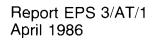
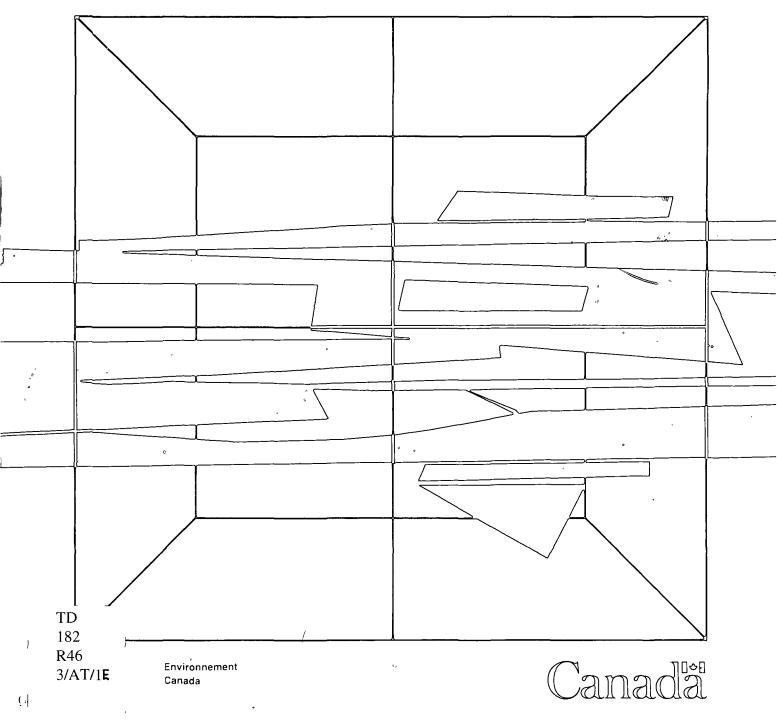
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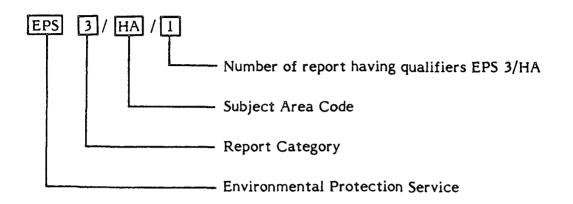
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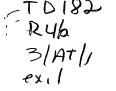
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DEVELOPMENT AND APPLICATIONS OF A MULTIPLE-BATCH LEACHING PROCEDURE

by

T.W. Constable and P.L. Côté Wastewater Technology Centre Environmental Protection Service Environment Canada

Report EPS 3/AT/1 April 1986

#### **READERS COMMENTS**

Readers who wish to comment on the content of this report should address their comments to:

T.W. Constable or P.L. Côté Environmental Protection Service Wastewater Technology Centre Canada Centre for Inland Waters P.O. Box 5050, 867 Lakeshore Road Burlington, Ontario L7R 4A6

#### ABSTRACT

Preliminary studies were conducted to determine the test conditions in a multiple-batch leaching procedure used to evaluate waste leachability. The results of applications of this procedure to a variety of wastes are described in this report. The leaching procedure comprised six batch extractions using three different leaching media (distilled water, an acidic solution buffered at pH 4.5, and a synthetic municipal landfill leachate) at two liquid-to-solid ratios (4:1 and 20:1). A wide range of leaching conditions was selected to simplify comparisons with the results of other leaching tests and to indicate potential changes in the leachability of a waste under different test conditions.

### RÉSUMÉ

1

Des études préalables ont été effectuées pour déterminer les conditions d'essai d'une méthode de lessivage par lots multiples permettant d'évaluer le rendement du lessivage de divers résidus. Le présent rapport décrit les résultats de l'application de cette méthode à ces résidus. La méthode de lessivage utilisée comprenait six extractions par lots réalisées avec trois agents de lessivage différents (de l'eau distillée, une solution acide tamponnée à pH 4,5, et le lessivat\* synthétique d'une décharge municipale), avec deux rapports liquide-solide différents (4/1 et 20/1). Une vaste gamme de conditions de lessivage a été retenue pour simplifier les comparaisons avec les résultats d'autres essais de lessivage et pour déterminer les variations possibles de la capacité de lessivage de divers types de résidus dans différentes conditions d'essai.

<sup>\*</sup> Dans le présent texte, le terme "lessivat" désigne le produit de lessivage.

TABLE OF CONTENTS

			Page
ABSTRAC	т		iii
RÉSUMÉ			iv
LIST OF F	IGUR	ES	vi
LIST OF T	ABLE	S	vii
CONCLUS	IONS	AND RECOMMENDATIONS	viii
1	INTE	RODUCTION	1
2	VAR	IATIONS IN EXISTING BATCH LEACHING TESTS	4
2.1 2.2 2.3 2.4 2.5 2.6 2.7	Liqui Time Num Surfa Agita	hing Medium id-to-Solid Ratio e of Elution ber of Elutions ace of Contact ation Techniques ble Preparation	4 8 8 10 11 11
3		ELOPMENT OF THE MULTIPLE-BATCH LEACHING CEDURE (MBLP)	12
3.1 3.2 3.2.1 3.2.2 3.2.3 3.2.4 3.2.5 3.3 3.4	Resu Expe Expe Expe Expe The I	uation of Leaching Test Conditions Its and Discussion riment 1: Agitation Methods riment 2: Screening riment 3: Time Release Patterns riment 4: Leaching Media riment 5: Liquid-Solid Separation Multiple-Batch Leaching Procedure parison with Other Leaching Tests	12 17 17 17 21 21 23 25 26
4	RESU	JLTS OF MBLP APPLICATIONS	28
4.1 4.1.1 4.1.2 4.1.3	The I The I Leac	rved Trends Effect of Leaching Medium on Leachate pH Effect of Liquid-to-Solid Ratio on Contaminant Release hability of Selected Priority Pollutants under Various	28 28 30
4.2	Test Sumr	Conditions nary	34 41
REFEREN	CES		43
APPENDI> APPENDI>		THE MULTIPLE-BATCH LEACHING PROCEDURE LEACHING TEST RESULTS	45 55

vi

### LIST OF FIGURES

Figure		Page
1	TYPES OF RELEASE IN LONG-TERM LEACHING TEST ON TALCONITE TAILINGS	9
2	COMPARISON OF AGITATION METHODS	15
3	TEMPORAL VARIATION OF pH AND COPPER CONCENTRATION IN EXPERIMENT 3	22
4	LEACHATE PH FOR THE THREE LEACHING MEDIA AT LIQUID-TO-SOLID RATIOS (R) OF 4:1 AND 20:1	31
5	RELATIVE FREQUENCY HISTOGRAMS OF THE RATIO OF CONTAMINANT RELEASE AT R = 20:1 TO THAT AT R = 4:1	33
6	CADMIUM CONCENTRATIONS AND RELEASES FOR SAMPLE 14	35
7	LEAD CONCENTRATIONS AND RELEASES FOR SAMPLES 13 AND 20	36
8	ZINC CONCENTRATIONS AND RELEASES FOR SAMPLES 14 AND 20	37
9	CYANIDE CONCENTRATIONS AND RELEASES FOR SAMPLE 14	38
10	CHROMIUM CONCENTRATIONS AND RELEASES FOR SAMPLES 2, 14 AND 15	39
11	COPPER CONCENTRATIONS AND RELEASES FOR SAMPLES 1, 15 AND 20	40

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vii

## LIST OF TABLES

Table		Page
1	SUMMARY OF EXISTING LEACHING TEST CONDITIONS	5
2	LEACHING MEDIA FOR VARIOUS TYPES OF LANDFILLS	6
3	CHEMICAL COMPOSITION OF LEACHING MEDIA	7
4	SUMMARY OF EXPERIMENTAL CONDITIONS	13
5	CHARACTERISTICS OF RAW SLUDGES	14
6	DESCRIPTION OF AGITATION METHODS	16
7	PARTICLE SIZE DEFINITION	16
8	RESPONSES OF THE 2 <sup>5</sup> FACTORIAL DESIGN SCREENING EXPERIMENT	18
9	COEFFICIENTS FROM A REGRESSION ANALYSIS OF THE SCREENING EXPERIMENT	20
10	RESULTS OF THE LEACHING MEDIA COMPARISON	22
11	RESPONSES OF THE 2 <sup>3</sup> FACTORIAL DESIGN LIQUID-SOLID SEPARATION EXPERIMENT	24
12	COEFFICIENTS FROM REGRESSION ANALYSIS OF THE LIQUID-SOLID SEPARATION EXPERIMENT	24
13	PERCENT OF COPPER IN LEACHATE THAT WAS ORIGINALLY PRESENT IN THE FREE LIQUID PORTION OF THE SLUDGE	25
14	IDENTIFICATION OF THE SIX EXTRACTIONS USED IN THE MULTIPLE-BATCH LEACHING PROCEDURE	26
15	SAMPLES SUBJECTED TO THE MULTIPLE-BATCH LEACHING PROCEDURE	29



#### CONCLUSIONS AND RECOMMENDATIONS

#### Conclusions

- Most agitation methods used in existing batch leach tests either fail to provide good liquid-solid contact or are too severe and cause fragmentation of the solid particles. Slow rotation (2 to 3 rpm) of a square bottle laid on its side was found to be a satisfactory method of mixing.
- 2. A mixing time of 24 hours appears to be sufficient for equilibrium to be reached between most wastes and leaching solutions.
- 3. When a waste is leached with distilled water, the equilibrium pH of the leachate is controlled by the alkalinity or acidity of the waste. When a waste is leached with an acidic solution, leachate pH is a function of both the buffering capacity of the waste and the amount of acid available in the leaching medium to react with the waste.
- 4. Increasing the liquid-to-solid ratio when distilled water is used as the leaching medium has little effect on the equilibrium pH of a leachate. Differences in contaminant concentrations at the higher liquid-to-solid ratio are frequently due to dilution.
- 5. Increasing the liquid-to-solid ratio when an acidic solution is used as the leaching medium increases the amount of acid contacting the waste and shifts the equilibrium pH towards the pH of the leaching medium. This can increase or decrease contaminant release depending on the direction of the pH shift and the nature of the contaminants.
- 6. For some contaminants and wastes, good correlations exist between the logarithm of release and final leachate pH, and between the logarithm of release and the amount of acid in the leaching medium. The lack of correlation in some cases appears to be partially due to the apparent ability of the synthetic municipal landfill leachate to complex some contaminants and to increase their release above that to be expected from pH-solubility considerations alone.
- 7. The results of the Multiple-Batch Leaching Procedure (MBLP) are useful for comparing the leachability of various wastes under the same test conditions, but cannot be used to predict the long-term leachability of these wastes in field disposal situations.

#### Recommendations

- 1. The three batch extractions at the 4:1 liquid-to-solid ratio should be excluded from future applications of the MBLP, as they frequently add only marginally more information about waste leachability than do the 20:1 extractions.
- 2. For wastes where codisposal with municipal refuse is not an option, the extraction with the synthetic municipal landfill leachate should be omitted.
- 3. The MBLP (with the modifications noted above) should be used in future leaching studies as a prescreening test to provide information on the leachability of a waste relative to other wastes under the same test conditions.

#### 1 INTRODUCTION

Considering the large quantity and variety of industrial wastes that are now being produced, and the large number of widely distributed production sources and disposal sites, it is obvious that a case by case field evaluation of the hazards associated with the disposal of specific wastes in specific landfill sites is impossible. Nevertheless, the potential for environmental contamination dictates that some type of methodology must be used to assess the possible extent of contaminant release in a field disposal situation. This methodology has traditionally been in the form of bench-scale laboratory leaching tests.

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Leaching tests can be conducted for several different purposes. For example, they might be used to determine if a waste is hazardous, to measure the efficiency of a stabilization technique, or to characterize the leachate produced from a waste (for evaluating the potential for groundwater contamination or designing a leachate treatment system). In general, there are two approaches to leaching studies. The choice of the approach to be used depends on the purpose of the test.

In the first approach, a standard test is adopted which allows results between different laboratories to be compared on a common basis and provides a uniform criterion for the evaluation of different wastes. The standard test also permits development of a data base for comparison of laboratory and field data. A precise protocol is used for all wastes irrespective of the disposal situation and all wastes are treated on the same basis. This protocol must be precisely defined and yield reproducible results, and should be rapid, inexpensive, and universally applicable. One example of a standard test is the EPA Extraction Procedure which is used as part of the protocol to classify hazardous wastes (U.S. EPA, 1980).

In the second approach, the test conditions are made as site specific as possible. This approach attempts to evaluate the hazardousness of a waste in the context of an actual field disposal situation. As a result, decisions based on a site specific test are more conclusive than those arising from a standard test. The site specific test, however, is more time consuming and costly, and does not allow for the establishment of a data base or for the comparison of different wastes on the same basis.

A leaching test can be used, therefore, for either waste classification or leachate quality prediction. When a test is used for classification of a waste (e.g., hazardous or non-hazardous), a standard methodology is appropriate since it allows comparison among laboratories and ensures better reproducibility of the results. When a test is used for predicting the quality of the leachate in a field disposal situation, the major concern is to make the test conditions as site specific as possible.

A multitude of leaching test protocols have been proposed, however, there is no uniformity over the test conditions and no general agreement over the adoption of a standard protocol (Lowenback, 1978). There are also many important environmental conditions present in a field disposal situation which cannot be routinely reproduced in a laboratory. The inability to reproduce these conditions is principally due to temporal differences between the two leaching situations. For convenience, many investigators frequently attempt to condense several years of leaching into a short period of time by using a high liquid-to-solid ratio. This temporal contraction precludes reproduction of the kinetics of pollutant release in a landfill, and necessitates neglect of those factors which are time-dependent in a field leaching situation, such as microbial activity, temperature variations and possible interactions among wastes. These limitations of laboratory leaching tests should be recognized and taken into account in the interpretation of results.

Leaching tests can generally be classified as column tests or batch tests. In the former, the waste is placed in a column and an appropriate leaching medium passed through it. Soil attenuation can be modelled by adding a layer of soil at the bottom of the column. Batch tests consist of agitating a waste sample with a predefined quantity of liquid for a specified time. More than one elution can be performed, and either the waste or liquid is replaced at each elution in order to obtain information on the maximum concentration or the maximum release of contaminants, respectively. Although column tests are often considered to be more representative of field conditions than batch, they have been criticized because their duration can range from weeks to months and the results are often difficult to reproduce. The latter problem may arise from channeling, non-uniform packing of the waste, clogging, and biological growth. Batch tests are comparatively rapid and simpler to perform. The results are more reproducible than those from columns since test conditions can be closely controlled over a relatively short period of time. Consequently, most of the recent development work on leaching tests has been done by batch testing.

In 1980, a study was undertaken at the Wastewater Technology Centre (WTC), Burlington, Ontario, to investigate various aspects of batch leaching (Côté and Constable, 1981, 1982, 1983). After a literature review, those conditions that needed further consideration were identified and a series of experiments were performed to examine the effect of various test conditions on contaminant release from wastes. The results were subsequently used as the basis for a batch leaching protocol which is referred to herein as the Multiple-Batch Leaching Procedure (MBLP). The MBLP comprises six batch extractions using three different leaching media at two liquid-to-solid ratios. A wide range of test conditions was selected to simplify comparisons with the results of other leaching tests, and to indicate potential changes in the leachability of a waste under different test conditions.

The Multiple-Batch Leaching Procedure has been applied to various wastes from across Canada to establish a standardized data base on waste leachability. The data base allows comparisons to be made on the leachability of different wastes under the same test conditions and assists in the comparison of results from other leaching protocols including those proposed by ASTM (1979) and the U.S. EPA (1980).

This report describes the preliminary studies that were conducted to determine the six extraction conditions used in the Multiple-Batch Leaching Procedure, and presents the results of applications of the MBLP to a variety of wastes.

2

#### VARIATIONS IN EXISTING BATCH LEACHING TESTS

A partial survey of batch leaching tests was done by the U.S. EPA (Lowenbach, 1978). Thirty existing tests representing a large range of test conditions were considered (Table 1). The test conditions and procedures were found to frequently originate from the availability of laboratory material (e.g., shaker, bottles) and from the type of waste being tested. Many tests were developed by modifying an existing procedure to suit particular needs.

#### 2.1 Leaching Medium

The choice of a leaching medium should be dictated by expected landfill conditions and by the type of chemical species to be leached from the waste. For example, most metals will be solubilized by an acidic solution, whereas organic chemicals will leach more readily under basic conditions.

Ham et al. (1979a) identified three landfill situations that could represent extremes in leaching medium composition (Table 2). When waste is landfilled by itself with relatively small amounts of other wastes, the leaching media will consist of rainwater (after passing through the cover layer of soil) in the top layers of waste, and of leachate produced from the waste in the bottom layers. If the waste is co-disposed with municipal refuse, the leaching medium can have the characteristics of municipal refuse sanitary landfill leachate. If the waste is co-disposed with other industrial wastes, the composition of the leaching medium can vary considerably. Depending on the landfill situation, therefore, the appropriate leaching medium may range in composition from a synthetic leachate modeled on actively decomposing municipal sanitary landfill leachate to something approaching distilled water.

One way of accounting for these large variations is to consider the aggressiveness of a leaching medium, which refers its ability to extract chemical constituents from a waste. A non-aggressive leaching medium such as distilled water allows the waste to create its own leaching environment, whereas a strong chemical solution or synthetic leachate essentially controls the leaching environment. For example, a waste containing small amounts of a leachable basic salt will raise the pH of a distilled water leachate, and only materials that are soluble in basic solutions will be found in the leachate. Conversely, use of a heavily buffered acid solution will probably neutralize the basic salt while maintaining an acidic pH. In the first case the waste controls the pH of the solution, while in the second case, the leaching medium is the controlling factor.

#### TABLE 1 SUMMARY OF EXISTING LEACHING TEST CONDITIONS

Leaching Media (Typical: distilled water)

- water (distilled, deionized, rain)
  - water adjusted for pH (with different buffering capacities)
- site specific liquid
- synthetic municipal landfill leachate
- bacterial nutrient media

Liquid/Solid Ratio (Typical: 10:1)

• 1:1 to 500:1

Time per Elution (Typical: 24 hours)

• 1/2 hour to 28 days

Number of Elutions (Typical: 1)

• 1 to 10

Solid Preparation (Typical: as received)

- as received
- crushed and sieved
- dried
- vacuum filtered (0.45 µm)

Size of the Solid Sample (Typical: 100 g)

1 to 500 g

Agitation Technique (Typical: shaking)

- none
- stirring
- shaking: reciprocating, circular, wrist action
- gas bubbling

Temperature (Typical: room)

20°C to 33°C

## TABLE 2LEACHING MEDIA FOR VARIOUS TYPES OF LANDFILLS (Ham et al.,<br/>1979a)

Representative Landfill Situation	Leaching Solution
Monolandfill	Distilled, deionized water or leachate produced from the waste itself.
Sanitary landfill	Municipal refuse sanitary landfill leachate.
Industrial landfill	Leachate based on the characteristics of the wastes in the landfill.

Several characteristics of the leaching medium contribute to its aggressiveness, including:

- <u>pH</u>: The value of the pH and the buffering capacity that maintains that value are both important. Most leaching media encountered in the environment are acidic. The pH of rain falling in Ontario varies between 4.0 and 6.0 and is controlled by the nitrate, sulphate and carbonate systems. Leachate in an actively decomposing sanitary landfill can reach pH values of 4.0 to 4.5, and be heavily buffered by volatile acids (Stanforth et al., 1979).
- 2) <u>Redox Potential</u>: Redox potential is a measure of the oxidizing and/or reducing intensity of a system. It determines, in part, the aerobic or anaerobic conditions under which the material will be leached. Redox reactions are important in the solubilization of iron and manganese. In a landfill, bacterial activity plays a major role in controlling redox potential.
- 3) <u>Complexation Capacity</u>: Complexation is defined as the formation of a complex from a metal ion with a negative ion. Many different ligands, both organic and inorganic, can complex metals and leach them from wastes. Organic compounds containing nitrogen, oxygen or sulphur in the proper configuration can be very strong complexers.
- 4) <u>Ionic Strength</u>: Ionic strength may affect the leaching of materials in three ways:
   1) by increasing the solubility through lowered activity coefficients, 2) by ion exchange processes that replace an ion bound to an ion exchange site with one of the more predominant ions in solution, and 3) by decreasing the size of the double layer around colloidal particles and promoting coagulation.

Not all of these aggressive properties are of equal importance with respect to leaching chemical species from a waste. Synthetic leaching media have been developed that attempt to model one or more of these aggressive properties. For example, synthetic landfill leaching media were developed by researchers at the University of Wisconsin to model co-disposal of a waste in a municipal landfill site (Stanforth et al., 1979). The main advantage of using a synthetic leaching medium is a more realistic representation of the leaching conditions likely to be encountered in a field disposal situation. It may also be argued that, in a short test, it is better to use an aggressive medium that will control the leaching environment. The disadvantages include the increased laboratory work involved, the possible introduction of chemical impurities that could interfere with the results of the test, and the toxicity of the leaching medium of fish, thus preventing the use of bioassays. The chemical compositions of several leaching media are given in Table 3.

Le	aching Medium	Mnemonic	Chemicals	Concentrations (M)
1.	Distilled water	DW		
2.	Acidic solution (ASTM, 1979)	AS1	Acetic acid Sodium acetate	0.082 0.045
3.	Acidic solution (based on maximum acidity provided by Extraction Procedure (U.S. EPA, 1980))	AS2	Acetic acid Sodium acetate	0.20 0.11
4.	Synthetic leachate, anaerobic (Stanforth et al., 1979)	SL1	Acetic acid Sodium acetate Glycine Pyrogallol Ferrous sulphate	0.15 0.15 0.05 0.008 0.024
5.	Synthetic leachate, aerobic (Stanforth et al., 1979)	SL2	Acetic acid Sodium acetate Glycine Salicylic acid	0.15 0.15 0.05 0.007
6.	Synthetic leachate (Anon., 1977)	SL3	Acetic acid Proprionic acid Butyric acid Valeric acid Magnesium acetate Potassium sulphate Calcium chloride Ammonium chloride	0.066 0.041 0.114 0.029 0.033 0.016 0.050 0.103

#### 2.2 Liquid-to-Solid Ratio

The liquid-to-solid ratio (R) used in batch tests can vary from 1:1 to 500:1, with a typical test using a ratio of 10:1. 'R' values reported in the literature, however, are difficult to compare because of the different interpretations given to the determination of the liquid portion of a waste, and the role of that portion in the ratio.

There are six possible ways of defining R. The liquid portion of a waste sample can be defined as the difference between the wet and dry weights of the sample, or as the amount of water separable by filtration. Furthermore, the liquid portion, however determined, can be considered in the ratio to be (1) part of the waste, (2) part of the leaching medium, or (3) part of neither, as expressed in the following equations:

$$R = \frac{L}{W+S}$$
(1)

$$R = \frac{L+W}{s}$$
(2)

$$R = \frac{L}{S}$$
(3)

where: L = liquid added as leaching medium

W = liquid portion of the waste (which may be interpreted in two different ways)

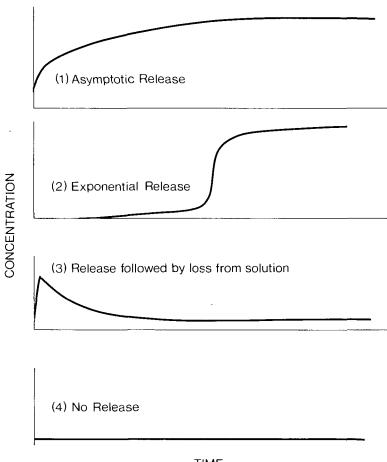
R = solid portion of the waste (complement of the liquid portion)

In the case where a waste contains a significant amount of liquid (e.g., a wastewater treatment sludge), the method used to compute R may have a significant effect on test results. This effect will become less significant as the value selected for R increases.

Selection of a suitable value for R is influenced by practical considerations, such as the availability of a proper agitation apparatus and the volume of leachate required for analysis. The ratio should be high enough to prevent limiting contaminant release into the leaching medium because of solubility constraints, yet small enough to provide concentrations that are above the detection limit of the analytical apparatus. A review of existing tests suggests that a ratio between 4:1 and 20:1 would satisfy these conditions.

#### 2.3 Time of Elution

The concentration of a chemical species in the leaching medium is a function of the time of elution up to the time where equilibrium is reached. Lee and Plumb (1974) found four release patterns in a 500-day leaching study using taconite tailings (Figure 1).



TIME

Types of release patterns

### Examples 1) specific conductance, alkalinity, Ca, Mg, and others

- 2) silica (a slow hydrolysis step needed before Si is solubilized)
- 3) Cu, Zn-loss due either to rising pH in solution, or absorption back onto solids
- 4) several species
- FIGURE 1 TYPES OF RELEASE IN LONG-TERM LEACHING TEST ON TALCONITE TAILINGS (Lee and Plum, 1974)

Not only did equilibration times for different parameters vary widely, but for some parameters a series of reactions occurred which produced concentration maxima with subsequent concentration decreases. The variety of release patterns found indicated that no one time of elution is best for all wastes. The results also showed that a time of elution on the order of hours (as opposed to days) should be sufficient to allow most leachable contaminants to approach equilibrium in the leachate.

The choice of an appropriate time of elution is often dictated by practical considerations. It should be long enough to allow rapidly dissolving species to approach equilibrium. A very short test (e.g., less than 2 hours) is not suitable because of the variability in the results induced by laboratory manipulations. The leaching medium and the waste are in contact before and after the agitation period for a certain length of time which depends on the number of test bottles and on the skill of the technician. This period of time can range from a few minutes to an hour; it should not be of the same order as the time of elution. The time of elution should also be convenient to personnel. If multiple elutions are needed, the time of elution should be compatible with working schedules. A practical time of elution would thus seem to be some multiple of one day; many leaching tests use 24 hours.

#### 2.4 Number of Elutions

Performing multiple elutions by replacing either the solid or liquid phase can be done in order to get an indication of the dynamics of the leaching process. Successive elutions can reveal the release pattern of a contaminant over time, and often can give an idea of the factors affecting its release. Successive elutions are particularly important when the release of one contaminant is inhibited by the release of another. For example, trace metals will not be leached from a waste with some acid neutralization capacity until this capacity has been expended by the leaching medium. If the test is ended before this occurs, the potential for trace metal leaching will be overlooked.

When the waste is replaced in successive elutions, information will be generated on the maximum concentration of species in solution. If the liquid is replaced in successive elutions, the maximum release of chemical species under test conditions can be evaluated. The results can be expressed as the ratio of mass of contaminant leached to mass originally present in the waste.

#### 2.5 Surface of Contact

The particle size of the waste controls the surface of contact between the waste and the leaching medium. The surface of contact should not affect the equilibrium concentrations of chemical species in leachate, although it may have profound effects on the kinetics of release. The importance of this factor is determined by the permeability of the waste and test conditions such as the agitation method and the time of elution. Three processes may limit the rate of dissolution of a species: 1) the rate of chemical reaction at the liquid-solid interface, 2) the diffusion of products away from the surface, and 3) the renewal of the species at the liquid-solid interface by diffusion through the waste. If condition 1 or 3 is the dissolution controlling factor, the ratio of the surface of contact to the volume of the waste then becomes most important.

#### 2.6 Agitation Techniques

The agitation method is important because it determines the degree of contact between the leaching medium and the waste. Existing methods include stirring, shaking or bubbling gas through the test bottle. An efficient agitation method must meet the following conditions: 1) the entire surface area of the waste must be contacted with the leaching medium, 2) the mixing technique must prevent stratification in the test bottle, and 3) the physical structure of the waste must be preserved.

The first condition eliminates the commonly used shaking techniques (e.g., reciprocating shaker and wrist action shaker where the waste remains on the bottom of a bottle and the liquid is agitated over it. It is possible to increase shaking speed to ensure good contact but this may result in violation of the third condition.

#### 2.7 Sample Preparation

A leaching test, in order to be reproducible and widely applicable, should include a sample preparation protocol. This should provide guidance for representative sampling, liquid-solid separation and particle size reduction of monolithic wastes. The need for a liquid-solid separation step before a leaching test depends on the method selected to compute the liquid-to-solid ratio and on the reason for conducting the test. If the purpose of the test is classification of wastes, liquid-solid separation can be performed to improve reproducibility. On the other hand, if the test is to be used to predict leachate quality in a landfill, the liquid portion can be considered to be an integral part of the waste and liquid-solid separation should not be performed.

#### 3 DEVELOPMENT OF THE MULTIPLE-BATCH LEACHING PROCEDURE (MBLP)

#### 3.1 Evaluation of Leaching Test Conditions

A series of five experiments was conducted at the WTC to measure the sensitivity of batch leaching test variables on the release of contaminants from wastes. The results of the experiments were then used to select a set of test conditions that would maximize test reproducibility and sensitivity, and also provide information for a wide range of leaching situations. The five experiments examined the effects of the following on contaminant release:

- 1) nine different methods for agitation;
- a 2<sup>5</sup> factorial screening experiment on five test conditions leaching medium, liquid-to-solid ratio, particle size, time of elution, and number of elutions;
- two different leaching media monitored during a 24-hour leaching period to evaluate the kinetics of release;
- 4) six different leaching media; and
- 5) liquid-solid separation of a waste sample prior to leaching.

A summary of the test conditions used in each experiment is given in Table 4. Two inorganic sludges were used (Row 1), a Basic Oxygen Furnace (BOF) sludge from a steel industry (Experiment 1), and a metal hydroxide (MH) sludge from a metal finishing industry (the other four experiments). In Experiments 2, 3 and 4, the MH sludge was solidified prior to leaching using 20 percent Portland cement and 5 percent lime in order to ensure particle size control. The solidified sludge was air cured for 28 days, then crushed and sieved to the required particle size. The characteristics of the raw sludges are presented in Table 5.

The agitation techniques used in each experiment are indicated in Row 2 of Table 4. Nine different techniques were considered in the first experiment. These techniques are depicted graphically in the first column of Figure 2, and described in Table 6. They included a wrist action shaker (A in Figure 2), a reciprocating shaker at two speeds with two bottle sizes (B, C and D), a circular shaker at two speeds with square and round bottles (E, F and G), a tumbler (H) and a stirrer(I). Based on the results of Experiment 1, the tumbler agitation method (H) was selected for use in subsequent experiments. In this method, the liquid-solid mixture is rotated slowly (2 to 3 rpm) in square bottles so that the waste gently tumbles through the liquid.

			E	Experiment	8	
Conditions		1) Agitation Methods	2) 25 Factorial	3) Time Release Pattern	4) Leaching Media	5) Liquid- solid Separation
1)	Sludge*	BOF	мн <sub>s</sub>	МН <sub>S</sub>	MH <sub>s</sub>	МН
2)	Agitation method	9 different + control	tumbler	tumbler	tumbler	tumbler
3)	Leaching medium**	AS1	AS1 (-1)*** DW(+1)	AS1 DW	DW, AS1 AS2, SL1 SL2, SL3	AS1 (-1) DW(+1)
4)	Liquid-to- solid ratio	10:1	4:1 (-1) 10:1 (+1)	10:1	10:1	4:1 (-1) 20:1 (+1)
5)	Particle size (cm)	1.1	0.34 (-1) 2.2 (+1)	0.34	0.34	
6)	Time of elution (h)	24	24 (-1) 48 (+1)	0.5,1,2, 4,8,24	24	24
7)	Number of elutions	1	1 (-1) 2 (+1)	1	1	1
8)	Number of replicates	3	2	1	2	2
9)	Measured parameters****	Ca,Mg	Cr,Cu,Mg	Cr,Cu,Mg	TOC,Cr, Cu,Mg,Zn	Cu <b>,</b> Mg

#### TABLE 4 SUMMARY OF EXPERIMENTAL CONDITIONS

 BOF = basic oxygen furnace sludge; MH = metal hydroxide sludge; MH<sub>s</sub> = solidified metal hydroxide sludge

\*\* DW = distilled water; AS1, AS2 = acidic solutions; SL1, SL2, SL3 = synthetic leaching media

\*\*\* the -1 and +1 indicate the two settings of each parameter in the level 2 factorial experiments

\*\*\*\*pH and conductivity were also measured in every experiment

Row 3 of Table 4 lists the leaching media used in the experiments. Distilled water and one of two acidic solutions were used in most of the experiments. The first acidic solution had a pH of 4.5, and was buffered to 82 meq of acid per litre by the addition of acetic acid and sodium acetate (ASTM, 1979). The second solution had a larger buffering capacity (200 meq/L), and was prepared to provide the same amount of acidity as the EPA Extraction Procedure (U.S. EPA, 1980) when the maximum amount of acid is added. Six different leaching media were used in Experiment 4, including distilled

Parameters	BOF sludge µg/g	e* %	MH sludge** µg/g	%
Moisture content		37.3	- <u></u>	84.8
Fixed residues at 550°C		97.3		81.2
Total carbon		10.6		1.5
Total organic carbon		8.9		1.2
Metals Al	2100		570	
Ca		12.3		7.6
Cd	0.8		44	
Cr	230			7.7
Cu	200			22.3
Fe		45.8		1.2
Mg		2.3		1.7
Mn	8400		200	
Ni	65		110	
Pb	230		2600	
Zn	8400			6.3

#### TABLE 5 CHARACTERISTICS OF RAW SLUDGES

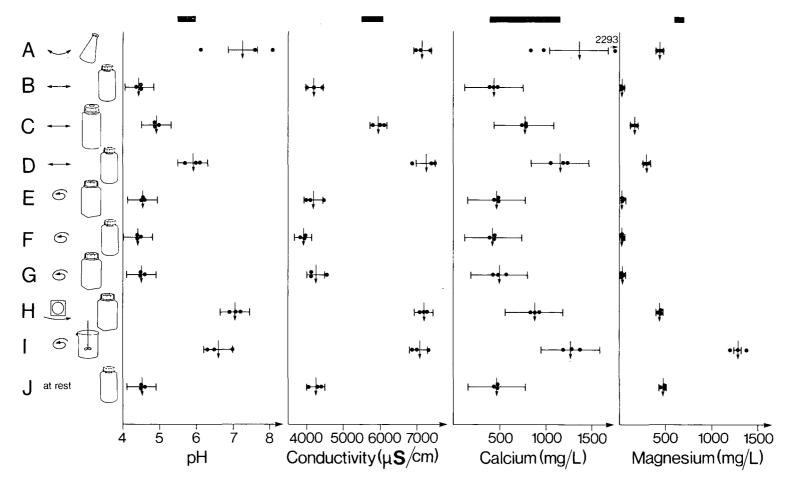
\* Basic Oxygen Furnace sludge: average of 2 analyses

\*\* Metal Hydroxide sludge: average of 3 analyses

water, the two acidic solutions, and three synthetic leachates (Stanforth et al., 1979; Anon., 1977). The chemical compositions of the media are given in Table 3. All six leaching media were analyzed for Cr, Cu, Mg and Zn. All metal concentrations were below the detection limit except for Mg in the Netherlands synthetic leachate (Anon., 1977). Leaching tests were conducted at liquid-to-solid ratios of 4:1, 10:1 and 20:1 (Row 4). The ratios were computed using Equation 3 (Section 2.2) in the first four experiments, and Equation 1 in Experiment 5.

