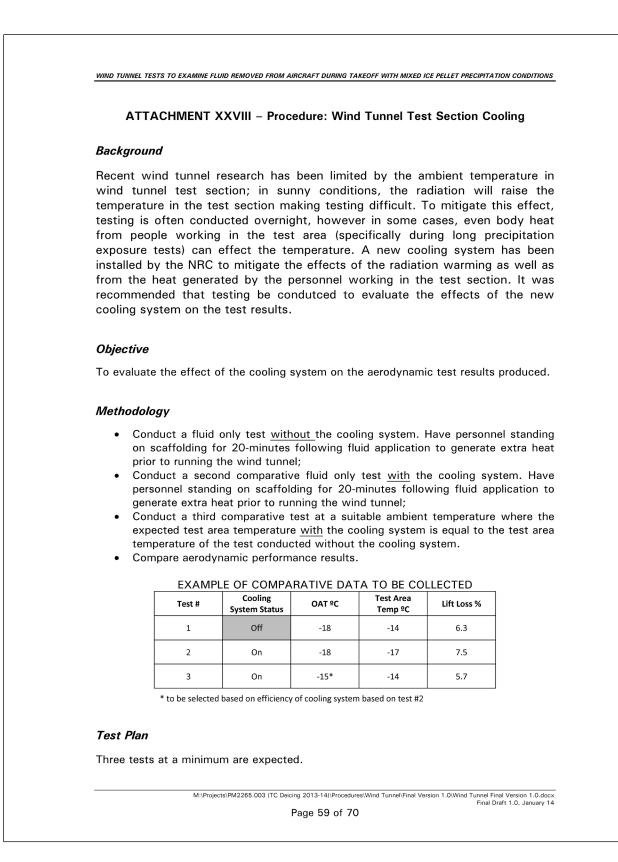
- For a chosen fluid, conduct a test simulating ice pellets, snow, or freezing rain, for an exposure time far exceeding the recommended HOT or allowance time;
- Record lift data, visual observations, and manually collected data;
- Compare aerodynamic performance results to fluid only or fluid and contamination tests at the same temperature.

Test Plan

One to four tests are anticipated. Previous work should be referenced to identify starting levels of heavy contamination.

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ATTACHMENT XXIX- Procedure: Effect of Fluid Viscosity

Background

Testing was previously conducted to evaluate the aerodynamic effects of fluid viscosity on flow-off. To do so, comparative testing was conducted with both mid-production fluid (used for ice pellet allowance time testing) and with lowest on-wing viscosity fluid (LOWV) (used for holdover time testing). Testing was conducted with the thin high performance airfoil in fluid only conditions. Additional testing was recommended to further substantiate the testing results.

Objective

To continue previous research evaluating the effect of fluid viscosity on aerodynamics.

Methodology

For each comparative test set, a baseline mid-production test should be conducted, and immediately followed by a lowest on-wing viscosity test of the same fluid type. Testing should be done with fluid only and fluid and contamination.

Test Plan

Two to four tests are anticipated.

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The general methodology to be used during these tests is in accordance with the methodologies used for typical ice pellet tests conducted in the wind tunnel.

- For a chosen fluid, conduct a test simulating ice pellets, snow, freezing fog, or frost, for an exposure time derived from the HOT table at the fluid LOUT.
- · Record lift data, visual observations, and manually collected data;
- Conduct a fluid only baseline test at the same temperature (at LOUT);
- Compare the aerodynamic performance.

Test Plan

Four or more tests are anticipated at a minimum. If LOUT temperatures for neat fluids are not likely to occur, investigate the possibility of using diluted fluids to obtain a higher LOUT.

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WIND TUNNEL TESTS TO EXAMINE FLUID REMOVED FROM AIRCRAFT DURING TAKEOFF WITH MIXED ICE PELLET PRECIPITATION CONDITIONS ATTACHMENT XXXI – Procedure: Small Hail Background Reports from primarily Asian operators have indicated that small hail can occur frequently during winter operations. The small hail will generally occur above freezing conditions; however no guidance for operating in the conditions is currently available. Questions have been raised as to whether the ice pellet allowance times can be used due to similarity in precipitation type. Although this concern has only been raised by Asian operators, it can be assumed that similar conditions can be expected by North American operators. WMO defines small hail as snow pellets encapsulated by ice, a precipitation halfway between graupel and hail. Objective To investigate the fluid aerodynamic flow-off characteristics of anti-icing fluid with contamination with small hail and to compare the results to ice pellets. Methodology The general methodology to be used during these tests is in accordance with the methodologies used for typical ice pellet tests conducted in the wind tunnel. For a chosen fluid, conduct a test simulating small hail for an exposure time derived from the current ice pellet allowance time table as a starting point; Record lift data, visual observations, and manually collected data; ٠ Conduct a fluid only baseline test at the same temperature; ٠ Compare the aerodynamic performance. Test Plan One to four tests are anticipated. A meteorologist should be consulted prior to the conduct to narrow down the exact conditions and temperatures at which small hail will occur, as well as to obtain the desired small hail diameter. M:\Projects\PM2265.003 (TC Deicing 2013-14)\Procedures\Wind Tunnel\Final Version 1.0\Wind Tunnel Final Version 1.0.docx Final Draft 1.0. January 14 Page 62 of 70

ATTACHMENT XXXII - Procedure: Frost Simulation in the Wind Tunnel

Background

Frost is an important consideration in aircraft deicing. The irregular and rough frost accretion patterns can result in a significant loss of lift on critical aircraft surfaces. This potential hazard is amplified by the frequent occurrence of frost accretion in winter operations. Frost is an area of research that has yet to be fully explored. Discussions regarding the aerodynamic effects of frost have been raised, and the possibility of doing wind tunnel testing has been considered. It was recommended that initial testing be performed to investigate whether it would be feasible to simulate frost conditions in the PIWT.

Objective

To investigate the feasibility of simulating frost conditions in the PIWT.

Methodology

This work is exploratory, so no exact procedure exists. It is recommended that the frost generating parameters be explored to try and stimulate frost accretion. This can be done by causing a negative temperature differential between the wing and the ambient air i.e. air is warmer than skin. A more specific methodology may be determined on site following a brain-storm with onsite technicians.

Test Plan

One or two tests is anticipated.

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ATTACHMENT XXXIII – Procedure: Flaps/Slats Testing to Support YMX Tests

Background

Flaps/slats testing has been conducted with the support of UPS during the winter sof 2011-12 and 2012-13, and is scheduled to continue during the winter of 2013-14. The initial results have indicated that extended configurations can result in earlier fluid failure on the flap and slats as compared to the main section of the wing. It was recommended that testing in the wind tunnel be conducted to evaluate how significant the aerodynamic penalties would be from having failed fluid in these isolated areas.

Objective

To investigate the aerodynamic performance degradation associated with failed fluid on flaps and slats.

Methodology

The general methodology to be used during these tests is in accordance with the methodologies used for typical snow condition tests conducted in the wind tunnel.

- For a chosen fluid, conduct a test simulating moderate snow conditions (rate of 25 g/dm²/h) for an exposure time derived from the HOT table based on the tunnel temperature at the time of the test;
- Simulate early fluid failure on the fixed leading edge by applying higher rates of contamination on this area (record additional amounts);
- The flap is a hinged flap, so will be subject to early failure by design;
- Record lift data, visual observations, and manually collected data;
- Conduct a fluid only baseline test at the same temperature;
- Compare the aerodynamic performance;
- Consideration should be given to conducting Type I tests.

Test Plan

Two to four comparative tests are anticipated.

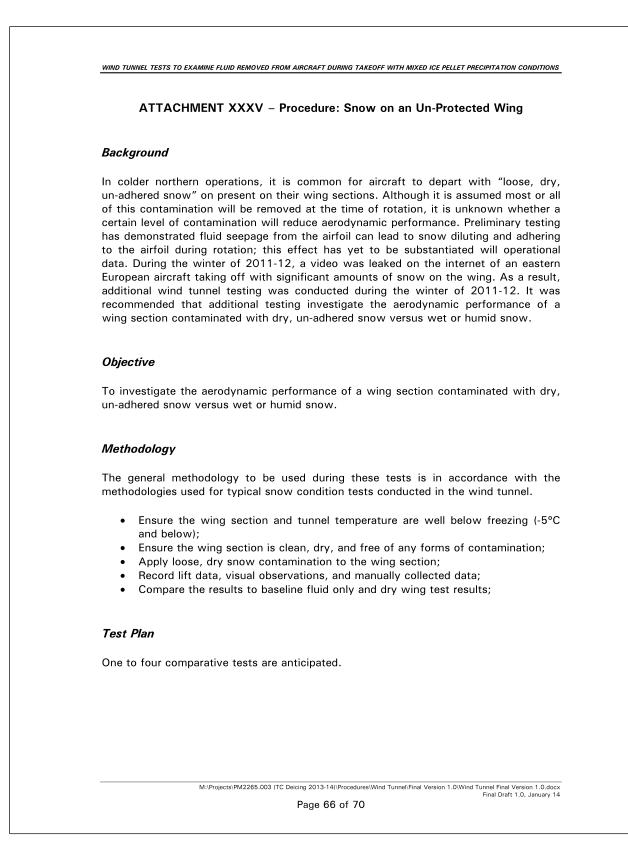
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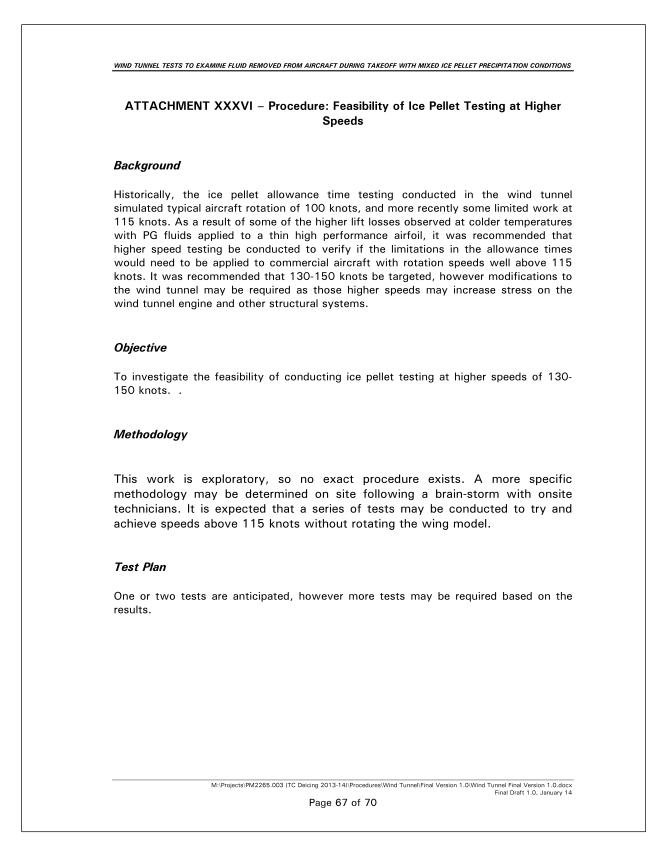
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WIND TUNNEL TESTS TO EXAMINE FLUID REMOVED FROM AIRCRAFT DURING TAKEOFF WITH MIXED ICE PELLET PRECIPITATION CONDITIONS **ATTACHMENT XXXIV – Procedure: Mixed HOT Conditions** Background As the accuracy of meteorological reporting continues to improve, there has been a need to provide improved guidance material during these transitional periods of mixed precipitation. During the winter of 2008-09, guidance material was developed for operations during light snow mixed with light rain conditions. As a result of this work, there was industry interest in guidance material for operations during light freezing rain and moderate snow conditions as well as other mixed conditions. The objective of these tests is to collect data to determine if the current HOT guidelines can be expanded to include other operational mixed conditions which may be of current interest to industry. Objective To investigate if the current HOT guidelines can be expanded to include mixed conditions i.e. light freezing rain and moderate snow conditions. Methodology The general methodology to be used during these tests is in accordance with the methodologies used for precipitation tests conducted in the wind tunnel. For a chosen fluid, conduct a test simulating mixed conditions for an exposure time derived from the HOT table based on relative condition. Record lift data, visual observations, and manually collected data; Conduct a fluid only baseline test at the same temperature; or Conduct a test with an existing relative HOT condition to evaluate the severity of the condition: Compare the aerodynamic performance. If the mixed condition results are severe, repeat the test with a reduced exposure time, if the results are good, repeat the test with a increased exposure time. Test Plan Two to four comparative tests are anticipated.

