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NO. 1227

**NATO REFERENCE MOBILITY MODEL
EVALUATION OF THE ILTIS 4 × 4 TRUCK (U)**

by

D.M. Hanna

and

D.M. Patterson

ACN 0316X

May 1988



DEFENCE RESEARCH ESTABLISHMENT SUFFIELD, RALSTON, ALBERTA

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ABSTRACT

//⁵⁰
The Directorate of Land Requirements (DLR), in an effort to assess the usefulness of the NATO Reference Mobility Model (NRMM) in vehicle procurement activities, initiated a study at the Defence Research Establishment Suffield with the following objectives: 1) to determine the difficulty and time required to provide all necessary NRMM input data for a typical wheeled vehicle; 2) to determine the time required to perform an NRMM evaluation; and 3) to establish a wheeled vehicle baseline. The vehicle chosen for this study was the Iltis 4X4 ½ ton truck. All required vehicle characteristics were obtained within an acceptable time frame with the exception of the pitch-mass-moment of inertia of the sprung mass, which eventually was measured at an American laboratory. The NRMM simulation of the Iltis 4X4 required approximately one month to complete. The baseline performance is represented by curves of speed versus cumulative percent of area and by a mobility rating speed of 40 kilometers per hour over representative German terrain.//

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ACKNOWLEDGEMENTS

The authors express their gratitude to the staff of the Land Engineering Test Establishment, particularly Maj. C. Guerette and Mr. G. Isnor, for their extensive contributions by way of measurement of vehicle characteristics and performance, and to members of the Directorate of Land Requirements, most notably Col. D.B. McGibbon and Maj. J. Sharpe, for entertaining the possibility of using mobility modelling in vehicle procurement activities and for subsequently initiating this task.

The authors also acknowledge the continual assistance rendered by the Computer Group of DRES in support of modelling activities.

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1.0 INTRODUCTION

The NATO Reference Mobility Model (NRMM), a comprehensive computer program for predicting the mobility of land vehicles, is used regularly by the US Armed Forces to aid in vehicle procurement activities. It is utilized both to establish specifications of desired vehicle performance and to evaluate contending vehicles against these specifications.

The Directorate of Land Requirements (DLR) of the Canadian Forces, motivated by upcoming vehicle acquisition projects, is considering NRMM usage as well. This is the result of a desire by DLR staff to modernize and improve the specification of mobility requirements and the evaluation of mobility performance of contending vehicles. However, DLR became aware that, while NRMM mobility evaluations may be more desirable than those previously used, an NRMM simulation requires that prospective manufacturers provide extensive data regarding the

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2.

specific characteristics of candidate vehicles. The following question resulted: "Are vehicle manufacturers prepared to devote the extra labour and expense required to provide this volume of vehicle data as an additional part of a proposal?"

Having had no prior requirements to determine the total complement of NRMM vehicle characteristics, it was deemed appropriate that DND gain experience with the determination of these data for an in-service vehicle, and hence establish the time and level of effort required to perform this chore. Also, it was obvious that a mobility evaluation of the same vehicle using the NRMM would provide an estimate of the time required for the analysis of a single vehicle and, at the same time, establish a wheeled vehicle baseline. For these reasons, DLR tasked the Vehicle Mobility Section of the Defence Research Establishment Suffield to perform an NRMM assessment of the Iltis 4X4 ½ ton truck. This document reports on the experience of acquiring vehicle data and on the results of simulation runs.

2.0 NRMM INPUT DATA

This section briefly describes the vehicle and terrain information required by the NATO Reference Mobility Model for mobility performance predictions.

2.1 Vehicle Information

The NRMM requires input data regarding vehicle geometrical, inertial, and mechanical characteristics. Required geometrical data include items such as vehicle wheel base, approach and departure angles, and vehicle bottom profile. Sprung and unsprung masses and

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pitch-mass-moment of inertia are some of the necessary inertial quantities. Suspension characteristics and power train description represent the majority of essential mechanical information.

The work involved in acquiring this large amount of data for the Iltis vehicle was divided as follows:

- 1) the Land Engineering Test Establishment (LETE) was tasked to measure or calculate the more intricate (or difficult to determine) vehicle characteristics; these are listed in Annex A;
- 2) Bombardier, the vehicle manufacturer, was requested to provide suspension and power train information; and
- 3) DRES was left to measure the more easily determined geometrical characteristics.

A package of data sheets was assembled which itemizes all of the vehicle characteristics required to perform NRMM simulation runs for wheeled vehicles (see Annex B).

2.2 Terrain Information

In addition to vehicle characteristics, the NRMM requires much terrain information before providing meaningful predictions of vehicle performance. For NRMM purposes, large areas of complex terrain (transects) are simplified by dividing them into many small areas which are essentially uniform in terms of physical characteristics (see Figure 1). These finite areas of terrain are referred to as terrain units. Terrain units are described by 22 independent terrain charac-

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teristics such as slope, soil type, seasonal soil strengths, ground roughness, and vegetation stem size and spacing. In like fashion, long stretches of road are divided into road segments which are described by nine independent characteristics, some of which are the same as for terrain units (i.e. ground roughness and slope). Examples of other road characteristics are curvature and surface condition. Also specified is the amount of off-road area or on-road distance associated with each homogeneous unit (see Annex C for a list of all terrain and road characteristics). With terrain described in this way, NRMM mobility predictions for large areas of terrain are achieved by providing speed predictions for numerous terrain units and road segments.

Upon initiation of this task, one set of data for on and off-road terrain from the Federal Republic of Germany was available for use. In the interim, new data became available for an area of Canadian terrain located within CFB Petawawa. Mobility predictions are provided for both areas. Annex C provides a summary of the distribution of terrain features for the FRG and CFB Petawawa off-road terrain areas.

3.0 RESULTS AND DISCUSSION

An assessment of the vehicle data acquisition experience and a discussion of NRMM modelling results are reported below.

3.1 Acquisition of Vehicular Data

As noted earlier, LETE was tasked to measure a number of items listed at Annex A. With the exception of pitch-mass-moment of inertia, LETE was able to respond to the task of measuring vehicle characteristics with existing equipment although, in several instances, unfamiliar

procedures were involved. The gross vehicle weight as well as the weight of each axle, when the vehicle is loaded to gross vehicle weight, were easily measured on the LETE weigh scale. The weight of the unsprung mass was determined by disassembling the axles and by summing the entire weight of totally unsprung components (i.e., tires, drums, etc.) and one half of the weight of partially sprung components (i.e., one end fixed to the sprung mass such as springs, shocks, axle, shafts, etc.). The weight of the sprung mass was then easily determined from the difference of the unsprung mass and the gross vehicle weight [2].

The weight supported by the tires at fording depth was determined by suspending the vehicle by a single cable and lowering it into the LETE swim tank to the rated fording depth. The load supported by each tire was subsequently calculated from the cable tension by applying ratios of tire weight to gross vehicle weight (measured while the vehicle is not fording) for each of the four wheel locations (see Annex D).

The centers of gravity for the vehicle at gross vehicle weight, at curb weight, and for the sprung mass were determined in each case by suspending the vehicle in three different fore/aft inclinations. The center of gravity location was then determined by sighting a vertical line from the suspension point down to the vehicle for each inclination. The resulting intersection of lines on the vehicle body located the center of gravity.