The sizes (diameters) of the particles used in the first four experiments are indicated in Row 5 of Table 4. The waste was passed through two different sieves and the particles retained on the bottom sieve were used in the experiments (Table 7). The diameters given in Row 5 (Table 4) are the geometric mean of the two sieve sizes used to segregate the particles. Particle size segregation was not performed in Experiment 5.

- Experimental measurement
- Mean of three measurements
- → 95% confidence interval for the mean (Student's t distribution)
  - Minimum difference between means for significance (95% confidence) according to Tukey's paired comparison procedure.



### FIGURE 2 COMPARISON OF AGITATION METHODS

Method	Agitation Apparatus	Speed	Bottle Type
A	Wrist Action	l on a 0 to 10 scale	1L Erlenmeyer
В	Reciprocating	65 excursions/min	1L round
С	Reciprocating	65 excursions/min	1.75 L round
D	Reciprocating	130 excursions/min	1L round
E	Circular	60 <b>r</b> pm	1L square
F	Circular	80 rpm	1L round
G	Circular	80 rpm	1L square
Н	Tumbler	2.5 rpm	0.5 to 1.0 L square
I	Stirrer	60 rpm	1.75 L beaker
J	Control*		1L round

#### TABLE 6DESCRIPTION OF AGITATION METHODS

\* The control was limited to one minute of shaking by hand at the beginning and end of the 24-hour elution period.

Nominal Particle Size	Sieve Sizes		Calculated Area per Unit Volume*	
(cm)	Small (cm)	Large (cm)	(cm <sup>-1</sup> )	
0.34	0.238	0.475	0.36	
1.1	0.475	2.57	3.80	
2.2	1.9	2.54	15.2	

#### TABLE 7PARTICLE SIZE DEFINITION

\* assuming each particle is a spheriod

The time of elution in most experiments was 24 hours (Row 6, Table 4). Experiment 2 also used an elution time of 48 hours, and Experiment 3 used times ranging from 0.5 to 24 hours.

Only one elution was performed in most of the experiments (Row 7, Table 4). A second elution was used in Experiment 2 to compare contaminant release during the first and second contacts of a waste with equal amounts of fresh leaching medium. Replicates were performed in most of the experiments to estimate error variance and evaluate the statistical significance of the results (Row 8, Table 4).

The parameters measured in the filtered (0.45  $\mu$ m) leachates from each experiment are listed in Row 9 (Table 4).

#### 3.2 Results and Discussions

**3.2.1 Experiment 1: Agitation Methods.** The first experiment was conducted to find a suitable agitation technique for use in all subsequent experiments. Nine agitation methods were evaluated on their ability to satisfy the three conditions listed in Section 2.6, their reproducibility (triplicates were run), and the difference between their results and those of a control ('J' in Table 6). The control was not agitated except for one minute of shaking by hand at the beginning and end of the 24-hour elution period.

The results for four of the parameters measured in each leachate (pH, conductivity, Ca and Mg) are shown in Figure 2. Comparisons of the range of triplicate measurements for each parameter and of the differences between the results obtained from each technique and from the control show that some agitation methods are more reproducible and aggressive than others.

The methods that gave results different from those of the control for most parameters were A, D, H and I. Methods A, D and I, however, were deemed unacceptable because agitation was too severe and caused fragmentation of the waste particles. Method H, a tumbler, was judged to best meet the criteria established for an acceptable agitation method, and was used in all subsequent experiments.

Further work using the tumbler has shown that results are reproducible irrespective of bottle size or liquid level, as long as a square bottle is used. A square bottle allows the waste particles to gently tumble through the leaching medium, providing good liquid-solid contact without particle fragmentation.

**3.2.2 Experiment 2:** Screening. After determination of a suitable agitation technique, a replicated 2<sup>5</sup> factorial experiment was performed to examine the effect of five other test conditions on contaminant release: leaching medium (L), liquid-to-solid ratio (R), particle size (P), time of elution (T) and number of elutions (N). The two levels considered for each test condition were selected to be representative of the typical range of variation encountered in existing leaching tests, and are given in Table 4.

The response measured at each of the experimental settings are given in Table 8. These responses were analyzed using least-squares regression. The 32 (i.e.,  $2^5$ ) pieces of information generated were the average, 5 main effects, 10 two-factor

Variables L R P T N	Treatment Combination	рН	Conductivity (mS/cm)	Chromium (mg/L)	Copper (mg/L)	Magnesium (mg/L)
	1	9.85	11.00	8.10	1.090	2.60
+	1	10.70	9.30	12.50	1.910	0.25
- +	r	9.00	9.25	3.00	0.435	34.0
+ +	lr	10.45	5.15	6.45	0.975	0.30
+	р	9.30	10.70	6.70	0.860	7.10
+ - +	lp	10.50	8.75	11.50	1.705	0.25
- + +	rp	8.05	8.50	3.40	0.275	59.0
+ + +	lrp	10.65	4.95	5.45	0.765	0.15
+ -	t	9.80	11.35	8.05	1.260	3.70
+ + -	lt	10.90	8.40	10.00	1.815	0.10
- + - + -	rt	9.30	9.80	3.30	0.495	46.0
+ + - + -	lrt	10.60	5.00	6.90	0.875	0.20
++-	pt	9.80	11.45	6.70	0.995	6.10
+ - + + -	lpt	10.75	7.75	11.50	1.450	0.40
- + + + -	rpt	8.85	8.30	3.80	0.460	56.5
+ + + + -	lrpt	10.90	4.60	5.40	0.780	0.10
+	n	9.30	8.50	2.95	0.390	25.0
+ +	ln	10.65	4.90	5.85	0.795	0.20
- + +	rn	8.50	8.30	1.25	0.175	143.
+ + +	lrn	10.35	1.65	2.10	0.225	0.25
+ - +	pn	8.55	8.35	2.30	0.265	58.5
+ - + - +	lpn	10.60	4.00	5.30	0.585	0.20
- + + - +	rpn	7.25	7.50	0.95	0.625	111.
+ + + - +	lrpn	10.50	1.60	1.85	0.155	0.15
<b></b> ++	tn	9.35	8.75	3.05	0.425	27.0
+ + +	ltn	10.80	4.65	6.00	0.785	0.10
- + - + +	rtn	8.50	8.50	1.30	0.185	173.
+ + - + +	lrtn	10.45	1.80	2.45	0.210	0.25
+++	ptn	8.95	9.15	2.35	0.295	50.5
+ - + + +	lptn	10.70	3.65	5.60	0.490	0.15
- + + + +	rptn	7.85	7.50	1.20	0.145	123.
+ + + + +	lrptn	10.65	1.45	1.80	0.175	0.10
Error Variance* 0.004		0.0049	0.0028	0.068	0.0039	8.747

# TABLE 8RESPONSES OF THE 25 FACTORIAL DESIGN SCREENING<br/>EXPERIMENT

\*52 degrees of freedom

interaction effects, 10 three-factor interaction effects, 5 four-factor interaction effects, and 1 five-factor interaction effect. If the higher order interaction effects are neglected, the results can be represented by the following regression equation:

 $\hat{\mathbf{Y}} = \hat{\beta}_{0} + \hat{\beta}_{L} \cdot \mathbf{L} + \hat{\beta}_{R} \cdot \mathbf{R} + \hat{\beta}_{P} \cdot \mathbf{P} + \hat{\beta}_{T} \cdot \mathbf{T} + \hat{\beta}_{N} \cdot \mathbf{N} + \hat{\beta}_{LR} \cdot \mathbf{L} \cdot \mathbf{R} + \hat{\beta}_{LP} \cdot \mathbf{L} \cdot \mathbf{P} + \hat{\beta}_{LT} \cdot \mathbf{L} \cdot \mathbf{T} + \hat{\beta}_{LN} \cdot \mathbf{L} \cdot \mathbf{N} + \hat{\beta}_{RP} \cdot \mathbf{R} \cdot \mathbf{P} + \hat{\beta}_{RT} \cdot \mathbf{R} \cdot \mathbf{T} + \hat{\beta}_{RN} \cdot \mathbf{R} \cdot \mathbf{N} + \hat{\beta}_{PT} \cdot \mathbf{P} \cdot \mathbf{T} + \hat{\beta}_{PN} \cdot \mathbf{P} \cdot \mathbf{N} + \hat{\beta}_{TN} \cdot \mathbf{T} \cdot \mathbf{N}$ (4)

where:  $\hat{Y}$  = predicted response (pH, conductivity, etc.) L,R,P,T,N = experimental factors assuming the values -1, 0 or +1  $\hat{\beta}_0, \hat{\beta}_L, \dots, \hat{\beta}_{TN}$  = estimated values of the regression coefficients

The settings of the test conditions corresponding to the -1 and +1 levels of the experimental factors are given in Table 4. The regression coefficients ( $\beta$ 's) that were significantly different from zero (Student t test, 95 percent confidence interval) are presented in Table 9. The first line of the table gives the overall average of the response. The next five lines give the main effects. The rest of the table lists the 2-factor interaction affects.

The importance of each test condition can be evaluated by considering the magnitude of each coefficient in Table 9. The larger the absolute magnitude of a coefficient for a particular measured response, the more influence the corresponding experimental factor had on that response in a leaching test. The sign of each coefficient indicates whether changing an experimental factor from its minus to plus level increased (positive coefficient) or decreased (negative coefficient) the response magnitude.

While all coefficients in Table 9 are statistically significant, most of the variation in response magnitude that is caused by changes in test conditions can be accounted for by considering only those having the largest absolute values. These are indicated by the underlined values in Table 9, and account for at least 90 percent of the variation observed in each response. In order to facilitate the interpretation, the results can be presented as regression equations for each response. The only terms included in each equation are the underlined coefficients in Table 9.

pН	=	9.76 + 0.88 L - 0.27 R - 0.20 N + 0.21 LR + 0.17 LP	(5)
conductivity	=	4.73 - 1.14 R - 1.39 N - 0.44 LR - 0.50 LN	(6)
Cr	=	4.97 + 1.32 L - 1.81 R - 2.08 N	(7)
Cu	=	0.69 + 0.17 L - 0.26 R - 0.32 N - 0.11 LN + 0.12 RN	(8)
Mg	=	29.0 - 28.8 L + 17.6 R + 15.5 N - 17.7 LR - 15.5 LN	(9)

Experimental Factor (Independent Variable)	рН	Conductivity (mS/cm)	Chromium (m/L)	Copper (mg/L)	Magnesium (mg/L)
Average	9.76	4.73	4.97	0.69	29.0
Leaching Medium (L)	0.88	0.13	1.32	0.17	-28.8
Liquid-to-Solid Ratio (R)	-0.27	- <u>1.14</u>	- <u>1.81</u>	-0.26	17.6
Particle Size (P)	-0.15	-0.24	-0.24	-0.07	
Time of Elution (T)	0.13				1.4
Number of Elutions (N)	- <u>0.20</u>	- <u>1.39</u>	-2.08	-0.32	15.5
LR interaction	0.21	- <u>0.44</u>	-0.44	-0.08	- <u>17.7</u>
LP interaction	0.17				
LN interaction	0.16	- <u>0.50</u>	-0.35	-0.11	- <u>15.5</u>
RP interaction		-0.05		-0.05	-4.5
RT interaction	0.03		0.12		1.8
RN interaction	-0.03	0.29	0.53	0.12	6.7
PT interaction	0.04				-1.4
PN interaction	-0.04			0.03	-2.2
TN interaction	-0.03		0.09	-0.02	0.8

 TABLE 9
 COEFFICIENTS FROM A REGRESSION ANALYSIS OF THE SCREENING

 EXPERIMENT

Notes:

- the settings of the experimental factors are given in Table 4

- only the significant coefficients are included in this table (i.e., those whose 95 percent confidence interval (Student t test) does not include zero)

- the summation of the sum of squares of underlined coefficients is greater than 90 percent of the total sum of squares

- the LT interaction was confounded with blocks

Note that these regression equations are specific to the waste and the environmental conditions of this experiment. The independent variables are transformed variables which take the values -1 and +1; the test conditions corresponding to these two settings are given in Table 4.

Examination of the response equations indicates that the major experimental factors are the leaching medium, the liquid-to-solid ratio and the number of elutions. The effect of each of these three factors on test results cannot be evaluated independently of the other two because of the relatively large LR and LN interaction coefficients. The

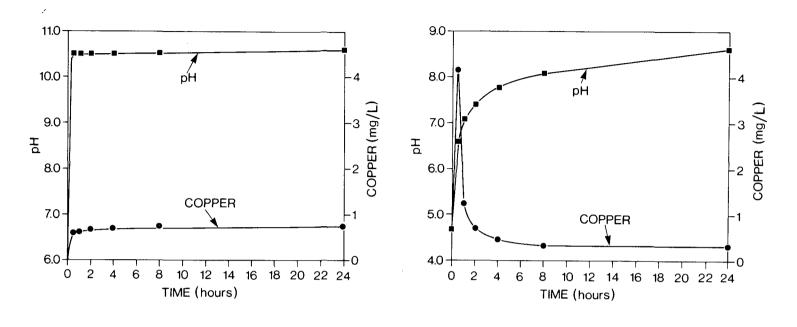
significance of these interaction coefficients can be explained by considering the different leachate pH's observed in each test. Leachate pH was found to be essentially independent of R and N when distilled water was used as the leaching medium. When a buffered acidic solution was used, however, the acidity of the leaching medium resulted in a lower leachate pH than observed with the distilled water leach. Increasing the liquid-to-solid ratio or performing a second elution increased the amount of acidity brought into contact with the waste, and resulted in a further decrease in leachate pH.

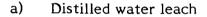
**3.2.3 Experiment 3: Time Release Patterns.** Since the results of Experiment 2 indicated that 24-hour leach tests gave approximately the same results as 48-hour leach tests, it was decided to examine the effects on test results of using leaching periods less than 24 hours. Tests were conducted for 0.5, 1, 2, 4, 8 and 24 hours using two media (distilled water and an acidic solution). Leachates were analyzed for pH, conductivity, Cr, Cu and Mg.

The temporal variations in pH and copper concentrations over a 24-hour leaching period are shown in Figure 3a for the distilled water leach and Figure 3b for the acidic solution leach. It is apparent that the release patterns were considerably different for the two leaching media. With distilled water, both pH and Cu reached or approached their final values within the first half-hour. However, with the acidic solution, pH increased gradually over 24 h, whereas Cu peaked at 4.2 mg/L at 0.5 h and then decreased to reach its final value of 0.32 mg/L at 8 h. The peak occurred because the copper was solubilized in the initial stages when pH was low, but reprecipitated as pH increased. The increase in pH was caused by neutralization of the acidic medium by the waste.

Release patterns for conductivity, Cr and Mg in both leaching media were similar to that shown for pH in Figure 3a (i.e., final values were reached within the first half hour).

**3.2.4. Experiment 4:** Leaching Media. The results of Experiments 2 and 3 showed that the leaching medium was a major factor, therefore, Experiment 4 was undertaken to compare the effect of six different leaching media on contaminant release. Other experimental conditions were kept the same during all six tests (Table 4). The results are presented in Table 10, and provide further evidence of the importance of the leaching medium in batch tests. All parameters displayed wide variability among tests, particularly the metals. While some of the differences in leached metal concentrations can be explained by solubility considerations, many of the high metal concentrations observed in





b) Acid solution leach

FIGURE 3	TEMPORAL VARIATION OF pH AND COPPER CONCENTRATION IN
	EXPERIMENT 3

Leaching Medium*	Final pH	Conductivity** (mS/cm)	Chromium (mg/L)	Copper (mg/L)	Magnesium (mg/L)	Zinc (mg/L)
DW	10.8	3.8	10.5	0.58	0.1	0.02
AS1	8.55	3.0	4.15	0.27	57	0.02
AS2	7.35	2.1	3.50	3.24	248	2.0
SL1	7.10	3.0	0.15	907	420	6.2
SL2	7.60	2.7	3.95	836	316	1.0
SL3	8.65	6.0	6.55	50	_***	1.0

\* see Table 3

\*\* the values shown are the measured conductivities minus the conductivity of the leaching media

\*\*\* the concentration of Mg in the leachate was lower than the original concentration in the leaching medium

tests using synthetic leaching media are probably due to the complexing agents contained in these media.

**3.2.5** Experiment 5: Liquid-Solid Separation. A replicated 2<sup>3</sup> factorial experiment using two leaching media and two liquid-to-solid ratios was conducted to evaluate the importance of performing liquid-solid separation of a waste sample prior to a leaching test.

A raw metal hydroxide sludge (TS = 10%) was used in the runs without liquidsolid separation. In those runs with separation, the sludge was pressure filtered following the U.S. EPA Extraction Procedure (EPA, 1980), and the filter cake (TS = 20%) used in the tests. The filtrate was analyzed and discarded.

The responses measured at each of the experimental settings are given in Table 11. These responses were analysed using least-squares regression. The significant main and interaction effects (at a 95 percent confidence level) for pH, conductivity, Cu and Mg are given in Table 12. The largest effects arose from changes in the liquid-to-solid ratio and the leaching medium. Performing liquid-solid separation on the waste prior to leaching had relatively little effect on Cu and Mg concentrations and pH, and no significant effect on conductivity.

Analyses of the filtrate from the liquid-solid separation step revealed that the pH of the free liquid was 12.0. This value is close to the average pH of 11.1 obtained in the tests when distilled water was the medium. The conductivity of the filtrate varied from 10.5 to 14.0 mS/cm, while the Cu concentration was 1 mg/L and Mg was non-detectable.

Based on the concentration of Cu found in the filtrate, the percent of Cu in the leachate originally present in the free water of the sludge was computed for the extractions where no liquid-solid separation had been performed (Table 13). It can be seen that when distilled water was the leaching medium, a significant fraction of the Cu found in the leachate (37 percent and 50 percent depending on the liquid-to-solid ratio) came from the free water associated with the sample, the rest being extracted from the solid. With the acidic solution, these values dropped significantly to 0.10 percent and 0.01 percent due to a higher release of Cu from the solid fraction of the waste. Thus when distilled water was the leaching medium, a considerable amount of the Cu found in the leachate was not extracted from the solid portion of the waste, but originated from the free liquid portion.

Variables S R L	Treatment Combination	pН	Conductivity (mS/cm)	Copper (mg/L)	Magnesium (mg/L)
	1	5.47	7.2	112.	58.0
+	S	6.54	7.5	2.	61.0
- + -	r	4.80	4.7	364.	36.0
+ + -	sr	5.05	5.0	444.	50.0
+	1	11.38	5.8	0.30	0.1
+ - +	sl	11.40	5.6	0.10	0.1
- + +	rl	10.62	1.6	0.01	0.1
+ + +	srl	10.87	1.4	0.03	0.1
Error Variance	*	0.0112	0.055	8.64	4.06

## TABLE 11RESPONSES OF THE 2<sup>3</sup> FACTORIAL DESIGN LIQUID-SOLID<br/>SEPARATION EXPERIMENT

\*8 degrees of freedom

## TABLE 12COEFFICIENTS FROM REGRESSION ANALYSIS OF THE LIQUID-SOLID<br/>SEPARATION EXPERIMENT

Experimental Factor (Independent Variable)	рН	Conductivity (mS/cm)	Copper (mg/L)	Magnesium (mg/L)
Average	8.27	4.84	115.2	25.6
Liquid-Solid Separation (S)	0.20		-3.7	2.2
Liquid-to-Solid Ratio (R)	-0.44	-1.66	86.8	-4.1
Leaching Medium (L)	2.80	-1.26	-115.2	-25.5
SR interaction			23.7	1.3
SL interaction	-0.13		3.7	-2.2
RL interaction	-0.11	-0.44	-86.9	-4.1

1) The settings of R and L are given in Table 4. The -1 and +1 levels of S were without and with liquid-solid separation, respectively.

2) Only the significant coefficients are included in this table (i.e., those whose 95 percent confidence interval (Student t test) does not include zero).

	Leachin	g Medium
Liquid-to-Solid Ratio	Distilled Water	Acidic Solution
4:1	37%	0.10%
20:1	50%	0.01%

## TABLE 13PERCENT OF COPPER IN LEACHATE THAT WAS ORIGINALLY<br/>PRESENT IN THE FREE LIQUID PORTION OF THE SLUDGE

### 3.3 The Multiple-Batch Leaching Procedure.

Based on the literature survey and the results of the laboratory work previously described, a leaching procedure involving six batch extractions was defined which would allow comparisons of the leachability of various wastes and indicate potential changes in the leachability of a waste under different test conditions. In selecting the test conditions to be used in the leaching procedure, a choice had to be made between single and multiple elutions. Multiple elutions are useful for evaluating the kinetics of contaminant release, particularly when the leaching medium has some buffering capacity; however, they add considerably to the time and effort required to complete a leaching test. It was decided to restrict the procedure to single elutions, but to use a variety of test conditions to provide a wider data base for examination of the effects of different conditions on waste leachability. The test conditions were chosen in order to maximize test sensitivity and reproducibility, and to envelop the range of test conditions used in the standard leaching tests proposed by ASTM (1979) and the U.S. EPA (1980). Consideration was also given to developing a relatively inexpensive test by using available laboratory equipment and attempting to minimize the amount of training required to perform the procedure.

The MBLP comprises a set of six batch extractions (Table 14) using three leaching media (distilled water, an acidic solution buffered at pH 4.5 (ASTM, 1979), and a synthetic municipal landfill leachate (Stanforth et al., 1979)), at two liquid-to-solid ratios (4:1 and 20:1). The chemical compositions of the latter media are given in Table 3 (Numbers 2 and 5).

The two liquid-to-solid ratios of 4:1 and 20:1 correspond to those used in the proposed ASTM (1979) and U.S. EPA (1980) leaching tests. The batch extractions are performed in square plastic bottles that are rotated slowly (2 to 3 rpm) for 24 hours. The leachates are then decanted, filtered (0.45  $\mu$ m), and analyzed for the parameters of

		Leaching Medium									
Liquid-to- Solid Ratio	Distilled Water	Acidic Solution pH = 4.5 (H+) = 82 meq/L	Synthetic Leachate pH = 4.5 (H+) = 157 meq/L								
4:1	DW4 (0)*	AS4 (0.33)	SL4 (0.63)								
20:1	DW20 (0)	AS20 (1.63)	SL20 (3.14)								

# TABLE 14IDENTIFICATION OF THE SIX EXTRACTIONS USED IN THE<br/>MULTIPLE-BATCH LEACHING PROCEDURE

\*the numbers in brackets indicate the meq of (H+) available per g of waste

interest. A detailed step-by-step protocol for conducting the MBLP is given in Appendix I.

#### 3.4 Comparison With Other Leaching Tests

Some extractions of the MBLP are similar to the proposed ASTM leaching test (ASTM, 1979) and the Extraction Procedure (U.S. EPA, 1980).

The proposed ASTM leaching test consists of two extractions, one with distilled water (Method A) and one with an acidic solution (Method B). The ASTM tests are similar to MBLP Extractions DW4 and AS4 except for three conditions: the ASTM test uses a reciprocating table for agitation, the ASTM protocol does not include any particle size reduction, and the time of elution is 48 hours. The laboratory work described in Section 3.2 showed leaching test results were not markedly changed by those conditions. The two ASTM tests and Extractions DW4 and AS4, therefore, should give comparable results.

The MBLP extractions DW20 and AS20 are similar to the U.S. EPA Extraction Procedure (EP) except for liquid-solid separation and the amount of acid added to the waste sample. In the EP, provision is made for liquid-solid separation before the test. The solid portion is then extracted, and the extract mixed with the liquid portion prior to analysis for the contaminants of interest. The amount of acid added in the EP is variable. The pH is continuously monitored and adjusted to 5.0 up to a maximum acid addition of 2 meq of H<sup>+</sup> per gram of waste (the amount of acid added is dependent on the buffering capacity of the waste). In the MBLP, no acid is added in the DW20 extraction, whereas 1.63 meq/g is added in the AS20 extraction. Thus these two extractions can be interpreted approximately as the lower and upper extremes of acid addition in the EPA Extraction Procedure.

#### 4 RESULTS OF MBLP APPLICATIONS

The Multiple-Batch Leaching Procedure has been applied to a number of wastes, including bottom and fly ashes from coal-fired power generating stations, metal finishing and chemical plant residues, mine tailings and industrial wastewater treatment sludges. Some of the wastes have also been subjected to the U.S. EPA Extraction Procedure (U.S. EPA, 1980) and the ASTM proposed leaching tests (ASTM, 1979).

The wastes that were tested are listed in Table 15. The results of these tests are given in Appendix II, and are expressed in three formats:

 <u>Concentration</u> - the ratio of the mass of chemical species X in a leachate (M<sub>XL</sub>) to the volume of leachate (V<sub>L</sub>):

$$C_{XL} = \frac{M_{XL}}{V_L}$$
(10)

2) <u>Release</u> - the ratio of the mass of chemical species X in a leachate (M<sub>XL</sub>) to the mass of the leached sample (M<sub>S</sub>); it is also equal to the product of the liquid-to-solid ratio (R) and the concentration of chemical species X in the leachate (C<sub>XL</sub>):

$$\operatorname{REL}_{X} = \frac{M_{XL}}{M_{S}} = \frac{M_{XL}}{M_{S}} \times \frac{V_{L}}{V_{L}} = \frac{V_{L}}{M_{S}} \times \frac{M_{XL}}{V_{L}} = \operatorname{R.C}_{XL}$$
(11)

3) <u>Efficiency</u> - the ratio of the mass of chemical species X in a leachate (M<sub>XL</sub>) to the mass of that species in the leached sample (M<sub>XS</sub>) expressed as a percentage:

$$EFF_{X} = \frac{M_{XL}}{M_{XS}} \times 100\%$$
(12)

### 4.1 Observed Trends

Some of the trends that have been observed on the effects that different leaching media and liquid-to-solid ratios have on test results are described in subsequent sections.

**4.1.1** The Effect of Leaching Medium on Leachate pH. One of the major conclusions of the background study leading to the development of the MBLP was that the release of contaminants from a waste was largely governed by the final pH of the leachate. This is to be expected as leachate pH has a major influence on contaminant solubility. Leachate pH, in turn, is a function of the alkalinity of the waste, and of the amount of acid available in the leaching medium to react with the waste. The amount of acid in the six batch extractions used in the MBLP varies from none for distilled water to 3.14 meq/g

Waste Type	Sample Numbers
1 Coal-fired power generating stations	
Fly ash Bottom ash	5*, 8, 9 6*, 7, 10
2. FBC coal-fired power generating stations	
Baghouse material Bed material 40:60, baghouse:bed mixture	48, 50 47, 49 51
3. FGD coal-fired power generating stations	
Fly ash Bottom ash Sludge	62 61 58, 63, 67, 68
4. Tailings	
Mine Cyanide Bulk sulphide flotation process	13*, 19, 20, 21, 22 11, 56, 64 57
5. Sludges and Residues	
Metal finishing sludge Anaerobically digested WWTP sludge Solidified metal cleaning waste Leaded-fuel tank bottom Zinc sulphide residue Zinc hydroxide sludge High arsenic residue Phosphorus production slag Catalytic cracker residue Refinery sludge mixed with soil Filter cake solids Aluminum production red mud Lagoon sludge Leather tannery sludge Copper wool scrap Foundry sand Oily sand Solidified pickling liquor and baghouse dust Dredge spoils Impregnated Charcoal	1*, 2*, 14* 12* 15* 18 23 24 25 29 32 33 40, 41* 42, 43 54*, 55* 52 53* 3* 45 4* 16 70

# TABLE 15SAMPLES SUBJECTED TO THE MULTIPLE-BATCH LEACHING<br/>PROCEDURE

\* indicates samples were also subjected to EPA's Extraction Procedure and/or ASTM's batch leaching tests

of waste for the synthetic municipal landfill leachate at the 20:1 liquid-to-solid ratio (Table 14). For comparison, the U.S. EPA Extraction Procedure specifies a maximum acid addition of 2.0 meq/g of waste (U.S. EPA, 1980).

To examine the influence of the leaching medium on leachate pH, the pH data from the 51 MBLP applications listed in Table 15 were compared both with respect to the volume of leaching medium (i.e., the liquid-to-solid ratio), and the acidity of the medium. The results are shown in Figure 4.

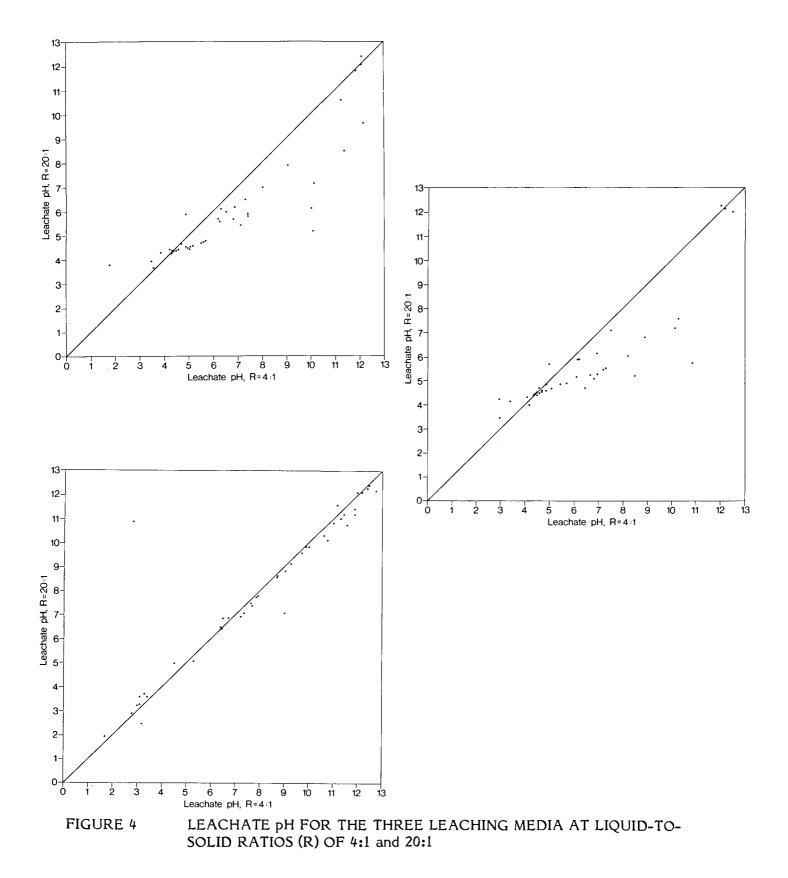
When distilled water was used as the leaching medium, final leachate pH was controlled by the acidity or alkalinity of the waste and was largely independent of liquid-to-solid ratio, as shown by the coincidence of most of the data points in Figure 4a with the diagonal. Replicates were run on three wastes to measure the reproducibility of the test. The standard deviation of the pH measurements was 0.32 (11 degrees of freedom); the largest difference was 0.55.

When the acidic solution or the synthetic municipal landfill leachate was used as the leaching medium (Figures 4b and 4c), the spread in the leachate pH data decreased. The leachate pH's were shifted towards pH 4.5, the value at which the leaching media were buffered. As expected, shifts were larger in the synthetic leachate extractions than in the acidic solution extractions since the former medium contained almost twice as much acid (157 meq/L versus 82 meq/L). Not only was the range decreased, but the data was skewed to the right (i.e., leachate pH's were lower at the higher liquid-to-solid ratio). This occurred because more acid was available to react with the waste at the higher ratio.

4.1.2 The Effect of Liquid-to-Solid Ratio on Contaminant Release. The effect of the liquid-to-solid ratio 'R' on test results was examined by comparing contaminant release at R = 20:1 to that at R = 4:1. This value, denoted as REL<sub>20</sub>/4, is simply the ratio of the mass of a contaminant in the 20:1 leachate to that in the 4:1 leachate:

$$REL_{20/4} = \frac{REL_{20}}{REL_4} = \frac{M_{XL20/MS}}{M_{XL4}/MS} = \frac{M_{XL20}}{M_{XL4}}$$
(13)

REL<sub>20/4</sub> ratios were calculated for the results of the 51 MBLP applications listed in Table 15. Ratios could only be calculated for those cases where species were detectable at both liquid-to-solid ratios. A total of 317 and 310 REL<sub>20/4</sub> ratios could be calculated for the acidic solution and synthetic leachate extractions, respectively, whereas only 292 ratios could be calculated for the distilled water extractions, indicating the more aggressive leaching characteristics of the former media. Furthermore, for the distilled water extractions, 58 percent of the measured species were above detection limits at the



4:1 liquid-to-solid ratio but only 48 percent at the 20:1 ratio, because dilution at the higher ratio decreased contaminant concentrations below detection limits. Approximately the same percentage of species, however, were detected at the two ratios when the other leaching media were used (60 percent for the acidic solution and 64 percent for the synthetic municipal landfill leachate).

If it is assumed that 1) equilibrium between the leaching medium and the waste is achieved within the 24 hour elution period, 2) contaminant solubilities are dependent only on final leachate pH, and 3) the final leachate pH's (and thus contaminant solubilities) are the same in extractions with the same leaching medium but different liquid-to-solid ratios, then the theoretical range for  $REL_{20/4}$  is 1 to 5. The lower limit of unity will occur when the same mass of contaminant is released at the two liquid-to-solid ratios. This suggests that there is a limited mass of contaminant available for leaching, and that adding 5 times more leaching medium simply dilutes the concentration by a factor of 5. The upper limit of 5 will be achieved when five times as much mass of contaminant is leached at the higher ratio. This will occur if there is a sufficient amount of contaminant available for leaching to achieve saturation at both ratios. Intermediate values between 1 and 5 will be obtained when there is sufficient contaminant available to fully saturate the leachate at the 4:1 liquid-to-solid ratio, but not enough to produce saturation at the 20:1 ratio.

The REL<sub>20</sub>/4 ratios from the distilled water and the acidic solution extractions are shown in Figure 5 in the form of relative frequency histograms. The histogram for the synthetic municipal landfill leachate extractions is similar to the acidic solution histogram. It is interesting to note that there is a peak at  $REL_{20/4} = 1$  when distilled water was used as the leaching medium, indicating that concentration differences between the two liquid-to-solid ratios were simply due to dilution. The effect of dilution was also apparent when the acidic solution and synthetic leachate were used, but was not as pronounced. Eighty-two percent of the REL20/4 ratios fell within the theoretical range of 1 to 5 when distilled water was used as the leaching medium (Figure 5a) but only 70 percent and 77 percent of the ratios were within this range when the acidic solution and synthetic leachate, respectively, were used (Figure 5b). The poorer fit of the acidic solution and synthetic leachate release ratios between the theoretical limits is to be expected because leachate pH's at the two liquid-to-solid ratios were frequently different (Figure 4c); violating the third assumption in the development of the theoretical limits. It also appears that the synthetic leachate complexes some metals, which would increase metal solubilities (and thus their release) above those expected from pH considerations alone.