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APPENDIX A

ATTACHMENT XXXVII - Procedure: Windshield Washer Used as Type I Deicer

Background

Based on recent industry reports, it has become apparent that in more remote airports or with general aviation aircraft with smaller operations, aircraft deicing is not being conducted with SAE aircraft ground deicing Type I fluid, but rather with off-the-shelf windshield washer fluid. Although the basic chemistry of the windshield washer fluid may be similar, questions regarding the fluid freeze point, holdover time, aerodynamics, and material compatibility have been raised. It was recommended that some preliminary testing be conducted to investigate fluid flow off in the wind tunnel with and without contamination. Limited test was conducted during the winter of 2011-12. It was recommended that testing should continue if necessary based on operational needs.

Objective

To evaluate the holdover time and aerodynamic effects windshield washer fluid when used a substitute for an aircraft ground deicing Type I fluid.

Methodology

- Purchase various formulations of windshield washer fluid with varying freeze points;
- Apply fluid heated to 20°C using a garden sprayer;
- Expose to simulated freezing contamination (snow, freezing rain, or ice pellets). The exposure time is to be determined based on Type I fluid HOT's (45 minutes at a rate of 0.3 g/dm²/h);
- Document condition of the wing;
- Run the wind tunnel and collect data; and
- Compare results to baseline uncontaminated windshield washer tests and potentially with standard Type I tests.

Test Plan

No testing is planned unless indicated otherwise by TC.

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ATTACHMENT XXXVIII – Procedure: Effect of Fluid Seepage on Dry Wing Performance

Background

Preliminary observations have indicated that fluid seepage from the airfoil can lead to lift losses and other aerodynamic impacts. This is especially of concern after a long series of fluid tests followed by a baseline dry wing test. It was recommended that testing investigate the aerodynamic impacts of residual fluid seepage on the airfoil performance.

Objective

To investigate the aerodynamic impacts of residual fluid seepage on the airfoil performance.

Methodology

The general methodology to be used during these tests is in accordance with the methodologies used for typical tests conducted in the wind tunnel.

- To be conducted following a long series of fluid and/or contamination tests;
- Ensure the wing section is clean, dry, and free of any forms of contamination;
- Record lift data, visual observations, and manually collected data;
- Compare results to the first dry wing test of the season;
- Re-clean the wing using a wet-vac or other alternative method to try and remove any residual fluid;
- Record lift data, visual observations, and manually collected data;
- Compare the results;

Test Plan

One to three comparative tests are anticipated

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APPENDIX A ATTACHMENT XXXIX – Procedure: 2nd Wave of Fluid during Rotation Background Previous wind tunnel testing has shown that during a simulated take-off roll following de/anti-icing, fluid will shear off the wing section; however a small amount of fluid can remain trapped along the leading edge at the stagnation point. This "trapped" fluid begins to flow over the wing only once the wing is rotated; the stagnation point shifts below the leading edge, and the "trapped" fluid begins to shear off as a second wave. Previous testing was simulated in a static model using strips of speed tape and cork tape strategically located on the leading edge of the wing section (along the span where the separation bubble will typically occur). A separate set of dynamic tests simulated the second wave with actual anti-icing fluid; sheared fluid prior to rotation was left only in select areas either below or above the stagnation point and then the flow was observed during a typical rotation. The results showed the stalling characteristics of the wing with fluid (or fluid with contamination) appear to be driven by secondary wave effects near the leading edge; these effects are difficult to interpret on the two-dimensional model relative to a fully three-dimensional wing and should not be used in developing allowance times. Additional testing may be useful to better understand this effect. Objective

To investigate the aerodynamic effects of the second wave of fluid flow during rotation.

Methodology

- Simulate the 2nd wave of fluid using strips of tape applied at specific areas at different thicknesses on the wing, or with fluid; and
- Compare the different results.

Test Plan

One to four tests are anticipated.

M:\Projects\PM2265.003 (TC Deicing 2013-14)\Procedures\Wind Tunnel\Final Version 1.0\Wind Tunnel Final Version 1.0.docx Final Draft 1.0, January 14