The aerodynamic drag coefficient was measured at the National Research Council wind tunnel facility for a range of wind speeds, and an average value was calculated (see Annex E). The hydrodynamic drag coefficient was determined by LETE using a method developed by ORAE.

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The procedure involved rolling the vehicle down a known incline from a predetermined height into a measured depth of water. The hydrodynamic drag coefficient was calculated from the original potential energy and the total distance travelled in the water.

The pitch-mass-moment of inertia was measured by the University of Michigan Transport Research Institute (UMTRI) by the pendulum method, in which the vehicle is suspended by cables and made to oscillate like a simple pendulum. Originally, this measurement was to be made by LETE. However, errors which are often induced by the friction in the pivot joint of all but the most carefully constructed assemblies, compounded by errors in the length of the pivot arm which are further magnified in parallel axis theorem calculations, often result in grossly inaccurate results. A considerable amount of time was spent by LETE engineers investigating alternative means of measuring this quantity. However, after making several attempts to construct jigs to permit proper measurement, it was concluded that these methods were not possible within the time frame and cost constraints of this task.

Consequently, UMTRI was contracted to measure the pitch moment of inertia. The measurement was performed in less than a day after a vehicle was delivered to UMTRI. The vehicle's gross weight for this test was 3050 lb, and the measured moment of inertia was 13240 lb-in-sec². Hence the radius of gyration is 41.0 in or 1.04 m.

However, it should be noted that the value of the pitch-mass-moment of inertia actually measured by UMTRI was for the entire vehicle mass whereas the desired value, to be used in vehicle dynamic simulations, is for the sprung vehicle mass only. Therefore, it was necessary to adjust the value of the pitch-mass-moment of inertia to reflect the deletion of the unsprung mass. This was accomplished by assuming that the above value of radius of gyration was also valid for the

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sprung mass.

Power train and suspension information were received within two calendar months of the date they were requested from the vehicle manufacturer, Bombardier (see Annex F). The information received was readily changed into NRMM compatible form.

Measurement of the required geometrical data took approximately two person-days of effort. The entire complement of required vehicle characteristics is assembled in Annex B in the NRMM Input Data Package.

3.2 NRMM Mobility Predictions

The NRMM quantifies mobility by providing predictions of speed-made-good for a vehicle in road or off-road operation. Speed-made-good between two points is defined as the straight line distance between the points divided by the total travel time, irrespective of the path chosen. A speed-made-good prediction for a terrain unit constitutes the basic output of NRMM. Speed predictions for all of the terrain units of the FRG and CFB Petawawa transects are listed in Annex G.

The baseline performance of the Iltis may be represented by graphs of speed versus cumulative percent of area. Figures 2 and 3 are graphs of speed versus cumulative percent of area for FRG and CFB Petawawa off-road terrain, respectively. These curves provide graphical summaries of the speed predictions for all terrain units of each transect. They give an easy means of obtaining an average predicted speed for any percentage of the total area of a transect. As the cumulative percentage of the total area of the transect increases,

it can be seen that the average achievable speed decreases. For example, in Figure 2 the Iltis is able to achieve a speed-made-good of approximately 22 kilometers per hour over 50 percent of the terrain. However, the speed-made-good value for 100 percent of this terrain decreases to approximately half that value. Such curves also provide a very clear indication of the no-go percent of area; in other words, the percentage of the area of the transect where the vehicle will have no mobility. For example, this value is approximately 75 percent of the total area of the Petawawa transect, Figure 3. Figure 4 is a similar graph for the three types of road surfaces found in the FRG transect.

In situations where the graphic representation is undesirable, the speed corresponding to a specific cumulative percent of area value is an alternative means of representing the baseline performance of a vehicle. The selected percent of area value is generally derived from the mobility level expected of a vehicle fulfilling a specified role. For example, established mobility levels used by the US Army are tactical high mobility, tactical standard mobility, and tactical support mobility. The mobility level dictates the percentage of off-road/on-road terrain on which the vehicle must be mobile (see Table 1). It follows that the speed corresponding to a specified percentage of off-road terrain (extracted from a graph such as Figure 2) is a single number which represents the baseline mobility of the vehicle on that terrain. The average speed corresponding to 80 percent of the cumulative area (V_{80}) of FRG off-road terrain is 20 kilometers per hour. This value represents a predicted average speed in the best (most easily trafficable) 80 percent of the terrain. Results of this form for on-road and off-road terrain (given a tactical standard mobility level as defined in Table 1) for the Iltis are summarized in Table 4.

In the case where, for a given area of terrain, both road and

off-road information are available, another single number called the mobility rating speed may be used to represent the vehicle baseline. The mobility rating speed (V_{MRS}) combines V_x values (where V_x is the average speed corresponding to $x\%$ of the cumulative area) from trails, primary and secondary roads, and off-road terrain into a more global measure of a vehicle's mobility. The mobility rating speed is calculated using

$$V_{MRS} = \frac{100}{\frac{\% \text{ off-road}}{V_x} + \frac{\% \text{ trails}}{V_x} + \frac{\% \text{ secondary roads}}{V_x} + \frac{\% \text{ primary}}{V_x} + TP}$$

where the V_x speeds are taken from applicable speed versus cumulative percent of area curves. The percent off-road, percent trails, etc., weighting factors are defined by the expected mission profile of the vehicle (see Table 2). For the Iltis in a tactical support role, for example, a typical mission profile specifies 5 percent of all distance is travelled off-road, 10 percent on trails, 55 percent on secondary roads, and 30 percent on primary roads.

While negotiating areas of off-road terrain, linear features such as streams, ditches, and roads are often encountered. In order to achieve a comprehensive mobility prediction, which is the aim of the mobility rating speed, some indication of the difficulty that a vehicle experiences when negotiating linear features must be included. The NRMM does not currently have, as a support module, an analytical model to predict retardation of vehicle progress when crossing such features. Therefore, this is accounted for empirically in the above equation by specifying a time penalty, TP.

Several factors influence the value of TP. The frequency of encountering linear features may be quite different from one geographical area to another. Also, the problems of ingress and egress depend, to a large extent, on the soil strength and soil moisture content of the banks or sides of the feature. Therefore, time penalties change for different weather scenarios (soil moisture content) and for different geographical areas as shown in Table 3.

For the example of an Iltis 4X4 in a tactical support role (V_x shown in Table 4) on FRG terrain and assuming a dry weather scenario, the mobility rating speed is calculated to be 40 kilometers per hour.

4.0 CONCLUSIONS

Conclusions regarding the process of obtaining vehicle characteristics are summarized as follows:

- 1) geometrical vehicle data were easily measured in a matter of days,
- 2) power train and suspension information was readily obtained from the vehicle manufacturer,
- 3) the majority of vehicle characteristics requested from LETE were measured with existing equipment using established techniques,
- 4) several unfamiliar (to LETE) characteristics were determined using existing equipment in new ways and by developing novel experimental procedures,

- 5) the pitch-mass-moment of inertia of the sprung mass was the most difficult characteristic to determine. LETE did not have and was not able to construct (within the time and financial constraints of this task) the facilities to accurately measure this value. A value for the pitch-mass-moment of inertia of the entire vehicle mass was obtained by contracting the University of Michigan Transport Research Institute. However, the corresponding value for the sprung vehicle mass is unavailable. An approximated value has been used in this report.

Concerning NRMM mobility predictions, the baseline mobility of a vehicle can be represented in several ways:

- 1) by graphs or tables of average speed versus cumulative percent of area, or
- 2) by mobility rating speeds (V_{MRS}).