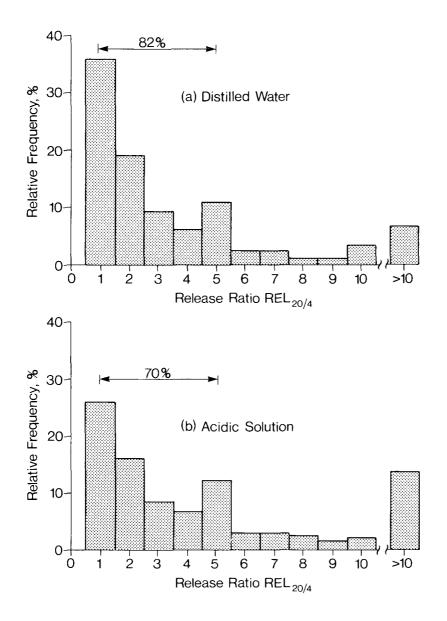


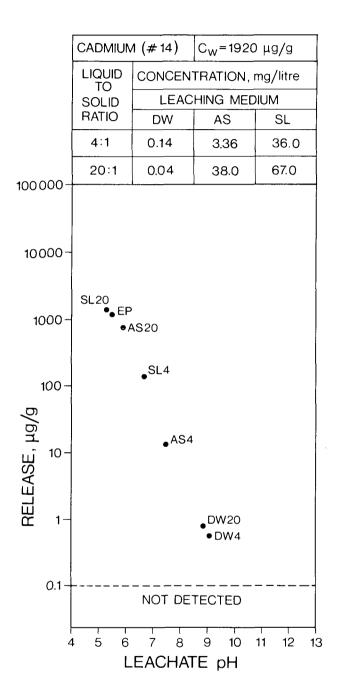
FIGURE 5 RELATIVE FREQUENCY HISTOGRAMS OF THE RATIO OF CONTAMINANT RELEASE AT R = 20:1 TO THAT AT R = 4:1

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**4.1.3** Leachability of Selected Priority Pollutants under Various Test Conditions. Concentrations of Cd, Cr, Cu, Pb, Zn and cyanide in leachates are given in the tabular portion of Figures 6 to 11 for several of the residues subjected to the MBLP. The concentration of the contaminant in the waste sample, expressed on a dry weight basis, is also given ( $C_W$ ). Interpretation of leaching data in this form is very difficult because of the effects of the different leaching media and liquid-to-solid ratios on contaminant concentrations. Data evaluation can be simplified by considering contaminant release (Eq. 11) rather than contaminant concentration, and by plotting the logarithm of release versus final leachate pH. The resulting graphs are shown in Figures 6 to 11. The U.S. EPA Extraction Procedure (U.S. EPA, 1980) and the ASTM proposed leaching tests a and b (ASTM, 1979) were also performed on several of the residues. Releases from these tests are indicated in Figures 6 to 11 by the symbols EP, ASTMa and ASTMb.

For cadmium, lead, zinc and cyanide, a strong linear trend existed between the logarithm of contaminant release and final leachate pH over the pH range experienced in the leachates. There was also good correlation between the relative degree of release and the amount of acid available in the leaching medium to react with the waste. The latter values indicate that the order of increasing contaminant release to be expected, assuming release to be solely dependent on the amount of acid contacting the waste, would be DW4 and DW20 with the same amount of release, followed by AS4, SL4, AS20 and SL20 (Table 14). Examination of Figures 6 to 9 show this progression to be true in all cases except the reversed order of SL4 and AS20 in Figure 7a.

The results suggest that it would be possible, in some cases, to predict the release of these contaminants into a different leaching medium and/or at a different L/S ratio if the pH of the leachate could be evaluated from knowledge of the interaction that occurs between the waste and leaching medium (i.e., through a titration curve of the waste). This would be very helpful in trying to compare the results from different batch leaching tests. This supposition is supported by some of the release data obtained from application of the Extraction Procedure (EP) to Sample 14. Acid was added in the EP of Sample 14 at a rate of 2 meq/g of waste. From Table 14, it would be expected that release from the EP at this acid addition rate would fall between releases from the AS20 and SL20 extractions. This was indeed the case for cadmium and zinc (Figures 6 and 8). This linear trend, however, was not observed for all contaminants. No readily discernable pattern was apparent for the release-pH curves for chromium (Figure 10) and copper



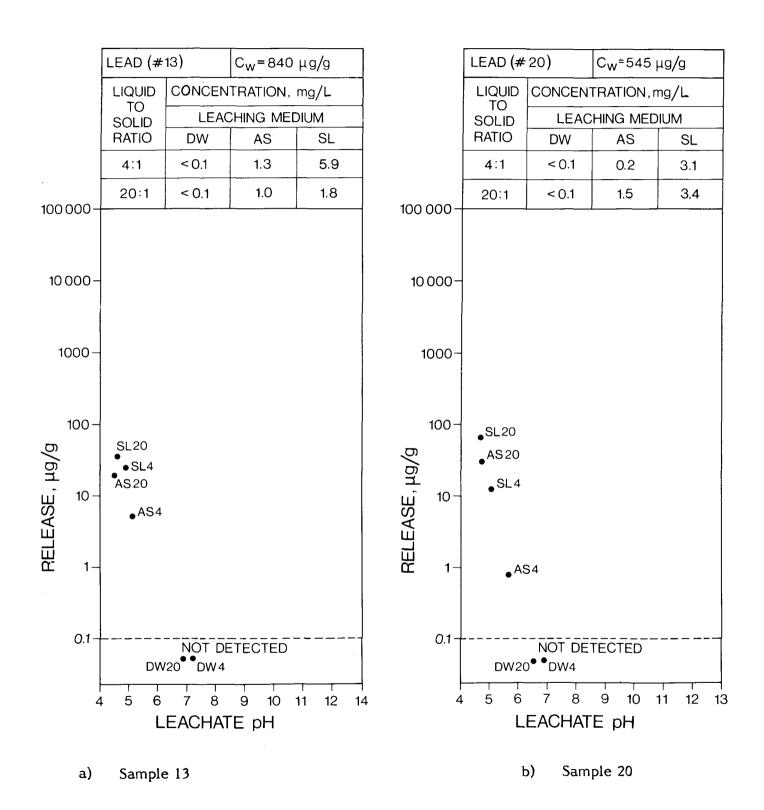


FIGURE 7 LEAD CONCENTRATIONS AND RELEASES FOR SAMPLES 13 AND 20

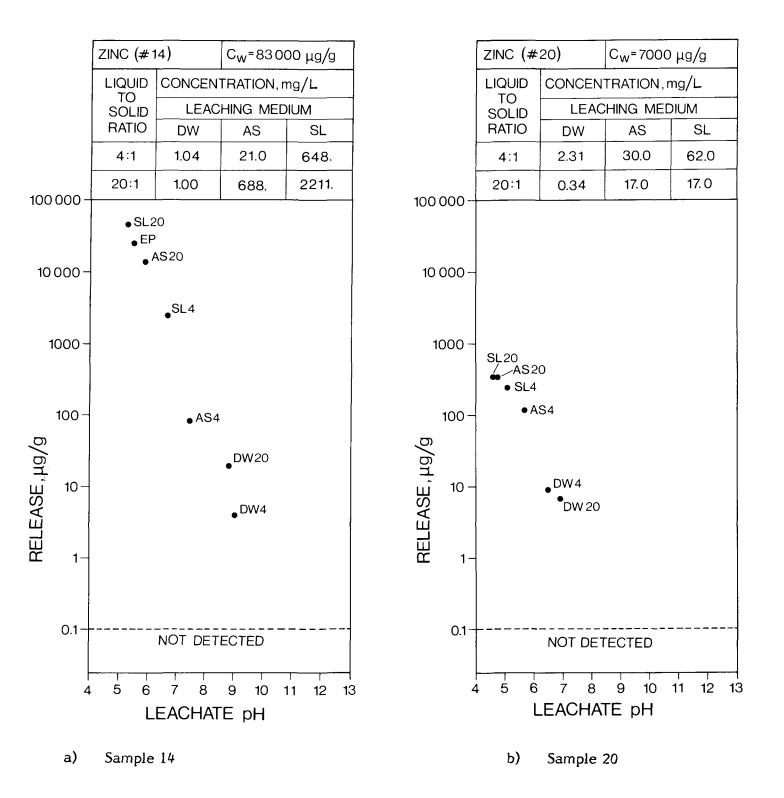
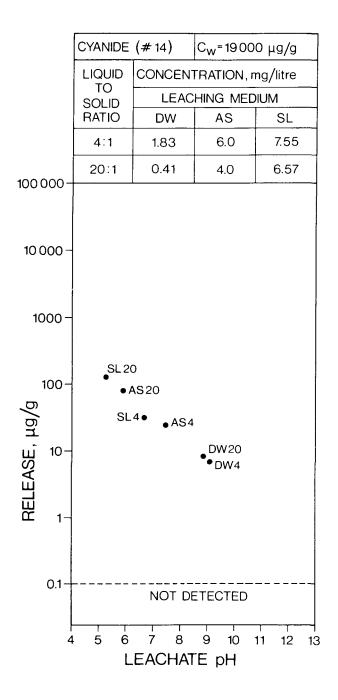


FIGURE 8 ZINC CONCENTRATIONS AND RELEASES FOR SAMPLES 14 AND 20



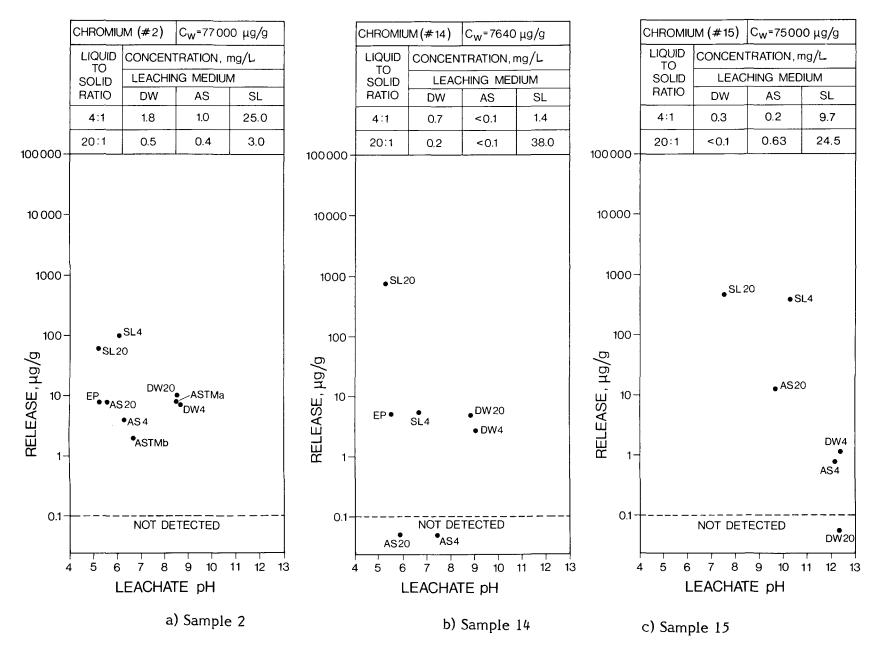


FIGURE 10 CHROMIUM CONCENTRATIONS AND RELEASES FOR SAMPLES 2, 14 AND 15

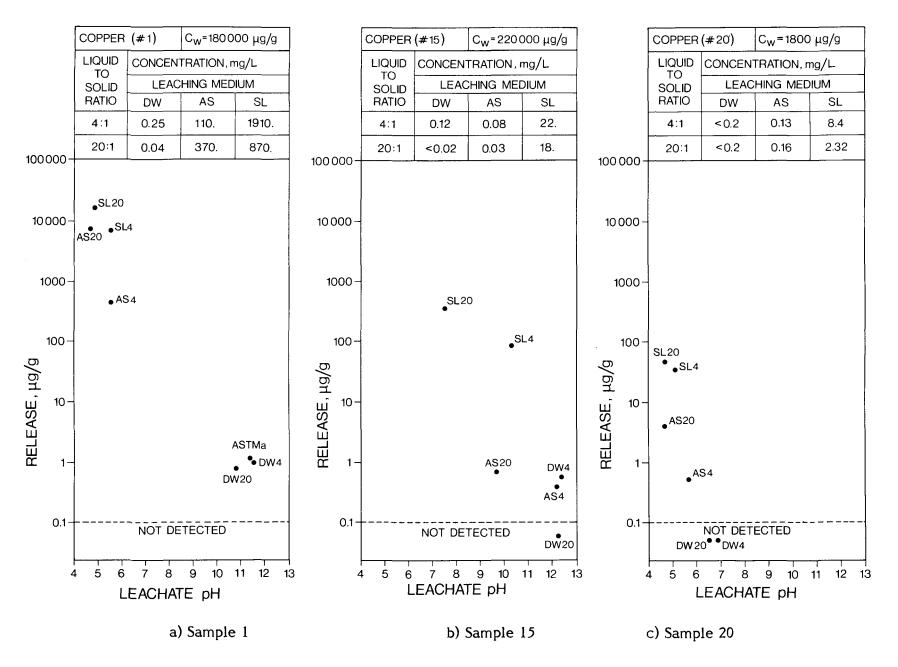


FIGURE 11 COPPER CONCENTRATIONS AND RELEASES FOR SAMPLES 1, 15 AND 20

(Figure 11). Comparison of chromium and copper releases from the ASTM tests and the MBLP provides further evidence that it may be possible to predict contaminant release from knowledge of a leaching medium's acid content. ASTM Method A is similar to the distilled water extraction at the 4:1 liquid-to-solid ratio, except that a different mixing procedure is used and the medium is contacted with the waste for 48 hours instead of 24 hours. Chromium release in Sample 2 (Figure 10a) and copper release in Sample 1 (Figure 11a) were identical for both methods. Similarly, ASTM Method B is similar to the acidic solution extraction at the 4:1 liquid-to-solid ratio. The same leaching medium is used in both extractions, but the mixing procedure and contact time differ as in ASTM Method A. As shown in Figure 10a, chromium releases in Sample 2 were similar for ASTM Method B and MBLP Extraction AS4.

It appears from Figures 10 and 11 that the synthetic municipal landfill leachate may have complexed chromium and copper since releases were higher than those of the acidic solution, even though final leachate pH's were similar at equal liquid-to-solid ratios. The ability of some leaching media to complex chemical species complicates the task of predicting contaminant release under different leaching conditions. More work is required to determine if the effects of complexing on release can be predicted from a knowledge of the chemical composition of the leaching medium and the waste.

## 4.2 Summary

When distilled water was used as the leaching medium, the final pH of the leachate was controlled by the alkalinity or the acidity of the waste. Changing the liquid-to-solid ratio had little effect on leachate pH. The difference in the concentrations observed at the two liquid-to-solid ratios were the result of dilution in a large number of cases.

When an acidic solution or synthetic leachate was used as the leaching medium, final leachate pH appeared to be a function of the interaction between the waste pH and the amount of acid available in the leaching medium to react with the waste. Increasing the liquid-to-solid ratio increased the amount of acid contacting the waste and shifted the leachate pH towards the pH of the leaching medium. This decreased or increased contaminant release depending on the direction of the pH shift.

Use of a synthetic leachate appeared to complex some contaminants and increase their release above that to be expected from pH - solubility considerations alone.

For some contaminants and wastes, there were strong linear relationships between the logarithm of release and final leachate pH, and a good correlation between

the logarithm of release and the amount of acid in the leaching medium. This linear relationship, although not evident in all cases, suggests that it may be possible to predict release under different test conditions simply by knowing the final pH of the leachate.

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## REFERENCES

Anonymous, "Standard Leachate Test", Stiching Verwijdering Afvalstoffen, Report SVA/2302, Amersfoort, The Netherlands (1977).

ASTM, "Proposed Methods for Leaching for Waste Materials", In: <u>1979 Annual Book of</u> ASTM Standards, Part 31 (Water) (1979).

Bridges, T., personal communication, Limnology and Toxicity Section, Ontario Ministry of the Environment (July, 1981).

Côté, P. and T.W. Constable, "Important Factors of a Batch Leaching Test", presented at the <u>Sixteenth Canadian Symposium on Water Pollution Research in Canada</u>, Toronto, Ontario (Feb. 19, 1981).

Coté, P. and T.W. Constable, "Evaluation of Experimental Conditions in Batch Leaching Procedures", presented at the <u>Symposium on Resource Recovery and Environmental Issues</u> of <u>Industrial Solid Wastes</u>, Gatlingburg, Tennessee (Oct. 28-30, 1981); published in Resources and Conservation, No. 9 (1982).

Côté, P. and T.W. Constable, "Development of a Canadian Data Base on Waste Leachability", <u>Hazardous and Industrial Solid Waste Testing</u>: <u>Second Symposium</u>, <u>ASTM STP 805</u>, R.A. Conway and W.P. Gulledge (eds.), American Society for Testing and Materials (1983).

Ham, R.K., M.A. Anderson, R. Stegmann and R. Stanforth, "Bachground Study on the Development of a Standard Leaching Test", Industrial Environmental Research Laboratory, U.S. EPA, EPA-600/2-79-109 (1979a).

Ham, R.K., M.A. Anderson, R. Stegmann and R. Stanforth, "Comparison of Three Waste Leaching Tests", Industrial Environmental Research Laboratory, U.S. EPA, EPA-600/2-79-071 (1979b).

Lee, G.F. and R.H. Plumb, "Literature Review on Research Study for the Development of Dredged Material Disposal Criteria", Contract Report D-74-1, Office of Dredged Material Research, U.S. Army Engineer Waterways Experiments, Slakon, Vicksburg, MS, (1974).

Lowenback, W., "Compilation and Evaluation of Leaching Test Methods", Municipal Environmental Research Laboratory, U.S. EPA, EPA-600/2-78-095 (1978).

Stanforth, R., R. Ham, M.A. Anderson and R. Stegmann, "Development of a Synthetic Municipal Landfill Leachate", Journal WPCF, 51(7) (1979).

Subcommittee on Oversight and Investigation, Committee on Interstate and Foreign Commerce, Ninety-Sixth Congress, "Waste Disposal Site Survey", U.S. Government Printing Office, Washington (1979).

U.S. EPA, Newsletter, "Solid Waste News Brief" (May, 1979).

U.S. EPA, "Test Methods for the Evaluation of Solid Waste, Physical Chemical Methods", Office of Solid Wastes, U.S. EPA, Report No. SW-846 (1980).

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APPENDIX I THE MULTIPLE-BATCH LEACHING PROCEDURE

## APPENDIX I THE MULTIPLE-BATCH LEACHING PROCEDURE

The Multiple-Batch Leaching Procedure comprises a set of six batch extractions using three leaching media (distilled water, an acidic solution buffered at pH 4.5, and a synthetic municipal landfill leachate) at two liquid-to-solid ratios (4:1 and 20:1). The extractions are performed in square plastic bottles that are rotated slowly for 24 hours. The leachates are then decanted, filtered (0.45  $\mu$ m) and analyzed for the parameters of interest. A flowchart of the steps involved in the procedure is presented in Figure I.1. A description of each of these steps follows.

## I.1 Sampling (after ASTM, 1979)

- 1. Obtain a representative sample of the waste to be tested (e.g., ASTM standard technique for sampling wastes). Two kilograms of waste are necessary for each set of the six extractions included in the Leaching Procedure.
- Samples should be kept in closed containers prior to testing. Biologically active samples should be stored at 4°C and their extraction should be started within eight hours if possible.

## I.2 Particle Size Reduction

1. The waste is crushed, cut or ground so that it passes through a 9.5 mm (0.375 inch) sieve.

## I.3 Structural Integrity Procedure (after U.S. EPA, 1980)

If the waste sample is monolythic, this procedure should be followed for each of the 6 extractions of Step I.5.

- A Structural Integrity Tester having a 3.18 cm (1.25 in) diameter hammer weighing 0.33 kg (0.73 lb) and having a free fall of 15.24 cm (6 in) shall be used. This device is available from various suppliers (Millipore, Nuclepore) or it may be fabricated to meet the specifications shown in Figure I.2.
- 2. Fill the elastomeric sample holder with the material to be tested. If the sample of waste is a large monolithic block, cut a portion from the block having the dimensions of a 33 mm (1.3 in) diameter x 7.1 cm (2.8 in) long cylinder. For a chemically fixed waste, samples may be cast in the form of a 33 mm (1.3 in) diameter x 7.1 cm (2.8 in) cylinder and allowed to cure in a 100 percent humidity environment for 7 days prior to further testing.

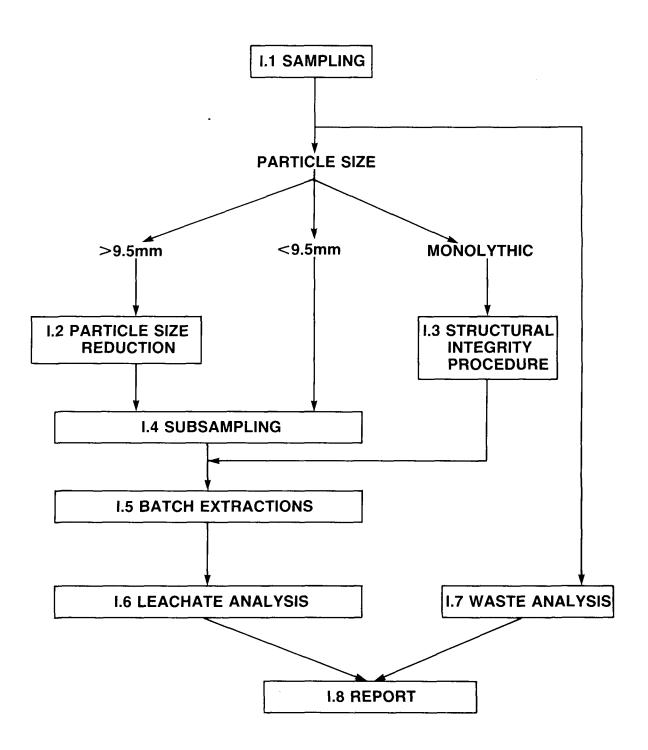
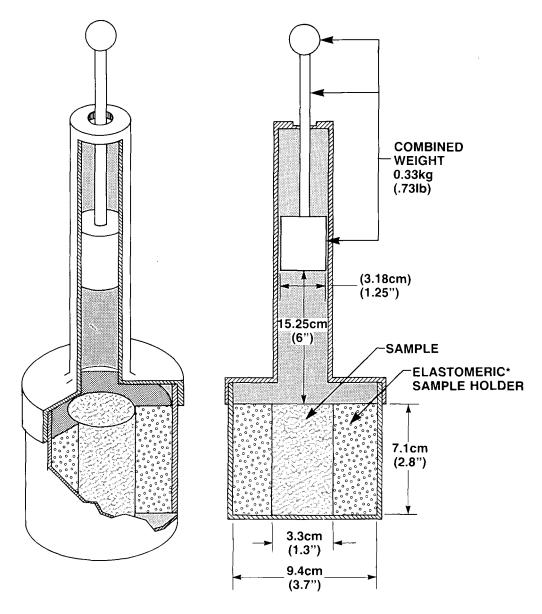


FIGURE I.1 FLOWCHART OF THE MULTIPLE-BATCH LEACHING PROCEDURE



\*ELASTOMERIC SAMPLE HOLDER FABRICATED OF MATERIAL FIRM ENOUGH TO SUPORT THE SAMPLE

FIGURE I.2 STRUCTURAL INTEGRITY TESTER (U.S. EPA, 1980)

- 3. Place the sample into the Structural Integrity Tester. Raise the hammer to its maximum height and release it. Repeat the hammering procedure fifteen times.
- 4. Remove the material from the sample holder, weigh it, and proceed to Extraction Step I.5.

### I.4 Subsampling (after ASTM, 1979)

This procedure is applicable to free-flowing particles. It is used for subsampling from the main sample (Steps I.1 or I.2) to obtain samples for the extractions (Step I.5). The sample is quartered on an impermeable sheet of glazed paper, oil cloth, or other flexible material as follows:

- 1. Empty the sample container into the centre of the sheet.
- 2. Flatten out the sample gently with a suitable straight edge until it is spread uniformly to a depth approximately equal to its particle size.
- 3. Remix the sample by lifting a corner of the sheet and drawing it across, low down, to the opposite corner in a manner that the material is made to roll over and over and does not merely slide along. Continue operation with each corner proceeding in a clockwise direction. Repeat this operation ten times.
- 4. Lift all four corners of the sheet towards the centre. Holding all four corners together, raise the entire sheet into the air to form a pocket for the sample.
- 5. Repeat Step 2.
- 6. With a straight edge at least as long as the flattened mound of sample (such as a thin-edged yard stick), gently divide the sample into quarters. An effort should be made to avoid using pressure on the straight edge sufficient to cause damage to the particles.

## I.5 Batch Extractions

The extractions are done in square closed bottles. Polyethylene bottles are used when the contaminants of interest are inorganic while glass bottles are used for organics.

The amount of waste and leaching medium added in each test bottle is computed on a weight basis (wet weight of the waste) according to the calculations given below. Instructions for preparing the acidic and synthetic leaching media are given in Table I.1.

1. The six extraction bottles containing the waste and the leaching medium are filled to approximately 90 percent of their capacity.

## TABLE I.1 LEACHING MEDIA PREPARATION

	Acid Solution (ASTM, 1979)	Synthetic Leachate (Stanforth et al., 1979)
Chemical Recipe	- sodium acetate (0.0451 M) - glacial acetic acid (0.0816 M)	<ul> <li>sodium acetate (0.15 M)</li> <li>glacial acetic acid (0.15 M)</li> <li>glycine (0.05 M)</li> <li>salicylic acid (0.007 M)</li> </ul>
Recipe Preparation	<ol> <li>Prepare a concentrated solution (x10) by dissolving 49 g (46.8 mL) of glacial acetic acid and 37 g of anhydrous sodium acetate in 1 L of distilled water. (If trihydrate sodium ac- etate is used, 64.4 g should be added).</li> </ol>	<ol> <li>Prepare a concentrated solution (x10) by dis- solving 90.1 g (85.9 mL) of glacial acetic acid, 123.1 g of anhydrous sodium acetate, 37.5 g of glycine and 9.7 g of salicylic acid in 1 L of distilled water. (If tri- hydrate sodium acetate is used, 204.1 g should be added).</li> </ol>
	<ol> <li>Prepare 1 L of the acid solution by using 100 mL of the concentrated so- lution and making up to 1 L by adding distilled water.</li> </ol>	<ol> <li>Prepare 1 L of the syn- thetic leachate by using 100 mL of the concen- trated solution and making up to 1 L by adding distilled water.</li> </ol>
	<ul> <li>Adjust the pH to 4.5 ∓</li> <li>0.1 by the drop wise addition of acetic acid or sodium hydroxide (40 g/L) as required.</li> </ul>	

Calculate the amount of waste to be added in each bottle using the following approximate formula, neglecting specific gravity considerations:

$$W_{W} = \frac{0.9 V}{R+1}$$

where: V = volume of the bottle (mL)

minimum: 500 mL if R = 4:1 1000 mL if R = 20:1 R = liquid to solid ratio W<sub>W</sub> = weight of waste (g)

- 2. Add the calculated amount of waste to each of the six bottles.
- 3. Add each leaching medium to the test bottles according to the formula:

 $W_L = R W_W$ 

where:  $W_L$  = weight of leaching medium (g)

4. Agitate the bottles using an apparatus similar to the one illustrated in Figure I.3 for  $24 \text{ h} \neq 0.5 \text{ h}$  at room temperature. Set the speed of rotation between 2 and 3 rpm.

## I.6 Leachate Analysis

- After the period of agitation, separate the bulk of the aqueous phase from the solid phase by decantation, centrifugation or filtration through filter paper as appropriate. Vacuum filter the aqueous phase through a 0.45 µm membrane filter. For oily wastes, use a 8 µm filter (ASTM, 1979).
- 2. Measure the pH and conductivity of the filtrate.
- 3. Transfer the filtrate to sample bottles and preserve in a manner consistent with the chemical analyses to be performed.

## I.7 Waste Analysis

- 1. Determine the total solids content of the waste as follows:
  - dry dishes at 104 + 2°C
  - cool a dish in a dessicator and weigh it  $(W_0)$
  - put approximately 50 g of waste into the dish and weigh (W<sub>1</sub>)
  - dry at 104 + 2°C for 24 h
  - cool to room temperature in a dessicator and reweigh (W<sub>2</sub>)
  - calculate the total solids content (S<sub>T</sub>) from:

$$S_{T} = \frac{W_2 - W_0}{W_1 - W_0}$$

- 2. Determine the fixed solids content as follows:
  - muffle sample and dish at 550°C for 1 hour
  - air cool briefly, then place in a dessicator to cool
  - weigh (W 3)
  - calculate the fixed solids content (S<sub>F</sub>) from:

$$S_{\rm F} = \frac{W_3 - W_0}{W_2 - W_0}$$

3. When possible, analyse the waste for the contaminants of interest in the leachate.

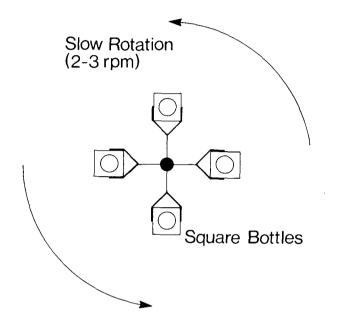


FIGURE I.3 ILLUSTRATION OF TUMBLER

## I.8 Report

- 1. The report should include a description of the waste:
  - source,
  - observed physical characteristics (e.g., colour, odour, particle size, homogeneity, phases),
  - total solids and fixed solids contents, and
  - chemical composition on a dry weight basis.
- 2. The results of the leachate analyses can be expressed using the three following formats (the chemical composition of the waste must be available to compute leaching efficiency):

a) <u>Concentration</u> - the ratio of the mass of chemical species X in a leachate (M<sub>XL</sub>) to the volume of leachate (V<sub>L</sub>):

$$C_{XL} = \frac{M_{XL}}{V_L}$$

b) <u>Release</u> - the ratio of the mass of chemical species X in a leachate (M<sub>XL</sub>) to the mass of the leached sample (M<sub>S</sub>); it is also equal to the product of the liquid-to-solid ratio (R) and the concentration of chemical species X in the leachate (C<sub>XL</sub>):

$$REL_{X} = \frac{M_{XL}}{M_{S}} = \frac{M_{XL}}{M_{S}} \times \frac{V_{L}}{V_{L}} = \frac{V_{L}}{M_{S}} \times \frac{M_{XL}}{V_{L}} = R.C_{XL}$$

c) <u>Efficiency</u> - the ratio of the mass of chemical species X in a leachate  $(M_{XL})$  to the mass of that species in the leached sample  $(M_{XS})$  expressed as a percentage:

$$EFF_{X} = \frac{M_{XL}}{M_{XS}} \times 100\%$$

.

APPENDIX II LEACHING TEST RESULTS

## SAMPLE NO.: 1 WASTE TYPE: Raw Metal Finishing Sludge

DATE TESTED: June 1981

COMMENTS: Green, silt-sized particles

SL 4:1

SL 20:1

43.8

100

36.6

89.0

SOLID PHASE

TOTAL SOLIDS: 9.7% VOLATILE SOLIDS: 9.8%

	PARAMETER		Cu	Mg	1							
	Concentratio	n (ppm)	180 000	13 200							1	
L			- <b>I</b>		<b>-</b>	<b>.</b>	 <b>-</b>	- <b>I</b>	- <b>L</b>	 	_	
MULTIPLE-BA	TCH LEACHING	PROCEDU	RE									
MEASURED CHARACTER IS		ST	Cu	Mg							pH (Units)	Conductivity (mS/cm)
Concentrati (mg/L)	DW AS AS SL	4:1 20:1 4:1 20:1 4:1 20:1	0.24 0.05 110 371 1910 873	<0.1 <0.1 53.5 32 117 57							11.55 10.80 5.55 4.70 5.45 4.85	8.90 1.70 8.25 4.90 12.15 9.85
Release (µg∕g)	DW AS AS SL	20:1 4:1	0.96 1.00 440 7420 7640 17 460	214 640 468 1140								
Efficiency (%)	DW AS	4:1 20:1 4:1 20:1	<0.01 <0.01 2.52 42.5	16.7 50.0								

## SAMPLE NO.: 1 WASTE TYPE: Raw Metal Finishing Sludge

DATE TESTED: June 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure =  $68.8 \text{ mL} = 0.737 \text{ meq H}^+/\text{g}$  of waste.

EPA EXTRACTION PR	ROCEDURE AND AS	TM LEACHI	NG TESTS								
MEASURED CHARACTERISTIC	TEST CONDITION	Cr	Cu	Fe	Mg	Ni	РЪ	Zn		pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	1.5 3.7 3.5	74. 0.3 137.	<0.1 <0.1 <0.1	29. 0.1 36.	<0.1 <0.1 <0.1	<0.1 <0.1 <0.1	68. 0.3 97.		5.30 11.4 5.30	2.70 4.80 6.40
Release (µg/g)	EPA ASTM DW ASTM AS	30.0 14.8 14.0	1480. 1.20 548.		580. 0.40 144.			1360. 1.20 388.			
Efficiency (%)	EPA ASTM DW ASTM AS		24.3 0.02 8.98		45.3 0.03 11.2						

MEASURED CHARACTER I ST IC	TEST CONDITION					pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS						
Release (µg/g)	EPA ASTM DW ASTM AS						
Efficiency (%)	EPA ASTM DW ASTM AS						

#### SAMPLE NO.: 2 WASTE TYPE: Dewatered Metal Finishing Sludge

DATE TESTED: May 1981

COMMENTS: Green, particle size = 3 to 50 mm

SOLID PHASE

TOTAL SOLIDS: 20,5% VOLATILE SOLIDS: 15.0%

PARAMETER	Cr	Cu	Fe	Mg	NĪ	Pb	Zn	Al	Ga	Cd
Concentration (ppm)	77 000	223 000	12 200	16 900	105	2620	62 800	573	75 500	44

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Cr	Cu	Fe	Mg	NÎ	Pb	Zn		pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	1.8	0.47	<0.1	5.95	<0.1	<0.1	0.04		8.7	3.25
(mg/L)	DW 20:1	0.5	0.20	<0.1	3.85	<0.1	<0.1	0.12		8.6	1.40
	AS 4:1	1.0	168	<0.1	99.0	0.5	<0.1	110		6.3	6.40
	AS 20:1	0.4	3.57	<0.1	231.1	<0.1	<0.1	4.41		5.6	7.10
	SL 4:1	25	922	<0.1	109	0.6	<0.1	106		6.1	11.00
	SL 20:1	3.0	767	<0.1	273	0.5	<0.1	21.0		5.2	9.10
Release	DW 4:1	7.2	1.9	-	23.8			0.16			
(µg/g)	DW 20:1	10.0	4.0		77.0			2.40			
	AS 4:1	4.0	672		396	2.00		440			
	AS 20:1	8.0	71		4620			88.2			
	SL 4:1	100	3688		436	2.40		424			
	SL 20:1	60.0	15 340		5640	10.0		420			
Efficiency	DW 4:1	0.05	· · · · · · · · ·		0.69			<0.01			
(%)	DW 20:1	0.06	0.01		2.22			0.02			
	AS 4:1	0.03	1.5		11.4	9.3		3.42			
	AS 20:1	0.05	0.16		133			0.69			
	SL 4:1	0.63	8.1		12.5	11.1		3.29			
	SL 20:1	0.38	33.6		158	46.5		3.26	4 1		

#### SAMPLE NO.: 2 WASTE TYPE: Dewatered Metal Finishing Sludge

DATE TESTED: May 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure = 242 mL = 1.03 meq H<sup>+</sup>/g waste.

EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

MEASURED CHARACTER I ST IC	TEST CONDITION	Cr	Cu	Fe	Mg	NÎ	Pb	Zn	pH (Units)	Conductivity (mS/cm)
Concentration	EPA	0.4	74.0	<0.1	99.	0.5	<0.1	68.0	5.20	2,80
(mg/L)	ASTM DW	2.0	0.35	<0.1	4.9	<0.1	<0.1	0.05	8.50	2.90
	ASTM AS	0.5	2,39	<0.1	108.	<0.1	<0.1	2.24	6.70	6.80
Release	EPA	8.0	1480.		1980.	10.		1360.		
(µg/g)	ASTM DW	8.0	1.40		19.6			0.20		
	ASTM AS	2.0	9.56		432.			8.96		
Efficiency	EPA	0.05	3.24		57.2	46.5		10.6		
(%)	ASTM DW	0.05	<0.01		0.57			<0.01		
	ASTM AS	0.01	0.02		12.5			0.07		

MEASURED CHARACTER I ST I C	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Release (µg/g)	EPA ASTM DW ASTM AS	2						
Efficiency (%)	EPA ASTM DW ASTM AS							

#### SAMPLE NO.: 3 WASTE TYPE: Foundry Sand

DATE TESTED: June 1981

COMMENTS: Black

SOLID PHASE

TOTAL SOLIDS: 92.0% VOLATILE SOLIDS: 1.5%

PARAMETER	TOC	y Phenol	 [		 	
Concentration (ppm)	10 100	<1				

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTERISTIC	TEST CONDITION	тос	Phenol	BOD	COD				1	pH nits)	Conductivity (mS/cm)
Concentration	DW 4:1	3.8		4	59				3	.1	0.96
(mg/L)	DW 20:1	2.1	0.05	4	2.0				3	.3	1.25
	AS 4:1						ļ	ł	4	.9	4.30
	AS 20:1	6							5	.9	5.00
	SL 4:1						ļ	1	5	.0	10.0
	SL 20:1				1			1	5	•7	12.5
Release	DW 4:1	15.2		16	236	 					
(µg/g)	DW 20:1	42.0	1.00	80	40						
	AS 4:1										
	AS 20:1							1			
	SL 4:1										
	SL 20:1										
Efficiency	DW 4:1	0.16			1	 1					
(\$)	DW 20:1	0.45	ļ					]			
	AS 4:1								-		
	AS 20:1										
	SL 4:1					1				Ì	
	SL 20:1			ł							

SAMPLE NO.: 3 WASTE TYPE: Foundry Sand

DATE TESTED: June 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure = 11 mL =  $0.054 \text{ meq H}^+/\text{g}$  waste.

#### EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

MEASURED CHARACTER I ST IC	TEST CONDITION	Phenol	BOD5	COD	тос				pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	0.010 0.015	4.	<1.	3.7				5.50 5.20	0.27 5.40
Release (µg/g)	EPA ASTM DW ASTM AS	0.20 0.06	16.		14.8					
Efficiency (%)	EPA ASTM DW ASTM AS				0.16					<u> </u>

MEASURED CHARACTERISTIC	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Release (µg/g)	EPA ASTM DW ASTM AS							
Efficiency (%)	EPA							

## SAMPLE NO.: 4 WASTE TYPE: Solidified Pickling Liquor and Baghouse Dust

DATE TESTED: June 1981

COMMENTS: Reddish brown, particle size = 30 to 100 mm, solidified by addition of silicates and lime

#### SOLID PHASE

TOTAL SOLIDS: 82.8% VOLATILE SOLIDS: 7.6%

PARAMETER	Cd	Fe	Мо	Pb			
Concentration (ppm)	750	170 000	675	9980			

MEASURED CHARACTERISTIC	TEST CONDITION	Cd	Fe	Мо	РЪ							pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.01	<0.1	13.0	<0.1		<u> </u>		1			9.0	15.0
(mg/L)	DW 20:1	<0.01	<0.1	6.3	<0.1							7.1	5.4
	AS 4:1	0.02	0.1	9.8	<0.1		4					9.1	17.8
	AS 20:1	0.25	0.2	1.8	<0.1							7.9	10.9
	SL 4:1	9.66	0.7	8.9	<0.1							8.9	23.5
	SL 20:1	11.1	2.3	0.3	0.7							6.8	16.5
Release	DW 4:1			52					1				
(µg/g)	DW 20:1			126									
	AS 4:1	0.08	0.40	39.2		Ì							
	AS 20:1	5.0	4.0	36.0									
	SL 4:1	38.6	2.8	35.6	ļ								
	SL 20:1	223	46	6.0	14	E.							
Efficiency	DW 4:1	1		9.3									
(%)	DW 20:1			22.5									
	AS 4:1	0.01	<0.01	7.0							•		
	AS 20:1	0.81	<0.01	6.4	l I		1	1	1				
	SL 4:1	6.2	<0.01	6.4							ŀ		
	SL 20:1	35.9	0.03	1.1	0.17			1					

## SAMPLE NO.: 4 WASTE TYPE: Solidified Pickling Liquor and Baghouse Dust

DATE TESTED: June 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure = 400 mL = 2.0 meq H<sup>+</sup>/g waste.

EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

MEASURED CHARACTER I ST I C	TEST	Cd	Fe	Мо	Pb				pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	7.98 <0.01 2.90	0.1 0.1 3.7	8.0 0.3	1.6 <0.1 4.3				5.80 9.00 9.10	8.30 12.0 14.0
Release (µg/g)	EPA ASTM DW ASTM AS	160 <b>.</b> 11.6	2.0 0.4 14.8	32 <b>.</b> 1.2	32.0 17.2					
Efficiency (%)	EPA ASTM DW ASTM AS	25 <b>.</b> 7 1.87	<0.01 <0.01 0.01	5.73 0.21	0.39 0.21					

MEASURED CHARACTER I ST I C	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Release (µg/g)	EPA ASTM DW ASTM AS							
Efficiency (%)	EPA ASTM DW ASTM AS							

SAMPLE NO.: 5 WASTE TYPE: Fly Ash from a Coal Fired Generating Station

DATE TESTED: June 1981

COMMENTS: Grey, particle size: 75 to 100 µm

SOLID PHASE

TOTAL SOLIDS: 99.5% VOLATILE SOLIDS: 0.2%

PARAMETER	Ag	AI	Be	Б	Cd	Ċr	Qu	Fe	к	Mg
Concentration (ppm)	<0.5	128 000	10.8	27 900	<0.8	23.3	77.6	112 000	134 000	5720

MEASURED CHARACTERISTIC	TEST CONDITION	Ag	AI	Be	Са	Са	Cr	Cu	Fe	к	Mg	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1		1.07	<0.001	626	0.01	0.43	0.045	0.16	56	0.23	2.8	3.6
(mg/L)	DW 20:1		5.57	<0.001	287	<0.01	0.11	<0.008	<0.01	6	0.74	10.9	1.8
	AS 4:1		1.37	<0.001	1630	0.02	<0.01	0.028	0.17	81	109	5.7	8.4
	AS 20:1		33.7	0.012	637	<0.01	0.15	0.172	2.65	14	55.5	4.8	5.5
	SL 4:1		16.2	0.028	1910	0.04	<0.01	1.54	3.44	69	225	5.7	13.0
	SL 20:1		44.9	0.022	601	<0.01	0.28	0.431	9.75	11	54.2	4.9	9.3
Release	DW 4:1		4.28		2500	0.04	1.72	0.18	0.64	224	0.92		
(µg/g)	DW 20:1		111		5740		2.20			120	14.8		
	AS 4:1		5.48	1	6520	0.08		0.11	0.68	324	436		
	AS 20:1		674	0.24	12 700		3.00	3.44	53.0	280	1110		
	SL 4:1		64.8	0.11	7640	0.16		6.16	13.8	276	900		
	SL 20:1		898	0.44	12 000		5.60	8.62	195	220	1084		
Efficiency	DW 4:1		<0.01		9.02		7.42	0.23	<0.01	0.17	0.02		
(\$)	DW 20:1		0.09	ļ	20.7		9.49			0.09	0.26		
	AS 4:1		<0.01		23.5			0.15	<0.01	0.24	7.66		
	AS 20:1		0.53	2.23	45.9		12.9	4.46	0.05	0.21	19.5		
	SL 4:1		0.05	1.04	27.5			7.98	0.01	0.21	15.8		
	SL 20:1		0.71	4.09	43.3		24.2	11.2	0,17	0.17	19.1		

SAMPLE NO.: 5 WAS	STE TYPE:	Fly	Ash
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DATE TESTED: June 1981

COMPLENTS: Continued from previous page

SOLID PHASE

TOTAL SOLIDS: 99.5% VOLATILE SOLIDS: 0.2%

PARAMETER	Mn	Мо	Na	NI	Р	Pb	Sr	TI	v	Zn
Concentration (ppm)	208	<30	8800	93	830	45	1230	6420	48.2	103

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Mn	Мо	Na	Nİ	Р	РЬ	Sr	Ti	v	Zn		
Concentration	DW 4:1	0.01	1.9	93	0.09	0.7	<0.05	14.5	<0.005	0.176	0.23		
(mg/L)	DW 20:1	<0.01	<0.3	20	<0.05	<0.6	<0.05	4.62	<0.005	0.089	<0.05		
	AS 4:1	0.03	2.0		0.07	1.0	<0.05	15.9	<0.005	0.036	<0.05		
	AS 20:1	1.23	<0.3		0.16	1.0	<0.05	6.79	0.188	0.038	0.43		
	SL 4:1	4.81	1.1		0.71	<0.6	<0.05	21.5	0.040	0.005	0.70	ļ	
	SL 20:1	1.20	<0.3		0.13	<0.6	<0.05	6.30	0.188	0.313	0.34		
Release	DW 4:1	0.04	7.6	372	0.36	2.8	1	58.0		0.70	0.92		
(µg∕g)	DW 20:1			400				92.4		1.78	{		
	AS 4:1	0.12	8.0		0.28	4.0		63.6		0.14			
	AS 20:1	24.6			3.20	20		136	3.76	0.76	8.60		
	SL 4:1	19.2	4.4		2.84			86.0	0.16	0.02	2.80		
	SL 20:1	24.0			2.60			126	3.76	6.26	6.80		
Efficiency	DW 4:1	0.02		4.25	0.39	0.34		4.74		1.47	0.90		
(%)	DW 20:1			4.57				7.55		3.71			
	AS 4:1	0.06			0.30	0.48		5.20		0.30			
	AS 20:1	11.9			3.46	2.42		11.1	0.06	1.58	8.39		
	SL 4:1	9.3			3.07	1		7.03	0.01	0.04	2.73		
	SL 20:1	11.6			2.81			10.3	0.06	13.1	6.64		

## SAMPLE NO.: 5 WASTE TYPE: Fly Ash

EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

DATE TESTED: June 1981

**COMMENTS:** Continued from previous page. Acid addition in EPA extraction procedure = 77 mL = 0.39 meq  $H^{+}/g$  waste.

MEASURED CHARACTER I ST IC	TEST CONDITION	AI	В	Ва	Be	Са	Cd	٥r	Cu	Fe	к	pH (Units)	Conductivity (mS/cm),
Concentration	EPA	1.43	6.06	0.110	<0.001	338.	<0.01	<0.01	0.052	0.08	18.	5.00	1.60
(mg/L)	ASTM DW	3.55	12.9	0.115	<0.001	375.	<0.01	0.13	0.034	0.05	41.	3.30	2.65
	ASTM AS	32.7	22.3	0.089	0.012	795.	0.02	0.38	0.219	16.9	57.	4.70	6.00
Release	EPA	28.6	121.	2.20		6760.			1.04	1.60	360.		
(µg/g)	ASTM DW	14.2	51.6	0.46		1500.		0.52	0.14	0.20	164.		
	ASTM AS	131	89.2	0.36	0.05	3180.	0.08	1.52	0.88	67.6	228.		
Efficiency	EPA	0.02				24.4			1.35	<0.01	0.27		
(%)	ASTM DW	0.01				5.40		2.24	0.18	<0.01	0.12		
	ASTM AS	0.10			0.45	11.5		6.56	1.13	0.06	0.17		

MEASURED CHARACTERISTIC	TEST CONDITION	Mg	Mn	Мо	Na	Ni	Р	РЬ	Si	Sr	ті	v	Zn	
Concentration	EPA	17.2	0.20	0.6	26.0	0.13	0.8	<0.05	6.14	4.45	0.008	0.036	0.05	
(mg/L)	ASTM DW	7.59	0.03	0.7	62.0	0.07	<0.6	<0.05	0.26	7.05	<0.005	0.082	<0.05	
	ASTM AS	42.1	0.89	0.5		0.27	5.1	<0.05	24.0	9.55	1.21	0.505	0.48	
Release	EPA	344.	4.00	12.0	520.	2.60	16.0		123.	89.0	0.16	0.72	1.00	
(µg/g)	ASTM DW	30.4	0.12	2.80	248.	0.28			1.04	28.2		0.33		1
	ASTM AS	168.	3.56	2.00		1.08	20.4		96.0	38.2	4.84	2.02	1.92	
Efficiency	EPA	6.04	1.93		5.94	2.81	1.94			7.27	<0.01	1.50	0.98	
(%)	ASTM DW	0.53	0.06		2.83	0.30				2.30		0.68		
	ASTM AS	2.96	1.72			1.17	2.47			3.12	0.08	4.21	1.87	l

SAMPLE NO.: 6 WASTE TYPE: Bottom Ash from a Coal Fired Generating Station

DATE TESTED: September 1981

COMMENTS: Black, particle size = 0.075 to 10 mm

SOLID PHASE

TOTAL SOLIDS: 99.1% VOLATILE SOLIDS: 2.2%

PARAMETER	Ag	Al	Be	Ca	Cd	C۲	Cu	Fe	к	Mg
Concentration (ppm)	<0.5	121 000	9.15	21 200	<0.8	<0.8	74.9	197 000	12 800	5280

MEASURED CHARACTER I ST IC	TEST CONDITION	Ag	Al	Ве	Ca	Cd	Cr	Cu	Fe	к	Mg	pH (units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.005	0.11	<0.001	169	<0.01	0.02	0.016	0.04	<1	6.31	4.5	0.89
(mg/L)	DW 20:1	<0.005	<0.01	<0.001	40.2	<0.01	0.01	<0.008	<0.01	<1	1.66	5.0	0.28
	AS 4:1	<0.005	17.5	0.005	371	<0.01	0.06	0.291	16.7	<1	9.56	4.5	4.20
	AS 20:1	<0.005	2.24	0.001	53.9	<0.01	0.03	0.124	1.22	<1	2.76	4.4	3.60
	SL 4:1	<0.005	7.11	0.003	330	<0.01	0.02	0.367	1.01	<1	10.6	4.7	9.40
	SL 20:1	<0.005	5.74	0.002	62.4	<0.01	0.03	0.122	9,80	<1	2,46	4.6	8.90
Release	DW 4:1	1	0.44		676		0.08	0.06	0.16		25.2		
(µg/g)	DW 20:1				804		0.20	1			33.2		
	AS 4:1		70.0	0.020	1484		0.24	1.16	66.8		38.2		4
	AS 20:1		44.8	0.020	1078		0.60	2.48	24.4		55.2		
	SL 4:1		28.4	0.012	1320		0.08	1.47	4.04		42.4		
	SL 20:1		115	0.040	1248		0.60	2.44	196		49.2		
Efficiency	DW 4:1		<0.01	1	3.22			0.09	<0.01		0.48		
(\$)	DW 20:1	1	)	)	3.83	Ì					0.63		
	AS 4:1		0.06	0.22	7.06			1.57	0.03		0.73		
	AS 20:1		0.04	0.22	5.13			3.34	0.01		1.05		
	SL 4:1		0.02	0.13	6.28	l		1.98	<0.01		0.81		
	SL 20:1		0.10	0.44	5.94			3.29	0.10		0.94		

#### SAMPLE NO.: 6 WASTE TYPE: Bottom Ash

DATE TESTED: September 1981

COMMENTS: continued from previous page

SOLID PHASE

TOTAL SOLIDS:

•/

VOLATILE SOLIDS:

PAI	RAMETER	Mn	Мо	Na	NI	Р	РЪ	Sr	Ti	v	Zn
Co	ncentration (ppm)	380	<30	6800	97	520	10	1010	6000	195	57

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Mn	Мо	Na	NÎ	Р	РЬ	Sr	ті	v	Zn	в	Ва	Si
Concentration	DW 4:1	0.90	<0.3	1	0.11	<0.6	<0.05	0.977	<0.005	<0.005	0.07	0.375	0.040	4.68
(mg/L)	DW 20:1	0.20	<0.3	1	<0.05	<0.6	<0.05	0.286	<0.005	<0.005	<0.05	0.108	0.108	0.90
	AS 4:1	1.45	<0.3	ļ	0.16	<0.6	<0.05	1.30	0.072	<0.005	3.48	0.500	0.154	16.0
	AS 20:1	0.30	<0.3	1	0.06	<0.6	<0.05	0.320	<0.005	<0.005	0.15	0.103	0.246	2.20
	SL 4:1	1.47	<0.3		0.18	<0.6	<0.05	1.35	<0.005	<0.005	0.30	0.514	0.074	9.83
	SL 20:1	0.39	<0.3		<0.05	<0.6	<0.05	0.475	0.105	<0.005	0.14	0.132	0.428	5.16
Release	DW 4:1	3.60		4	0.44		<b></b>	3.91			0.28	1.50	0.16	18.7
(µg/g)	DW 20:1	4.00		20				5.72		1		2.16	2.16	18.0
	AS 4:1	5.80			0.64	)	1	5.20	0.29	)	13.9	2.00	0.62	64.0
	AS 20:1	6.00			1.20			6.40			3.0	2.06	4.92	44.0
	SL 4:1	5.88			0.72			5.40		1	1.2	2.06	0.30	39,3
	SL 20:1	7.80						9.50	2.10	ł	2.8	2.64	8.56	103
Efficiency	DW 4:1	0.96		0.06	0.46			0.39			0.50			
(%)	DW 20:1	1.06		0.30				0.57		1				
	AS 4:1	1.54			0.67			0.52	<0.01		24.6			
	AS 20:1	1.59			1.25		1	0.64			5.31			
	SL 4:1	1.56	l		0.75			0.54			2.12			
	SL 20:1	2.07			1			0.95	0.04		4.96			

## SAMPLE NO.: 6 WASTE TYPE: Bottom Ash

DATE TESTED: September 1981

**COMMENTS:** Continued from previous page. Acid addition in EPA extraction procedure =  $0 \text{ mL} = 0 \text{ meq H}^+/g$  waste.

MEASURED CHARACTER ISTIC	TEST CONDITION	Ag	AI	в	Ва	Ве	Са	Са	Cr	Qu	Fe	pH (Units)	Conductivity (mS/cm)
Concentration	EPA	<0.005	<0.01	0.123	0.084	<0.001	39.2	<0.01	<0.01	0.035	0.14	5.20	0,60
(mg/L)	ASTM DW	<0.005	0.93	0.401	0.059	<0.001	102.	<0.01	<0.01	0.067	0.11	2.70	0,69
	ASTM AS	<0.005	3.54	0.513	0.067	0.001	184.	<0.01	0.02	0.097	0.84	3.70	4.38
Release	EPA	1		2.46	1.68	T	784.		1	0.70	2.80	1	
(µg/g)	ASTM DW		3.72	1.60	0.24		408.			0.27	0.44		
	ASTM AS		14.2	2.05	0.27	0.01	736.		0.08	0.39	3.36		
Efficiency	EPA	1	1				3.73			0.94	<0.01		
(%)	ASTM DW		<0.01				1.94			0.36	<0.01		
	ASTM AS		0.01			0.04	3.50			0.52	<0.01		

MEASURED CHARACTER ISTIC	TEST CONDITION	к	Mg	Mn	Мо	Na	Nİ	Р	РЬ	Si	Sr	ті	v	Zn
Concentration (mg/L)	EPA ASTM DW ASTM AS	<1. <1. <1.	1.42 4.83 9.32	0.21 0.68 1.03	<0.3 <0.3 <0.3	2. 1.	0.18 0.09 0.12	<0.6 <0.6 <0.6	<0.05 <0.05 <0.05	0.87 3.00 4.01	0.679	<0.005	<0.005 <0.005 <0.005	0.09 0.08 0.35
Release (µg/g)	EPA ASTM DW ASTM AS		28.4 19.3 37.3	4.20 2.72 4.12		40. 4.	3.60 0.36 0.48			17.4 12.0 16.0	5•32 2•72 3•41			1.80 0.32 1.40
Efficiency (%)	EPA ASTM DW ASTM AS		0.54 0.37 0.71	1.12 0.72 1.09		0.59 0.06	3.75 0.37 0.50				0.53 0.27 0.34			3.19 0.57 2.48

## SAMPLE NO.: 7 WASTE TYPE: Bottom Ash from a Coal Fired Generating Station

DATE TESTED: September 1981

COMMENTS: Brown-grey.

#### SOLID PHASE

TOTAL SOLIDS: 60.1% VOLATILE SOLIDS: 8.0%

PARAMETER	Ag	AI	В	Be	Ca	Cd	۵r	Qu	Fe	к
Concentration (ppm)	<0.05	86 400.	268.	2.21	78 800.	3.8	20.3	22.8	33 100.	3800.

MEASURED CHARACTER ISTIC	TEST CONDITION	Ag	AI	В	Ве	Ca	Cd	Cr	Cu	Fe	к	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.005	<0.01	3.13	<0.001	48.9	<0.1	0.02	<0.008	<0.01	<1.	9.7	0.5
(mg/L)	DW 20:1	<0.005	<0.01	0.853	<0.001	31.7	<0.1	0.01	0.012	0.02	<1.	9.6	0.2
	AS 4:1	<0.005	6.12	6.45	<0.001	833.	0.2	0.02	0.028	0.67	<1.	5.2	5.4
	AS 20:1	<0.005	26.3	1.89	0.004	273.	<0.1	0.06	0.061	10.8	<1.	4.6	3.8
	SL 4:1	<0.005	96.6	8.21	0.017	1170.	<0.1	0.06	0.161	63.0	<1.	4.2	11.4
	SL 20:1	<0.005	58.3	2.20	0.007	359.	<0.1	0.04	0.054	38.3	<1.	4.0	9.5
Release	DW 4:1			12.5		196.		0.08	1				
(µg/g)	DW 20:1			17.1	ļ	634.		0.20	0.24	0.40			
	AS 4:1		24.5	25.8		3330.	0.08	0.08	0.11	2.68			
	AS 20:1		526.	37.8	0.08	5460.		1.20	1.22	216.			
	SL 4:1		386.	32.8	0.07	4680.		0.24	0.64	252.			
	SL 20:1		1170.	44.0	0.14	7180.		0.80	1.08	766.			
Efficiency	DW 4:1	<b>†</b>		7.77		0.41		0.66					
(%)	DW 20:1			10.6		1.34		1.64	1.75	<0.01			
	AS 4:1		0.05	16.0		7.04	3.5	0.66	0.82	0.01			
	AS 20:1		1.01	23.5	6.2	11.5		9.84	8.90	1.09			
	SL 4:1		0.74	20.4	5.0	9.88		1.97	4.70	1.27			
	SL 20:1		2.25	27.3	10.5	15.2		6.56	7.88	3.85		1	ļ

#### SAMPLE NO.: 7 WASTE TYPE: Bottom Ash

DATE TESTED: September 1981

COMMENTS: Continued from previous page.

SOLID PHASE	TOTAI	SOLIDS:		VOLATIL	E SOLIDS	:								
	PARAMETER	Mg	Mn	Мо	Na	Ni	Р	РЪ	Sr	ті	v	Zn	60	Th
	Concentration (ppm)	7170.	587.	<30.	3200.	34.	630.	5.	250.	2870.	48.	20.	16.	23
MULTIPLE-BA	TCH LEACHING PROCEDI	RE												
MEASURED CHARACTER IS		Mg	Mn	Mo	Na	Ni	Р	РЪ	Sr	TI	v	Zn	ŵ	Th
Concentrati (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.64 0.70 43.5 16.5 64.7 22.3	<0.01 <0.01 1.36 0.79 3.84 1.50	<0.3 <0.3 0.3 <0.3 0.5 0.3	8. 2.	<0.05 <0.05 0.20 0.22 0.18 0.06	<0.6 <0.6 0.7 <0.6 0.9 <0.6	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05	0.292 0.127 2.48 0.858 3.56 1.17			<0.05 <0.05 <0.05 0.07 <0.05 <0.05	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05	<0.0 <0.0 <0.0 <0.0 <0.0
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	2.56 14.0 174. 330. 259. 446.	5.44 15.8 15.4 30.0	1.2 2.0 6.0	32. 40.	0.80 4.40 0.72 1.20	2.8 3.6		1.17 2.54 9.92 17.2 14.2 23.4	3.52 7.36 21.2	0.56 0.84 0.33 0.62	1.40		
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.06 0.32 4.04 7.66 6.01 10.4	1.54 4.48 4.35 8.50		1.66 2.08	3.92 21.5 3.52 5.87	0.74 0.95		0.78 1.69 6.60 11.4 9.48 15.6	0.20 0.43 1.23	1.96 2.91 1.15 2.15	11.7		

#### SAMPLE NO.: 7 WASTE TYPE: Bottom Ash

DATE TESTED: September 1981

COMMENTS: Continued from previous page.

SOLID PHASE

TOTAL SOLIDS:

VOLATILE SOLIDS:

PARAMETER	Zr	U				
Concentration (ppm)	223.	18.5				

MEASURED CHARACTER I ST IC	TEST CONDITION	Zr	Ва	Hg	Si				1 1	
Concentration	DW 4:1	<0.05	0.189	<1.	15.9	1				
(mg/L)	DW 20:1	<0.05	0,192	<1.	5.73					
	AS 4:1	<0.05	1.31	<1.	70.6	ļ		1		
	AS 20:1	<0.05	2.74	<1.	53.9			1		
	SL 4:1	0.09	1.18	<1.	155.					
	SL 20:1	0.05	2,13	<1.	102.					
Release	DW 4:1		0.76		63.6			 1	1	
(µg/g)	DW 20:1		3.84		115.	1				(
	AS 4:1		5.24		282.					
	AS 20:1		54.8		1078.					
	SL 4:1	0.36	4.72		620.					
	SL 20:1	1.00	42.6		2040.					
Efficiency	DW 4:1	1 1						 		
(%)	DW 20:1									-
	AS 4:1					1				
	AS 20:1									
	SL 4:1	0.27							1	
	SL 20:1	0.75							Į	

#### SAMPLE NO.: 8 WASTE TYPE: Fly Ash from a Coal Fired Generating Station

DATE TESTED: September 1981

COMMENTS: Light grey

SOLID PHASE

TOTAL SOLIDS: 100% VOLATILE SOLIDS:

PARAMETER	Ag	AI	в	Be	Са	Cd	0r	Qu	Fe	к
Concentration (ppm)	<0.5	111 000.	442	3.28	94 600.	4.7	28.8	38.	31 300.	6200.

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Ag	Al	В	Be	Са	Cd	Cr	Cu	Fe	к	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.005	1.09	8.45	<0.001	457.	<0.01	0.83	0.012	0.05	4.	11.4	3.0
(mg/L)	DW 20:1	<0.005	3.77	3.92	<0.001	192.	<0.01	0.21	0.008	0.03	1.	11.2	1.5
	AS 4:1	<0.005	1.26	20.7	<0.001	1830.	0.02	1.01	0.008	0.11	3.	10.1	7.0
	AS 20:1	<0.005	13.0	10.5	<0.001	944.	0.01	0.27	0.095	3.05	<1.	5.2	6.5
	SL 4:1	<0.005	0.89	30.3	<0.001	2890.	0.02	0.76	0.387	0.21	2.	8.5	15.0
	SL 20:1	<0.005	168.	14.4	0.022	1410.	0.01	0.19	0.213	145	<1.	5.2	12.5
Release	DW 4:1		4.36	33.8		1828.		3.32	0.05	0.20	16.		
(µg/g)	DW 20:1		75.4	78.4		3840.		4.20	0.16	0.60	20.		
	AS 4:1		5.04	82.8		7320.	0.08	4.04	0.03	0.44	12.		
	AS 20:1		260.	210.		18 880.	0.20	5.40	1.90	61.0			
	SL 4:1		3.56	121.		11 560.	0.08	3.04	1.55	0.84	8.		
	SL 20:1		3360.	288.	0.44	28 200.	0.20	3.80	4.26	2900.			
Efficiency	DW 4:1		<0.01	7.65		1.93		11.5	0.13	<0.01	0.26		
(%)	DW 20:1		0.07	17.7		4.06		14.6	0.42	<0.01	0.32		
	AS 4:1		<0.01	18.7		7.74	1.70	14.0	0.08	<0.01	0.19		
×	AS 20:1		0.23	47.5		19.9	4.26	18.8	5.00	0.19	1		
	SL 4:1		<0.01	27.4		12.2	1.70	10.6	4.07	<0.01	0.13		
	SL 20:1		3.03	65.2	13.3	29.8	4.26	13.2	11.2	9.27			

## SAMPLE NO.: 8 WASTE TYPE: Fly Ash

DATE TESTED: September 1981

COMMENTS: Continued from previous pages.

SOLID PHASE	TOT	L SOLIDS:		VOLATIL	E SOLIDS	:								
	PARAMETER	Mg	Mn	Мо	Na	NI	P	Pb	Sr	TI	v	Zn	Co	Th
ĺ	Concentration (ppm	9310.	721.	60.	4100.	44.	710.	40.	327.	3700.	65.4	43.	23.	25.
MULTIPLE-BA	TCH LEACHING PROCE	URE												
MEASURED CHARACTER IS		Mg	Mn	Мо	Na	Nİ	Ρ	Pb	Sr	TI	v	Zn	60	Th
Concentrati (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.05 0.13 2.12 67.4 134. 112.	<0.01 <0.01 <0.01 1.31 0.26 6.08	1.1 0.4 1.3 0.5 1.6 0.8	6. 1.	0.05 <0.05 <0.05 0.23 0.21 0.31	<0.6 <0.6 0.9 1.0 1.6 1.9	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	3.18 0.864 5.85 2.81 8.75 4.18	<0.005 <0.005 <0.005 0.112 <0.005 6.67	0.028 0.091 0.410 0.048 0.744 0.505	<0.05 0.05 <0.05 0.40 <0.05 0.21	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	0.05 0.08 <0.01 0.03 <0.01 <0.01
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.20 2.60 8.48 1348. 536. 2240.	26.2 1.04 122.	4.4 8.0 5.2 10.0 6.4 16.0	24. 20.	0.20 4.60 0.84 6.20	3.6 20.0 6.4 38.0		12.7 17.3 23.4 56.2 35.0 83.6	2.24 133.	0.11 1.82 1.64 0.96 2.98 10.1	1.0 8.0 4.2		0.2 1.6 0.6
Efficiency (\$)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.01 0.03 0.09 14.5 5.76 24.1	3.63 0.14 16.9	7.33 13.3 8.67 16.7 10.7 26.7	0.59 0.49	0.45 10.5 1.91 14.1	0.51 2.82 0.90 5.35		3.89 5.28 7.16 17.2 10.7 25.6	0.06 3.61	0.17 2.78 2.51 1.47 4.55 15.4	2.33 18.6 9.77		0.8 6.4 2.4

SAMPLE NO.:	8	WASTE TYPE:	Fly Ash
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DATE TESTED: September 1981

COMMENTS: Continued from previous page.

SOLID PHASE	TOT <b>A</b>	L SOLIDS:		VOLATILI	E SOLIDS:	:						
ſ	PARAMETER	Zr	U		1				1		7	
	Concentration (ppm	) 275.	17.5									
. <u></u>				<u> </u>			 			4. i		
MULTIPLE-BA	TCH LEACHING PROCED	URE						_				
MEASURED CHARACTER IS		Zr		Ва	SI							
Concentrati (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.05 <0.05 0.05 <0.05 <0.05 0.79		0.187 0.146 <0.005 0.361 <0.005 0.634	7.29 23.8 128. 64.6							
Release (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.20 15.8		0.75 2.92 7.22 12.7	21.4 146. 95.2 2560. 258. 4290.							
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.07										

SAMPLE NO.: 9 WASTE TYPE: Fly Ash from a Coal Fired Generating Station

DATE TESTED: September 1981

COMMENTS: Light grey-brown.

SOLID PHASE

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TOTAL SOLIDS: 99.6% VOLATILE SOLIDS: 3.2%

PARAMETER	Ag	AI	Be	Ca	Cd	۲r	Qu	Fe	к	Mg
Concentration (ppm)	<0.5	137 000.	9.95	6030.	<0.8	<0.8	142.	180 000.	31 400.	9000.