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APPENDIX C

FLUID THICKNESS, TEMPERATURE, AND BRIX DATA FORM

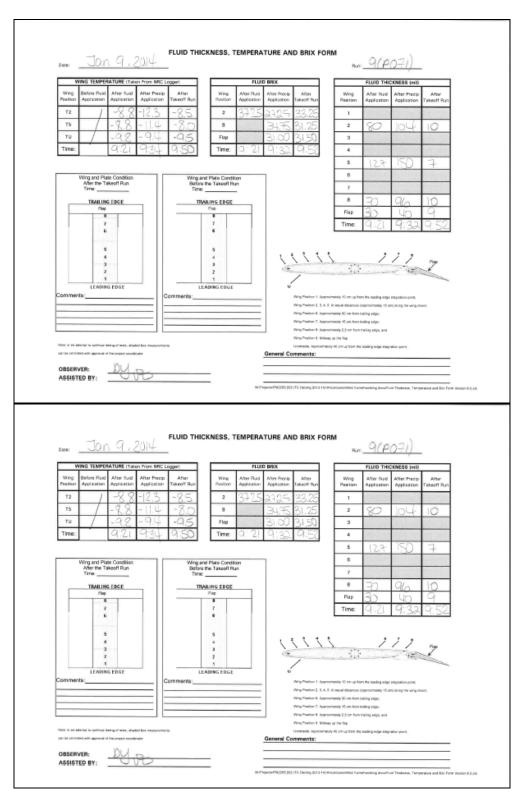


Figure C1: Test # 9

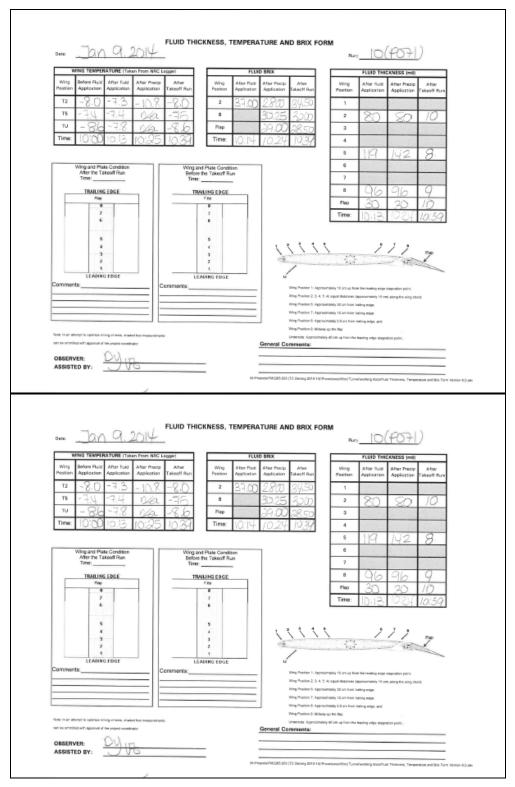


Figure 2: Test # 10

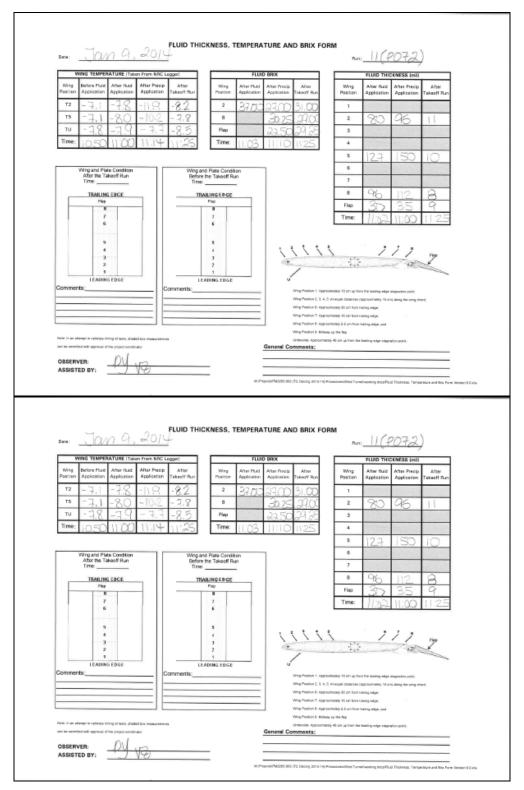


Figure C3: Test # 11

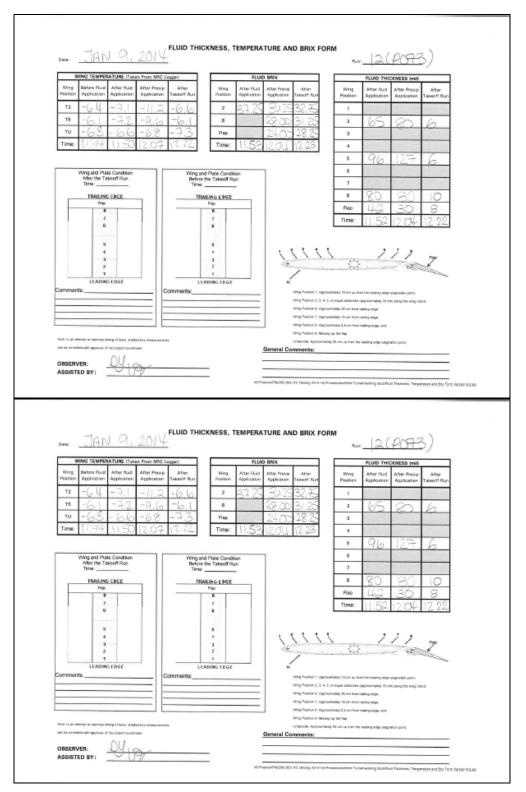


Figure C4: Test # 12

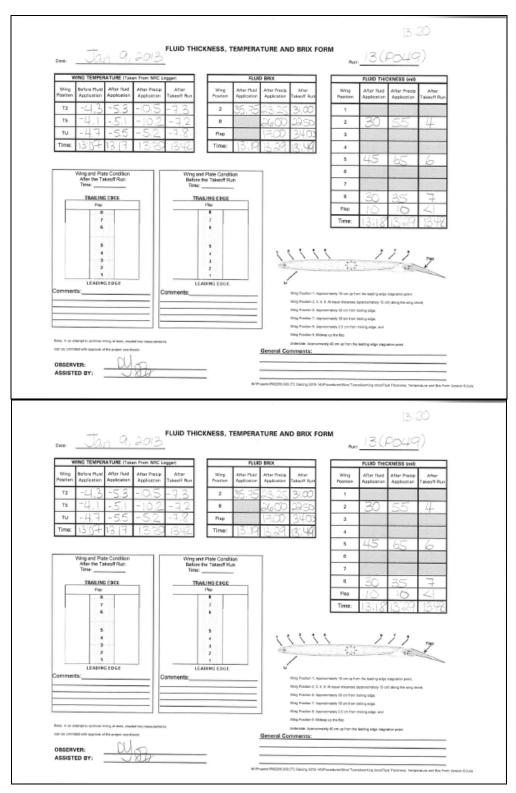


Figure C5: Test # 13

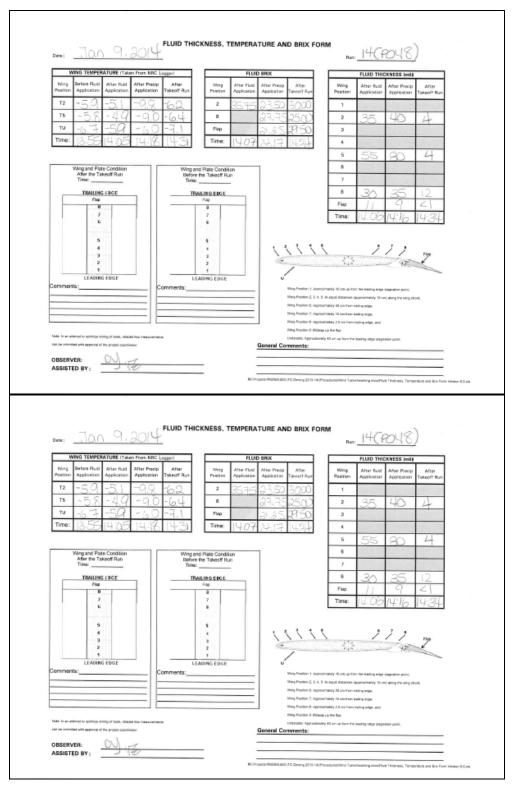


Figure C6: Test # 14

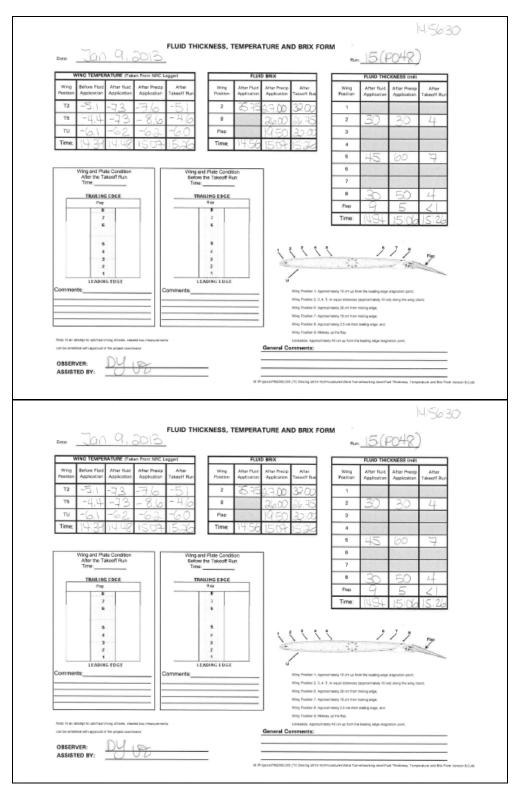


Figure C7: Test # 15