The mobility rating speed is the most concise representation of overall performance. A set of graphs of speed versus cumulative percent of area for all surface categories (trails, off-road, etc) contains the most information regarding baseline performance. Both are useful ways of representing the baseline performance. Accordingly, the baseline performance of the Iltis 4X4 is represented by Figures 2 through 4 and by a mobility rating speed for FRG terrain (scenario = dry) of 40 kilometers per hour.

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REFERENCES

1. Haley, P.W., Jurkat, M.P., Brady, P.M. Jr., "NATO Reference Mobility Model, Edition I, User's Guide. Volume I". Technical Report No. 12503. U.S. Army Tank Automotive Research and Development Command. October 1979.
2. Isnor, G., "Iltis Input Data for VEHDYN II". Personal communication. November 1987.
3. Haley, P.W., "Parameters for Mobility Rating Speed Equation". Personal communication. October 1985.

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MOBILITY LEVEL	PERCENTAGE OF TOTAL DISTANCE/AREA CHALLENGED			
	PRIMARY ROADS	SECONDARY ROADS	TRAILS	OFF-ROAD
Tactical High	100	100	100	90
Tactical Standard	100	100	90	80
Tactical Support	100	100	50	50

Table 1

Percentage of Total Distance/Area Challenged for Various Mobility Levels Within Each Surface Type on FRG Terrain

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MOBILITY LEVEL	MISSION PROFILE - PERCENTAGE OF TOTAL DISTANCE/AREA TRAVELED IN EACH SURFACE TYPE			
	PRIMARY ROADS	SECONDARY ROADS	TRAILS	OFF-ROAD
Tactical High	10	30	10	50
Tactical Standard	20	50	15	15
Tactical Support	30	55	10	5

Table 2

Percentage of Total Distance/Area Travelled on Different Surface
Types for Specified Mobility Levels on FRG Terrain

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SOIL CONDITION	TIME PENALTY	
	FRG	MID-EAST
DRY	.101	.025
WET	.109	.032

Table 3

Scenario Dependent Time Penalties for Off-Road Terrain

V_{100} Primary Roads (km/hr)	V_{100} Secondary Roads (km/hr)	V_{80} Trails (km/hr)	V_{80} Off-Road (km/hr)
68	52	15	20

Table 4

Selected Mobility Speeds (V_x) for the Iltis 4X4 Assuming a
Tactical Support Mobility Level on FRG Roads and Off-Road Terrain

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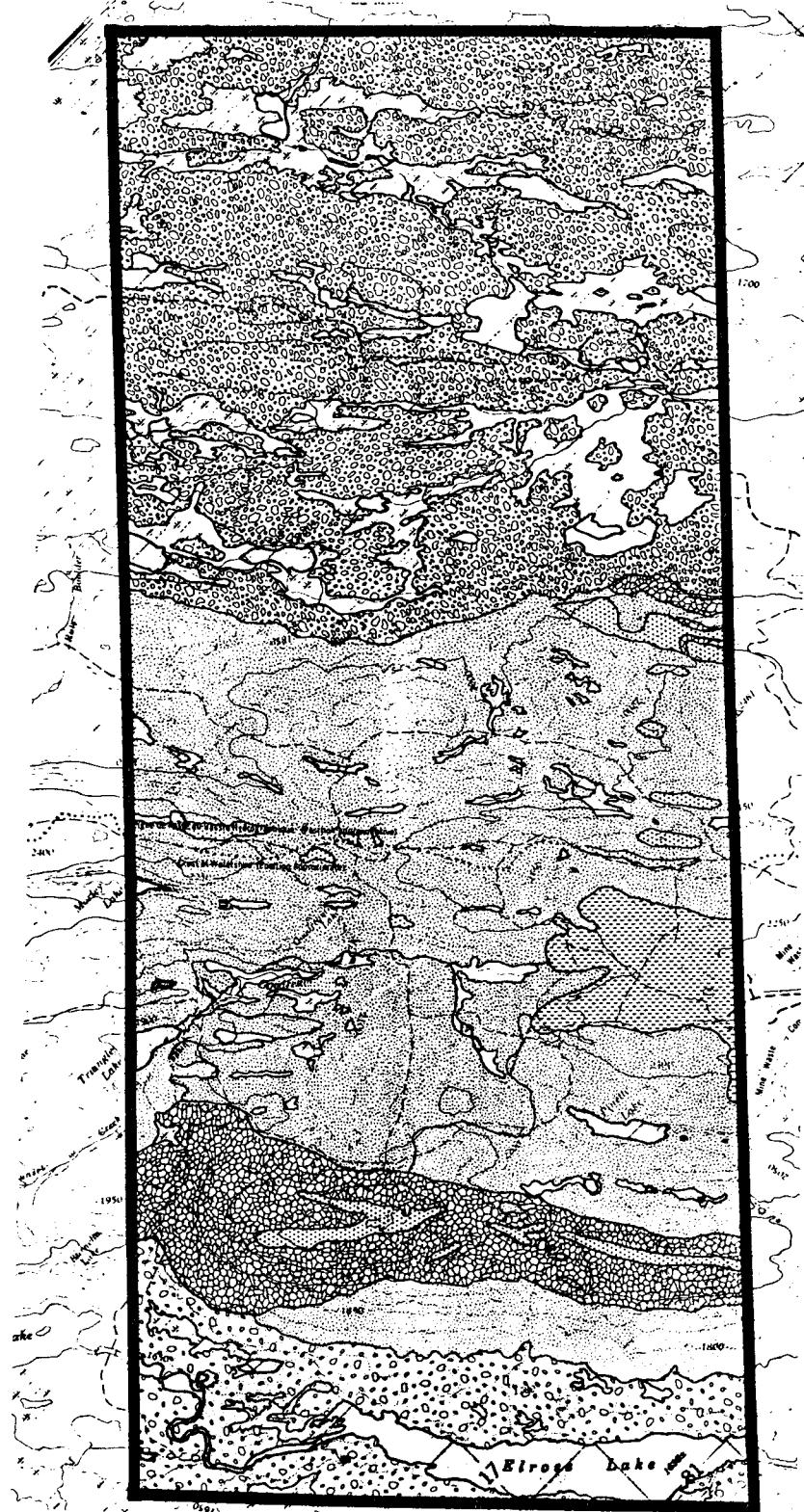


Figure 1. Partial map sheet with terrain unit map superimposed.