MEASURED CHARACTERISTIC	TEST CONDITION	Ag	Ał	Ве	Са	Cd	ᠬ	Cu	Fe	к	Mg	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.005	53.9	0.016	262.	0.09	0.02	1.32	1.82	111.	22.7	3.2	2.43
(mg/L)	DW 20:1	<0.005	12.5	0.004	52.9	<0.01	0.01	0.36	0.99	22.	4.68	2.5	0.92
	AS 4:1	<0.005	113.	0.022	302.	0.09	0,58	1.45	18.6	118.	23.5	3.6	4.90
	AS 20:1	<0.005	24.5	0.006	63.2	<0.01	0.16	0.40	5.48	24.	5.24	3.7	3.60
	SL 4:1	<0.005	121.	0.026	308.	0.09	0.78	2.33	38.6	129.	23.7	4.6	9.00
	SL 20:1	<0.005	28.5	0.006	63.9	<0.01	0.19	0.59	15.5	22.	5.31	4.7	8.00
Release	DW 4:1		216.	0.06	1048.	0.36	0.08	5.28	7.28	444.	90.8		
(µg/g)	DW 20:1		250.	0.08	1058.		0.20	7.20	19.8	440.	93.6		
	AS 4:1		452.	0.09	1208.	0.36	2.32	5.80	74.4	472.	94.0		
	AS 20:1	1	490.	0.12	1264.		3.20	8.02	110.	480.	105.		
	SL 4:1		484.	0.10	1232.	0.36	3.12	9.32	154.	516.	94.8		
	SL 20:1		570.	0.12	1278.		3.80	11.7	310.	440.	106.		
Efficiency	DW 4:1		0.16	0.65	17.5			3.73	<0.01	1.42	1.01		
(%)	DW 20:1		0.18	0.81	17.6			5.09	0.01	1.41	1.04		
	AS 4:1		0.33	0.89	20.1			4.10	0.04	1.51	1.05		
	AS 20:1		0.36	1.21	21.1			5.67	0.06	1.53	1.17		
	SL 4:1		0.35	1.05	20.5			6.59	0.09	1.65	1.06		
	SL 20:1		0.42	1.21	21.3			8.27	0.17	1.41	1.18		

## SAMPLE NO.: 9 WASTE TYPE: Fly Ash

DATE TESTED: September 1981

COMMENTS: Continued from previous page.

SOLID PHASE	_	TOTAL	SOLIDS:		VOLATILE	SOLIDS:									
ſ	PARAME	ETER	Mn	Мо	Na	Ni	Р	Pb	Sr	ті	v	Zn	1		]
-	Concer	ntration (ppm)	578.	<30	7900.	113.	<50.	325.	365.	5400.	217.	594.			
MULTIPLE-BA	TCH LE	ACHING PROCEDU	RE												
MEASURED CHARACTER IS		TEST CONDITION	Mn	Мо	Na	NĪ	Р	Pb	Sr	Ti	v	Zn	В	Ва	Si
Concentrati (mg/L)	on	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	2.26 0.44 3.34 0.61 3.42 0.60	0.3 <0.3 0.5 0.3 1.0 0.6	96. 20.	0.53 0.13 0.47 0.12 0.51 0.12	0.9 <0.6 1.9 <0.6 1.5 0.7	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05	2.44 0.502 2.65 0.585 2.78 0.656	0.011 0.008 0.338 0.048 0.290 0.092	0.011 0.008 0.157 0.044 0.333 0.455	2.98 0.62 2.83 0.66 2.87 0.64	3.94 0.771 4.19 0.832 3.99 0.780	0.059 0.165 0.059 0.090 0.070 0.380	16.9 3.31 34.7 7.63 40.9 12.1
Rəleasə (µg/g)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	9.04 8.80 13.4 12.2 13.7 12.0	1.2 2.0 6.0 4.0 12.	384. 400.	2.12 2.60 1.88 2.40 2.04 2.40	3.6 7.6 6.0 14.0		9.76 10.0 10.6 11.7 11.1 13.1	0.04 0.16 1.35 0.96 1.16 1.84	0.04 0.16 0.63 0.88 1.33 9.10	11.9 12.4 11.3 13.2 11.5 12.8	15.8 15.4 16.8 16.6 16.0 15.6	0.24 3.30 0.24 1.80 0.28 7.60	67.6 66.2 139. 153. 164. 242.
Efficiency (%)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	1.57 1.53 2.32 2.12 2.38 2.08		4.88 5.08	1.88 2.31 1.67 2.13 1.81 2.13			2.68 2.76 2.92 3.22 3.06 3.61	<0.01 <0.01 0.03 0.02 0.02 0.03	0.02 0.07 0.29 0.41 0.62 4.21	2.01 2.10 1.91 2.23 1.94 2.16			

SAMPLE NO.: 10 WASTE TYPE: Bottom Ash from a Coal Fired Generating Station

DATE TESTED: September 1981

COMMENTS: Black,

SOLID PHASE

TOTAL SOLIDS: 99.6% VOLATILE SOLIDS: 3.5%

PARAMETER	Ag	Al	Ве	Са	Cd	٥٢	Qu	Fe	к	Mg
Concentration (ppm)	<0.5	135 000.	6.36	5250.	<0.8	<0.8	74.	177 000.	31 300.	9420.

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST	Ag	Al	Ве	Ga	Cd	Cr	Cu	Fe	к	Mg	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.005	0.86	<0.001	67.4	0.10	0.03	0.150	0.06	8.	7.85	3.4	0.52
(mg/L)	DW 20:1	<0.005	<0.01	<0.001	10.9	<0.01	0.02	0.080	0.06	<1.	1.21	3.6	0.18
	AS 4:1	<0.005	5.06	0.002	79.6	0.15	0.16	0.464	0.75	8.	9.18	4.4	3.40
	AS 20:1	<0.005	1.04	0.007	13.6	<0.01	0.04	0.147	0.52	<1.	1.61	4.4	3.20
	SL 4:1	<0.005	11.2	0.002	71.5	0.09	0.21	0.627	17.9	6.	8.56	4.6	8,50
	SL 20:1	<0.005	3.64	<0.001	19.5	0.02	0.07	0.196	12.3	<1.	2.37	4.5	8.50
Release	DW 4:1		3.44		270.	0.40	0,12	0.60	0.24	32.	31.4		
(µg/g)	DW 20:1				218.		0.40	1.60	1.20		24.2		
	AS 4:1		20.2	0.01	318.	0.60	0.64	1.86	3.00	32.	36.7		
	AS 20:1		20.8	0.14	272.		0.80	2.94	10.4		32.2		
	SL 4:1		44.8	0.01	286.	0.36	0.84	2.51	71.6	24.	34.2		
	SL 20:1		72.8		390.	0.40	1.40	3.92	246.		47.4		
Efficiency	DW 4:1		<0.01		5,16		· _ ·	0.81	<0.01	0.10	0,33		
(%)	DW 20:1				4.17			2.17	<0.01		0.26		
	AS 4:1		0.02	0.13	6.09			2.52	<0.01	0.10	0.39		
	AS 20:1		0.02	2.21	5.20			3.99	0.01		0.34		
	SL 4:1		0.03	0.13	5.47			3.40	0.04	0.08	0.36		
	SL 20:1		0.05		7.46			5.32	0.14		0.51		

## SAMPLE NO.: 10 WASTE TYPE: Bottom Ash

DATE TESTED: September 1981

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COMMENTS: Continued from previous page.

SOLID PHASE	TOTAL	SOLIDS:		VOLATILE	SOLIDS	:								
ſ	PARAMETER	Mn	Мо	Na	NI	Р	Pb	Sr	TI	v	Zn			7
-	Concentration (ppm)	639.	<30.	7700.	91.	<50.	30.	288.	5090.	172.	103.			
MULTIPLE-BA	TCH LEACHING PROCEDU	RE			-									
MEASURED CHARACTERIS		Min	Мо	Na	NI	Р	РЪ	Sr	TI	v	Zn	В	Ва	SI
Concentratio (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	1.98 0.31 2.34 0.44 2.43 0.63	<0.3 <0.3 <0.3 <0.3 <0.3 <0.3 <0.3	5. <1.	1.41 0.25 2.11 0.31 1.68 0.53	<0.6 <0.6 <0.6 <0.6 <0.6 <0.6 <0.6	<0.05 <0.05 0.05 <0.05 0.05 <0.05	0.377 0.062 0.404 0.085 0.427 0.111	<0.005 <0.005 <0.005 <0.005 <0.005 <0.005	<0.005 <0.005 <0.005 <0.005 <0.005 <0.005	0.89 0.16 1.35 0.31 1.12 0.40	0.107 <0.004 0.108 <0.004 0.084 <0.004	0.062 0.049 0.096 0.091 0.190 0.140	2.4 0.6 4.2 0.4 4.9
Release (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	7.92 6.20 9.36 8.80 9.72 12.6		20.	5.64 5.00 8.44 6.20 6.72 10.6		0•20 0•20	1.51 1.24 1.62 1.70 1.71 2.22			3.56 3.20 5.40 6.20 4.48 8.00	0.43 0.43 0.34	0.25 0.98 0.38 1.82 0.76 2.80	9.9 12.2 17.0 9.0 19.9 30.0
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	1.24 0.97 1.47 1.38 1.53 1.98		0.26	6.22 5.52 9.31 6.84 7.41 11.7		0.67 0.67	0.53 0.43 0.56 0.59 0.60 0.77			3.47 3.12 5.26 6.04 4.37 7.80			

## SAMPLE NO.: 11 WASTE TYPE: Gold Mine Tailings

DATE TESTED: August 1981

COMMENTS: Blanket cyanide treatment. Mercury used to form amalgam. Arseno-pyrite ore.

SOLID PHASE

TOTAL SOLIDS: 86.1% VOLATILE SOLIDS: 0.7%

PARAMETER	Cu	Hg	Pb	Zn	TCN			
Concentration (ppm)	128.	0.88	48.	194.	1.26			

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER ISTIC	TEST CONDITION	Cu	Hg	Pb	Zn	TCN				pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.03	0.00030	<0.1	0.05	0.021				6.7	2.48
(mg/L)	DW 20:1	<0.03	0.00015	<0.1	0.07	0.020		1		6.9	1.75
	AS 4:1	0.36	0.00025	<0.1	2.31	0.022				4.3	7.00
	AS 20:1	0.16	0.00040	<0.1	0.92	0.012				4.3	5.00
	SL 4:1	2.52	0.00020	0.3	3.57	0.046				4.4	11.3
	SL 20:1	0.66	0.00043	0.3	0.82	0.034				4.4	9.70
Release	DW 4:1		0.001		0.20	0.08					
(µg/g)	DW 20:1		0.003		1.40	0.40					
	AS 4:1	1.44	0.001		9.24	0.09				1 1	
	AS 20:1	3.20	0.008		18.4	0.24					
	SL 4:1	10.1	0.008	1.2	14.3	0.18					
	SL 20:1	13.2	0.008	6.0	16.4	0.68					
Efficiency	DW 4:1		0.16		0.1?	7.74					
(%)	DW 20:1	1	0.40		0.84	36.9					
	AS 4:1	1.31	0.13		5.53	8.11					
	AS 20:1	2.90	1.06		11.0	22.1	1				
	SL 4:1	9.15	0.11	2.9	8.55	17.0					
	SL 20:1	12.0	1.14	14.5	9.82	62.7					

#### SAMPLE NO.: 12 WASTE TYPE: Anaerobically Digested WWTP Sludge

DATE TESTED: July 1981

COMMENTS: From an activated sludge treatment plant with anaerobic digestion. The following organic compounds were detected in the sludge: phenanthrene at 17 µg/g, flourene at 3 µg/g, di-n-butylphthalate at 116 µg/g, and bis-(2-ethylhexyl) phthalate at 408 µg/g. None of these were detected in the leachates, except for di-n-butylphthalate at 0.01 mg/L in the DW 20:1 leachate

SOLID PHASE

TOTAL SOLIDS: 3.2% VOLATILE SOLIDS: 46.0%

PARAMETER					
Concentration (ppm)					

MEASURED CHARACTER ISTIC	TEST CONDITION	As	Cd	٥r	Min	NĪ	РЪ	Zn		pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1										
(mg/L)	DW 20:1	0.004	<0.03	<0.1	<0.03	<0.1	<0.1	0.09		8.1	0.113
	AS 4:1 AS 20:1	0.013	<0.03	<0.1	0.20	<0.1	<0.1	3,36		4.8	3.00
	SL 4:1										
	SL 20:1										
Release	DW 4:1										
(µg/g)	DW 20:1	0.08						1.8			
	AS 4:1										
	AS 20:1	0.26			0.8			67.2			
	SL 4:1										
	SL 20:1										
Efficiency	DW 4:1										
(%)	DW 20:1										
	AS 4:1										
	AS 20:1										
	SL 4:1										
	SL 20:1										

## SAMPLE NO.: 12 WASTE TYPE: Anaerobically Digested WWTP Sludge

DATE TESTED: July 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure = 61 mL = 1.10 meq  $H^+/g$  waste.

EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

MEASURED CHARACTERISTIC	TEST CONDITION	CD	Gr	Cu	Mn	NÎ	РЬ	Zn		pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	<0.03	<0.10	<0.03	0.67	0.1	<0.1	3.15		6.70	3.90
Release (µg/g)	EPA ASTM DW ASTM AS				13.4	2.0		63.0			
Efficiency (%)	EPA ASTM DW ASTM AS										

MEASURED CHARACTER I ST I C	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Release (µg/g)	EPA ASTM DW ASTM AS							
Efficiency (%)	EPA ASTM DW ASTM AS							

## SAMPLE NO.: 13 WASTE TYPE: Mine Tailings

DATE TESTED: July 1981

COMMENTS: Grey

SOLID PHASE

TOTAL SOLIDS: 16.2% VOLATILE SOLIDS: 1.3%

PARAMETER	As	Cd	Cu	Мо	Pb	Zn		
Concentration (ppm)	24.	110.	196.	1240.	840.	4790.		

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	As	Cd	Qu	Мо	РЬ	Zn		1	pH nits)	Conductivity (mS/cm)
Concentration	DW 4:1	0.170	<0.3	0.05	<0.1	<0.1	0.07			7.20	0.291
(mg/L)	DW 20:1	0.020	<0.3	<0.03	<0.1	<0.1	<0.03			6.95	0.120
	AS 4:1	0.084	<0.3	0.57	<0.1	1.3	1.14			5.10	4.49
	AS 20:1	0.005	<0.3	0.28	<0.1	1.0	0.65			4.55	3.58
	SL 4:1		<0.3	0.32	<0.1	5.9	0.76			4.85	10.0
	SL 20:1		<0.3	0.09	<0.1	1.8	0.41			4.60	9.80
Release	DW 4:1	0.68		0.20			0.28	 			
(µg/g)	DW 20:1	0.40									
	AS 4:1	0.34		2.28		5.2	4.56				
	AS 20:1	0.10		5.60		20.0	13.0				
	SL 4:1			1.28		23.6	3.04				
	SL 20:1			1.80		36.0	8.20				
Efficiency	DW 4:1	17.5		0.63			0.04				
(%)	DW 20:1	10.3									
	AS 4:1	8.64		7.18		3.82	0.59	1			
	AS 20:1	2.57		17.6		14.7	1.67				
	SL 4:1			4.03	l I	17.3	0.39	{			
	SL 20:1			5.67		26.5	1.06				

SAMPLE NO.: 13 WASTE TYPE: Mine Tailings

DATE TESTED: July 1981

**COMMENTS:** Continued from previous page. Acid addition in EPA extraction procedure =  $31.0 \text{ mL} = 0.26 \text{ meq H}^+/\text{g}$  of waste.

MEASURED CHARACTER I ST IC	TEST CONDITION	Cd	Cu	Мо	РЪ	Zn			pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	<0.3	0.06	<0.1	<0.1	0.31			4.95	1.30
Release (µg/g)	EPA ASTM DW ASTM AS		1.20			6.2				
Efficiency (≴)	EPA ASTM DW ASTM AS		3.78			0.8				

EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

MEASURED CHARACTER I ST IC	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS				L.			
Release (µg/g)	EPA ASTM DW ASTM AS							
Efficiency (%)	EPA ASTM DW ASTM AS							

## SAMPLE NO.: 14 WASTE TYPE: Metal Finishing Sludge

DATE TESTED: September 1981

COMMENTS: Gold-brown, cake from pressure filter.

SOLID PHASE

## TOTAL SOLIDS: 29.6% VOLATILE SOLIDS: 35.2%

PARAMETER	Cd	Gr	Cu	Fe	РЬ	Sn	Zn	TCN	
Concentration (ppm)	1920.	7640.	518.	41000.	200.		83000.	19000.	

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Cd	٥r	Cu	Fe	РЪ	Sn	Zn	TCN		pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.14	0.7	2.63	<0.1	<0.1	0.026	1.04	1.83		9.05	2.10
(mg/L)	DW 20:1	0.04	0.2	0.06	<0.1	<0.1	<0.020	1.00	0.41	ļ	8.85	2.32
	AS 4:1	3.36	<0.1	6.30	<0.1	<0.1	<0.020	21.0	6.00		7.45	7.60
	AS 20:1	38.0	<0.1	2.18	<0.1	<0.1	<0.020	688.	4.00		5.90	6.85
	SL 4:1	36.0	1.4	9.66	0.3	<0.1	0.032	648.	7.55		6.65	12.50
	SL 20:1	67.0	38.0	2.65	8.9	<0.1	0.592	2211.	6.57		5.25	11.15
Release	DW 4:1	0.56	2.8	10.5			0.10	4.16	7.32			
(µg∕g)	DW 20:1	0.80	4.0	1.2				20.0	8.20			
	AS 4:1	13.4		25.2				84.0	24.0			
	AS 20:1	760.		43.6				13 760.	80.0			
	SL 4:1	144.	5.6	38.6	1.2		0.13	2590.	30.2			
	SL 20:1	1340.	760	53.0	178.		11.8	44 220.	131			
Efficiency	DW 4:1	0.10	0.12	6.86				0.02	0.13			
(%)	DW 20:1	0.14	0.18	0.78	l i			0.08	0.15			
	AS 4:1	2.36		16.4				0.34	0.43			
	AS 20:1	134.		28.4				56.0	1.42			
	SL 4:1	25.3	0.25	25.2	0.01			10.6	0.54	1		
	SL 20:1	235.	33.6	34.6	1.47			180.	2.34			

SAMPLE NO.: 14 WASTE TYPE: Metal Finishing Sludge

DATE TESTED: September 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure = 400 mL = 2.00 meq H<sup>+</sup>/g waste.

EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS	
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MEASURED CHARACTER I ST IC	TEST CONDITION	Cđ	Cr	Qu	Fe	РЪ	Sn	Zn	-		pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	6.1	0.2	0.87	<0.1	<0.1	<0.02	1265.			5.50	4.30
Release (µg/g)	EPA ASTM DW ASTM AS	1220.	4.0	17.4				25 300.				
Efficiency (%)	EPA ASTM DW ASTM AS	214.	0.18	11.4				103.				

MEASURED CHARACTER I ST IC	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Re∤ease (µg∕g)	EPA ASTM DW ASTM AS							
Efficiency (%)	EPA ASTM DW ASTM AS							

#### SAMPLE NO.: 15 WASTE TYPE: Caustic Metal Cleaning Waste

DATE TESTED: July 1981

COMMENTS: Grey. Neutralized spent caustic metal cleaner, solidified with Portland cement.

## TOTAL SOLIDS: 87.7% VOLATILE SOLIDS: 6.7%

PARAMETER	Cd	Cr	Cu	Fe	NĪ	Zn		
Concentration (ppm)	5.71	74 900.	220 000	6000.	57.1	73200.		

#### WTC LEACHING PROCEDURE

MEASURED CHARACTER ISTIC	TEST CONDITION	Cd	G	Cu	Fe	NI	Zn				pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.03	0.30	0.12	0.1	<0.10	0.07				12.40	12.30
(mg/L)	DW 20:1	<0.03	<0.10	<0.03	<0.1	<0.10	<0.03				12.30	5.10
	AS 4:1	<0.03	0.20	0.08	0.1	<0.10	0.03		1		12.20	12.20
	AS 20:1	<0.03	0.63	0.03	0.1	<0.10	0.05				9.65	7.70
	SL 4:1	<0.03	9.7	22.0	0.2	0.20	0.97				10.30	15.30
	SL 20:1	0.03	24.5	18.0	9.3	0.22	2.51				7.55	12.75
Release	DW 4:1	1	1.2	0.48	0.4		0.28					
(µg/g)	DW 20:1											
	AS 4:1		0.8	0.32	0.4		0.12					
	AS 20:1		12.5	0.60	1.5		1.00					
	SL 4:1		38.8	88.0	0.8	0.8	3.88				1	
	SL 20:1	0.6	490.	360.	186.	4.4	50.2					
Efficiency	DW 4:1		<0.01	<0.01	0.01		<0.01	 <b>.</b>				
· (%)	DW 20:1		l									
	AS 4:1	ļ	<0.01	<0.01	0.01		<0.01					
	AS 20:1		0.02	<0.01	0.03		<0.01					
•	SL 4:1		0.06	0.05	0.02	1.60	0.01					
	SL 20:1	12.0	0.75	0.19	3.53	8.79	0.08			Î .		

## SAMPLE NO.: 15 WASTE TYPE: Caustic Metal Cleaning Waste

DATE TESTED: July 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure = 400 mL = 2.00 meq H<sup>+</sup>/g of waste.

EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

MEASURED CHARACTER I ST IC	TEST CONDITION	Cd	Cr	Qu	Fe	Nİ	Zn			pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	<0.03 <0.03	<0.1 6.8	0.04 1.38	0.2 1.8	<0.1	<0.03 0.53			11.55 5.50	6.65 7.50
Release (µg/g)	EPA ASTM DW ASTM AS		27.2	0.80 5.52	4.0 7.2		2.12				
Efficiency (≴)	EPA ASTM DW ASTM AS		0.04	<0.01 <0.01	0.08 0.14		<0.01				

Conductivity MEASURED TEST pН (mS/cm) CHARACTERISTIC CONDITION (Units) Concentration EPA (mg/L) ASTM DW ASTM AS Release EPA (µg/g) ASTM DW ASTM AS Efficiency EPA (%) ASTM DW ASTM AS

## SAMPLE NO.: 16 WASTE TYPE: Halifax Harbour Dredge Spoils

DATE TESTED: July 1981

COMMENTS: Black. Dredge spoils disposed in bermed site on DND property in Spring, 1980.

SOLID PHAS	E TOTAL	SOLIDS:	68.3%	VOLATILE	SOLIDS:	9.5%					
	PARAMETER	Cd	Cu	Pb	Zn	PCB				7	
	Concentration (ppm)	17.6	171.	448.	534.	N.D.				1	
								 		_	
MULTIPLE-B/	ATCH LEACHING PROCEDU	RE									
MEASURED CHARACTER IS		Cd	Cu	Рb	Zn	PCB	Hg			pH (Units)	Conductivity (mS/cm)
Concentrat (mg/L)	ion DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.03 <0.03	<0.03 <0.03	<0.1 1.9	0.07 6.09	<0.01 <0.01	0.000 24			7.7 4.6	0.64 4.90
Release (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.06		38.	1.4 122.		0.005				
Efficiency (≴)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	4.99		12.4	0.38 33.4						

## SAMPLE NO.: 18 WASTE TYPE: Leaded Refinery Organic Fuel Tank Sludge

DATE TESTED: August 1981

COMMENTS: Black, gasoline odour.

## SOLID PHASE

TOTAL SOLIDS: 76.7% VOLATILE SOLIDS: 12.3%

PARAMETER	Pb	TOC	Phenol				
Concentration (ppm)	286.	29 700.	42.8				

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	РЬ	тос	Phenol				pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.1 <0.1	1220 <b>.</b> 288.	590 <b>.</b> 75.				10.65 10.35	4.80 1.23
Release (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.4	4880. 5760.	2360 <b>.</b> 1500 <b>.</b>					
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.18	21.4 25.3						

## SAMPLE NO.: 19 WASTE TYPE: Fresh Mining and Smelting Tailings

DATE TESTED: February 1982

COMMENTS: From copper/lead/zinc mine/mill/smelter.

SOLID PHASE	TOTAL	SOLIDS: 7	4.5%	VOLATILE	SOL IDS :	4.4%		
	PARAMETER							
-	Concentration (ppm)							

# MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Cd	Cu	Pb	Zn	SO4				pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1										
(mg/L)	DW 20:1 AS 4:1	<0.01	0.02	<0.1	0.06	62.				7.10	0.32
	AS 20:1	0.02	0.21	13.0	9.66	44.				4.95	4.90
	SL 4:1 SL 20:1					1					
Release	DW 4:1										
(µg/g)	DW 20:1 AS 4:1		0.4		1.2	1240.					
	AS 20:1	0.4	4.2	260.	193.	880.		i			
	SL 4:1 SL 20:1										
Efficiency	DW 4:1										
(%)	DW 20:1			1							
	AS 4:1										
	AS 20:1										
	SL 4:1 SL 20:1										

## SAMPLE NO.: 20 WASTE TYPE: Mining and Smelting Tailings

DATE TESTED: August 1981

COMMENTS: See Sample 19. Tailings approximately two years old

SOLID PHASE

TOTAL SOLIDS: 89.9% VOLATILE SOLIDS: 3.8%

PARAMETER	Cd	Cu	Pb	Zn			
Concentration (ppm)	10.	1800.	545	6990.			

MEASURED CHARACTERISTIC	TEST CONDITION	Cd	Cu	Pb	Zn	so <sub>4</sub>				pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.02	<0.02	<0.1	2.31	1065.				6,50	2.42
(mg/L)	DW 20:1	<0.02	<0.02	<0.1	0.34	388.				6.90	1.13
	AS 4:1	0.31	0.13	0.2	30.0	954.	1			5.65	7.70
	AS 20:1	0.10	0.16	1.5	17.0	356.		1		4.75	5.50
	SL 4:1	0.48	8.40	3.1	62.0	1454.	(	1	(	5,10	13.00
	SL 20:1	0.11	2.32	3.4	17.0	464.				4.70	9.70
Release	DW 4:1	0.08			9.24	4260.					
(µg/g)	DW 20:1				6.80	7760.					
	AS 4:1	1.24	0.52	0.8	120.	3816.					
	AS 20:1	2.00	3.20	30.0	340.	7120.					
	SL 4:1	1.92	33.6	12.4	248.	5816.					
	SL 20:1	2.20	46.4	68.0	340.	9280.					
Efficiency	DW 4:1	0.89			0.15						
(\$)	DW 20:1				0.11						
	AS 4:1	13.8	0.03	0.16	1.91						
	AS 20:1	22.3	0.20	6.12	5.41		1				
	SL 4:1	21.4	2.07	2.53	3.95						
	SL 20:1	24.5	2.86	13.9	5.41						

SAMPLE NO.: 21	WASTE TYPE:	Mining and	Smelting	Tailings

DATE TESTED: March 1982

COMMENTS: See Sample 19. Tailings Approximately 6 to 10 years old

SOLID PHASE

TOTAL SOLIDS: 92.5% VOLATILE SOLIDS: 10.4%

PARAMETER					
Concentration (ppm)					

MEASURED CHARACTER I ST IC	、 TEST CONDITION	Cd	Cu	Pb	Zn	so <sub>4</sub>					pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1									-		
(mg/L)	DW 20:1 AS 4:1	0.16	4.83	<0.1	57.	1718.					2.80	2.70
	AS 20:1 SL 4:1	0.26	1.72	<0.1	57.	1912.					4.15	4.90
	SL 20:1											
Release	DW 4:1	-				<b>-</b>						
(µg/g)	DW 20:1 AS 4:1	3.2	96.6		1140.	34 360.						
	AS 20:1 SL 4:1	3.2	34.4		1140.	38 240.			,			
	SL 20:1											
Efficiency	DW 4:1						· ,	1				
(%)	DW 20:1											
	AS 4:1		1									
	AS 20:1		1									
	SL 4:1											
	SL 20:1											

## SAMPLE NO.: 22 WASTE TYPE: Mining and Smelting Tailings

DATE TESTED: August 1981

COMMENTS: See Sample 19. Tailings approximately 15 years old.

SOLID PHASE

TOTAL SOLIDS: 77.8% VOLATILE SOLIDS: 3.6%

PARAMETER	Cd	Cu	Mg	Pb	Zn			
Concentration (ppm)	21.9	1190.	283 000.	555.	8220.			

MEASURED CHARACTER ISTIC	TEST CONDITION	Cd	Cu	Mg	РЬ	Zn	SO <sub>4</sub>	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.02	<0.02	294.	0.1	7.77	2306.	6.40	3.30
(mg/L)	DW 20:1	0.06	<0.02	63.	<0.1	11.0	876.	6.50	1.69
	AS 4:1	0.09	<0.02	294.	4.0	282.	2394.	5.00	7.90
	AS 20:1	0.68	0.21	95.	6.1	115.	768.	4.50	5.20
	SL 4:1	1.43	0.02	315.	18.0	441.	2300.	4.70	12.50
	SL 20:1	0.62	1.39	84.	10.0	115.	1082.	4.55	9.30
Release	DW 4:1			1176.	0.4	31.1	9224.		
(µg/g)	DW 20:1	1.20		1260.		220.	17 520.		
	AS 4:1	0.36		1176.	16.0	1128.	9576.		
	AS 20:1	13.6	4.20	1900.	122.	2300.	15 360.		
	SL 4:1	5.72	0.08	1260.	72.	1764.	9200.		
	SL 20:1	12.4	27.8	1680.	200.	2300.	21 640.		
Efficiency	DW 4:1			0.53	0.09	0.49			
(%)	DW 20:1	7.04		0.57		3.44			
	AS 4:1	2.11		0.53	3.71	17.6			
	AS 20:1	79.8	0.45	0.86	28.3	36.0			
	SL 4:1	33.6	0.01	0.57	16.7	27.6			
	SL 20:1	72.8	3.01	0.76	46.3	36.0			

## SAMPLE NO.: 23 WASTE TYPE: Zinc Sulphide Residue

DATE TESTED: August 1981

COMMENTS: Excess residue from zinc plant (acid leach solids)

SOLID PHASE

TOTAL SOLIDS: 75.2% VOLATILE SOLIDS: 0.8%

PAF	RAMETER	Fe	Zn				
Cor	ncentration (ppm)	359 000.	372 000.				

MEASURED CHARACTER I ST IC	TEST CONDITION	Fe	Zn	SO <sub>4</sub>						pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.1	3461.	5460.						5.30	6.00
(mg/L)	DW 20:1	<0.1	893.	1478.						5.10	2.18
	AS 4:1	0.2	4504.	6500.	•					4.60	9.70
	AS 20:1	0.2	1204.	1340.						4.45	5.70
	SL 4:1	2.6	4723.	7170.						4.50	12.75
	SL 20:1	4.7	1297.	1560.						4.50	9.20
Release	DW 4:1		13 844.	21 840.	 		1	 			
(µg/g)	DW 20:1		17 860.	29 560.							
	AS 4:1	0.8	18 016.	26 000.							
	AS 20:1	4.0	24 080.	26 800.							
	SL 4:1	10.4	18 892.	28 680.							
	SL 20:1	94.0	25 940.	31 200.							
Efficiency	DW 4:1		4.94								
(%)	DW 20:1		6.38		1	ļ					
	AS 4:1	0.01	6.43	J							
	AS 20:1	0.01	8.60								
	SL 4:1	0.01	6.75	1							
	SL 20:1	0.03	9.27	1	1		1		<b> </b>		

## SAMPLE NO.: 24 WASTE TYPE: Zinc Hydroxide Sludge

DATE TESTED: August 1981

COMMENTS: Originated from floor washings, overflow from zinc oxide pond, etc., which is mixed with slurried lime to precipitate zinc for recovery.

SOLID PHASE

TOTAL SOLIDS: 14.3% VOLATILE SOLIDS: 8.7%

PARAMETER	Cu	Pb	Zn				
Concentration (ppm)	1180.	371.	385 000.				

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Cu	Pb	Zn				pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.02	<0.1	0.16				8.90	2.22
(mg/L)	DW 20:1	<0.02	<0.1	0.37				2.90	3.18
	AS 4:1	0.04	1.4	560.				6.85	6.60
	AS 20:1	5.25	0.9	1760.				5.70	7.40
	SL 4:1	8.82	4.5	2871.				6.45	11.20
	SL 20:1	6.93	1.5	1667.				4.70	10.80
Release	DW 4:1			0.64					
(µg/g)	DW 20:1			7.4					
	AS 4:1	0.16	5.6	2240.					
	AS 20:1	105.	18.	35 200.					
	SL 4:1	35.3	18.	11 484.		-			
	SL 20:1	139.	30.	33 340.					_
Efficiency	DW 4:1			<0.01					
(%)	DW 20:1			0.01					
	AS 4:1	0.10	10.6	4.07					
	AS 20:1	62.5	33.9	64.0					
	SL 4:1	21.0	33.9	20.9					
	SL 20:1	82.5	56.6	60.6					

SAMPLE NO.: 25 WASTE TYPE: High Arsenic Residue from Flotation/Cyanidation Process

DATE TESTED: September 1981

COMMENTS: High arsenic concentrations interfered with gold recovery. Therefore residue was stockpiled until technology could be developed to extract the gold.

SOLID PHASE

TOTAL SOLIDS: 87.8% VOLATILE SOLIDS: 9.8%

PARAMETER	Cu	Fe	Pb	Zn	TCN			
Concentration (ppm)	271.	74 000.	45.	1640.	15.7			

MEASURED CHARACTER ISTIC	TEST CONDITION	Cu	Fe	Pb	Zn	TCN	As		pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	2.63	146.	<0.1	10.0	0.06	11.5		3.00	3, 55
(mg/L)	DW 20:1	0.35	37.	<0.1	2.14	0.02	26.9		3,25	1.75
	AS 4:1	0.35	61.	<0.1	8.67	0.05	37.0		3.85	6.25
	AS 20:1	<0.02	11.	<0.1	2.39	0.04	27.3		4.30	5.50
	SL 4:1	1.93	56.	<0.1	7.98	0.09	37.0	1	4.10	10.00
	SL 20:1	0.54	26.	<0.1	1.84	0,11	30.0		4.35	9.00
Release	DW 4:1	10.5	584.		40.0	0.24	46.	1		
e⊺ease µg∕g)	DW 20:1	7.0	740.		42.8	0.40	538.			
	AS 4:1	1.4	244.		34.7	0.20	148.			
	AS 20:1		220.		47.8	0.80	546.			
	SL 4:1	7.7	224.		31.9	0.36	148.			
	SL 20:1	10.8	520.		36.8	2.20	600.			
Efficiency	DW 4:1	4.42	0.90		2.78	1.74				
(%)	DW 20:1	2.94	1.14		2.97	2.90				
	AS 4:1	0.59	0.38		2.41	1.45				
	AS 20:1		0.34		3.32	5.80				
	SL 4:1	3.24	0.35		2.22	2.61				
	SL 20:1	4.54	0.80		2.56	16.0				

SAMPLE NO.: 29 WASTE TYPE: Phosphate Process Slag

DATE TESTED: September 1981

COMMENTS: Grey, particle size = 5 to 10 cm

SOLID PHASE

TOTAL SOLIDS: 99.9% VOLATILE SOLIDS: 0.1%

PARAMETER					
Concentration (ppm)	_				

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTERISTIC	TEST CONDITION	Р	SO <sub>Ц</sub>	AI	Ca	٥r	Cu	Fe	Mn	NÎ	Zn	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.1	41.5									10.75	0.69
(mg/L)	DW 20:1	<0.1	9.2									10.15	0.21
	AS 4:1	<0.1	29.1									8.50	7.75
	AS 20:1	<0.1	18.5										
	SL 4:1			<1.	<0.02	<0.1	0.06	0.1	3.34	<0.1	0.04	8.20	15.5
	SL 20:1			<1.	<0.02	<0.1	0.06	0.3	3.01	0.5	0.31	6.05	16.1
Release	DW 4:1		166.		 								
(µg/g)	DW 20:1		184.										
	AS 4:1		116.										
	AS 20:1		370.	i									
	SL 4:1				ļ		0.24	0.4	13.4		0.16		
	SL 20:1			2			1.20	6.0	60.2	10.0	6.20		
Efficiency	DW 4:1	1			1								
(%)	DW 20:1											1	
	AS 4:1										1		
	AS 20:1												
	SL 4:1	1								ţ		1	
	SL 20:1				l	l	1						

SAMPLE NO.: 32 WASTE TYPE: Equilibrium Fluid Catalyst from Catalytic Cracker Unit

DATE TESTED: September 1981

COMMENTS: Grey. From oil refinery.