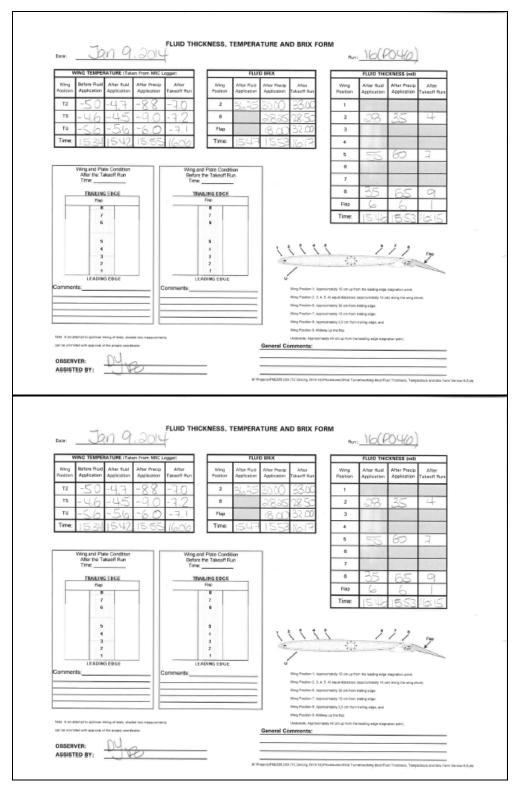


Figure C8: Test # 16

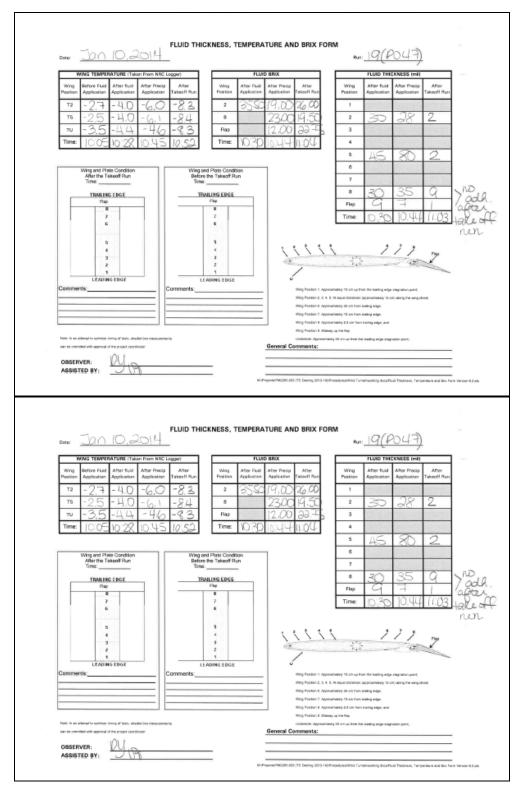


Figure C9: Test # 19

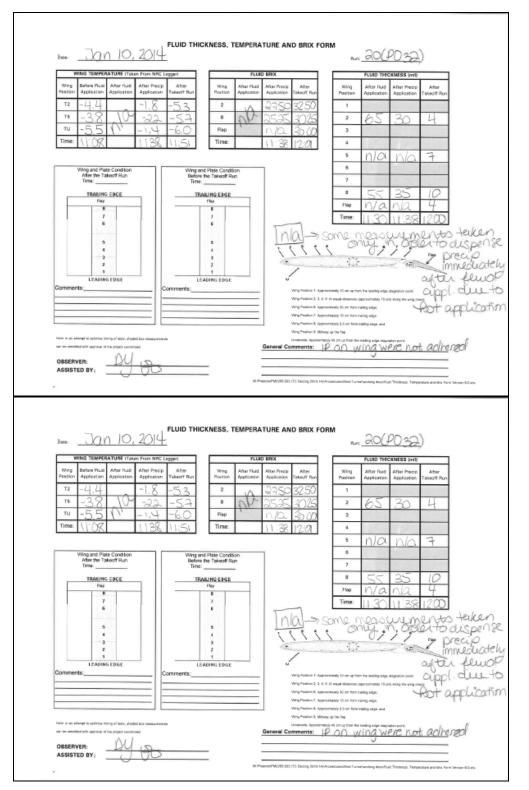


Figure C10: Test # 20

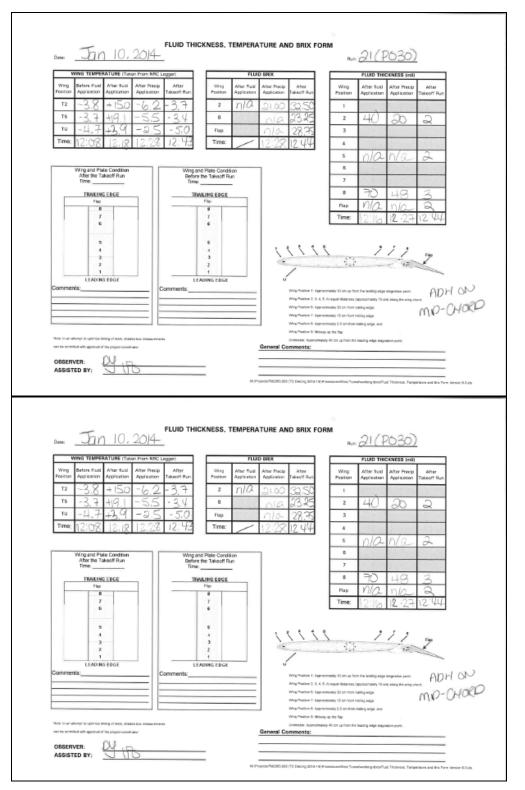


Figure C11: Test # 21

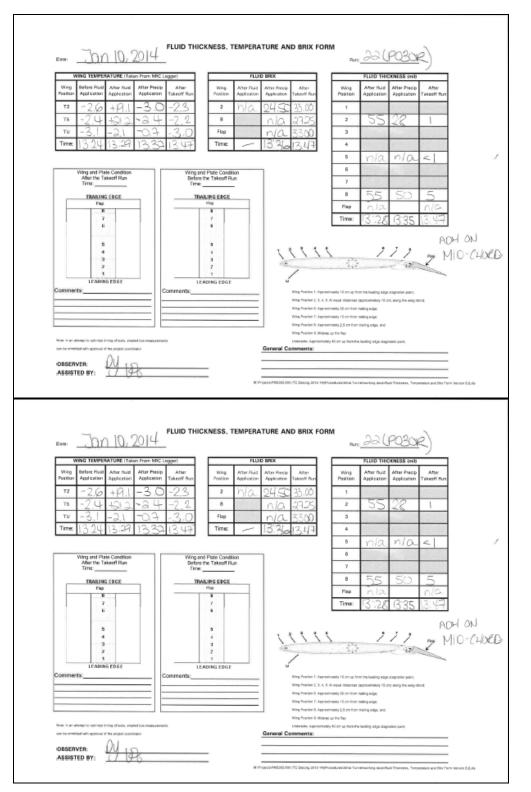


Figure C12: Test # 22

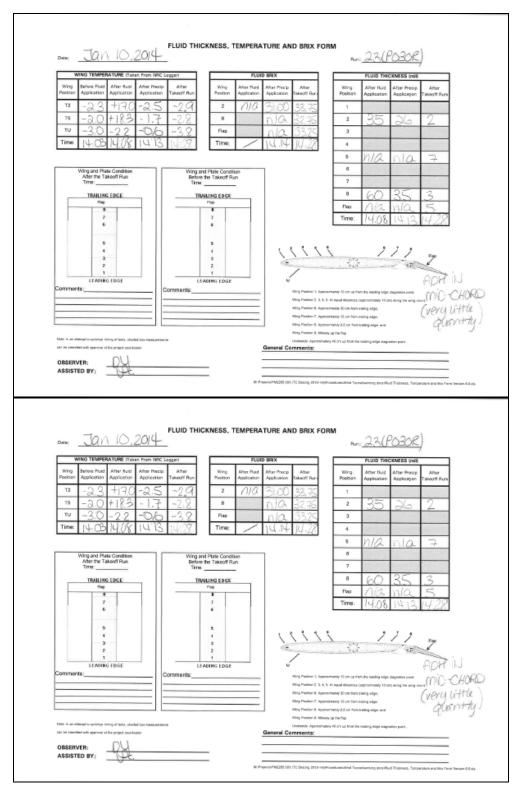


Figure C13: Test # 23

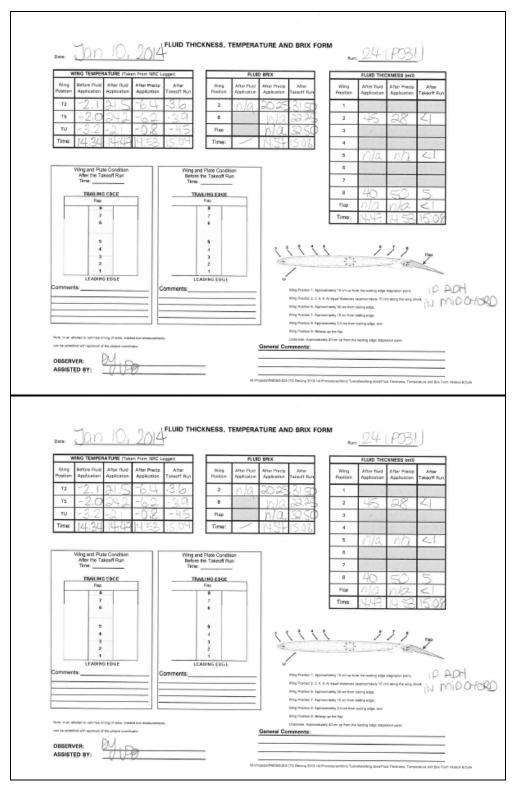


Figure C14: Test # 24

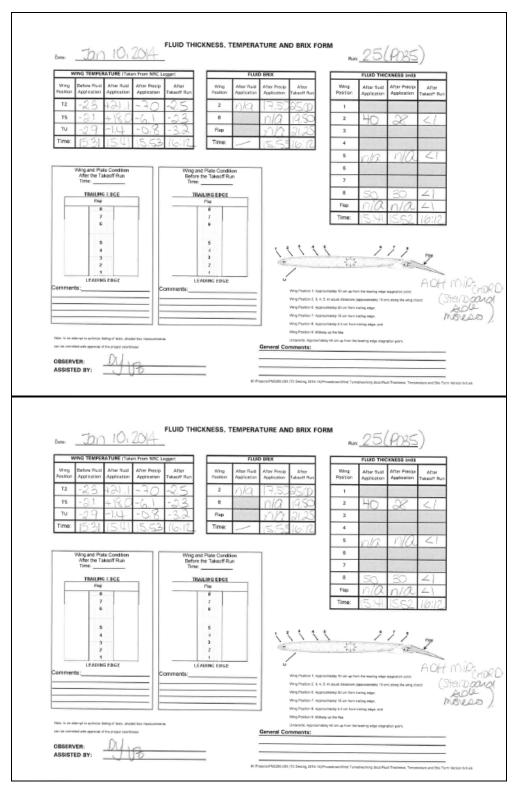


Figure C15: Test # 25

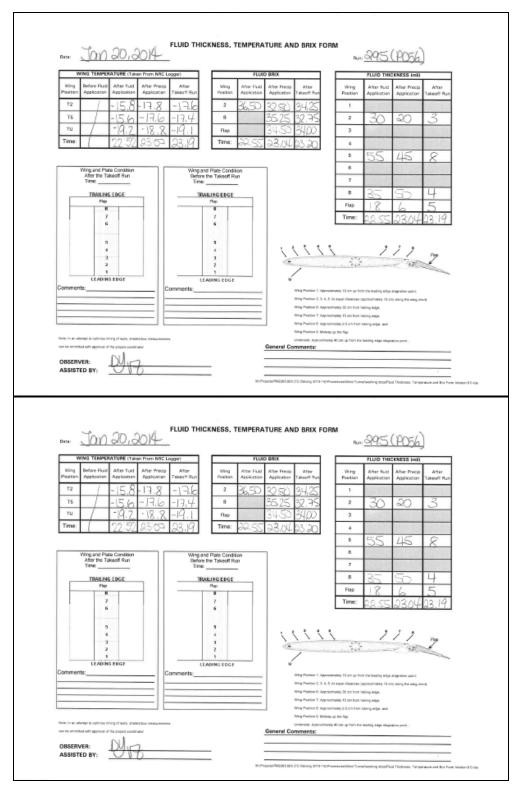