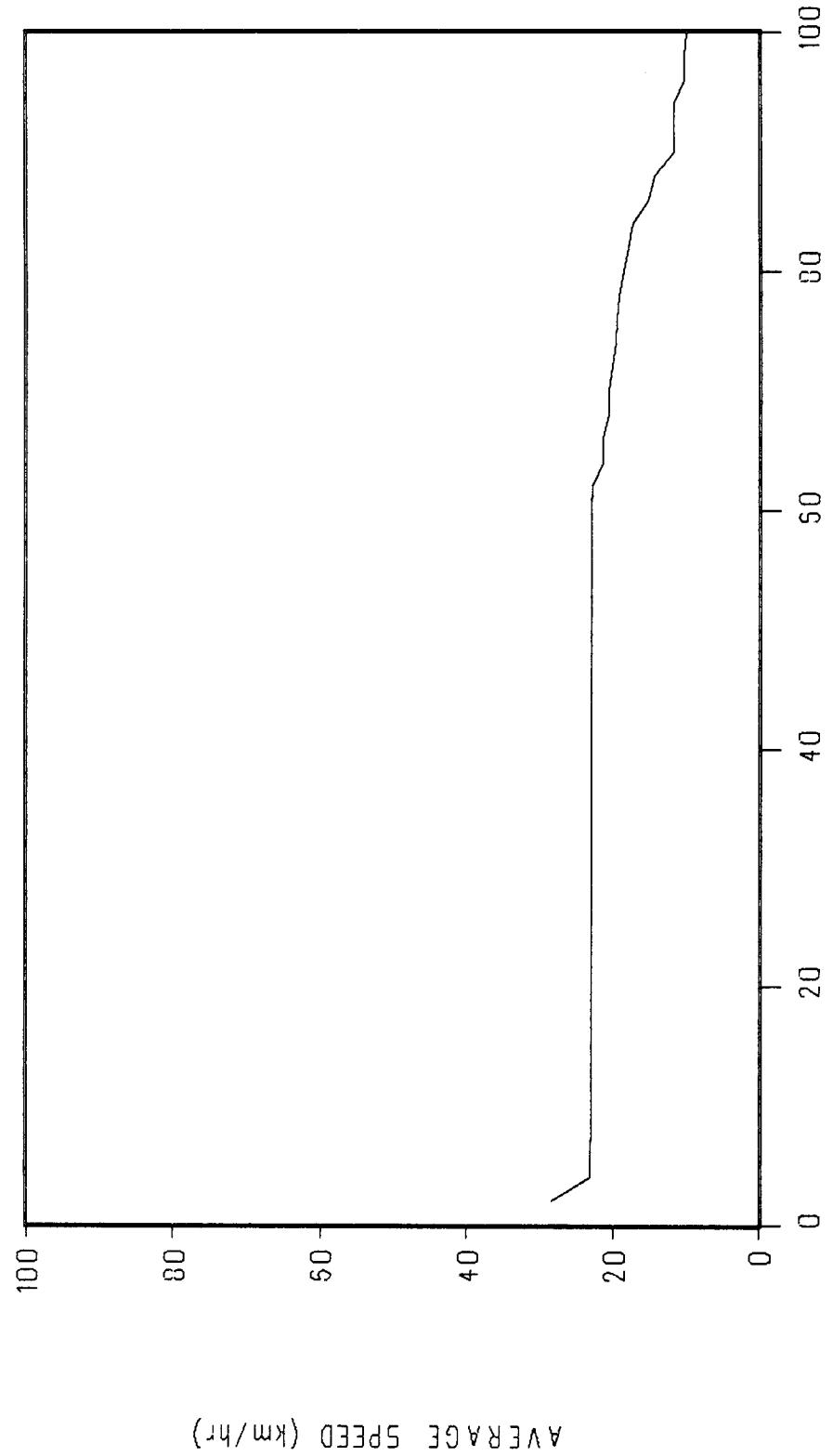


FIGURE 2. GRAPH OF CUMULATIVE AREA VERSUS AVERAGE SPEED FOR THE
ILTIS 4x4 TRUCK ON FRG OFF-ROAD TERRAIN.

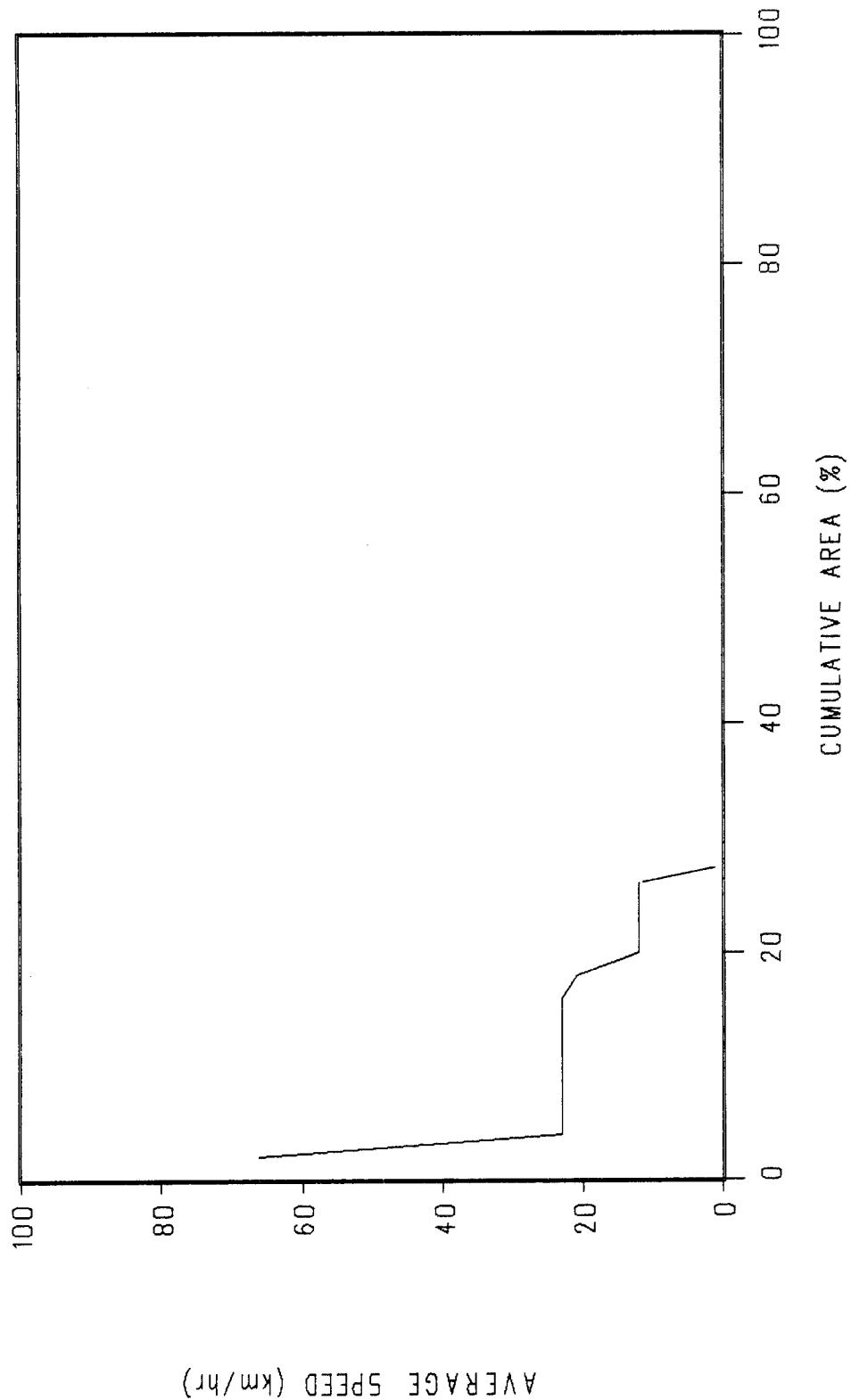


FIGURE 3. GRAPH OF CUMULATIVE AREA VERSUS AVERAGE SPEED FOR THE
TITAN 4x4 TRUCK ON CFB PETAWAWA OFF-ROAD TERRAIN.