SOLID PHASE

TOTAL SOLIDS: 94.4% VOLATILE SOLIDS: 1.4%

PARAMETER					
Concentration (ppm)					

MEASURED CHARACTER I ST IC	TEST CONDITION	Cu	Fe	Na	Ni	v				pH (Units	Conductivity ) (mS/cm)
Concentration	DW 4:1	<0.02	<0.1	5.9	<0.1	0.95				6.45	0.06
(mg/L)	DW 20:1	<0.02	<0.1	3.7	<0.1	0.30		}		6.45	0.05
	AS 4:1	<0.02	0.4		0.4	0.05				4.60	5.10
	AS 20:1	<0.02	0.4		<0.1	0.04				4.55	5.20
	SL 4:1	<0.02	4.5		0.5	0.11				4.50	8.25
	SL 20:1	<0.02	3.6	}	0.1	0.14				4.40	8.40
Release	DW 4:1			23.6		3.80					
elease µg∕g)	DW 20:1			74.0		6.00					
	AS 4:1		1.6		1.6	0.20	4				
	AS 20:1		8.0			0.80					
	SL 4:1		18.		2.0	0.44					
	SL 20:1		72.		2.0	2.80					
Efficiency	DW 4:1										
(%)	DW 20:1										
	AS 4:1										
	AS 20:1		l			ļ	l	1	ļ		ļ
	SL 4:1										
	SL 20:1				i						

# SAMPLE NO.: 33 WASTE TYPE: Refinery Sludge

DATE TESTED: October 1981

COMMENTS: Dark-brown.

SOLID PHASE

TOTAL SOLIDS: 92.9% VOLATILE SOLIDS: 15.6%

PARAMETER	Cd	ᠬ	Qu	Fe	Mg	NĪ	Pb	Zn	TOC	
Concentration (ppm)	<0.3	629.	183.	16 800.	4890.	87.	41.	353.	188 000.	

MEASURED CHARACTERISTIC	TEST CONDITION	Cr	Qu	Fə	Mg	NĪ	Pb	Zn	TOC	pH (Units	Conductivity ) (mS/cm)
Concentration	DW 4:1	<0.1	0.02	1.0	15.	<0.1	<0.1	0.10	120.	7,65	0.75
(mg/L)	DW 20:1	<0.1	<0.02	0.7	4.1	<0.1	<0.1	0.11	22.	7.50	0.32
	AS 4:1	<0.1	0.04	0.7	44.	<0.1	<0.1	2.02		6.35	7.84
	AS 20:1	<0.1	0.03	0.4	16.	<0.1	<0.1	2.08		6.10	7.70
	SL 4:1										
	SL 20:1										
 Release	DW 4:1		0.08	4.0	60.			0.40	480.		
(µg/g)	DW 20:1			14.0	82.		Ì	2.20	440.		
	AS 4:1		0.16	2.8	176.			8.08			
	AS 20:1	Ì	0.60	8.0	320.			41.6		{	
	SL 4:1				1	Ì					
	SL 20:1										
Efficiency	DW 4:1		0.05	0.03	1.32			0.12	0.27		
(\$)	DW 20:1			0.09	1.81			0.67	0.25		
	AS 4:1		0.09	0,02	3.88		1	2.46			
	AS 20:1		0.35	0.05	7.05			12.7			
	SL 4:1										
	SL 20:1	1					1	1	[		1

SAMPLE NO.: 40 WASTE TYPE: Filter Cake Solids from a Chemical Plant

DATE TESTED: December 1981

COMMENTS: Dark-grey.

SOLID PHASE

TOTAL SOLIDS: 76.0% VOLATILE SOLIDS: 32.0%

PARAMETER	AI	Cu	Fe	Mg	Pb	Sn	ті	Sb	
Concentration (ppm)	4410.	184.	7260.	2730.	3.5	1.9	16 800.	<0.2	

MEASURED CHARACTER I ST IC	TEST CONDITION	AI	Qu	Fe	Mg	РЪ	Sn	Ti	Sb	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	294.	14.0	529.	245.	<0.01	<0.01	7.40	<0.03	1.65	27.0
(mg/L)	DW 20:1	64.	3.13	92.	61.	<0.01	<0.01	0.60	<0.03	1.95	7.9
	AS 4:1	294.	14.0	397.	230.	<0.01	<0.01	4.40	<0.03	1.80	18.5
	AS 20:1	42.	1.03	34.	56.	<0.01	<0.01	0.04	<0.03	3.80	5.2
	SL 4:1	294.	12.0	275.	235.	<0.01	<0.01	0.16	<0.03	2, 95	13.5
	SL 20:1	65.	2,50	25.	56.	<0.01	<0.01	0,58	<0.03	4.25	10.6
Release	DW 4:1	1176.	56.0	2116.	980.			29.6			
(µg/g)	DW 20:1	1280.	62.6	1840.	1220.			12.0			
	AS 4:1	1176.	56.0	1588.	920.			17.6			
	AS 20:1	840.	20.6	680.	1120.			0.80			
	SL 4:1	1176.	48.0	1100.	940.			0.64			
	SL 20:1	1300.	50.0	500.	1120.			11.6	1		
Efficiency	DW 4:1	35.1	40.1	38.4	47.2			0.23			
(%)	DW 20:1	38.2	44.8	33.4	58.8			0.09			
	AS 4:1	35.1	40.1	28.8	44.3			0.14			
	AS 20:1	25.1	14.7	12.3	54.0			0.01			
	SL 4:1	35.1	34.3	19.9	45.3			0.01			
	SL 20:1	38.8	35.8	9.06	54.0			0.09			

SAMPLE NO.: 41 WASTE TYPE: Neutral Filter Cake Solids from a Chemical Plant

DATE TESTED: December 1981

COMMENTS: Dark-grey.

## SOLID PHASE

TOTAL SOLIDS: 76.0% VOLATILE SOLIDS: 30.0%

PARAMETER	AI	Cu	Fe	Mg	Pb	Sn	TI	Sb	
Concentration (ppm)	3150.	105.	2750.	1250.	7.5	<0.2	5000.	0.2	

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	AI	Cu	Fe	Mg	РЪ	Sn	TI	Sb	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	15.0	4.73	0.84	17.0	<0.01	<0.01	0.01	<0.03	3.10	1.38
(mg/L)	DW 20:1	4.4	1.19	0.61	4.47	<0.01	<0.01	0.02	<0.03	3.60	0.35
	AS 4:1	3.1	2,98	0.04	17.0	<0.01	<0.01	<0.01	<0.03	4.35	5.00
	AS 20:1	2.4	1.66	0.04	8.37	<0.01	<0.01	<0.01	<0.03	4.40	4.60
	SL 4:1	11.0	3.97	3.78	19.0	0.05	0.11	<0.01	<0.03	4.45	10.1
	SL 20:1	2.6	0.95	0.07	4.65	<0.01	<0.01	<0.01	<0.03	4.45	10.2
Release	DW 4:1	60.0	18.9	3.36	68.0			0.04			
(µg/g)	DW 20:1	88.0	23.8	12.2	89.4			0.40			
	AS 4:1	12.4	11.9	0.16	68.0						
	AS 20:1	48.0	33.2	0.80	167.		1				
	SL 4:1	44.0	15.9	15.1	76.0	0.20	0.44		i i		
	SL 20:1	52.0	19.0	1.40	93.0						
Efficiency	DW 4:1	2.51	23.7	0,16	7.16			<0.01			
(%)	DW 20:1	3.68	29.8	0.58	9.41			0.01			
	AS 4:1	0.52	14.9	0.01	7.16						
	AS 20:1	2.01	41.6	0.04	17.6						
	SL 4:1	1.84	19.9	0.72	8.00	3.51					
	SL 20:1	2.17	23.8	0.07	9.79						

# SAMPLE NO.: 41 WASTE TYPE: Neutral Filter Cake Solids

DATE TESTED: December 1981

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure =  $0 \text{ mL} = 0.0 \text{ meq H}^+/\text{g}$  waste.

## EPA EXTRACTION PROCEDURE AND ASTM LEACHING TESTS

MEASURED CHARACTER ISTIC	TEST CONDITION	AI	Cu	Fe	Mg	РЬ	Sn	ті	Sb		pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	4.	0.64	<0.1	3.8	<0.01	0.01	<0.01	<0.03		3,95	0.34
Release (µg/g)	EPA ASTM DW ASTM AS	80.	12.8		76.			0.2				
Efficiency (%)	EPA ASTM DW ASTM AS	3.34	16.0		8.0			0.01				

MEASURED CHARACTER ISTIC	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS					-		
Release (µg∕g)	EPA ASTM DW ASTM AS							
Efficiency (\$)	EPA ASTM DW ASTM AS							

## SAMPLE NO.: 42 WASTE TYPE: Aluminum Production Red Mud

DATE TESTED: February 1982

COMMENTS: Rust red.

#### SOLID PHASE

TOTAL SOLIDS: 56.8% VOLATILE SOLIDS: 8.4%

PARAMETER						
Concentration (ppm)	-					

# MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	AI	Са	Cd	٥r	Qu	Fe	Mn	Nİ	Zn	so <sub>4</sub>	pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	DW 4:1 DW 20:1	15.	1.9	<0.03	<0.1	<0.03	0.9	<0.03	<0.1	0.05	326.	10.85	4.0
-	AS 4:1 AS 20:1 SL 4:1 SL 20:1	<1.	165.	<0.03	<0.1	0.05	<0.1	<0.03	<0.1	0.04	297.	7.70	6.4
Retease (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	60.	7.6 660.			0.20	3.6			0.20 0.16	1304 <b>.</b> 1188.		
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1												

SAMPLE NO.: 43 WASTE TYPE: Aluminum Production Red Mud (De	(Dewatered)
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DATE TESTED: February 1982

COMMENTS: Rust-red.

SOLID PHASE TOTAL SOLIDS: 59.1% VOLATILE SOLIDS: 6.8%

PARAMETER					
Concentration (ppm)					

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTERISTIC	TEST CONDITION	AI	Ca	Cd	Cr	Cu	Fe	Mn	Nİ	Zn	so <sub>4</sub>	pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	DW 4:1 DW 20:1	168.	0.80	<0.03	0.4	<0.03	<0.1	<0.03	<0.1	<0.03	55.	12.05	4.9
	AS 4:1 AS 20:1 SL 4:1 SL 20:1	4.	10.0	<0.03	0.4	<0.03	<0.1	<0.03	<0.1	<0.03	64.	9.15	5.5
Release (µg/g)	DW 4:1 DW 20:1	672.	3.2		1.6						220.		
	AS 4:1 AS 20:1 SL 4:1 SL 20:1	16.	40.		1.6						256.		
Efficiency (\$)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1										~		

#### SAMPLE NO.: 45 WASTE TYPE: Decontaminated Oily Refinery Sand

DATE TESTED: February 1982

COMMENTS: Light brown.

#### SOLID PHASE

TOTAL SOLIDS: 92.5% VOLATILE SOLIDS: 0.4%

PARAMETER						
Concentration	(ppm)					

#### MULTIPLE-BATCH LEACHING PROCEDURES

MEASURED CHARACTERISTIC	TEST	Са	Qu	Fe	Mg	NÎ	РЬ	Zn	тос		pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	DW 4:1 DW 20:1	1.1 0.5	0.05 <0.03	0.8 0.3	0.2 <0.1	<0.1 <0.1	<0.1 <0.1	<0.03 <0.03	9.4 2.0		10.00 9.85	0.64 0.17
	AS 4:1 AS 20:1 SL 4:1 SL 20:1	244 <b>.</b> 51.	0.19	1.8 0.8	18.0 5.6	<0.1 <0.1	<0.1 <0.1	0.25 0.09			4•90 4•55	3.75 2.72
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	4.4 10. 976. 1020.	0.20 0.76 1.20	3.2 6.0 7.2 16.0	0.8 72. 112.			1.0 1.8	37.6 40.0			
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1											

SAMPLE NO.: 47 WASTE TYPE: Bed Material from an FBC Coal Fired Generating Station

DATE TESTED: January 1982

COMMENTS: White and brown.

# SOLID PHASE

TOTAL SOLIDS: 99.9% VOLATILE SOLIDS:

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ſ	PARAMETER	Ag	At	As	В	Ba	Be	Ca	Cd	Cr .	Cu
	Concentration (ppm)	<0.5	12 400.	82.	59.	<30.	<0.05	443 000	11.1	14.6	19.2

## MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Ag	AI	As	В	Ba	Be	Са	Cd	٥r	Cu	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.09	0.7	0.001	0.10	0.16	<0.005	1570.	<1.	<0.1	<0.05	12.0	9.4
(mg/L)	DW 20:1	0.18	1.7	0.002	0.14	0.13	<0.005	1530.	<1.	<0.1	<0.05	12.1	8.7
	AS 4:1	<0.05	<0.5	0.003	0.14	0.16	<0.005	2540.	<1.	<0.1	<0.05	11.9	13.5
	AS 20:1	<0.05	<0.5	0.004	0.28	0.15	<0.005	2580.	1.	<0.1	<0.05	11.8	13.8
	SL 4:1	<0.05	<0.5	0.001	0.19	0.37	<0.005	5140.	<1.	<0.1	<0.05	12.5	17.5
	SL 20:1	<0.05	<0.5	0.001	0.14	0.16	<0.005	5200.	<1.	<0.1	<0.05	12.0	18.2
Release	DW 4:1	0.36	2.8	<0.01	0.40	0.64		6280.					
(µg/g)	DW 20:1	3.6	34	0.04	2.80	2.60		30 600.			1		
	AS 4:1			0.01	0.56	0.64		10 160.					
	AS 20:1			0.08	5.60	3.00		51 600.	20.	ļ			
	SL 4:1	i i	1	<0.01	0.76	1.48		20 560.					
	SL 20:1			0.02	2.80	3.20		104 000.					
Efficiency	DW 4:1		0.02	<0.01	0.68			1.42					· ····
(%)	DW 20:1		0.28	0.05	4.75			6.92					
	AS 4:1			0.01	0.95			2.30					
	AS 20:1			0.10	9.50			11.7					
	SL 4:1			<0.01	1.29			4.65					
	SL 20:1			0.02	4.75			23.5		ļ	•		

107

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# SAMPLE NO.: 47 WASTE TYPE: FBC Bed Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE	<u>E</u>	TOTAL	SOLIDS	:	VOLATIL	E SOLIDS:	:								
ſ	PARAME	TER	Fe	Hg	к	Mg	Mn	Мо	Na	NĬ	Р	РЬ	Se	Si	Sr
	Concen	tration (ppm)	15 1	00. 0.002	2850.	2990.	584.	120.	1500.	44.	430.	12.5	0.06	26 900.	96.
MULTIPLE-B/	ATCH LEA	Ching Procedu	RE												
MEASUREE	1	TEST CONDITION	Fe	Hg	к	Mg	Mn	Мо	Na	NĪ	Р	Pb	Se	SI	Sr
Concentrati (mg/L)	ion	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1	0.000 03 0.000 09 <0.000 02 <0.000 02 <0.000 02 <0.000 03	10. <10. 20. 30.	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1 0.3	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1 <0.1	3. 3. <2. <2. <2. <2. <2.	<20. <20.	<0.5 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	6. <5. <5. <5. 9. 8.	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	<0.001 <0.001 <0.001 <0.001 <0.001 <0.001	<0.5 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	3.55 1.43 3.89 1.60 3.96 2.12
Release (µg∕g)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		<0.01 <0.01 <0.01	40. 200. 400. 120. 400.	6.0		12. 60.			24. 36. 160.				14.2 28.6 15.6 32.0 15.8 42.4
Efficiency (≴)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		6.0 90.1 30.0	1.4 7.0 14.0 4.2 14.0	0.2		10 <b>.</b> 50.			5.59 8.38 37.2				14.8 29.8 16.2 33.4 16.5 44.2

## SAMPLE NO.: 47 WASTE TYPE: FBC Bed Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE	_	TOTAL	SOLIDS:		VOLATIL	E SOLIDS:	:								
ſ	PARAMETER	<u> </u>	ті	v	Zn	60	Th	Zr	υ	Li	ТІ	TOC	]		
-	Concentra	tion (ppm)	514.	25.	35.	79.	<1.	31.7	2.5	14.	<5.	0.81			
MULTIPLE-BA	TCH I FACHII	NG PROCEDU	RF	<u> </u>											
														1	1
MEASURED CHARACTER IS		TEST	ті	v	Zr	\$	Th	Zr	U	Li	ті		CI	F	so <sub>4</sub>
Concentratio	on [	₩ 4:1	<0.05	0.06	<0.5	1.0	1.1	<0.2	<1.	0.26	<0.1		39.8	<0.5	1380
(mg/L)	<b>1</b> E	DW 20:1	<0.05	<0.05	<0.5	0.7	0.8	<0.2	<1.	0.10	<0.1		10.0	<0.5	1560
	1	AS 4:1	<0.05	<0.05	<0.5	<0.5	<0.1	<0.2	<1.	0.20	<0.1		49.3	<0.5	12 800
		AS 20:1	<0.05	<0.05	<0.5	<0.5	<0.1	<0.2	<1.	0.06	<0.1		11.3	<0.5	1580
		SL 4:1	<0.05	<0.05	<0.5	<0.5	<0.1	<0.2	<1.	0.14	<0.1		58.7	<0.5	1650
	5	SL 20:1	<0.05	<0.05	<0.5	<0.5	<0.1	<0.2	<1.	0.32	<0.1		24.0	<0.5	1820
Release	[	DW 4:1		0.24		4.	4.4			1.04			159.		5520
(µg/g)		DW 20:1	-			14.	16.			2.00			200.		31 200
	(	AS 4:1								0.80			197.		51 200
		AS 20:1								1.20			226.		31 600
		SL 4:1								0.56			235.		6600
		SL 20:1								6.40			480.		36 400
Efficiency	1			0.96		5.07				7.43				1	
(%)	1	DW 20:1				17.7				14.3					
		AS 4:1								5.72					
		AS 20:1	•		Ì					8.58				1	
		SL 4:1								5.00					
		SL 20:1								45.7					1

# SAMPLE NO.: 47 WASTE TYPE: FBC Bed Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE

TOTAL SOLIDS:

VOLATILE SOLIDS:

PARAMETER					
Concentration (ppm)					

MEASURED CHARACTER I ST IC	TEST CONDITION	TCN	NH4	COD	Sb								
Concentration	DW 4:1	5.	0.17	35.	<0.001								
(mg/L)	DW 20:1	5.	0.34	25.	<0.001				1				
	AS 4:1	4.	0.17		<0.001			i i					į
	AS 20:1	3.	0.17		<0.001			1					ļ
	SL 4:1	5.	2.38		<0.001			ŀ					
	SL 20:1	5.	2.04		<0.001								
Release	DW 4:1	20.	0.68	140.									
(µg/g)	DW 20:1	100.	6.80	500.									
	AS 4:1	16.	0.68										
	AS 20:1	60.	3.40					ļ					
	SL 4:1	20.	9.52										
	SL 20:1	100.	40.8	ĩ									
Efficiency	DW 4:1							1					
(\$)	DW 20:1							4					1
	AS 4:1							1		1	1		1
	AS 20:1					1							1
	SL 4:1						ł			1		1	1
	SL 20:1	1					ł						

## SAMPLE NO.: 48 WASTE TYPE: Baghouse Material from FBC Coal Fired Generating Station

DATE TESTED: January 1982

COMMENTS: Brown.

SOLID PHASE

TOTAL SOLIDS: 95.7% VOLATILE SOLIDS:

PARAMETER	Ag	AI	As	В	Ва	Be	Са	Cd	٥r	Cu
Concentration (ppm)	<0.5	71 800.	300.	121.	445.	10.1	147 000.	16.3	203.	112.

### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER ISTIC	TEST CONDITION	Ag	Al	As	в	Ba	Be	Ca	Cd	ç	Cu	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.30	1.7	0.006	4.99	0.51	<0.005	3020.	1.	0.6	0.18	11.15	11.0
(mg/L)	DW 20:1	<0.05	<0.5	0.016	0.71	0.36	<0.005	1170.	2.	0.2	<0.05	11.60	3.9
	AS 4:1	<0.05	<0.5	0.015	0.19	0.50	<0.005	3980.	<1.	<0.1	<0.05	11.25	13.1
	AS 20:1	<0.05	<0.5	0.017	9.60	0.14	<0.005	3240.	<1.	<0.1	<0.05	10.60	11.2
	SL 4:1	<0.05	<0.5	0.032	0.75	0.64	<0.005	4300.	1.	<0.1	<0.05	10.85	19.0
	SL 20:1	<0.05	25.5	0.086	3.92	0.29	0.043	3660.	2.	<0.1	<0.05	5.75	13.4
Release	DW 4:1	1.2	6.8	0.02	20.0	2.04		12 080.	4.	2.42	0.72		
(µg/g)	DW 20:1			0.32	14.2	6.80		23 400.	40.	4.00			
	AS 4:1			0.06	0.76	2.00		15 920.					
	AS 20:1		1	0.34	192.	2.80		64 800.					
	SL 4:1			0.13	3.00	2.56		17 200.	4.				
	SL 20:1		510.	1.72	78.4	5.80	0.86	73 200.	40.				
Efficiency	DW 4:1		0.01	<0.01	17.4	0.48	1	8.68	25.8	1.24	0.68		
(%)	DW 20:1	Ì	l .	<0.01	12.4	1.61		16.8	258.	2.06			
	AS 4:1			<0.01	0.66	0.47		11.4					
	AS 20:1			<0.01	167.	0.66		46.6					
	SL 4:1			0.01	0.65	0.61		12.3	25.8				
	SL 20:1		0.04	0.03	68.2	1.37	8.90	50.0	258.			[ [	

# SAMPLE NO.: 48 WASTE TYPE: FBC Baghouse Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

TOTAL SOLIDS:

VOLATILE SOLIDS:
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Concentration (ppm) 125 000. 2150. 13 100. 3930. 494. <30. 5300. 180. 2250. 240. 6.	Concentration (ppm)	3930. 494. <30. 5300.	180. 2250. 240. 6.7 115 000. 686.

## MULTIPE-BATCH LEACHING PROCEDURE

		<u>.</u>	·			•								•
MEASURED CHARACTER I ST IC	TEST CONDITION	Fe	Hg	к	Mg	Min	Мо	Na	NÍ	Р	РЬ	Se	Si	Sr
Concentration	DW 4:1	<0.1	0.000 26	140.	0.7	<0.1	8.	40.	<0.5	9.	<0.05	<0.001	8.8	21.4
(mg/L)	DW 20:1	<0.1	0.000 14	30.	0.7	<0.1	<2.	<20.	<0.5	<5.	<0.05	<0.001	8.1	5.63
	AS 4:1	<0.1	0.000 14	150.	0.3	<0.1	<2.		<0.5	8.	<0.05	<0.001	1.8	21.0
	AS 20:1	<0.1	0.000 15	30.	<0.1	<0.1	<2.		<0.5	9.	<0.05	0.022	<0.5	4.44
	SL 4:1	<0.1	0.000 17	160.	1.1	<0.1	<2.		<0.5	11.	<0.05	<0.001	1.9	22.7
	SL 20:1	23.2	0.000 23	40.	37.1	4.3	<2.		<0,5	7.	<0.05	0.065	47.7	7.81
Release	DW 4:1		<0.01	560.	2.8		32.	160.		36.			35.2	85.6
(µg/g)	DW 20:1	ĺ	<0.01	600.	14.0		í					1	162.	112.
	AS 4:1		<0.01	600.	1.2					32.		ļ	7.2	84.0
	AS 20:1		<0.01	600.						180.		0.44	ļ	88.8
	SL 4:1		<0.01	640.	4.4	Ì				44.		{	7.6	90.8
	SL 20:1	464.	<0.01	800.	742.	86.				140.		1.30	954.	156.
Efficiency	DW 4:1	1	<0.01	4.50	0.07			3.17		1.68			0.03	13.1
(\$)	DW 20:1		<0.01	4.82			ļ				l	1	0.15	17.2
	AS 4:1		<0.01	4.82	0.03					1.49			0.01	12.8
	AS 20:1	]	<0.01	4.82		]	j			8.39		6.89	ļ	13.6
	SL 4:1		<0.01	5,12	0.12		l			2.05			0.01	13.9
	SL 20:1	0.39	<0.01	6.41	19.8	18.3	1			6.63		20.3	0.86	23.9

# SAMPLE NO.: 48 WASTE TYPE: FBC Baghouse Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE	TOTAL	SOLIDS:		VOLATILE	E SOLIDS:	:								
Γ	PARAMETER	Ti	v	Zn	60	Th	Zr	U	Li	ті	TOC			
	Concentration (ppm)	3900.	236.	229.	122.	69.	108.	6.5	195.	<5.	7500.			
MULTIPLE-BA	TCH LEACHING PROCEDU	RE												
MEASURED CHARACTER IS		τi	v	Zn	8	Th	Zr	U	Li	TI		CI	F	SOL
Concentratio (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	0.13 0.07 <0.05 <0.05 <0.05 <0.05	0.6 <0.5 <0.5 0.6 0.6 0.7	0.9 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	1.8 0.4 <0.1 <0.1 <0.1 <0.1 <0.1	<0.2 <0.2 <0.2 <0.2 <0.2 <0.2 <0.2 <0.2	<0.001 0.002 0.001 0.001 <0.001 0.035	2.00 0.38 1.70 0.38 1.70 0.66	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05		3910. 780. 4250. 815. 4120. 1030.	<0.5 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	138 159 142 140 163 174
Release (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		0.52 1.40	2.4 12.0 2.4 14.0	3.6	7•2 8•0		0.04 0.004 0.02 0.70	8.00 7.60 6.80 7.60 6.80 13.2			15 640. 15 600. 17 000. 16 300. 16 480. 20 600.		552 31 80 568 28 00 652 34 80
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		0.23 0.62	1.10 5.50 1.10 6.41	3.1	10.9 12.2		0.65 0.06 0.32 11.3	4.30 4.09 3.64 4.09 3.64 7.07					

SOLID PHASE	TOTAL	SOLIDS:		VOLATIL	E SOLIDS								
PARAM	ETER									1	1	7	
		+	+		+			+	+	+	-	4	
Conce	ntration (ppm)			<u> </u>								J	
MULTIPLE-BATCH LE	ACHING PROCEDUR	RE		<u></u>	<u> </u>								
MEASURED	TEST				·	1	1	l				1	
CHARACTERISTIC	CONDITION	TCN	NH3	COD						-			
Concentration	DW 4:1	3.	3.94	35.	†								
(mg/L)	DW 20:1	3.	0.75	10.		1							
	AS 4:1	4.	4.15			ī						(	
	AS 20:1	5.	1.90					•					
	SL 4:1	4.	7.75					l I					Į
	SL 20:1	7.	3.74									}	
Release	DW 4:1	12.	15.8	140.									
(µg∕g)	DW 20:1	60.	15.0	200.								ĺ	
	AS 4:1	16.	16.6										
	AS 20:1	100.	38.0									l	1
	SL 4:1	16.	31.0										
	SL 20:1	140.	74.8							I			
Efficiency	DW 4:1							1					
(%)	DW 20:1											1	
	AS 4:1												1
	AS 20:1										1		1
	SL 4:1										1		1
	SL 20:1				1	1		1			i i		

## SAMPLE NO.: 49 WASTE TYPE: Bed Material from FBC Coal Fired Power Generating Station

DATE TESTED: January 1982

COMMENTS: White and brown.

### SOLID PHASE

TOTAL SOLIDS: 99.1% VOLATILE SOLIDS:

PARAMETER	Ag	Al	As	В	Ba	Be	Ca	Cd	Ċr	Cu
Concentration (ppm)	<0,5	16 000.	90.	60.	30.	<0.05	470 000.	13.4	13.1	32.1

MEASURED CHARACTERISTIC	TEST CONDITION	Ag	AI	As	в	Ba	Be	Ca	Cd	٥r	Cu	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.13	0.7	0.002	0.24	0.16	<0.005	1530.	<1.	<0.1	<0.05	12.20	8.0
(mg/L)	DW 20:1	0.27	1.1	0.001	21.6	0.20	<0.005	1520.	1.	<0.1	0.19	12.15	8.5
	AS 4:1	<0.05	<0.5	0.003	0.14	0.16	<0.005	2580.	<1.	<0.1	<0.05	12.10	12.0
	AS 20:1	<0.05	<0.5	0.031	1.18	0,16	<0.005	2550.	2.	<0.1	<0.05	12.40	16.3
	SL 4:1	<0.05	<0.5	0.006	0.19	0.35	<0.005	5350.	<1.	<0.1	<0.05	12.00	19.0
	SL 20:1	<0.05	<0.5	0.019	0.10	0.16	<0.005	5200.	<1.	<0.1	<0.05	12.25	18.4
Release	DW 4:1	0.52	2.8	0.01	0.96	0.64		6120.					
(µg/g)	DW 20:1	5.40	22.	0.02	432.	4.00		30 400.	20.		3.8		
	AS 4:1			0.01	0.56	0.64		10 320.					
	AS 20:1			0.62	23.6	3,20		51 000.	40.				
	SL 4:1		1 1	0.02	0.76	1.40		21 400.					
	SL 20:1			0.38	2.00	3.20		104 000.					
Efficiency	DW 4:1		0.02	0.01	1.61	2.15		1.31					
(%)	DW 20:1		0.14	0.02	727.	13.5		6,53	150.		12.0		
	AS 4:1			0.01	0.94	2.15		2.22	I	ł		ļ	
	AS 20:1			0.70	39.7	10.8		11.0	301.	ĺ			
	SL 4:1			0.03	1.28	4.71		4.60			•		
	SL 20:1			0.43	3.36	10.8		22.3		!			

## SAMPLE NO.: 49 WASTE TYPE: FBC Bed Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE

TOTAL SOLIDS: VOLATILE SOLIDS:

PARAMETER	Fe	Hg	к	Mg	Mn	Мо	Na	Nİ	Р	РЬ	Se	Si	Sr
Concentration (ppm)	14 200.	0.002	3850.	4840.	644.	165.	2200.	51.	880.	<5.	0.07	37 100.	98.1

# MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER ISTIC	TEST CONDITION	Fe	Hg	к	Mg	Mn	Мо	Na	NĪ	Р	Pb	Se	SI	Sr
Concentration	DW 4:1	0.1	<0.000 02	20.	0.3	<0.1	3.	<20.	<0.5	6.	<0.05	<0.001	<0.5	5.67
(mg/L)	DW 20:1	<0.1	0.000 03	10.	<0.1	<0.1	4.	<20.	<0.5	6.	<0.05	<0.001	<0.5	2.08
	AS 4:1	<0.1	0.000 11	20.	<0.1	<0.1	<2.		<0.5	<5.	<0.05	<0.001	<0.5	6.14
	AS 20:1	<0.1	0.000 03	20.	<0.1	<0.1	<2.		<0.5	7.	<0.05	<0.001	<0.5	2.12
	SL 4:1	<0.1	0.000 08	40.	<0.1	<0.1	<2.		<0.5	10.	<0.05	<0.001	42.	6.21
	SL 20:1	<0.1	0.000 11	30.	<0.1	<0.1	<2.		<0.5	8.	0.10	<0.001	<0.5	2.25
Release	DW 4:1	0.4		80.	1.2		12.			24.		<b></b>		22.7
(µg/g)	DW 20:1		<0.01	200.			80.		ł	120.				41.6
	AS 4:1		<0.01	80.					ł					24.6
	AS 20:1		<0.01	400.						140.				42.4
	SL 4:1		<0.01	160.					ļ	40.			168.	24.8
	SL 20:1		<0.01	600.						160.	2.0			45.0
Efficiency	DW 4:1	<0.01		2.10	0.03		7.34			2.75				23.3
(%)	DW 20:1		30.3	5.24			48.9			13.8				42.8
	AS 4:1		22.2	2.10	,									25.3
	AS 20:1		30.3	10.5						16.1				43.6
	SL 4:1		16.2	4.19		ļ				4.59		1	0.46	25.6
	SL 20:1		1111.	15.7			Ì			18.4				46.3

# SAMPLE NO.: 49 WASTE TYPE: FBC Bed Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHAS	E TOTAL	SOLIDS:		VOLATILE	SOLIDS:	:								
	PARAMETER	ТІ	v	Zn	Co	Th	Zr	υ	LI	ТІ	TOC	]		
	Concentration (ppm)	465.	22.2	50.	106.	<1.	39.5	3.	16.	<5.	34 000.	4		
												_		
MULTIPLE-B	ATCH LEACHING PROCEDU	RE												
MEASUREI CHARACTER I		Ti	v	Zn	\$	Th	Zr	U	Li	ΤI		CI	F	so <sub>4</sub>
Concentrat (mg/L)	ion DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	<0.05 0.09 <0.05 <0.05 <0.05 <0.05	<0.5 <0.5 0.5 0.5 <0.5 <0.5 <0.5	0.6 1.2 <0.5 <0.5 <0.5 <0.5 <0.5	0.8 1.4 <0.1 <0.1 <0.1 <0.1	<0.2 <0.2 <0.2 <0.2 <0.2 <0.2 <0.2 <0.2	0.001 <0.001 0.003 0.001 <0.001 0.002	0.14 0.08 0.06 0.12 0.12 0.12	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1 <0.1		<0.5 <0.5 8.1 8.1 11.3 11.3	<0.5 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	1270 1480 1330 1280 1820 1860
Retease (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		1.8	2.0 10.0	2.4 24.	3.2 28.		<0.01 0.01 0.02 0.04	0.56 1.60 0.24 2.40 0.48 2.80			32.4 162. 45.2 226.		5080 29 600 5320 25 600 7280 37 200
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		8.18	4.0 20.2	2.29 22.9			0.13 0.40 0.67 1.35	3.53 10.1 1.51 15.1 3.03 17.7					

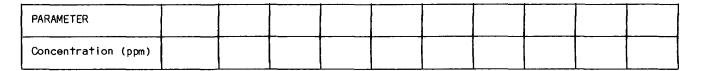
SAMPLE NO.: 49	WASTE TYPE:	FBC Bed Material
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DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE

TOTAL SOLIDS: VOLATILE SOLIDS:



### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST I C	TEST CONDITION	TCN	NH4	COD	Sb						pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	4.	0.20	15.	<0.001				 			
(mg/L)	DW 20:1	2.	0.20	15.	<0.001							
	AS 4:1	4.	0.14		<0.001						\$	
	AS 20:1	4.	0.48		<0.001							
	SL 4:1	4.	2.18		<0.001	1				1		
	SL 20:1	4.	1.56		<0.001							
Release	DW 4:1	16.	0.80	60.					 			
(µg/g)	DW 20:1	40.	4.00	300.			1	1				
	AS 4:1	16.	0.56		ļ							
	AS 20:1	80.	9.60								1	
	SL 4:1	16.	8.72					1				
	SL 20:1	80.	31.2				1	}				
Efficiency	DW 4:1											
(%)	DW 20:1											
	AS 4:1											
	AS 20:1				ļ		ļ	]		}		
	SL 4:1				ļ			l.			1	
	SL 20:1											

#### SAMPLE NO.: 50 WASTE TYPE: Baghouse Material from FBC Coal Fired Generating Station

DATE TESTED: January 1982

COMMENTS:

SOLID PHASE	TOTAL	SOLIDS:	97 <b>.0%</b>	VOLATIL	e solids	:							
	PARAMETER	Ag	AI	As	В	Ва	Be	Са	Cd	G	Cu	]	
	Concentration (ppm)	<0.5	42 100.	278.	56.	305.	13.3	143 000.	11.8	86.	152.		
MULTIPLE-BA	TCH LEACHING PROCEDU	RE											
MEASURED CHARACTER IS	TEST	Ag	AI	As	В	Ва	Ве	Ca	Cd	Cr-	Cu	pH (Units)	Conductivity (mS/cm)
Concentratic (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.27 0.20 <0.05 <0.05 <0.05 <0.05 <0.05	1.9 1.9 <0.5 <0.5 <0.5 22.0	0.050 0.084 0.082 0.560 0.195 0.185	0.75 0.57 1.60 1.57 2.65 1.61	0.07 <0.05 0.17 0.16 0.29 0.19	<0.005 <0.005 <0.005 <0.005 0.098 0.086	692. 2320. 2120. 4400.	1. <1. <1. <1. <1. <1.	0.2 <0.1 <0.1 <0.1 <0.1 <0.1	0.16 <0.05 <0.05 <0.05 <0.05 <0.05	9.30 9.15 8.05 7.00 7.30 5.55	3.75 1.90 8.20 7.50 13.0 12.0
Release (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	1.08 4.00	7.6 38.0 440.	0.20 1.68 0.33 11.2 0.78 3.70	3.00 11.4 6.40 31.4 10.6 32.2	0.28 0.68 3.20 1.16 3.80	0.39 1.72	4240. 13840. 9280. 42400. 17600. 55200.	4.	0.8	0.64		
Efficiency (\$)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		0.02 0.09 1.08	0.07 0.62 0.12 4.15 0.29 1.37	5.52 21.0 11.8 57.8 19.5 59.3	0.09 0.23 1.08 0.39 1.28	3.04 13.3	3.06 9.98 6.69 30.6 12.7 39.8		0.96	0.43		

# SAMPLE NO.: 50 WASTE TYPE: FBC Baghouse Material

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID	PHASE

TOTAL SOLIDS: VOLATILE SOLIDS:

PARAMETER	Fe	Hg	к	Mg	Mn	Мо	Na	NI	Р	РЬ	Se	SI	Sr
Concentration (ppm)	161 000.	4.5	9000.	3480.	1080.	<30.	2250.	130.	7670.	78.	4.45	87 700.	345.