Figure C16: Test # 295

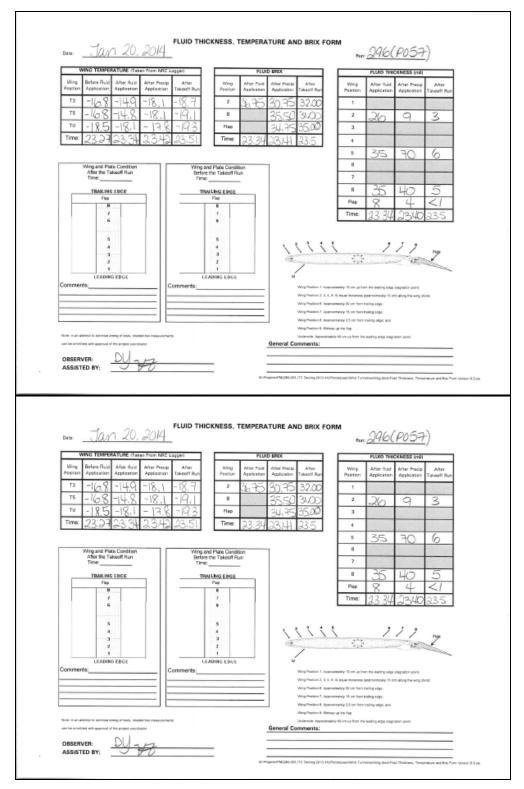


Figure C17: Test # 296

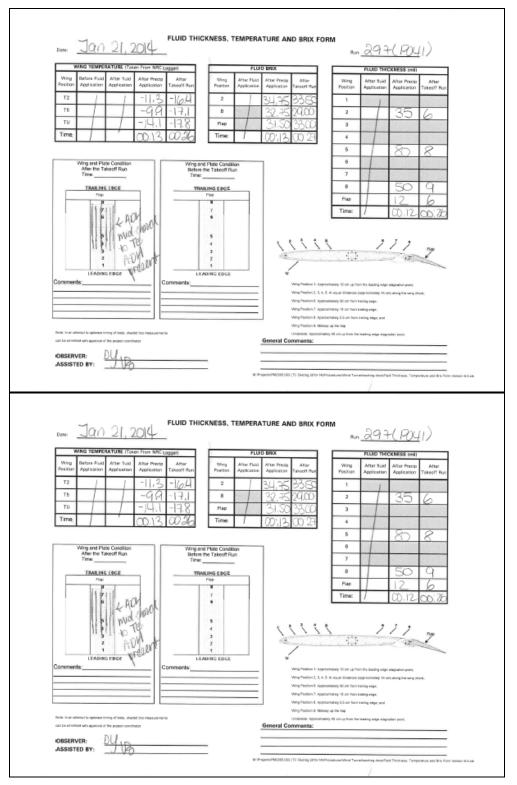


Figure C18: Test # 297

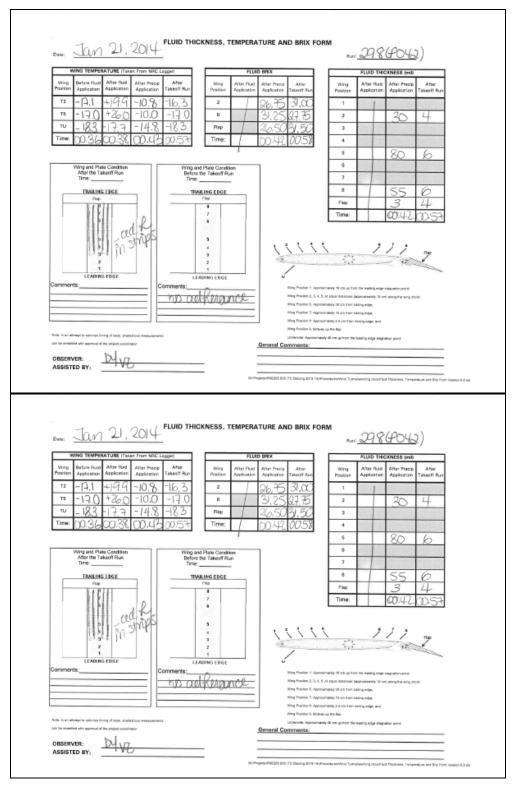


Figure C19: Test # 298

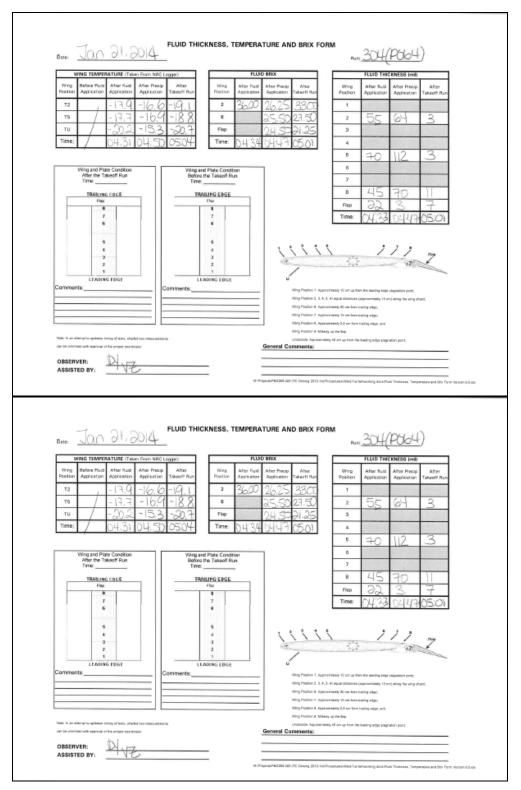


Figure C20: Test # 304

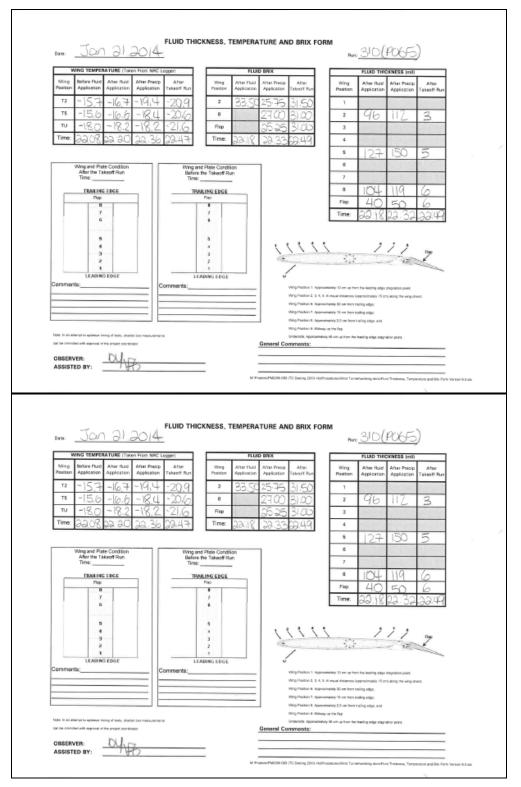


Figure C21: Test # 310

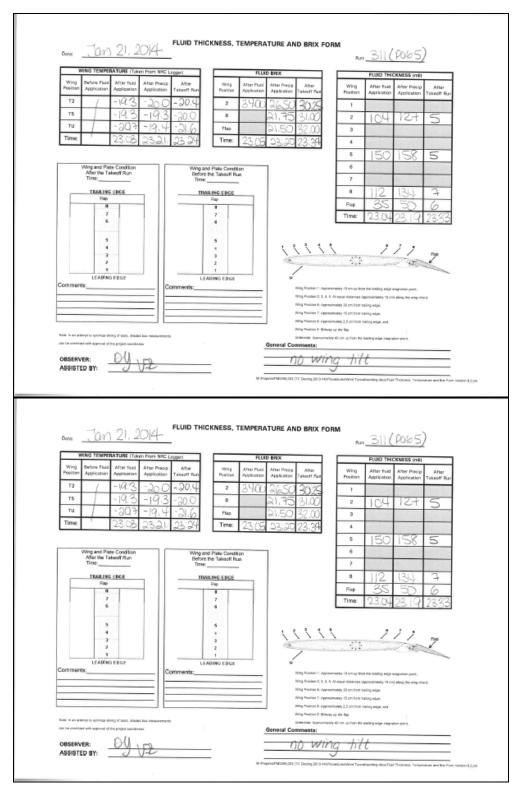


Figure C22: Test # 311

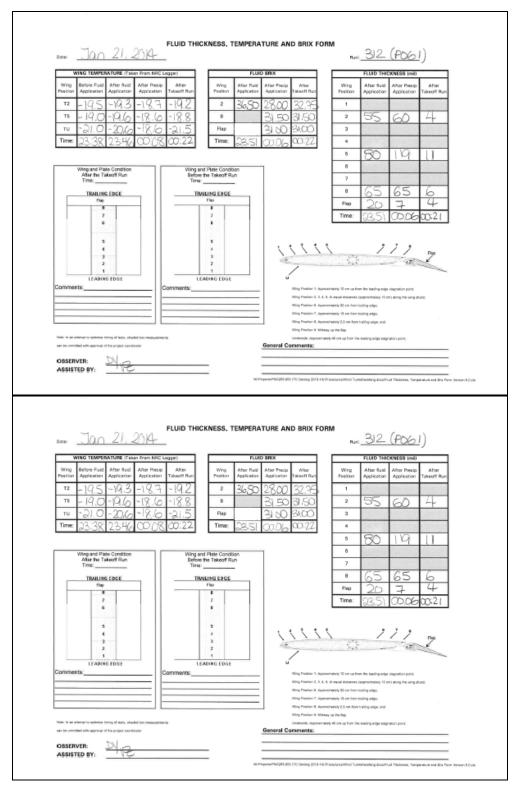


Figure C23: Test # 312

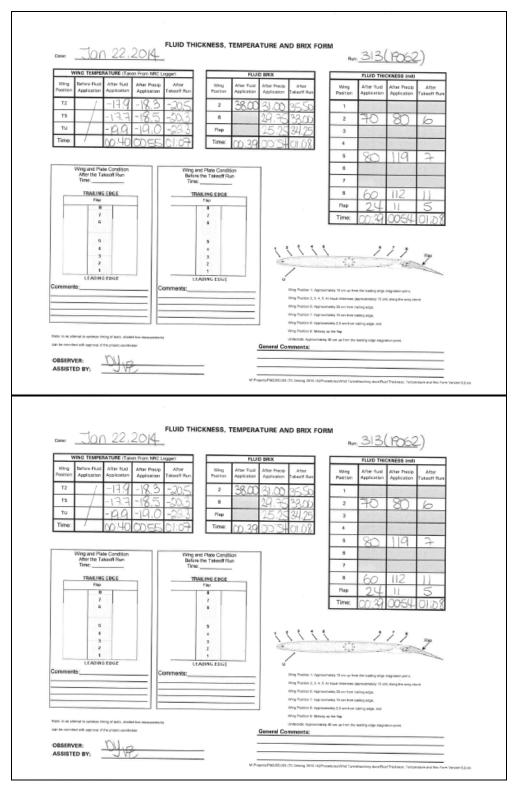


Figure C24: Test # 313