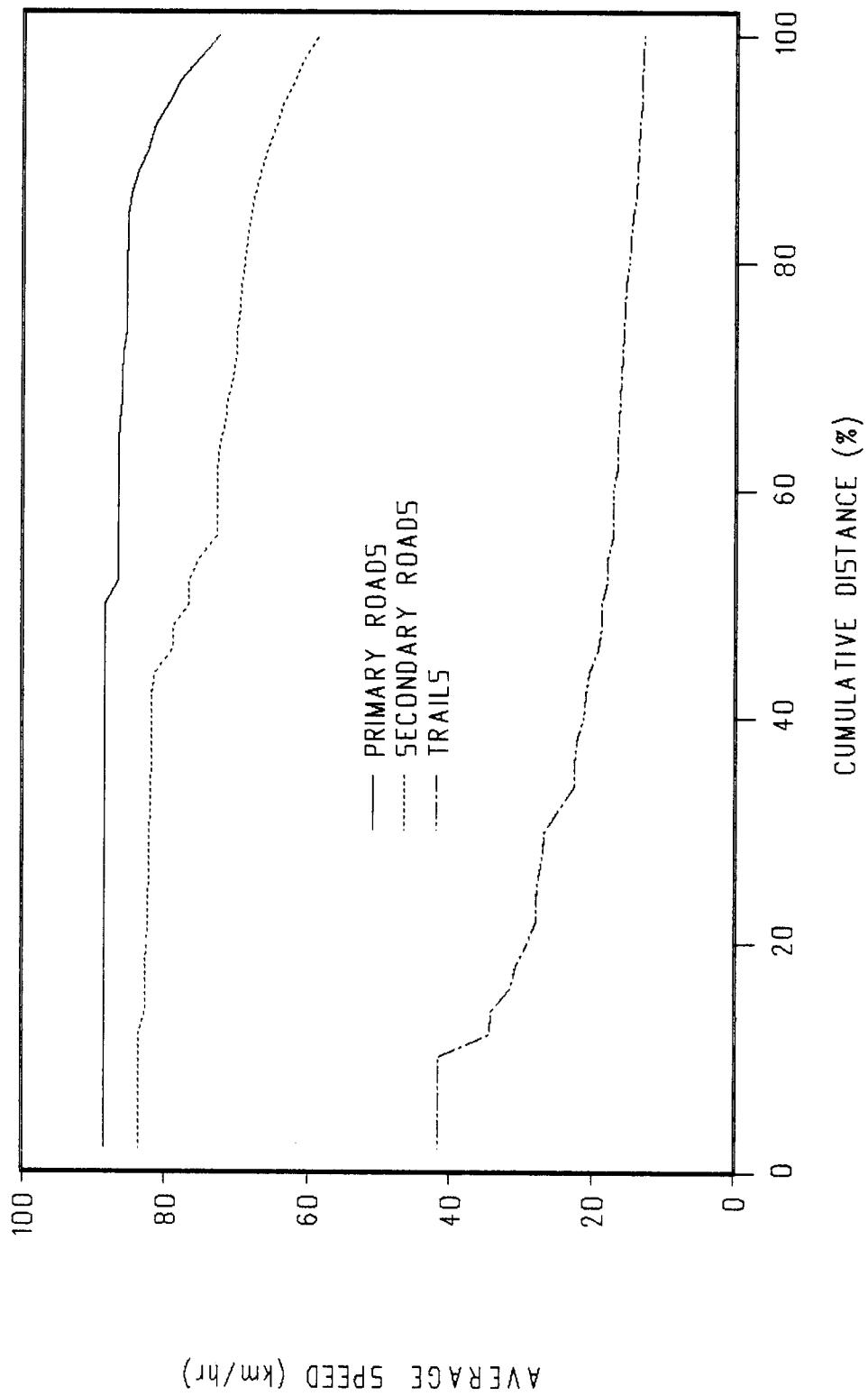


FIGURE 4. GRAPH OF CUMULATIVE DISTANCE VERSUS AVERAGE SPEED FOR THE ILLTIS 4X4 TRUCK ON FRG ROADS AND TRAILS.

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ANNEX A

VEHICLE CHARACTERISTICS REQUESTED FROM LETE

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The following list itemizes all of the Iltis vehicle characteristics which LITE was tasked to provide:

1. Gross vehicle weight.
2. Weight of each axle of vehicle when laden at gross vehicle weight.
3. Weight of sprung mass.
4. Weight of unsprung mass for each axle.
5. Weight supported by tires at fording depth.
6. Center of gravity of vehicle at gross vehicle weight.
7. Center of gravity of vehicle at curb weight.
8. Center of gravity of sprung mass of vehicle.
9. Aerodynamic drag coefficient.
10. Hydrodynamic drag coefficient.
11. Pitch mass moment of inertia of sprung mass.
12. Maximum driver's seat acceleration as the vehicle negotiates obstacles of various sizes (optional).
13. Average absorbed power at driver's seat as the vehicle negotiates random terrain of various roughness values (optional).

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ANNEX B

NRMM INPUT DATA PACKAGE C/W ILTIS VEHICLE CHARACTERISTICS

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NRMM DATA SHEETS FOR WHEELED FIRST UNIT

PROJECT ILTIS

- 1.0 Identification
- 2.0 Geometrical Vehicle Characteristics
 - 2.1 Driver's Seat and CG Dimensions
- 3.0 Bottom Profile
- 4.0 Highway Characteristics and Mobility Assist System
- 5.0 Running Gear
 - 5.1 Running Gear - Tire Characteristics
- 6.0 Suspension Force Characteristics
 - 6.1 Suspension - Spring/Damper Tables
 - 6.2 Suspension - DMC Tables
- 7.0 General Suspension Characteristics and Unsprung Suspension
 - 7.1 Independent and Walking Beam Suspensions
 - 7.2 Walking Beam Suspension
 - 7.3 Bogie Suspension
 - 7.4 Bogie Suspension
- 8.0 Power Train - Description
 - 8.1 Power Train - Engine Characteristics
 - 8.2 Power Train - Transmission Characteristics
 - 8.3 Power Train - Final Drive and Transfer Gears Characteristics
 - 8.4 Power Train - Overall Gear Ratio Combinations
 - 8.5 Power Train - Tractive Effort vs Speed Relation
- 9.0 Speed Limited by Obstacle Impact
 - 9.1 Speed Limited by Roughness
- 10.0 Extras and Doubles

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PROJECT ILTIS
VEHICLE ID

DATE 08/12/86
INITIALS

1.0 - IDENTIFICATION

Vehicle Identification ILTIS 4x4-.5 ton jeep

Gross weight of entire vehicle (kg)

Pitch mass moment of inertia about the CG of vehicle sprung mass (kg - m²)

Payload weight (kg)

Combined weight of the driver and the driver's seat
(Driver = 80 kg, DRWGWT = 0 if no seat suspension exists)

Tires 6.50 R 16 cross country radial tires

Drive Train

Engine VW 049 : 4 cyl 4 stroke gasoline engine

Transmission Manual gear box with integrated differential, dry single plate clutch