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER   ST IC	TEST CONDITION	Fe	Hg	к	Mg	Mn	Mo	Na	NĪ	Р	Pb	Se	SI	Sr
Concentration	DW 4:1	<0.1	0.000 05	120.	2.70	<0.1	8.	50.	<0.5	6.	<0.05	<0.001	2.5	5.07
(mg/L)	DW 20:1	<0.1	0.000 09	30.	0.30	<0.1	4.	<20.	<0.5	<5.	<0.05	<0.001	<0.5	1.74
	AS 4:1	<0.1	0.000 21	140.	19.4	0.3	<2.		<0.5	6.	<0.05	0.020	<0.5	6.81
	AS 20:1	<0.1	0.000 33	50.	26.8	3.3	<2.		<0.5	5.	<0.05	0.055	51.1	3.28
	SL 4:1	4.1	0.000 09	160.	74.9	5.0	<2.		<0.5	7.	<0.05	0.045	<0.5	9.04
	SL 20:1	16.4	0.000 03	50.	43.4	6.1	<2.		<0.5	<5.	<0.05	0.038	118.	4.81
Release	DW 4:1		<0.01	480.	10.8		32.	200.		24.			10.	20.3
(µg/g)	DW 20:1		<0.01	600.	6.0		80.					1		34.8
	AS 4:1		<0.01	560.	77.6	1.2				24.		0.08		27.2
	AS 20:1		<0.01	1000.	536.	66.				100.		1.10	1022.	65.6
	SL 4:1	16.4	<0.01	640.	299.	20.				28.		0.18	1 1	36.2
	SL 20:1	328.	<0.01	1000.	868.	122.						0.76	2360.	96.2
Efficiency	DW 4:1		<0.01	5,50	0.32			9,16		0.32			0.01	6.06
(%)	DW 20:1		0.04	6.87	0.18									10.4
	AS 4:1		0.02	6.41	2.30	0.11				0.32		1.85		8.14
	AS 20:1		0.15	11.5	15.9	6.30				1.34		25.5	1.20	19.6
	SL 4:1	0.01	<0.01	7.33	8.88	1.91				0.38		4.17		10.8
	SL 20:1	0.21	<0.01	11.5	25.7	11.7						17.6	2.77	28.8

# SAMPLE NO.: 50 WASTE TYPE: FBC Baghouse Materia!

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE	тоти	L SOLIDS:		VOLATILI	E SOLIDS:	:								
	PARAMETER	ТІ	v	Zn	Co	Th	Zr	U	LI	ТІ	TOC			
ĺ	Concentration (ppm	) 2980.	170.	163.	32.	16.	79.8	7.5	82.	<5.	20 800.			
MULT IPLE-BA	TCH LEACHING PROCED	URE							<u></u>			<u></u>		
MEASURED CHARACTER I S		ті	v	Zn	Co	Th	Zr	U	Li	TI		СІ	F	SO <sub>14</sub>
Concentrati (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	0.11 0.10 <0.05 <0.05 <0.05 <0.05 <0.05	<0.5 <0.5 <0.5 0.6 <0.5 0.6	0.9 1.2 <0.5 <0.5 <0.5 <0.5	1.3 1.2 <0.1 <0.1 <0.1 <0.1	<0.2 <0.2 <0.2 <0.2 <0.2 <0.2 <0.2 <0.2	0.001 <0.001 0.008 0.021 <0.001 0.05	0.14 0.14 0.20 0.16 0.22 0.42	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1 <0.1		1090. 231. 1220. 294. 1220. 294.	<0.5 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	1110 1360 1130 1160 1480 1410
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		0.44 2.0	12 <b>.</b> 12.	3.6 24.	5.2 24.		<0.01 0.03 0.42 1.00	0.56 2.80 0.80 3.20 0.88 8.40			4360. 4620. 4880. 5880. 4880. 5880.		4440 27 200 4520 23 200 5920 28 200
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		0.27 1.21	7.59 7.59	11.6 77.3	33.5 155.		0.05 0.44 5.77 13.8	0.68 3.52 1.01 4.02 1.11 10.4					

## SAMPLE NO.: 50 WASTE TYPE: FBC Baghouse Material

TOTAL SOLIDS:

DATE TESTED: January 1982

COMMENTS: Continued from previous page.

SOLID PHASE

VOLATILE SOLIDS:

PARAMETER					
Concentration (ppm)					

MEASURED CHARACTER I ST I C	TEST CONDITION	TCN	NH4	COD	Sb					
Concentration	DW 4:1	5.	1.36	35.	<0.001					·
(mg/L)	DW 20:1	5.	0.48	20.	<0.001					
	AS 4:1	4.	1.29		<0.001					
	AS 20:1	4.	0.14		<0.001					
	SL 4:1	6.	3.81		<0.001		(			
	SL 20:1	9.	3.04		<0.001					
Release	DW 4:1	20.	5.44	140.						
(µg/g)	DW 20:1	100.	9.60	400.						
	AS 4:1	16.	5,16							
	AS 20:1	80.	2.80			ļ				
	SL 4:1	24.	15.2							
	SL 20:1	180.	60.8							
Efficiency	DW 4:1				1	 		 	 	
(%)	DW 20:1		i							
	AS 4:1									
	AS 20:1						ļ			
	SL 4:1	1								
	SL 20:1									

SAMPLE NO.: 51 WASTE TYPE: 40:60 Mix of Baghouse: Bed Material from FBC Coal-Fired Generating Station

DATE TESTED: January 1982

COMMENTS:

# SOLID PHASE

# TOTAL SOLIDS: 97.6% VOLATILE SOLIDS:

PARAMETER	Ag	AI	As	В	Ba	Be	Са	Cd	Cr	Cu
Concentration (ppm)	<0.05	36 200.	169.	83.8	178.	4.04	325 000.	11.	131.	56.3

MEASURED CHARACTER I ST IC	TEST CONDITION	Ag	Al	As	В	Ba	Be	Са	Cd	œ	Cu	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.18	0.6	0.002	0.28	0.17	<0.005	2200.	<1.	0.1	0.17	12.45	10.2
(mg/L)	DW 20:1	<0.05	<0.5	0.004	0.14	0.16	<0.005	1720.	<1.	<0.1	<0.05	12.40	8.9
	AS 4:1	<0.05	<0.5	0.006	0.28	0.17	<0.005	3560.	<1.	<0.1	<0.05	12.10	16.1
	AS 20:1	<0.05	<0.5	0.009	<0.05	0.06	<0.005	3120.	<1.	<0.1	<0.05	12.10	12.5
	SL 4:1	<0.05	<0.5	0.011	0.29	0.33	<0.005	6110.	<1.	<0.1	<0.05	12.20	19.5
	SL 20:1	<0.05	<0.5	0.012	0.19	0.39	<0.005	5220.	1.	<0.1	<0.05	12.15	18.0
Release	DW 4:1	0.72	2.4	0.01	1.12	0.68		8800.		0.4	0.68		
(µg/g)	DW 20:1			0.08	2.80	3.20		34 400.					
	AS 4:1			0.02	1.12	0.68		14 240.					
	AS 20:1			0.18		1.20		62 400.					
	SL 4:1			0.04	1.16	1.32		24 440.					
	SL 20:1			0.24	3.80	7.80		104 400.	20.	1			
Efficiency	DW 4:1		0.01	<0.01	1.37	0.39		2.78		0.31	1.24		
(%)	DW 20:1		l	0.05	3.42	1.84		10.9					
	AS 4:1		{	0.01	1.37	0.39		4.49				1	
	AS 20:1		1	0.11		0.69		19.7					1
	SL 4:1			0.03	1.42	0.76		7.71					
	SL 20:1			0.15	4.64	4.49		32.9	187.				

# SAMPLE NO.: 51 WASTE TYPE: FBC Baghouse: Bed Mixture

DATE TESTED: January 1982

COMMENTS: Continued from previous page

SOLID PHASE	TOTAL	SOLIDS:	,	VOLATILE	SOLIDS:									
	PARAMETER	Fe	Hg	к	Mg	Mn	Мо	Na	Nİ	Р	Pb	Se	SI	Sr
-	Concentration (ppm)	59100.	0.88	6950.	3370.	548.	72.	3020.	98.4	1160.	104.	2.72	62 500.	332.
MULTIPLE-BAT	TCH LEACHING PROCEDU	RE												
MEASURED CHARACTER I ST	TEST TIC CONDITION	Fe	Hg	к	Mg	Mn	Мо	Na	Nİ	Р	РЪ	Se	Si	Sr
Concentratic (mg/L)	DW 4:1 DW 20:1 / AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1	0.000 09 0.000 11 0.000 15 0.000 12 0.000 09 0.000 09	20. 80. 20. 80.	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1 0.7	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1 0.1	4. 2. <2. <2. <2. <2.	<20. <20.	<0.5 <0.5 <0.5 <0.5 <0.5 <0.5	7. <5. 8. 5. 10. 8.	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05	<0.001 <0.001 <0.001 <0.001 0.005 0.005	0.9 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	10.4 3.4 13.1 4.2 14.5 5.0
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		<0.01 <0.01 <0.01 <0.01 <0.01 <0.01	200. 400. 320. 400. 320. 600.	14.		16. 40.			28. 32. 100. 40. 160.		0.02 0.10	3.6	41.6 69.0 52.4 85.4 58.0 101.
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1		0.04 0.26 0.07 0.28 0.04 0.21	2.95 5.89 4.72 5.89 4.72 8.84	0.43		22.8 56.9			2.48 2.83 8.84 3.54 14.2		0.75 3.77	0.01	12.8 21.3 16.2 26.3 17.9 31.0

# SAMPLE NO.: 51 WASTE TYPE: FBC Baghouse: Bed Mixture

DATE TESTED: January 1982

COMMENTS: Continued from previous page

SOLID PHASE	TOTAL	SOLIDS:		VOLATILI	E SOLIDS:									
	PARAMETER	Ti	v	Zn	Co	Th	Zr	U	Li	ТІ	тос			
-	Concentration (ppm)	1870.	109.	113.	96.2	27.6	62.2	4.1	104.	<5.	7900.			
									· · · · · · · · · · · · · · · · · · ·					
MULTIPLE-BA	TCH LEACHING PROCEDU	RE											<u></u>	
MEASURED CHARACTER IS		ті	v	Zn	60	Th	Zr	U	Li	ΤI		CI	F	so <sub>4</sub>
Concentratio (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	<0.5 <0.5 <0.5 0.6 0.5 <0.5	1.1 <0.5 <0.5 <0.5 <0.5 <0.5 <0.5	1.0 0.8 <0.1 <0.1 <0.1 <0.1	<0.2 <0.2 <0.2 <0.2 <0.2 <0.2 <0.2	<0.001 0.001 0.002 0.002 <0.001 <0.001	0.74 0.38 0.64 0.44 0.80 0.38	<0.1 <0.1 <0.1 <0.1 <0.1 <0.1 <0.1		1660. 362. 1590. 420. 2030. 412.	<0.5 <0.5	1380 1410 1340 1360 1600 1640
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1			12 <b>.</b> 2.	4.4	4. 16.		0.02 0.01 0.04	2.96 7.60 2.56 8.80 3.20 7.60			6640. 7240. 6360. 8400. 8120. 8240.		5520 28 200 5360 27 200 6400 32 800
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1			10.9 1.82	4.68	14.8 59.4		0.50 0.20 1.00	2.90 7.46 2.51 8.63 3.14 7.46					

					F. 601 452	 	 <del></del>	 	
SOLID PHASE	IOIAL	SOLIDS:		VOLATIL	E SOLIDS:				
PA	RAMETER								]
Co	ncentration (ppm)	1				1	+	1	
h <del>ama</del> ,				. <u>.</u>	• • • • •	 		 	_
MULTIPLE-BATCH	LEACHING PROCEDUR	RE			·	 	 		
MEASURED CHARACTER I ST IC	TEST CONDITION	TCN	NH <sub>4</sub>	COD	Sb				
Concentration (mg/L)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	4. 4. 3. 4. 3.	1.56 0.54 1.90 0.54 3.88 2.58	30 <b>.</b> 10 <b>.</b>	<0.001 <0.001 <0.001 <0.001				
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	16. 80. 16. 60. 16. 60.	6.24 10.8 7.60 10.8 15.5 51.6	120 <b>.</b> 200.					
Efficiency (\$)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1								

SL 20:1

SAMPLE NO.: 52	WASTE TYPE:	Leather	Tannery	Sludge
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DATE TESTED: March 1982

COMMENTS: Combined primary and waste activated sludge from leather tannery, dewatered on centrifuge. Grey.

SOLID PHAS	E	TOTAL	SOLIDS:	35%	VOLATIL	E SOLIDS	:		 	· · · · · · ·			
	PARAM	ETER						Total S				7	
	Conce	ntration (ppm)						14 600.			1		
MULTIPLE-B	ATCH LE	ACHING PROCEDU	RE										
MEASUREI CHARACTER I		TEST CONDITION	Cr	Cu	РЬ	Zn	Sn					pH (Units)	Conductivity (mS/cm)
Concentrati (mg/L)	Ion	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.72 0.13 0.37 0.10 0.29 0.49	0.02 0.01 0.11 0.04 0.06 0.05	0.08 0.02 0.04 0.07 0.04 0.15	0.69 2.06 1.39 1.37 0.48 0.84	0.054 0.037 0.052 0.052 0.161 0.214					7.85 7.75 7.15 5.45 6.85 5.10	5.60 1.62 9.40 6.20 12.20 9.10
Release (µg∕g)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	2.88 2.60 1.48 2.00 1.16 9.80	0.08 0.20 0.44 0.80 0.24 1.00	0.32 0.40 0.16 1.40 0.16 3.00	2.76 41.2 5.56 27.4 1.92 16.8	0.22 0.74 0.21 1.04 0.64 4.28						
Efficiency (≴)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1											

#### SAMPLE NO.: 53 WASTE TYPE: Copper Wool Scrap

DATE TESTED: February 1982

COMMENTS: Green. From a phosphoric acid plant. Cu is used to remove As in the production of phosphoric acid

SOLID PHASE TOTAL SOLIDS: 66.5% VOLATILE SOLIDS: 12.5% PARAMETER As Cu Concentration (ppm) 106 000. 206 000. MULTIPLE-BATCH LEACHING PROCEDURE MEASURED TEST Conductivity рΗ CHARACTERISTIC CONDITION As Cu (Units) (mS/cm) Concentration DW 4:1 100. 5557. 3.30 16.9 (mg/L)DW 20:1 1111. 3.70 4.4 20. AS 4:1 80. 6761. 3.50 17.2 1852. AS 20:1 18. 3.95 6.4 SL 4:1 120. 8613. 3.40 18.5 SL 20:1 26. 2593. 4.15 9.1 22 228. Release DW 4:1 400. 22 220. (µg/g) DW 20:1 400. 27 044. AS 4:1 320. 37 040. AS 20:1 360. SL 4:1 480. 34 452. 51 860. SL 20:1 520. Efficiency DW 4:1 0.57 16.2 (%) DW 20:1 0.57 16.2 AS 4:1 0.45 19.8 AS 20:1 27.1 0.51 0.68 25.2 SL 4:1 SL 20:1 37.9 0.74

SAMPLE NO.: 53 WASTE TYPE: Copper Wool Scrap

DATE TESTED: February 1982

COMMENTS: Continued from previous page. Acid addition in EPA extraction procedure =  $0.0 \text{ mL} = 0.0 \text{ meq H}^+/\text{g}$  waste

MEASURED CHARACTER I ST IC	TEST CONDITION	As	Си				pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	110.	1042.				3.80	4.40
Release (µg/g)	EPA ASTM DW ASTM AS	2200.	20 840.					
Efficiency (\$)	EPA ASTM DW ASTM AS	3.12	15.2					<u> </u>

MEASURED CHARACTERISTIC	TEST CONDITION					1	pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Release (µg/g)	EPA ASTM DW ASTM AS							
Efficiency (%)	EPA ASTM DW ASTM AS							

# SAMPLE NO.: 54 WASTE TYPE: Sodium Chlorate Sludge (unwashed)

DATE TESTED: February 1982

COMMENTS: Black. Sludge from the production of sodium chlorate.

# SOLID PHASE

TOTAL SOLIDS: 58.8% VOLATILE SOLIDS: 25.4%

PARAMETER	As	Cu				
Concentration (ppm)	360.	693.				

DW 4:1 DW 20:1	0.22	0.08					1				(Units)	(mS/cm)
		0.00									11.30	50.5
	0.12	<0.03				1					11.05	13.9
AS 4:1	0.32	0.14									6.90	48.0
AS 20:1	0.33	0.24									6.20	18.0
SL 4:1	0.51	16.0									6.55	51.0
SL 20:1	0.72	5.04									6.00	22.0
DW 4:1	0.88	0.32										
DW 20:1	2.40				ł							
AS 4:1	1.28	0.56										
AS 20:1	6.60	4.80										
SL 4:1	2.04	64.0			1							
SL 20:1	14.4	100.										
DW 4:1	0.42	0.08										
DW 20:1	1.13						9					1
AS 4:1	0.60	0.14				i .						
	3.12											
SL 4:1	0.96	15.7				1	1					
SL 20:1	6.80	24.7					ļ					
	SL 4:1 SL 20:1 DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1 DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1	SL 4:1       0.51         SL 20:1       0.72         DW 4:1       0.88         DW 20:1       2.40         AS 4:1       1.28         AS 20:1       6.60         SL 4:1       2.04         SL 20:1       14.4         DW 4:1       0.42         DW 20:1       1.13         AS 4:1       0.60         AS 20:1       3.12         SL 4:1       0.96	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	SL 4:1 $0.51$ $16.0$ SL 20:1 $0.72$ $5.04$ DW 4:1 $0.88$ $0.32$ DW 20:1 $2.40$ AS 4:1 $1.28$ $0.56$ AS 20:1 $6.60$ $4.80$ SL 4:1 $2.04$ $64.0$ SL 20:1 $14.4$ $100.$ DW 4:1 $0.42$ $0.08$ DW 20:1 $1.13$ AS 4:1 $0.60$ $0.14$ AS 4:1 $0.60$ $15.7$	SL 4:1 $0.51$ $16.0$ SL 20:1 $0.72$ $5.04$ DW 4:1 $0.88$ $0.32$ DW 20:1 $2.40$ AS 4:1 $1.28$ $0.56$ AS 20:1 $6.60$ $4.80$ SL 4:1 $2.04$ $64.0$ SL 20:1 $14.4$ $100.$ DW 4:1 $0.42$ $0.08$ DW 20:1 $1.13$ AS 4:1 $0.60$ $0.14$ AS 20:1 $3.12$ $1.18$ $SL 4:1$ $0.96$ $15.7$	SL 4:1 $0.51$ $16.0$ SL 20:1 $0.72$ $5.04$ DW 4:1 $0.88$ $0.32$ DW 20:1 $2.40$ AS 4:1 $1.28$ $0.56$ $4.80$ SL 4:1 $2.04$ $64.0$ $5L$ SL 4:1 $2.04$ $64.0$ $5L$ SL 20:1 $14.4$ $100.$ $0.08$ DW 20:1 $1.13$ AS 4:1 $0.60$ $0.14$ $3.12$ $AS$ 4:1 $0.96$ $0.14$ $5.7$	SL 4:1 $0.51$ $16.0$ SL 20:1 $0.72$ $5.04$ DW 4:1 $0.88$ $0.32$ DW 20:1 $2.40$ AS 4:1 $1.28$ $0.56$ AS 20:1 $6.60$ $4.80$ SL 4:1 $2.04$ $64.0$ SL 20:1 $14.4$ $100.$ DW 4:1 $0.42$ $0.08$ DW 20:1 $1.13$ AS 4:1 $0.60$ DW 20:1 $1.13$ AS 4:1 $0.60$ DW 20:1 $1.13$ AS 4:1 $0.60$ DW 20:1 $1.13$ AS 4:1 $0.60$ SL 4:1 $0.96$ J5.7	SL 4:1 $0.51$ $16.0$ SL 20:1 $0.72$ $5.04$ DW 4:1 $0.88$ $0.32$ DW 20:1 $2.40$ AS 4:1 $1.28$ $0.56$ AS 20:1 $6.60$ $4.80$ SL 4:1 $2.04$ 64.0 $5L$ 20:1DW 4:1 $0.42$ DW 20:1 $1.13$ DW 4:1 $0.60$ DW 20:1 $1.13$ AS 4:1 $0.60$ DW 20:1 $1.13$ AS 4:1 $0.60$ DW 20:1 $1.13$ SL 4:1 $0.96$ DW 20:1 $5.7$	SL 4:1       0.51       16.0         SL 20:1       0.72       5.04         DW 4:1       0.88       0.32         DW 20:1       2.40         AS 4:1       1.28         0.56       4.80         SL 4:1       2.04         64.0       5L 20:1         SL 20:1       14.4         100.       100.         DW 4:1       0.42         0.08       0.14         AS 4:1       1.13         AS 4:1       0.60         SL 20:1       1.13         AS 4:1       0.60         0.14       10.50         AS 20:1       3.12         1.18       1.18         SL 4:1       0.96	SL 4:1       0.51       16.0         SL 20:1       0.72       5.04         DW 4:1       0.88       0.32         DW 20:1       2.40         AS 4:1       1.28         AS 4:1       1.28         SL 20:1       6.60         AS 20:1       6.60         SL 20:1       14.4         100.       100.         DW 4:1       0.42         DW 20:1       1.13         AS 4:1       0.60         DW 20:1       1.13         AS 4:1       0.60         DW 20:1       1.13         AS 4:1       0.60         SL 4:1       0.96         J5.7       15.7	SL 4:1       0.51       16.0       6.55         SL 20:1       0.72       5.04       6.00         DW 4:1       0.88       0.32       6.00       6.00         DW 20:1       2.40       7       7       7       7         AS 4:1       1.28       0.56       7       7       7       7         AS 4:1       1.28       0.56       4.80       7       7       7       7         SL 4:1       2.04       64.0       64.0       7

# SAMPLE NO.: 54 WASTE TYPE: Sodium Chlorate Sludge (unwashed)

DATE TESTED: February 1982

**COMMENTS:** Continued from previous page. Acid addition in EPA extraction procedure =  $356 \text{ mL} = 2.00 \text{ meq H}^{+}/\text{g}$  waste

MEASURED CHARACTERISTIC	TEST CONDITION	As	Cu				pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	0.28	0.05				8.10	14.2
Retease (µg/g)	EPA ASTM DW ASTM AS	5.60	1.00					
Efficiency (%)	EPA ASTM DW ASTM AS	2.64	0.25					

MEASURED CHARACTER I ST IC	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Release (µg∕g)	EPA ASTM DW ASTM AS							
Efficiency (≴)	EPA ASTM DW ASTM AS							

# SAMPLE NO.: 55 WASTE TYPE: Sodium Chlorate Sludge (washed)

DATE TESTED: February 1982

COMMENTS: Black, Lagoon sludge from production of sodium chlorate.

SOLID PHASE

TOTAL SOLIDS: 36.5% VOLATILE SOLIDS: 10.4%

ſ	PARAMETER	As	Cu				
	Concentration (ppm)	450.	340.				

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST I C	TEST CONDITION	As	Cu	-						pH (Unit		Conductivity (mS/cm)
Concentration	DW 4:1	0.26	<0.03		 <b>†</b>					11.0	0	0.81
(mg/L)	DW 20:1	0.10	<0.03							10.8	35	0.32
	AS 4:1	0.24	0.05			l	1			7.3	55	5.40
	AS 20:1	0.29	0.10							6.5	50	5.20
	SL 4:1	14.0	14.0							6.9	95	8.10
	SL 20:1	0.61	4.83		[					6,1	5	8.60
Release	DW 4:1	1.04			 							
(µg/g)	DW 20:1	2.00				l .						
	AS 4:1	0.96	0.20								-	
	AS 20:1	5.80	2.00									
	SL 4:1	56.0	56.0			1		1				
	SL 20:1	12.2	96.6									
Efficiency	DW 4:1	0.63										
(\$)	DW 20:1	1.22				ļ						
	AS 4:1	0.58	0.16			Ì		1				
	AS 20:1	3.53	1.61								ĺ	
	SL 4:1	34.1	45.1									
	SL 20:1	7.43	77.8		1	1	Į					

### SAMPLE NO.: 55 WASTE TYPE: Sodium Chlorate Sludge (washed)

DATE TESTED: February 1982

**COMMENTS:** Continued from previous page. Acid addition in EPA Extraction procedure = 426 mL =  $2.00 \text{ meg H}^+/\text{g}$  waste.

MEASURED CHARACTERISTIC	TEST CONDITION	As	Cu			 		pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS	0.36	0.04					8.30	6.00
Release (µg/g)	EPA ASTM DW ASTM AS	7.20	0.80						
Efficiency (%)	EPA ASTM DW ASTM AS	4.38	0.64						

MEASURED CHARACTERISTIC	TEST CONDITION						pH (Units)	Conductivity (mS/cm)
Concentration (mg/L)	EPA ASTM DW ASTM AS							
Release (µg/g)	EPA ASTM DW ASTM AS							
Efficiency (%)	EPA ASTM DW ASTM AS							

#### SAMPLE NO.: 56 WASTE TYPE: Cyanide Leach Tailings

DATE TESTED: March 1982

COMMENTS: Tailings produced from cyanide leach of flotation concentrate. Note: SW = local river water, with As 1.0 mg/L, Cr 0.01 mg/L, Cu = 0.01 mg/L, Fe = 0.73 mg/L, Pb 0.01 mg/L, Zn = 0.02 mg/L and TCN = 0.02 mg/L. Concentrations shown for SW are minus the concentrations found in the site water leaching medium.

SOLID PHASE

TOTAL SOLIDS: VOLATILE SOLIDS:

PARAMETER	As	Cr	Cu	Fe	Hg	Pb	Zn	TCN	
Concentration (ppm)	1680.	96.	100.	137000.	32,6	56.	344.	1.71	

MEASURED CHARACTERISTIC	TEST CONDITION	As	Cr	Cu	Fe	Hg	Pb	Zn	TCN	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.01	<0.1	<0.03	0.6	0.00190	<0.1	<0.03	1.57	 7.35	2.50
(mg/L)	DW 20:1	<0.01	<0.1	<0.03		0.00113	<0.1	<0.03	0.11	7.10	0.90
	AS 4:1	<0.01	0.2	0.08		0.00038	<0.1	2.24	0.11	5.05	6.60
	AS 20:1	0.03	0.2	0.16		0.00038	<0.1	0.92	0.08	4.55	3.90
	SW 4:1	<0.01	<0.1	<0.03		0.00120	<0.1	<0.03	3.01	7.50	2.45
	SW 20:1	<0.01	<0.1	<0.03		0.00088	<0.1	<0.03	0.39	7.10	0.85
Release	DW 4:1				2.4	0.01			6.28	 	
(µg/g)	DW 20:1					0.02			2.20		
	AS 4:1		0.8	0.32	1060.	<0.01		8,96	0.44		
	AS 20:1	0.6	4.0	3.20	220.	0.01		18.4	1.60		
	SW 4:1				0.68	<0.01			12.0		
	SW 20:1					0.02			7.80		
Efficiency	DW 4:1										
(%)	DW 20:1										1
	AS 4:1										
	AS 20:1										
	SW 4:1										
	SW 20:1			:							

SAMPLE NO.: 57 WASTE TYPE: Bulk Sulphide Flotation Tank Tailings

TOTAL SOLIDS:

DATE TESTED: March 1982

COMMENTS: Brown. Note: SW = local river water, with As 1.0 mg/L, Cr 0.01 mg/L, Cu = 0.01 mg/L, Fe = 0.73 mg/L, Pb 0.01 mg/L, Zn=0.02 mg/L and TCN=0.02 mg/L. The concentrations shown for SW leachates are minus the concentrations in the site water leaching medium.

SOLID PHASE

VOLATILE SOLIDS:

PARAMETER	As	Cr	Cu	Fe	Hg	Pb	Zn	TCN	
Concentration (ppm)	90.	24.	41.	11 000.	28.4	3.0	30.	0.137	

MEASURED CHARACTER ISTIC	TEST CONDITION	As	Cr	Cu	Fe	Hg	Pb	Zn	TCN	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.07	0.8	2.21	97.	0.000 37	0.4	1.70	0.20	2.80	1.40
(mg/L)	DW 20:1	0.04	0.2	0.49	36.	0.000 34	0.1	0.50	0.17	2.90	0.72
	AS 4:1	0.09	0.6	2.15	87.	0.000 47	<0.1	1.82	0.21	4.25	2.90
	AS 20:1	0.05	0.2	0.38	31.	0.000 42	<0.1	0.43	0.18	4.45	2.60
	SW 4:1	0.04	0.4	2.96	37.	0.000 45	<0.1	1.40	0.17	3.00	0.93
	SW 20:1	0.01	0.1	0.53	10.	0.000 13	<0.1	0.31	0.15	3.45	0.35
Release	DW 4:1	0.28	3.2	8.84	388.	<0.01	1.6	6.80	0.80		
(µg/g)	DW 20:1	0.80	4.0	9.80	720.	0.01	2.0	10.0	3.40		
	AS 4:1	0.36	2.4	8.60	348.	<0.01	1	7.28	0.84		
	AS 20:1	1.00	4.0	7.60	620.	0.01		8.60	3.60		
	SW 4:1	0.16	1.6	11.8	148.	<0.01		5.60	0.68		
	SW 20:1	0.20	2.0	10.6	200.	<0.01		6.20	3.00		
Efficiency	DW 4:1										
(%)	DW 20:1										
	AS 4:1										
	AS 20:1					ł	l				
	SW 4:1										
	SW 20:1										

SAMPLE NO.: 58 WASTE TYPE: Dewatered Sludge from an FGD Coal-Fired Generating Station

DATE TESTED: March 1982

COMMENTS: Grey

SOLID PHASE

TOTAL SOLIDS: 68.5% VOLATILE SOLIDS:

PARAMETER	Ag	AI	В	Ва	Be	Ca	Cd	Cr	Cu	Fe
Concentration (ppm)	<0.5	43 300.	290.	250.	2.69	177 000.	6.4	24.9	50.2	46 900.

### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER ISTIC	TEST CONDITION	Ag	AI	в	Ba	Be	Ca	са	Cr	Cu	Fe	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.005	0.33	0.013	2.48	<0.0005	575.	0.02	0.10	0.032	0.17	12.75	5.25
(mg/L)	DW 20:1	<0.005	1.34	0.036	0.424	<0.0005	171.	0.01	0.07	0.014	0.06	12.20	1.70
	AS 4:1	<0.005	0.50	7.61	0.269	<0.0005	1390.	0.04	0.60	0.024	0.19	10.05	6.50
	AS 20:1	<0.005	3.20	5.70	0.166	<0.0005	1470.	0.07	0.54	0.263	4.16	6.15	7.00
	SL 4:1	<0.005	2.37	23.1	0.083	0.0331	2170.	0.07	1.06	0.757	3.45	6.95	11.60
	SL 20:1	<0.005	34.5	6.24	0.005	0.0071	1590.	0.06	0.78	0,236	16.0	5.30	10.70
Release	DW 4:1		1.32	0.05	9.92		2300.	0.08	0.40	0.13	0.68		
(µg/g)	DW 20:1	1	26.8	0.72	8.48		3420.	0.20	1.40	0.28	1.20		
-	AS 4:1		2.00	30.4	1.08		5560.	0.16	2.40	0.10	0.76		
	AS 20:1		64.0	114.	3.32		29 400.	1.40	10.8	5.26	83.2		
	SL 4:1		9.48	92.4	0.33	0.13	8680.	0.28	4.24	3.03	13.8		
	SL 20:1		690.	125.		0.14	31 800.	1.20	15.6	4.72	320.		
Efficiency	DW 4:1		<0.01	0.03	5.79		1.90	1.83	2.35	0.37	<0.01		
(%)	DW 20:1		0.09	0.36	4.95		2.82	4.56	8.21	0.81	<0.01		
	AS 4:1		0.01	15.3	0.63		4.59	3.65	14.1	0.28	<0.01		
	AS 20:1		0.22	57.4	1.94		24.3	31.9	63.3	15.3	0.26		
	SL 4:1		0.03	46.5	0.19	7.19	7.16	6.39	24.9	8.81	0.04		
	SL 20:1		2.33	62.8		7.71	26.2	27.4	91.5	13.7	1.00		

# SAMPLE NO.: 58 WASTE TYPE: FGD Sludge

DATE TESTED: March 1982

COMMENTS: Continued from previous page

SOLID PHAS	<u>E</u>	TOTAL	SOLIDS:		VOLATILE	SOLIDS	:								
	PARAME	ETER	к	Mg	Mn	Мо	Na	NI	Р	Pb	SI	Sr	ТІ	v	Zn
	Concer	ntration (ppm)	8600.	4580.	183.	<30.	1200	43.	370.	40.	134 000	80.3	1970.	83.9	177.
			<u> </u>												
MULTIPLE-B	atch le/	NCHING PROCEDU	RE												
MEASUREI CHARACTER I		TEST CONDITION	к	Mg	Mn	Мо	Na	NI	Р	Pb	SI	Sr	TI	v	Zn
Concentrat (mg/L)	Ion	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	44. 10. 57. 18. 82. 20.	<0.01 <0.01 27.4 26.1 51.7 33.9	<0.01 <0.01 <0.01 1.59 2.15 2.46	0.6 0.3 0.9 <0.3 0.9 0.4	10 <b>.</b> 2.	0.08 <0.05 0.16 0.25 0.31 0.25	1.1 <0.6 1.7 2.7 4.5 3.2	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	0.73 1.50 6.06 29.8 8.73 43.8	1.52 0.344 1.22 0.506 1.44 0.437	<0.005 <0.005 0.010 0.016 0.011 0.098	0.015 0.054 0.247 0.071 0.073 0.300	0.06 <0.05 0.10 0.35 0.20 0.59
Release (µg∕g)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	176. 200. 228. 360. 328. 400.	110. 522. 207. 678.	31.8 8.60 49.2	2.4 6.0 3.6 3.6 8.0	40 <b>.</b> 40.	0.32 0.64 5.00 1.24 5.00	4.4 6.8 54. 18. 64.		2.92 30.0 24.2 596. 34.9 876.	6.08 6.88 4.88 10.1 5.76 8.74	0.04 0.32 0.04 1.96	0.06 1.08 0.99 1.42 0.29 6.00	0.24 0.40 7.00 0.80 11.8
Efficiency (%)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	2.99 3.40 3.87 6.11 5.57 6.79	3.49 16.6 6.59 21.6	25.4 6.86 39.3		4.87 4.87	1.09 2.17 17.0 4.21 17.0	1.74 2.68 21.3 7.10 25.3		<0.01 0.03 0.03 0.65 0.04 0.95	11.1 12.5 8.87 18.4 10.5 15.9	<0.01 0.02 <0.01 0.15	0.10 1.88 1.72 2.47 0.51 10.4	0.20 0.33 5.77 0.66 9.73

### SAMPLE NO.: 58 WASTE TYPE: FGD Sludge

DATE TESTED: March 1982

COMMENTS: Continued from previous page.

SOLID PHASE

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TOTAL SOLIDS:

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VOLATILE SOLIDS:

MEASURED CHARACTER I ST I C	TEST CONDITION	õ	Th	Zr								
Concentration	DW 4:1	<0.05	<0.01	<0.05						 		
(mg/L)	DW 20:1	<0.05	0.04	<0.05					1			
	AS 4:1	0.06	<0.01						1			1
	AS 20:1	0.08	<0.01	<0.05								
	SL 4:1	<0.05	<0.01	<0.05								
	SL 20:1	0.10	<0.01	<0.05								
Release	DW 4:1											
(µg/g)	DW 20:1		0.08					1				
	AS 4:1	0.24	i i									
	AS 20:1	1.60										
	SL 4:1									1		
	SL 20:1	2.00							}			
Efficiency	DW 4:1											
(\$)	DW 20:1							ł				Į
	AS 4:1							9	ļ			1
	AS 20:1					ŀ	ł			4		
	SL 4:1				{						1	{
	SL 20:1							1				

#### SAMPLE NO.: 61 WASTE TYPE: Bottom Ash from an FGD Coal-Fired Generating Station

DATE TESTED: March 1982

COMMENTS: Rust brown

### SOLID PHASE

TOTAL SOLIDS: 88.8% VOLATILE SOLIDS:

PARAMETER	Ag	A1	В	Ba	Be	Са	Cd	Cr	Cu	Fe
Concentration (ppm)	<0.5	94 400.	540.	460.	7.94	30 900.	5.8	34.7	96.9	158 000.

# MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER ISTIC	TEST CONDITION	Ag	AI	В	Ba	Be	Ca	Cd	Cr	Cu	Fe	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.02	<0.05	0.29	<0.02	<0.002	44.7	<0.05	<0.05	<0.04	<0.05	7.65	0.33
(mg/L)	DW 20:1	<0.02	<0.05	<0.02	<0.02	<0.002	15.0	<0.05	<0.05	<0.04	<0.05	7.40	0.11
	AS 4:1	<0.02	<0.05	0.79	0.04	<0.002	192.	<0.05	<0.05	0.10	1.68	4.70	3.90
	AS 20:1	0.08	0.08	0.21	0.17	<0.002	46.6	<0.05	<0.05	0.09	2.55	4.70	3.50
	SL 4:1	0.07	4.10	1.01	0.07	<0.002	190.	0.06	<0.05	0.43	2.81	4.90	8.00
	SL 20:1	0.08	4.31	0.37	0.22	<0.002	50.2	<0.05	0.06	0.17	5.20	4.85	7.80
Release	DW 4:1			1.16			179.			,			
(µg/g)	DW 20:1						300.		;				
	AS 4:1			3.16	0.16		768.			0.40	6.72		
	AS 20:1	1.6	1.6	4.20	3.40		932.			1.80	51.0		
	SL 4:1	0.28	16.4	4.04	0.28		760.	0.24		1.72	11.2		
	SL 20:1	1.6	86.2	7.40	4.40		1004.	1	1.2	3.40	104.		
Efficiency	DW 4:1			0.24			0.65						
(%)	DW 20:1						1.09			1			
	AS 4:1			0.66	0.04		2.80			0.46	<0.01		
	AS 20:1		<0.01	0.88	0.83		3.40			2.09	0.04		
	SL 4:1		0.02	0.84	0.07		2.77	4.66		2.00	0.01		
	SL 20:1		0.10	1.54	1.08		3.66		3.89	3.95	0.07		

#### SAMPLE NO.: 61 WASTE TYPE: FGD Bottom Ash

DATE TESTED: March 1982

COMMENTS: Continued from previous page.

SOLID PHASE	TOTAL	SOLIDS:		VOLATILE	SOLIDS:									
ſ	PARAMETER	к	Mg	Mn	Мо	Na	Ni	Р	Pb	Si	Sr	TI	v	Zn
-	Concentration (ppm)	15 500.	4580.	395.	<30.	5600.	92.	850.	130.	224 000	407.	5300.	146.	328.
MULTIPLE-BA	TCH LEACHING PROCEDU	RE												
MEASURED CHARACTER IS		к	Mg	Mn	Мо	Na	NĪ	Р	Pb	Si	Sr	ті	v	Zn
Concentratio (mg/L)	on DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<5. <5. 10. 17. 12.	8.35 1.53 15.4 3.95 15.8 4.54	<0.05 <0.05 1.74 0.44 1.73 0.51	<1. <1. <1. 1. 2. 2.	<5. <5.	<0.3 <0.3 <0.3 <0.3 <0.3 <0.3 <0.3	5. <3. 17. 5. 17. 8.	<0.05 <0.05 <0.05 <0.05 <0.05 <0.05 <0.05	<0.3 <0.3 7.4 1.1 11.9 5.3	0.118 0.017 0.269 0.051 0.270 0.050	<0.02 <0.02 <0.02 <0.02 0.04 0.13	<0.02 <0.02 <0.02 0.09 0.17 0.13	<0.3 <0.3 2.9 0.9 2.0 0.9
Release (µg/g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	200. 68. 240.	33.4 30.6 61.6 79.0 63.2 90.8	6.96 8.80 6.92 10.2	20. 8. 40.			20. 68. 100. 68. 160.		29.6 22.0 47.6 106.	0.47 0.34 1.08 1.02 1.08 1.00	0.16 2.60	1.80 0.68 2.60	11.6 18.0 8.0 18.0
Efficiency (%)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	1.45 0.49 1.74	0.82 0.75 1.51 1.94 1.55 2.23	1.98 2.51 1.97 2.91				2.65 9.01 13.3 9.01 21.2		0.01 0.01 0.02 0.05	0.13 0.09 0.30 0.28 0.30 0.28	<0.01 0.06	1.39 0.52 2.01	3.9 6.1 2.7 6.1

### SAMPLE NO.: 61 WASTE TYPE: FGD Bottom Ash

DATE TESTED: March 1982

COMMENTS: Continued from previous page.

SOLID PHASE

TOTAL SOLIDS:

#### VOLATILE SOLIDS:

PARAMETER	¢0	Th	Zr		-		
Concentration (ppm)	<5.	13.	159.				

MEASURED CHARACTER I ST IC	TEST CONDITION	Co	Th	Zr							
Concentration	DW 4:1	<0.3	<0.05	<0.3	1						
(mg/L)	DW 20:1	<0.3	<0.05	<0.3							
	AS 4:1	<0.3	<0.05	<0.3							
	AS 20:1	0.5	0.60	<0.3							
	SL 4:1	0.7	0.79	<0.3					1		
	SL 20:1	0.7	0.71	<0.3							
Release	DW 4:1				 						
(µg/g)	DW 20:1						:				
	AS 4:1							1			
	AS 20:1	10.0	12.0								
	SL 4:1	2.8	3.16								
	SL 20:1	14.0	14.2								
Efficiency	DW 4:1		<b></b>								
(%)	DW 20:1										
	AS 4:1					1			1		
	AS 20:1		104.					l			
	SL 4:1		27.4		1	1	l	1			
	SL 20:1		123.			ł		1			

# SAMPLE NO.: 62 WASTE TYPE: Fly Ash Material from an FGD Coal-Fired Generating Station

DATE TESTED: March 1982

COMMENTS: Brown, particle size <150 µm

#### SOLID PHASE

.

TOTAL SOLIDS: 99.8% VOLATILE SOLIDS:

PARAMETER	Ag	AI	В	Ва	Be	Са	Cd	Cr	Cu	Fe
Concentration (ppm)	<0.5	86 000.	1320.	490.	10.6	20 300.	15.2	127.	94.6	91 200.

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Ag	AI	В	Ba	Be	Ca	Cd	Cr	Cu	Fe	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.02	5.84	116.	0.10	<0.002	525.	<0.05	0.29	<0.04	<0.05	9.90	4.10
(mg/L)	DW 20:1	<0.02	2.67	31.0	0.09	<0.002	455.	<0.05	0.08	<0.04	<0.05	9.85	2.35
	AS 4:1	<0.02	56.7	163.	0.36	0.018	850.	0,78	1.57	0.46	16.1	6.25	8.10
	AS 20:1	<0.02	39.1	36.7	0.17	0.027	581.	0.23	1.06	0.49	17.2	5.70	5.90
	SL 4:1	<0.02	197.	164.	0.55	0.129	1050.	0.85	5.60	4.06	167.	6.15	12.00
	SL 20:1	<0.02	59.1	41.4	0.21	0.041	630.	0.20	1.59	1.01	44.8	5,90	8.10
Release	DW 4:1		23.4	464.	0.40		2100.		1.16				
(µg/g)	DW 20:1		53.4	620.	1.80		9100.		1.60				
	AS 4:1		227.	652.	1.44	0.07	3400.	3.12	6.28	1.84	64.4		
	AS 20:1		782.	734.	3.40	0.54	11 620.	4.60	21.2	9.80	344.		
	SL 4:1		788.	656.	2.20	0.52	4200.	3.40	22.4	16.2	668.		
	SL 20:1		1182.	828.	4.20	0.82	12 600.	4.00	31.8	20.2	896.		
Efficiency	DW 4:1		0.03	35.2	0.08		10.4		0.91				
(%)	DW 20:1		0.06	47.0	0.37		44.9		1.26				
	AS 4:1		0.26	49.5	0.29	0.68	16.8	20.6	4.95	1.95	0.07		
	AS 20:1		0.91	55.7	0.69	5.10	57.3	30.3	16.7	10.4	0.38		
	SL 4:1		0.92	49.8	0.45	4.88	20.7	22.4	17.7	17.2	0.73		
	SL 20:1		1.38	62.8	0.86	7.75	62.2	26.4	25.1	21.4	0.98		

### SAMPLE NO.: 62 WASTE TYPE: FGD Fly Ash

DATE TESTED: March 1982

COMMENTS: Continued from previous page.

SOLID PHASE	-	TOTAL	SOLIDS:		VOLATILE	SOLIDS:									
ſ	PARAME	ETER	к	Mg	Mn	Мо	Na	Nİ	Р	Pb	SI	Sr	ТІ	v	Zn
-	Concer	ntration (ppm)	19 200.	5140.	243.	40.	10 700.	119.	1080.	150.	246 000	. 331.	5270.	201.	738.
MULTIPLE-BA	TCH LEA	ACHING PROCEDUR	E												
MEASURED CHARACTER IS		TEST CONDITION	к	Mg	Mn	Мо	Na	NĪ	Р	РЬ	SI	Sr	Ti	v	Zn
Concentrati (mg/L)	on	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	139. 29. 173. 41. 198. 45.	50.0 12.1 78.6 17.8 84.8 20.1	0.07 <0.05 13.0 3.16 16.0 3.64	9. 2. 2. <1. 5. <1.	296. 61.	<0.3 <0.3 1.6 0.4 1.6 0.4	<3. <3. 5. 4. 29. 3.	<0.05 <0.05 0.15 0.10 0.35 <0.05	<0.3 <0.3 30.8 17.1 72.7 25.1	3.06 2.05 6.45 2.55 8.35 2.94	<0.02 <0.02 0.45 0.42 5.24 0.61	0.08 0.05 0.30 0.25 3.08 0.44	<0.3 <0.3 8.2 2.2 8.9 2.3
Release		DW 4:1	556.	200.	0.28	36.	1184.					12.2		0.32	
(g/gµ)		DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	580. 692. 820. 792. 900.	242. 314. 356. 339. 402.	52.0 63.2 64.0 72.8	40. 8. 20.	1220.	6.4 8.0 6.4 8.0	20. 80. 116. 60.	0.60 2.00 1.40	123. 342. 291. 502.	41.0 25.8 51.0 33.4 58.8	1.80 8.40 20.9 12.2	1.00 1.20 5.00 12.3 8.80	32.8 44.0 35.6 46.0
Efficiency (%)		DW 4:1 DW 20:1 AS 4:1	2.90 3.03 3.61	3.90 4.72 6.13	0.12 21.4	90.1 100. 20.0	11.1 11.4	5.39	1.85	0.40	0.05	3.70 12.4 7.81	0.03	0.16 0.50 0.60	4.4
		AS 20:1 SL 4:1 SL 20:1	4.28 4.13 4.70	6.94 6.61 7.83	26.1 26.4 30.0	50 <b>.</b> 1		6.73 5.39 6.73	7.42 10.8 5.56	1.34 0.93	0.14 0.12 0.20	15.4 10.1 17.8	0.16 0.40 0.23	2.49 6.14 4.39	5.9 4.8 6.2

#### SAMPLE NO.: 62 WASTE TYPE: FGD Fly Ash

DATE TESTED: March 1982

COMMENTS: Continued from previous page.

SOLID PHASE

TOTAL SOLIDS:

VOLATILE SOLIDS:

PARAMETER	Co	Th	Zr				
Concentration (ppm)	14.	13.	150.				

### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Co	Th	Zr					
Concentration (mg/L)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	<0.3 <0.3 0.4 <0.3 <0.3 <0.3	<0.05 0.10 0.25 0.15 <0.05 <0.05	<0.3 <0.3 <0.3 <0.3 <0.3 <0.3 <0.3					
Release (µg∕g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	1.6	2.0 1.0 3.0						
Efficiency (g)	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	11.5	15.4 7.70 23.1						

## SAMPLE NO.: 63 WASTE TYPE: Sludge Material from an FGD Coal-Fired Generating Station

DATE TESTED: April 1982

COMMENTS: Biege

SOLID PHASE

TOTAL SOLIDS: 72.3% VOLATILE SOLIDS:

	PARAMETER	Ag	AI	В	Ва	Be	Ca	Cd	Cr	Cu	Fe
i	Concentration (ppm)	<0.5	1350.	119.	50.	<0.05	165 000.	3.2	<1.	18.8	1730.

### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I STIC	TEST CONDITION	Ag	AI	Ъ	Ва	Be	Са	Cd	Cr	Cu	Fe	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	<0.02	0.43	19.4	<0.02	<0.002	643.	<0.05	0.06	<0.04	<0.05	8.70	2.15
(mg/L)	DW 20:1	<0.02	<0.05	4.08	<0.02	<0.002	601.	<0.05	<0.05	<0.04	<0.05	8.65	1.85
	AS 4:1	<0.02	6.22	19.2	<0.02	<0.002	1610.	0.05	0.07	<0.04	1.92	6.55	5.64
	AS 20:1	<0.02	4.23	4.02	<0.02	<0.002	1220.	<0.05	<0.05	<0.04	2.21	6.00	5.50
	SL 4:1	<0.02	8,98	17.4	<0.02	<0.002	1820.	<0.05	0.11	0.06	7.98	6.20	10.90
	SL 20:1	<0.02	2.72	3.99	<0.02	<0.002	1430.	<0.05	<0.05	<0.04	3,28	5.90	10.10
Release	DW 4:1		1.72	77.6			2572.		0.24				
(µg/g)	DW 20:1			81.6	Ì		12 020.						
	AS 4:1		24.9	76.8			6440.	0.20	0.28		7.68		
	AS 20:1		84.6	80.4			24 400.				44.2		
	SL 4:1		35.9	69.6			7280.		0.44	0.24	31.9		
	SL 20:1		54.4	79.8			28 600.				65.6		
Efficiency	DW 4:1		0.18	90.2			2.16						
(%)	DW 20:1			94.8			10.1						
	AS 4:1		2.55	89.2			5.40	8.64			0.61		
	AS 20:1		8.67	93.4	]		20.5				3.53		
	SL 4:1	1	3.68	80.9	ĺ		6.10			2.55	2.55		
	SL 20:1		5.57	92.7			24.0				5.24		

### SAMPLE NO.: 63 WASTE TYPE: FGD Sludge

DATE TESTED: April 1982

COMMENTS: Continued from previous page.

SOLID PHASE	TOTAL	SOLIDS:		VOLATILE	SOL1DS:									
ſ	PARAMETER	к	Mg	Mn	Мо	Na	NI	Р	Pb	SI	Sr	Ті	v	Zn
-	Concentration (ppm)	300.	783.	34.6	<30	<100	13.	280.	<5.	4300.	14.7	81.	0.9	15.
	TCH LEACHING PROCEDUR			<u>_</u>			•		<u> </u>	<u>_</u>				
MULI IPLE-DA	TCH LEACHING PROCEDUR	ι <u>ε</u>	1	· · · · · · · · · · · ·										
MEASURED CHARACTER IS		к	Mg	Mn	Мо	Na	Ni	Ρ	Pb	SI	Sr	Ţi	v	Zn
Concentratio	on DW 4:1	<5.	20.4	0.71	<1.	<5.	<0.3	<3.	<0.05	<0.3	0.240	<0.02	<0.02	<0.
(mg/L)	DW 20:1	<5.	3.78	0.21	<1.	<5.	<0.3	<3.	<0.05	<0.3	0.100	<0.02	<0.02	<0.
0	AS 4:1	<5.	23.3	1.50	<1.		<0.3	<3.	<0.05	<0.3	0.613	<0.02	<0.02	0.
	AS 20:1	<5.	9.51	0.56	<1.		<0.3	<3.	<0.05	<0.3	0,237	<0.02	<0.02	<0.
	SL 4:1	<5.	22.2	1.41	<1.		<0.3	3.	<0.05	0.5	0.674	0.10	<0.02	<0.
	SL 20:1	<5.	8.28	0.54	<1.		<0.3	<3.	<0.05	<0.3	0.267	0.09	<0.02	<0.
Release	DW 4:1		81.6	2.84							0.96			
(µg/g)	DW 20:1		75.6	4.20			1				2.00			
	AS 4:1		93.2	6.00							2.45			1.
	AS 20:1		190.	11.2							4.74			
	SL 4:1		88.8	5.64				12.		2.0	2.70	0.4		
	SL 20:1		166.	10.8							5.34	1.8		
Efficiency	DW 4:1		14.4	11.4							9.03			
(%)	DW 20:1		13.4	16.8							18.8			
	AS 4:1		16.5	23.9							23.1	i		11.
	AS 20:1		33.6	44.8							44.6			
	SL 4:1		15.7	22.5				5.93		0.06	25.4	0.68		
	SL 20:1		29.2	43.2							50.2	3.07		

SAMPLE NO.: 63	WASTE	TYPE:	FGD	Sludge
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DATE TESTED: April 1982

COMMENTS: Continued from previous page.

SOLID PHASE	<u> </u>	TOTAL	SOLIDS:		VOLATILE	SOLIDS	:							
	PARAM	ETER	60	Th	Zr		1			<u> </u>	•		]	
	Conce	ntration (ppm)	<5.	<1.	<5.									
		ACHING PROCEDUR												
MEASURED		TEST						1	i					Γ
CHARACTERIS		CONDITION	Co	Th	Zr									
Concentrati	on	DW 4:1	<0.3	<0.05	<0.3			1						T
(mg/L)		DW 20:1	<0.3	<0.05	<0.3									l
		AS 4:1	<0.3	<0.05	<0.3									
		AS 20:1	<0.3	<0.05	<0.3									
		SL 4:1	<0.3	<0.05	<0.3							1		
		SL 20:1	<0.3	<0.05	<0.3									
Release		DW 4:1												
(µg/g)		DW 20:1												ŀ
		AS 4:1												
		AS 20:1												
		SL 4:1												
		SL 20:1												L
Efficiency		DW 4:1												
(%)		DW 20:1										ļ		
		AS 4:1				1		1	1				ļ	
		AS 20:1												
		SL 4:1		Į [				]	ļ			}	1	
_		SL 20:1		l I				1	1	1	1		1	1

# SAMPLE NO.: 64 WASTE TYPE: Cyanide and Arsenic Tailings from Gold Mine Effluent Treatment

DATE TESTED: September 1982

COMMENTS: Brown. Note: SW = holding pond water, pH = 7.8, contains 0.16 mg/L TCN

SOLID PHASE

TOTAL SOLIDS: 13.8% VOLATILE SOLIDS: 9.1%

PARAMETER	As	Cu	Fe	Nİ	Zn	TCN		
Concentration (ppm)	62 000.	35 700.	305 000.	2140.	2400.	0.35		

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTERISTIC	TEST CONDITION	As	Cu	Fe	Nİ	Zn	TCN			pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1										
(mg/L)	DW 20:1 AS 4:1	0.18	0.04	0.03	0.02	0.012	0.02			7.4	0.24
	AS 20:1 S₩ 4:1	0.10	79.0	0.29	9.80	9.80	<0.02			4.8	4.30
	SW 20:1	<0.01	<0.01	0.03	<0.005	<0.005	0.15			7.7	2.05
Release	DW 4:1										
(µg/g)	DW 20:1 AS 4:1	3.6	0.8	0.6	0.4	0.24	0.4				
	AS 20:1 SW 4:1	2.0	1580.	5.8	196.	196.					
	SW 20:1			0.6							
Efficiency	DW 4:1										
(\$)	DW 20:1 AS 4:1	0.04	0.02	<0.01	0.13	0.07					
	AS 20:1 SW 4:1	0.02	32.0	0.01	66.1	59.0					
	SW 20:1		ļ	<0.01		ł			1		

# SAMPLE NO.: 67 WASTE TYPE: Baghouse Sludge from an FGD Coal-Fired Generating Station

DATE TESTED: February 1983

COMMENTS: Grey

### SOLID PHASE

### TOTAL SOLIDS: 99.8% VOLATILE SOLIDS:

PARAMETER	Al	As	Ва	Ca	Cr	Cu	Fe	к	Mg	Nİ
Concentration (ppm)	51 500.	103.	8690.	108 000.	50.	133.	40 600.	6000.	26 700.	30.

# MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER ISTIC	TEST CONDITION	AI	As	Ва	Ca	Cr	Cu	Fe	к	Mg	Nİ	pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	50.	0.530	0.19	158.	0.2	0.09	0.5	483.	0.1	<0.1	11.9	55.0
(mg/L)	DW 20:1	38.	0.095	0.02	294.	0.1	<0.01	0.1	91.	0.1	<0.1	11.2	16.0
	AS 4:1	34.	0.198	1.65	452.	0.1	0.01	0.2	483.	0.1	<0.1	11.4	54.0
	AS 20:1	<0.1	0.230	0.11	567.	<0.1	0.02	0.1	100.	305.	<0.1	8.5	18.2
	SL 4:1												
	SL 20:1							1					
Release	DW 4:1	200.	2.12	0.76	632.	0.8	0.36	2.0	1932.	0.4			
(µg/g)	DW 20:1	760.	1.90	0.60	5880.	2.0		2.0	1820.	2.0	r		
	AS 4:1	136.	0.79	6.60	1808.	0.4	0.04	0.8	1932.	0.4			
	AS 20:1		4.60	2,20	11 340.		0.40	2.0	2000.	6100.			
	SL 4:1									•			
	SL 20:1												
Efficiency	DW 4:1	0.39	2.06	0.01	0.59	1.60	0.27	<0.01	32.2	<0.01			
(%)	DW 20:1	1.48	1.84	0.01	5.44	4.00		<0.01	30.3	0.01			
	AS 4:1	0.26	0.77	0.08	1.67	0.80	0.03	<0.01	32.2	<0.01			
	AS 20:1		4.47	0.03	10.5		0.30	<0.01	33.3	22.9			
	SL 4:1												
	SL 20:1								1				

#### SAMPLE NO.: 67 WASTE TYPE: FGD Baghouse Studge

DATE TESTED: February 1983

COMMENTS: Continued from previous page

SOLID PHASE

TOTAL SOLIDS:

VOLATILE SOLIDS:

PARAMETER	Se	SI	Sr	v	Zn	so <sub>4</sub>		
Concentration (ppm)	15.	108 000.	3530.	111.	110.	290 000.		

#### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTER I ST IC	TEST CONDITION	Se	SI	Sr	v	Zn	SO <sub>4</sub>					
Concentration	DW 4:1	0.93	41.	21.	4.6	0.13	37 800.					
(mg/L)	DW 20:1	0.40	2.4	21.	0.42	<0.01	7700.					
	AS 4:1	0,78	16.	23.	3.4	0.20	35 600.					
	AS 20:1	0.47	86.	32.	1.1	0.30	9300.			1		
	SL 4:1											
	SL 20:1											
Release	DW 4:1	3.72	164.	84.	18.4	0.52	151 200.		·			
(µg/g)	DW 20:1	8.00	48.	420.	8.4		154 000.					
	AS 4:1	3.12	64.	92.	13.6	0.80	142 400.	1				
	AS 20:1	9.40	1720.	640.	22.0	6.00	186 000.					
	SL 4:1					r						
	SL 20:1											
Efficiency	DW 4:1	24.8	0,15	2.38	16.6	0.47	52.1			-		
(%)	DW 20:1	53.3	0.04	11.9	7.57		53.1					1
-	AS 4:1	20.8	0.06	2.61	12.3	0.73	49.1					
	AS 20:1	62.7	1.59	18.1	19.8	5.45	64.1				ł	ļ
	SL 4:1											
	SL 20:1						1 1					

SAMPLE NO.: 68 WASTE TYPE: Cured Sludge from an FGD Coal-Fired Generating Station

VOLATILE SOLIDS:

TOTAL SOLIDS: 69%

DATE TESTED: February 1983

COMMENTS: Grey

SOLID PHASE

	PARAMETE	ER	AI	As	Ba	Ca	Cr	Cu	Fe	к	Mg	NĪ		
	Concentr	ation (ppm)	54 800.	13.5	2990.	116 000.	43.	151.	46 200.	5800.	30 300.	43.	1	
												<u>.</u>		
MULTIPLE-BA	TCH LEACH	HING PROCEDUR	Ε											
MEASURED CHARACTER IS	1	TEST CONDITION	AI	As	Ва	Са	Cr	Cu	Fe	к	Mg	Nİ	pH (Units)	Conductivity (mS/cm)
Concentrati (mg/L)	on	DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	38. 29. 42. <0.1	1.15 0.480 0.445 0.252	0.90 0.11 0.87 0.27	38. 42. 75. 578.	<0.1 <0.1 0.1 0.1	0.06 0.02 0.07 0.06	0.3 0.1 0.2 <0.1	210. 45. 210. 52.	0.1 0.1 0.6 244.	<0.1 <0.1 <0.1 <0.1	11.85 11.40 10.15 7.20	55.0 16.9 53.0 18.9
Release (µg∕g)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	152. 580. 168.	4.60 9.60 1.78 5.04	3.60 2.20 3.48 5.40	152. 840. 300. 11560.	0.4 2.0	0.24 0.40 0.28 1.20	1.2 2.0 0.8	840. 900. 840. 1040.	0.4 2.0 2.4 4880.			
Efficiency (%)		DW 4:1 DW 20:1 AS 4:1 AS 20:1 SL 4:1 SL 20:1	0.40 1.53 0.44	49.4 103. 19.1 54.1	0.17 0.11 0.17 0.26	0.19 1.05 0.37 14.4	1.35 6.74	0.23 0.38 0.27 1.15	<0.01 0.01 <0.01	5.25 22.5 21.0 26.0	<0.01 0.01 0.01 23.3			

# SAMPLE NO.: 68 WASTE TYPE: Cured FGD sludge

DATE TESTED: February 1983

COMMENTS: Continued from previous page

SOLID PHASE

TOTAL SOLIDS:

VOLATILE SOLIDS:

PARAMETER	Se	SI	Sr	v	Zn	SO <sub>L4</sub>		
Concentration (ppm)	14.	152 000.	3870.	104.	130.	481 000.		

MEASURED CHARACTER I ST IC	TEST CONDITION	Se	Si	Sr	v	Zn	SO <sub>4</sub>					
Concentration	DW 4:1	0.50	13.	3.1	4.1	0.06	40 400.					
(mg/L)	DW 20:1	0.19	17.	1.9	0.72	0.27	7400.	1.				
	AS 4:1	0.40	1.2	3,1	3.0	0.09	37 500.					1
	AS 20:1	0.17	28.	23.	0.17	0.06	7970.					
	SL 4:1											ŀ
	SL 20:1	1										
Release	DW 4:1	2.00	52.	12.4	16.4	0.24	161 600.					
(µg/g)	DW 20:1	3.80	340.	38.0	14.4	5.40	148 000.					
	AS 4:1	1.60	4.8	12.4	12.0	0,36	150 000.					
	AS 20:1	3.40	560.	460.	3.4	1.20	159 400.					
	SL 4:1		i i									
	SL 20:1											
Efficiency	DW 4:1	20.7	0.05	0.46	22.9	0.27	48.7		1			
(%)	DW 20:1	39.3	0.32	1.42	20.1	6.02	44.6			1		1
	AS 4:1	16.6	<0.01		16.7	0.40	45.2					
	AS 20:1	35.2	0.53	17.2	4.74	1.34	48.0	}	1	}	}	ļ
	SL 4:1											l
	SL 20:1											

#### SAMPLE NO.: 70 WASTE TYPE: Impregnated Charcoal

DATE TESTED: August 1983

COMMENTS: Spent charcoal from gas mask cartridges, R.M.S. Kingston

## SOLID PHASE

### TOTAL SOLIDS: 92.3% VOLATILE SOLIDS:

PARAMETER	Ag	Tot.Cr	Cr <sup>6</sup>	Cu	Pb	Zn		
Concentration (ppm)	139*	27 000	-	68 000	12.0	34.0		

\*Aqua-regia leach and nitric acid+H\_2O\_2 digestion

### MULTIPLE-BATCH LEACHING PROCEDURE

MEASURED CHARACTERISTIC	TEST CONDITION	Ag	Tot.Cr	0r <sup>6</sup>	Cu	РЪ	Zn				pH (Units)	Conductivity (mS/cm)
Concentration	DW 4:1	0.012	255	272	5.1	<.10	.60	 			7,90	2.39
(mg/L)	DW 20:1	0.005	122	136	.9	<.10	<.10				7.80	1.00
	AS 4:1	0.010	177	173	8.1	<.10	.30				7.45	6.69
	AS 20:1	0.014	15	15	210	<.10	.40				5.80	4.83
	SL 4:1	0.037	232	225	112	<.10	•20				7.20	12.02
	SL 20:1	0.030	88	88	1634	<.10	•70				5.50	9.62
Release	DW 4:1	0.05	1020	1088	20		2.4	 				· · · · · · · · · · · · · · · · · · ·
(µg∕g)	DW 20:1	0.10	2440	2720	18			1				
	AS 4:1	0.04	708	692	32		1.2					
	AS 20:1	0.28	300	300	4200		8.0					
	SL 4:1	0.15	928	900	448		.8		ļ			•
	SL 20:1	0.60	1760	1760	32 680		14					
Efficiency	DW 4:1	0.04	4.1		0.03		7.6					
(%)	DW 20:1	0.08	9.8		0.03				1			
	AS 4:1	0.03	2.8		0.05		3.8			1		
	AS 20:1	0.22	1.2		6.69		25		ļ			
	SL 4:1	0.12	3.7		0.71		2.5		Į			
	SL 20:1	0.47	7.1		52.1		45					