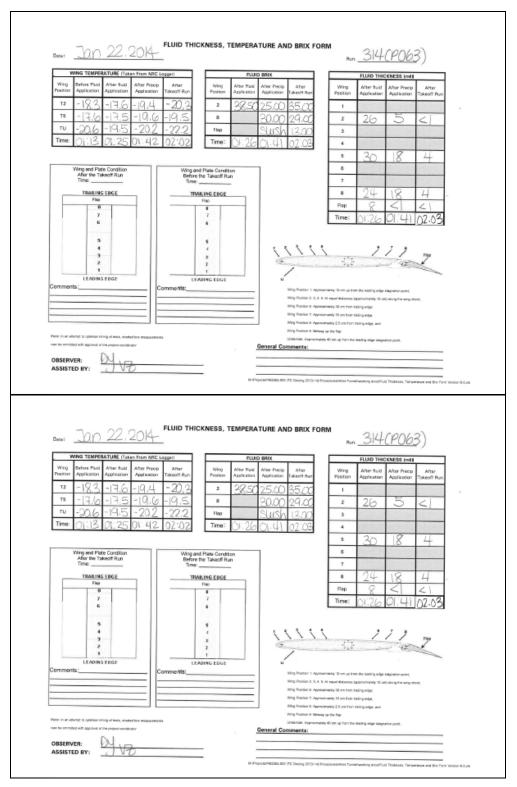


Figure C25: Test # 314

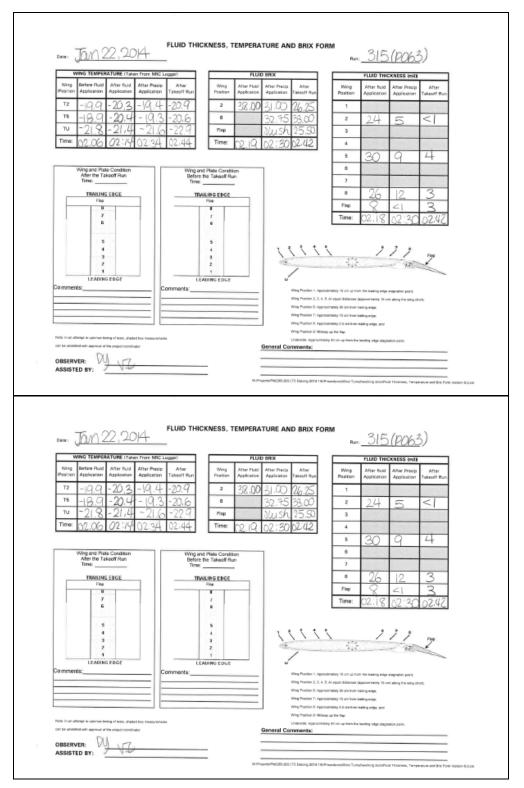


Figure C26: Test # 315

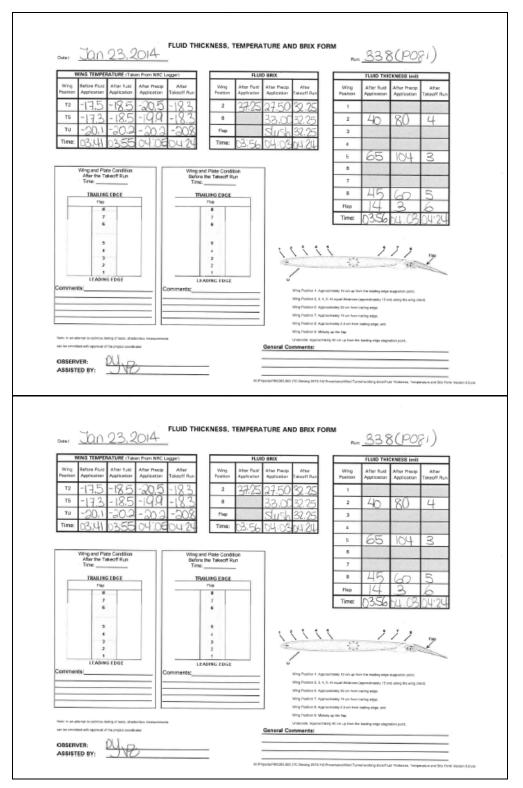


Figure C27: Test # 338

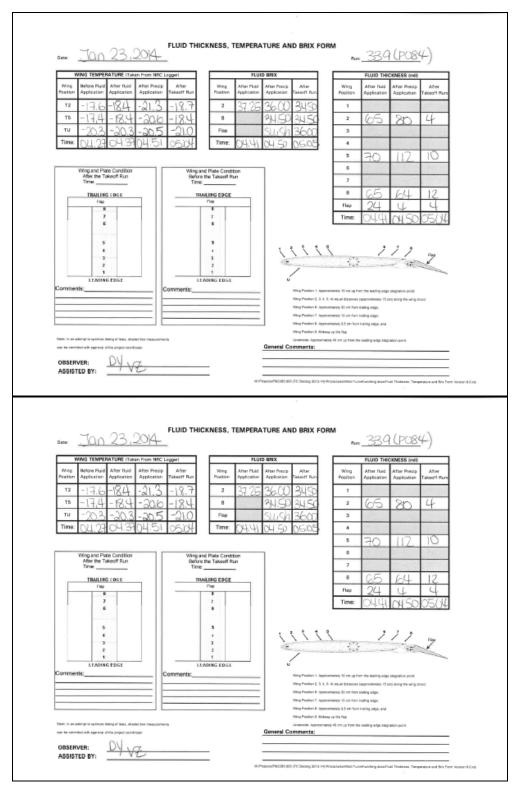


Figure C28: Test # 339

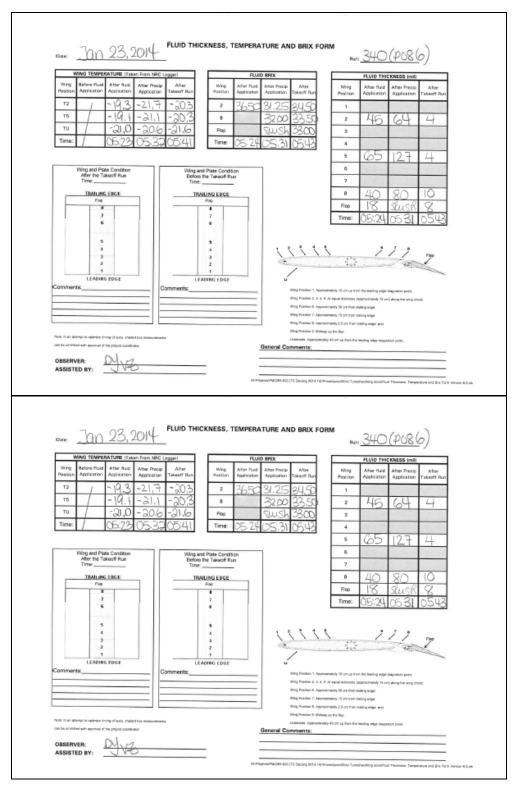


Figure C29: Test # 340

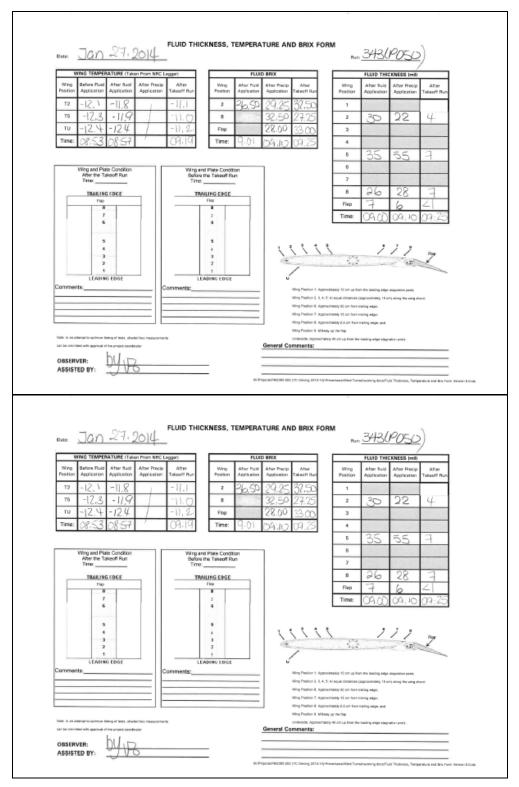


Figure C30: Test #343

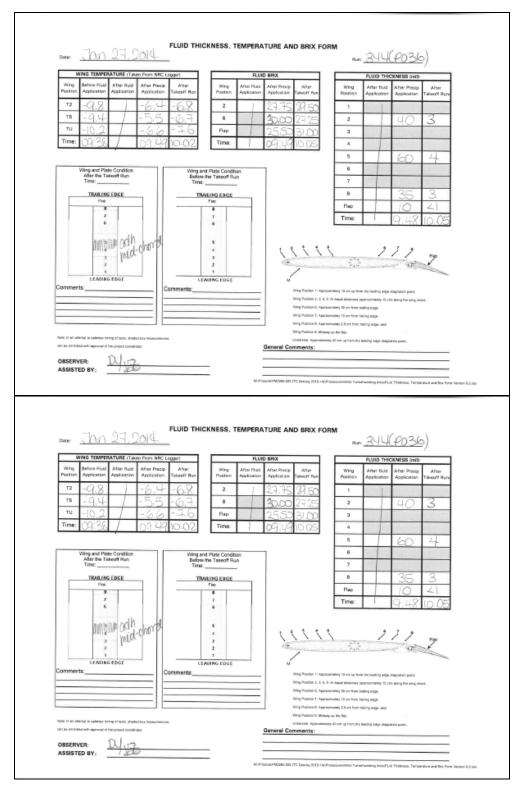


Figure C31: Test # 344

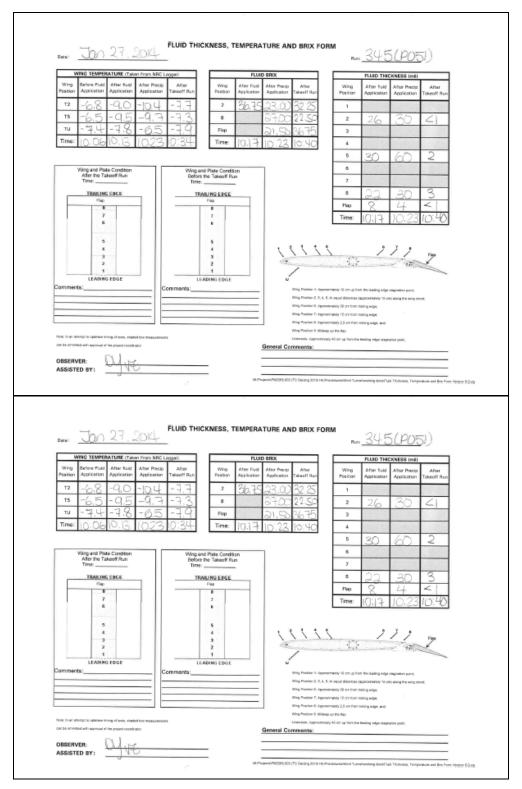


Figure C32: Test # 345

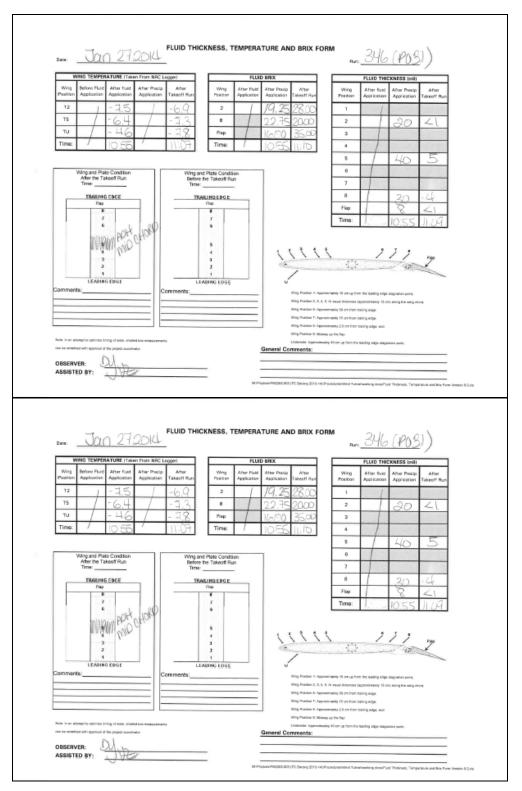