GVW	1755
VMMI	11170
DELTW1	348
DRVWGT	0

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B-4

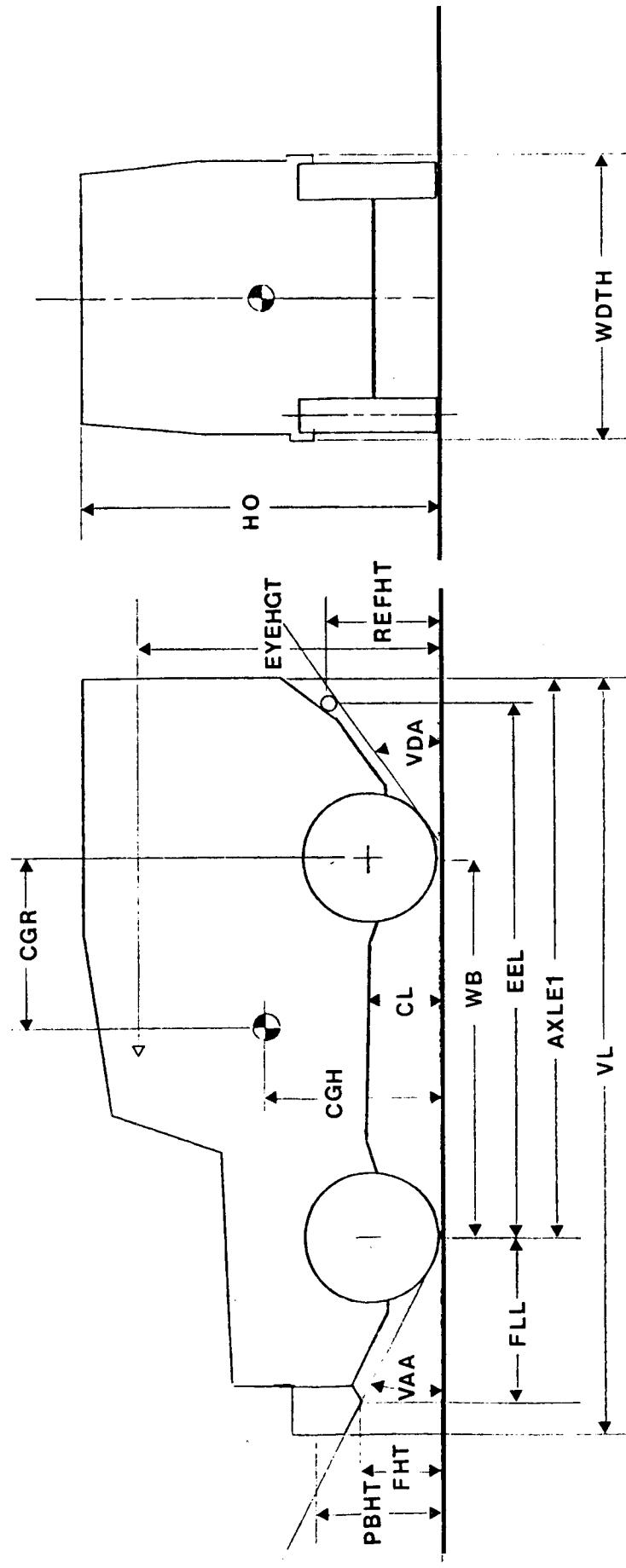
PROJECT ILITIS
 VEHICLE ID

DATE 08/12/86
 INITIALS

2.0 - GEOMETRICAL VEHICLE CHARACTERISTICS

FIRST UNIT	
Vehicle/Unit length (mm)	VL 3955
Vehicle/Unit height (mm)	HO 1836
Vehicle/Unit width (mm)	WDTH 1519
Front pushbar height (mm)	PBHT 800
Height of front hitch above ground (mm)	FHT 541
Height of rear hitch above ground (mm)	REFHT 490
Front axle to end of vehicle (mm)	AXLE1 3066
Front hitch to front axle (mm)	FLL 760
Front axle to rear hitch (mm)	EEL 2771
Wheel base (mm)	WB 2019
Minimum chassis clearance (mm)	CL 330
Approach angle (deg)	VAA 41.5°
Departure angle (deg)	VDA 32.5°
Horizontal coordinate of payload CG with respect to rear hitch (mm)	DEE1 0
Vertical coordinate of payload CG with respect to ground (mm)	ZEE1 0
Minimum width between running gear elements (mm)	WI 1064
Distance from front of first running gear assembly to rear of last (mm)	TL 2756
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PROJECT	ILTIS
VEHICLE ID	

DATE	08/12/86
INITIALS	2.1

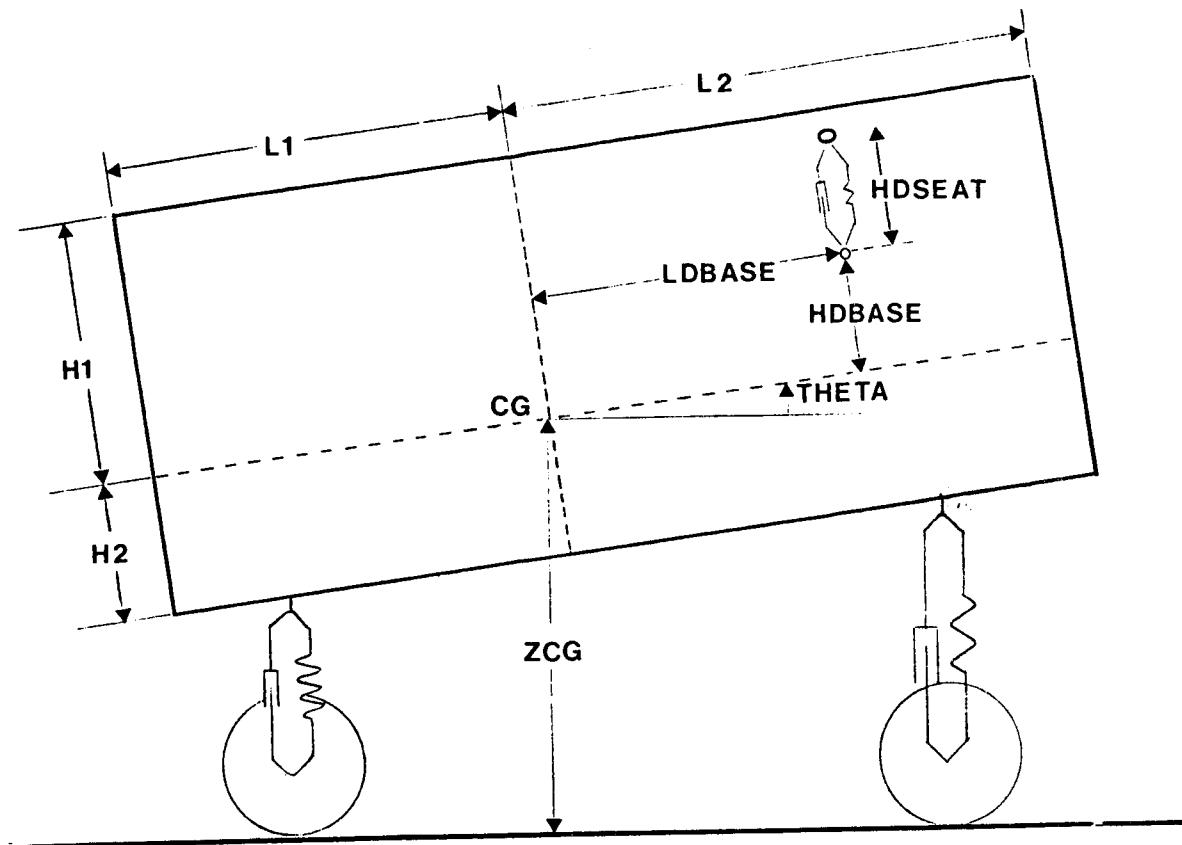
2.1 - DRIVER'S SEAT AND CG DIMENSIONS

FIRST UNIT	
Longitudinal distance from CG to base of driver's seat	LDBASE 186
Vertical distance from CG to the base of driver's seat	HDBASE 143
Vertical distance from the base of the driver's seat to driver's seat	HDSEAT 0
Number of the spring force deflection table to be used for driver's seat dynamics	ISDRV 0
Number of the damper force velocity table to be used for driver's seat dynamics	IDDRV 0
Driver's eye height	EYEHGT 1334
Front axle to driver station	0
Rear axle to CG	CGR 908
Height of CG above ground surface	*CGH 673
Vertical distance from bottom of vehicle's sprung mass to CG	H1 343
Vertical distance from CG to top of vehicle's sprung mass	H2 1164
Longitudinal distance from rear end of vehicle's sprung mass to CG	L1 1916
Longitudinal distance from the CG to the front end of vehicle's sprung mass	L2 2066
Sprung mass' angle with respect to and measured counterclockwise from horizontal	THETA 0
Lateral distance: center plane to CG	CGLAT 0

* CGH corresponds to CGZ1 and ZCG VMS use only

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PROJECT ILTIS
VEHICLE ID _____

DATE 08/12/86
INITIALS 3.0

3.0 - BOTTOM PROFILE

Number of x-y pairs in first unit bottom profile

19

NPTSC1

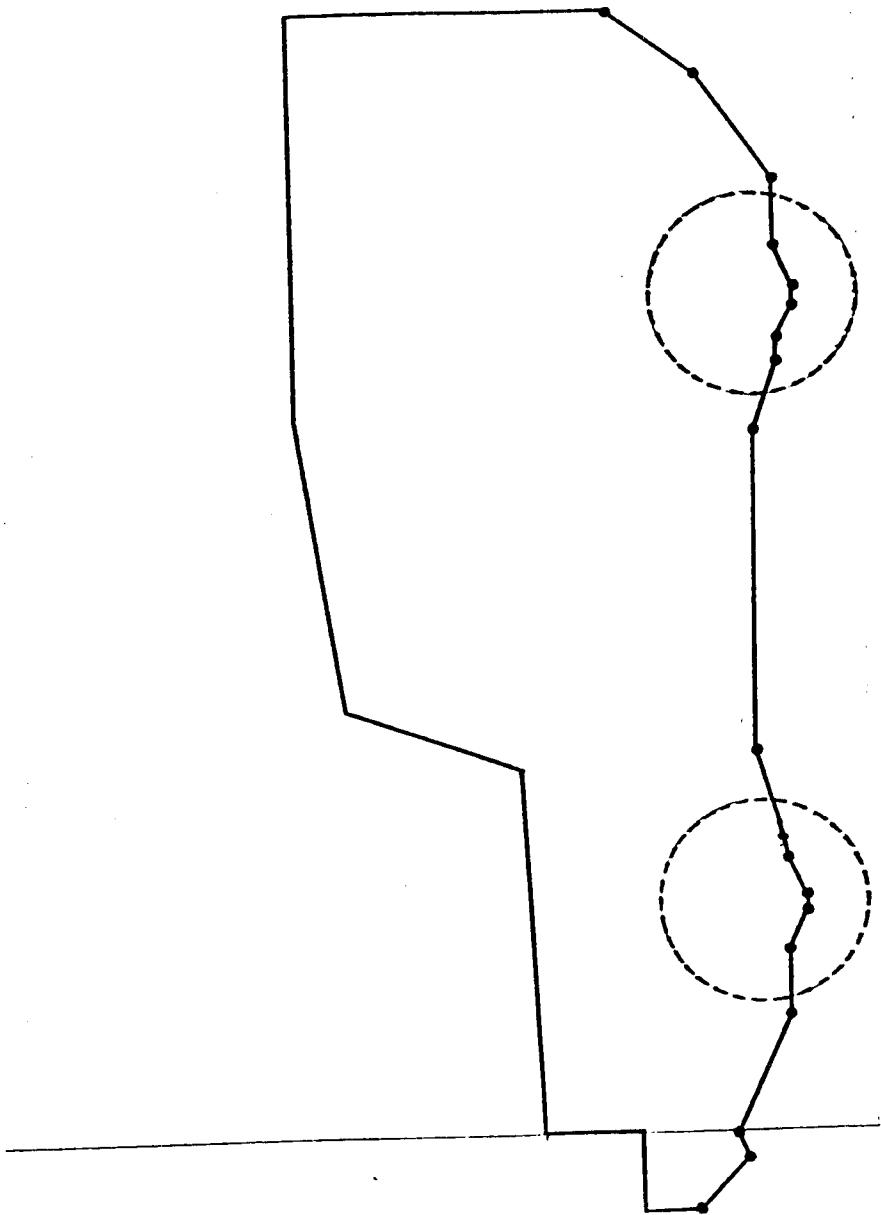
All heights are measured in mm from the ground with vehicle at operating load and cross-country conditions.

FIRST UNIT I = 1, NPTSC1

I	X	Y	X	Y
I	XCLC1 (I)	YCLC1 (I)	I	XCLC1 (I)
1	3725	800	13	783
2	3520	542	14	723
3	3160	270	15	600
4	2923	275	16	383
5	2801	205	17	0
6	2739	205	18	- 92
7	2617	255	19	-257
8	2550	265	20	
9	2320	350	21	
10	1263	360	22	
11	1023	285	23	
12	906	270	24	

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PROJECT ILTIS
VEHICLE ID

DATE 08/12/86
INITIALS

4.0

4.0 - HIGHWAY CHARACTERISTICS

Aerodynamic drag coefficient

0.537

Projected frontal area (m^2)

2.53

Coupling stiffness of tires (N/deg)

534

Hydrodynamic drag coefficient

1.2

- MOBILITY ASSIST SYSTEM

Pushbar/bumper capacity (N)

14200

PBF

Winch mounted? YES

NO

If YES:

Identification/description

Capacity (N)

WC

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4.0

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PROJECT LITIS
VEHICLE ID _____

DATE
INITIALS 08/12/86
5.0

5.0 - RUNNING GEAR
Total number of axles
Total number of suspension assemblies
Maximum braking coefficient

2
2
0.7

Axle number	1	1	2	2	3	3	4
Suspension assembly number							
Operating load on axle (N)	*WGHT(I)	7428	9786				
Steered (1) or unsteered (0) axle		1	0				
Powered (1) or unpowered (0) axle	*IP(I)	1	1	1			
Braked (1) or unbraked (0) axle	*IB(I)	1	1	1			
Number of tires on axle	NWHL(I)	2	2	2			
Singles (0) or duals (1)	ID(I)	0	0				
Chains ? Yes (1) or No (0)	NCHAIN(I)	0	0				
Wheel track (mm)	WT(I)	1230	1260				
Ground clearance under axles (mm)	CLRMIN(I)	250	9.8				
Lateral clearance between inner tires (mm)	WTE(I)	1064	1095				
Undelected radius of the wheel (mm)	*R(I)	370	370				
Weight of the wheel assembly (N)	W(I)	732	732				
Drive wheel (1) or towed wheel (0)	IDRIVE(I)	1	1				