Figure C33: Test # 346

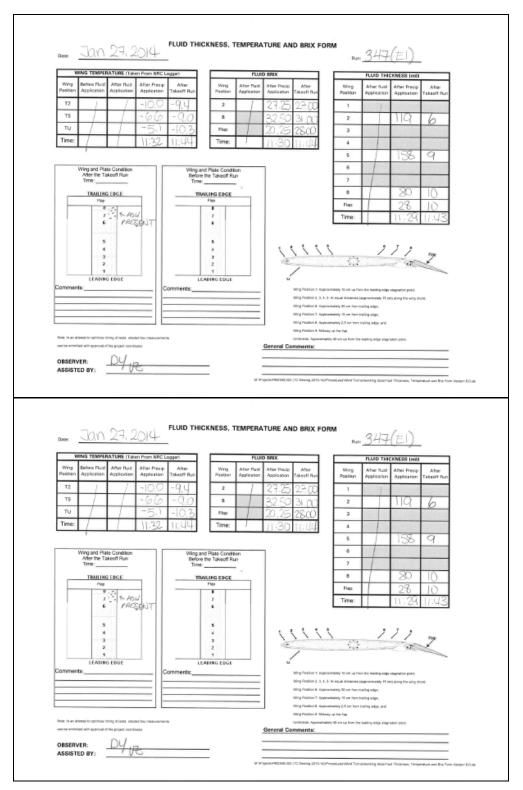


Figure C34: Test # 347

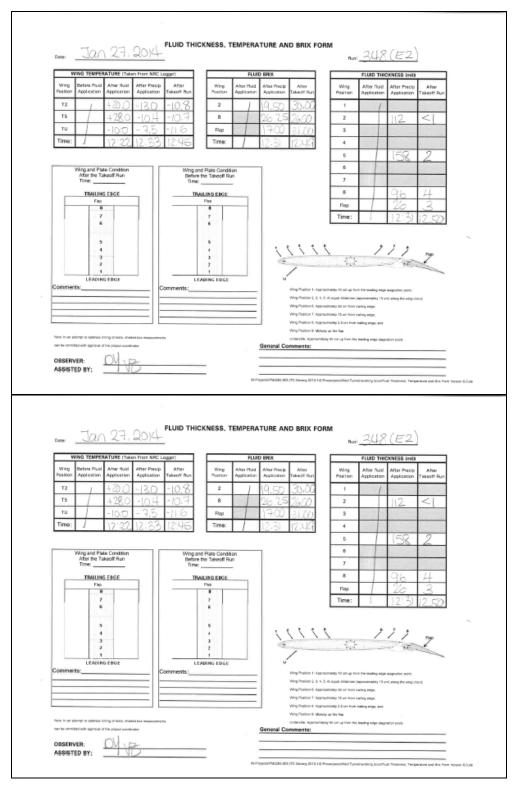


Figure C35: Test # 348

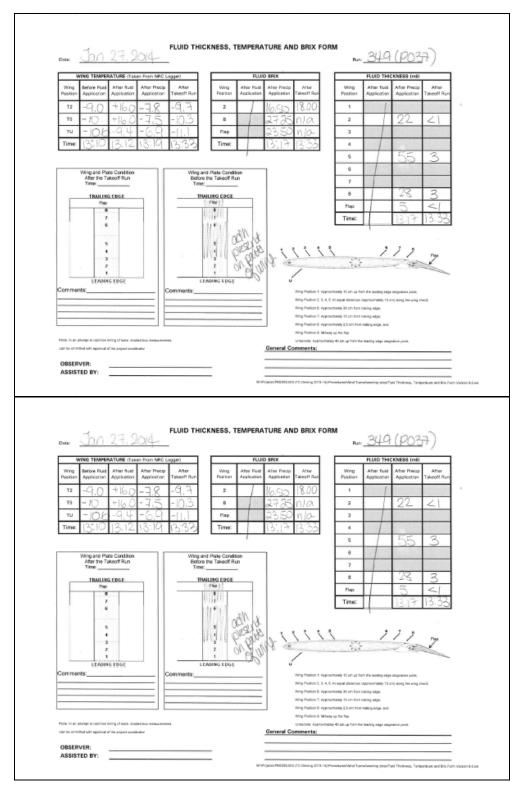


Figure C36: Test # 349

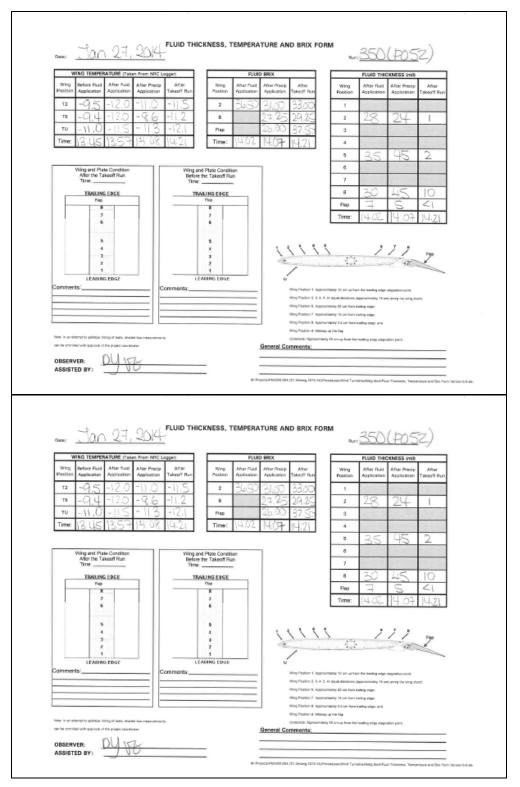


Figure C37: Test # 350

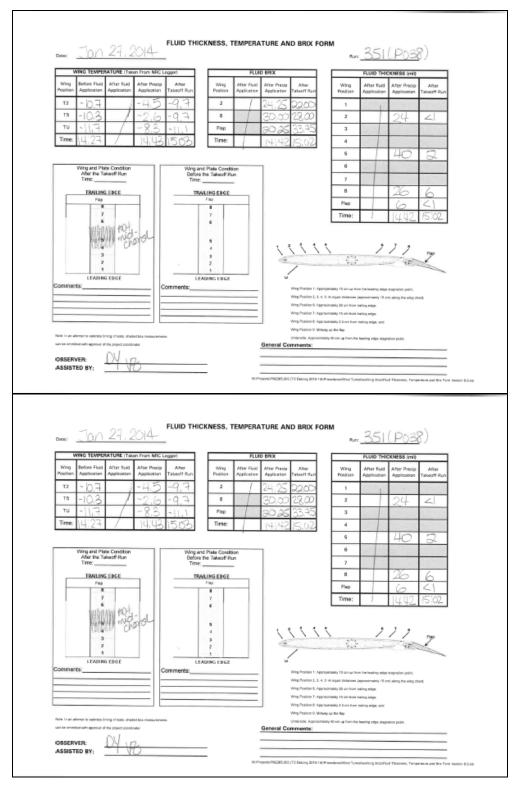


Figure C38: Test # 351

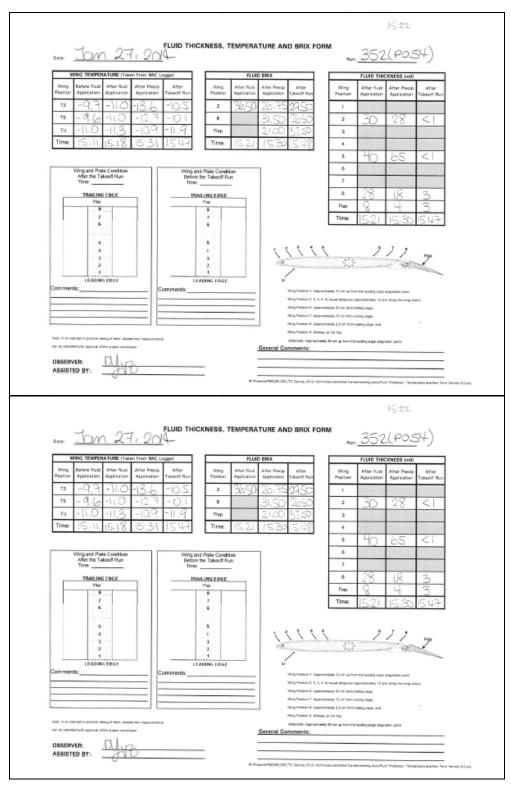


Figure C39: Test # 352

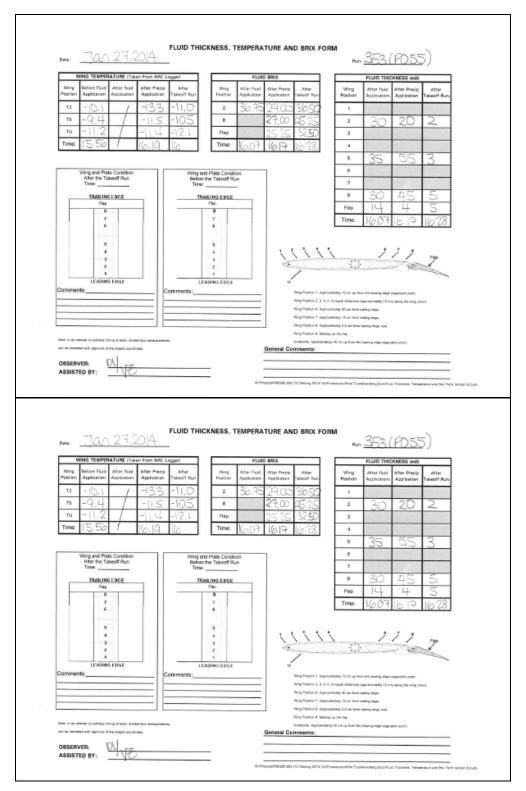


Figure C40: Test # 353

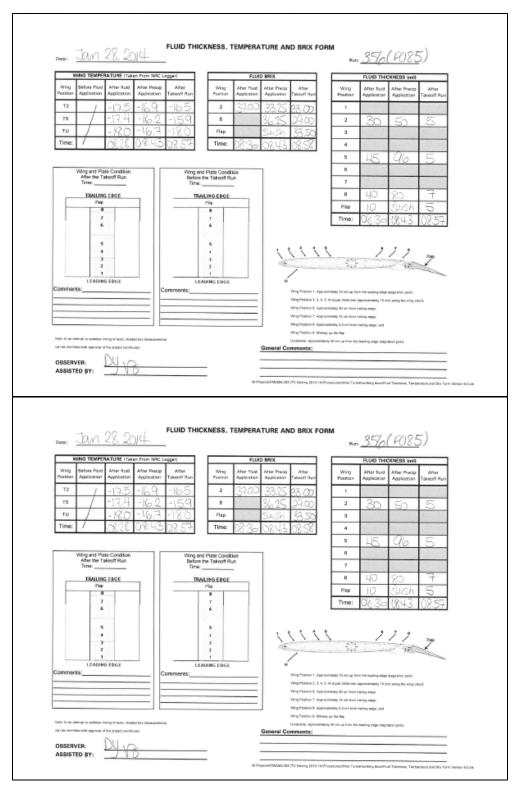


Figure C41: Test # 356

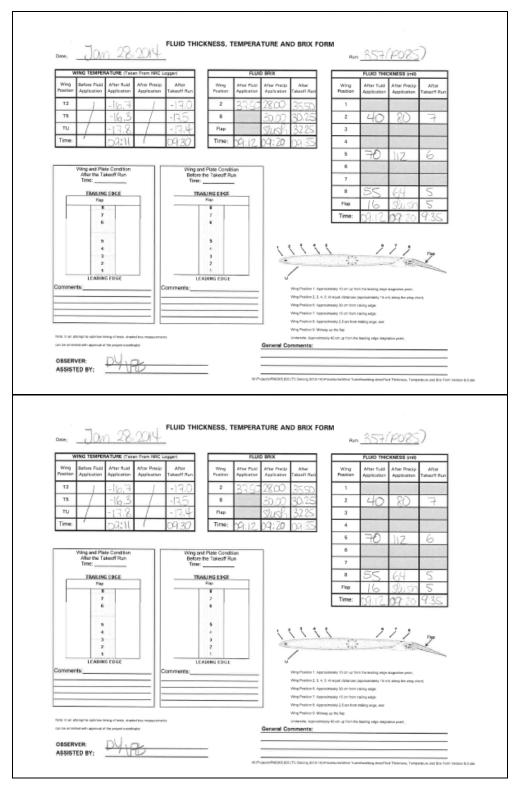


Figure C42: Test # 357

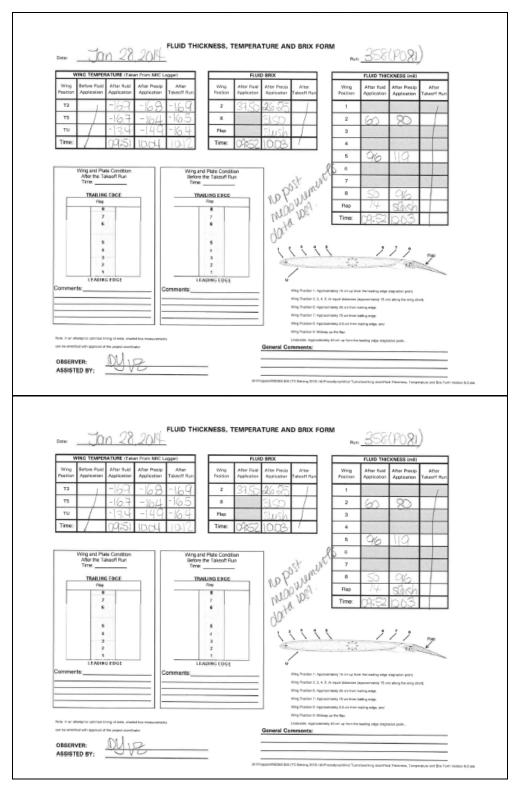


Figure C43: Test # 358

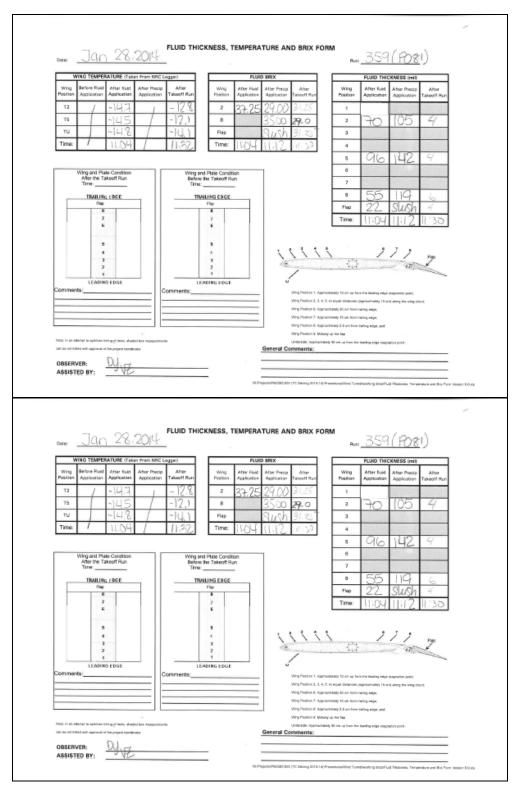


Figure C44: Test # 359

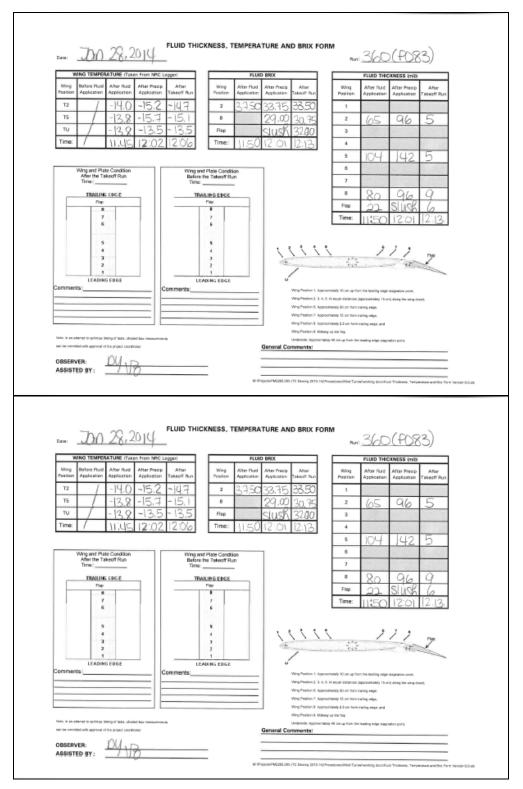


Figure C45: Test #360

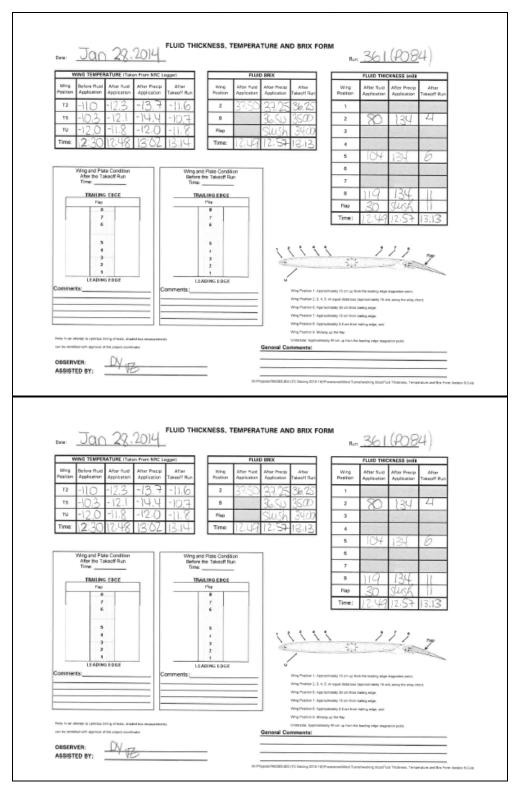


Figure C46: Test # 361

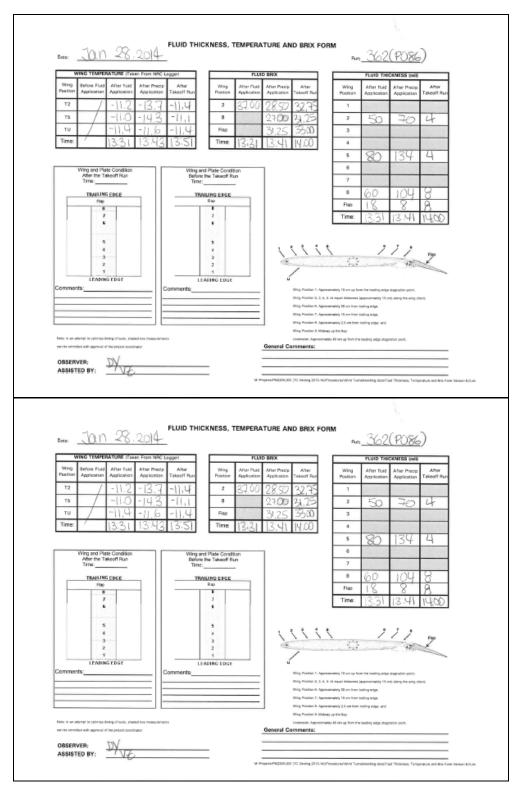


Figure C47: Test # 362

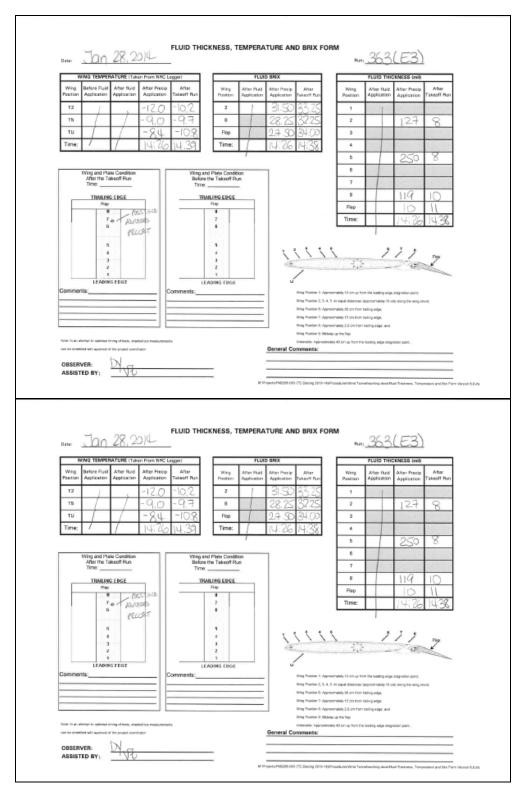


Figure C48: Test # 363

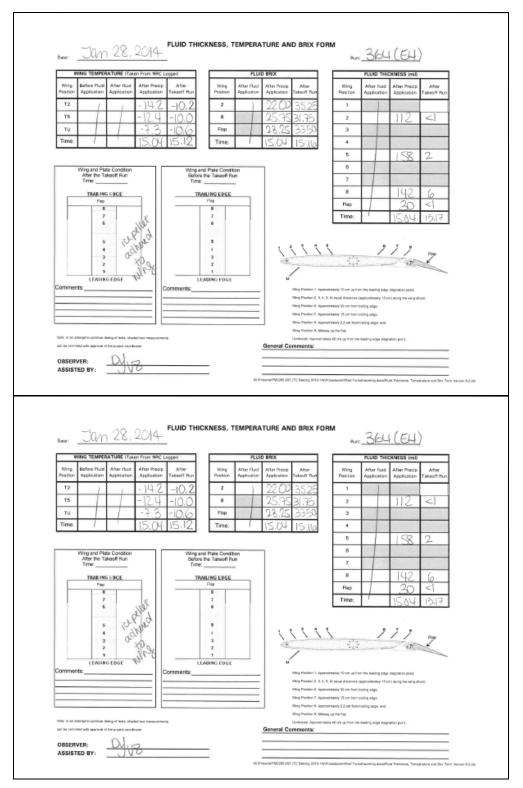


Figure C49: Test # 364

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