*WGHT(I) corresponds to FUNDWL and EQUILF

*R(I) corresponds to DIAW and EFFRAD

*IP(I) and IB(I) correspond to IIP(I) and IIB(I)

VMS use only

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PROJECT ILTIS
VEHICLE ID _____

DATE 08/12/86
INITIALS 5.1

5.1 - TIRE CHARACTERISTICS

Axle number	I	1	2	3	4
Bias (1) or Radial (0) tires	ICONST(I)	0	0	0	
Tire ply rating or load range	TPLY(I)	10	10		
Undeflected tire section width (mm)	SECTW(I)	165	165		
Undeflected tire section height (mm)	SECTH(I)	140	140		
Tire nominal revolutions/km	REVM(I)	450	450		
Central inflation system (yes/no)	*TPSI(I,3)	500	500		
Tire highway inflation pressure (Kpa)					
Deflection under load and highway inflation (mm)	*DFLCT(I,3)	10	13.5		
Max allowable speed at highway inflation (km/h)					
Tire sand inflation pressure (Kpa)	TPSI(I,2)	315	315		
Deflection under load and sand inflation (mm)	DFLCT(I,2)	13.5	18		
Max allowable speed at sand inflation (km/h)					
Tire cross-country inflation pressure (Kpa)	TPSI(I,1)	390	390		
Deflection under load and cross-country inflation pressure (mm)	DFLCT(I,1)	12	16		
Max allowable speed at cross-country inflation pressure (km/h)					
Rim diameter	RDIAM(I)	406	406		
Rim width	RIMW(I)	114	114		
Rim flange height					
Force at tire deflection for ride analysis					

*TPSI(I,J) and DFLCT(I,J) correspond to ZFORCE(I) and DEFL(I) respectively for VEHdyn. VMS use only

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PROJECT ILTIS
VEHICLE ID

DATE 08/12/86
INITIALS

DATE 6.0

6.0 - SUSPENSION FORCE CHARACTERISTICS

Number of unique Spring Force - Deflection Tables

Number of unique Damper Force - Velocity Tables

<u>1</u>	<u>NSTABL</u>
<u>1</u>	<u>NDTABL</u>

TABLE NUMBER J = 1, NSTABL or J = 1, NDTABL

J = 1 or J = 1

Spring Force
Deflection Table

Damper Force
Velocity Table

<u>9</u>	<u>NSLOAD(J)</u>
<u>0</u>	<u>NSUNLD(J)</u>
<u>0</u>	<u>ATSPOS(J)</u>
<u>0</u>	<u>BTSPOS(J)</u>
<u>0</u>	<u>ATSNEG(J)</u>
<u>0</u>	<u>BTSNEG(J)</u>
<u>0</u>	<u>STKNEG(J)</u>
<u>172</u>	<u>STKPOS(J)</u>

Number of data points in loading portion of the Jth table

Number of data points in unloading portion of the Jth table

Coefficient A1/A3 used for the Jth table

Exponential coefficient B1/B3 used for the Jth table

Coefficient A2/A4 used for Jth table

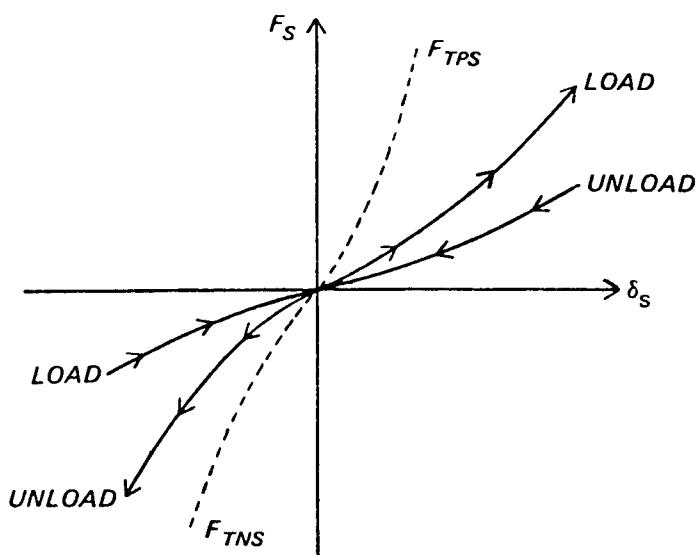
Exponential coefficient B2/B4 used for Jth table

Displacement of rebound bump stop from Jth table (mm)

Displacement of jounce bump stop from Jth table (mm)

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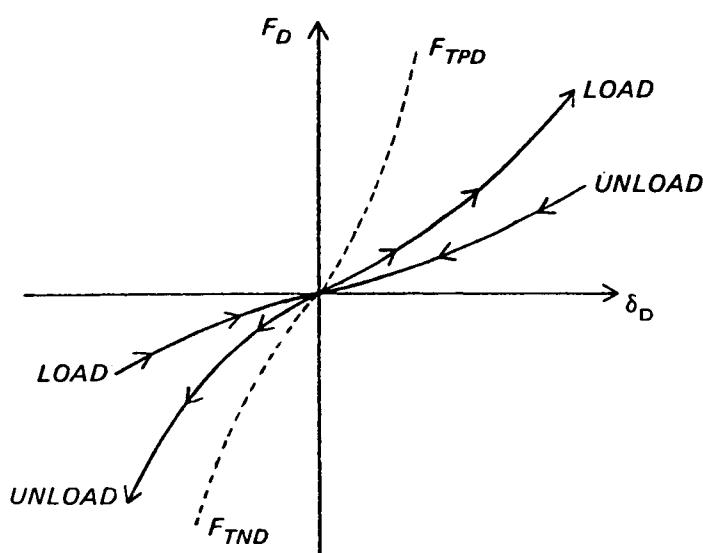


TRANSITION CURVES

$$F_{TPS} = A_1(e^{B_1 \cdot \delta_s} - 1), \delta_s > 0$$

$$F_{TNS} = A_2(1 - e^{-B_2 \cdot \delta_s}), \delta_s < 0$$

NON-LINEAR HYSTERETIC SPRING-FORCE DEFLECTION MODEL



TRANSITION CURVES

$$F_{TPD} = A_3(e^{B_3 \cdot \delta_D} - 1), \dot{\delta}_D > 0$$

$$F_{TND} = A_4(1 - e^{-B_4 \cdot \dot{\delta}_D}), \dot{\delta}_D < 0$$

NON-LINEAR HYSTERETIC DAMPER-FORCE VELOCITY MODEL

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PROJECT
VEHICLE ID
ILTIS

6.1 - SUSPENSION SPRING/DAMPER TABLES

SPRING FORCE - DEFLECTION

 $J = \frac{1}{1}$ $I = 1, \text{ NSLOAD}$

N S L O A D	DEFL. (mm)	FORCE LOAD (N)	FORSLD (I,J)
1	-25	-66700	1
2	0	0	2
3	25	1356	3
4	50	2712	4
5	75	4067	5
6	100	5423	6
7	125	6779	7
8	150	8135	8
9	175	74858	9
10			10
11			11
12			12
13			13
14			14
15			15
16			16

DAMPER FORCE - DEFLECTION

 $J = \frac{1}{1}$ $I = 1, \text{ NSUNLD}$

N S L O A D	DEFL. (mm)	FORCE UNLOAD (N)	FORSUN (I,J)
1	-2.5	-1690	1
2	-.34	-1690	2
3	-.22	-1550	3
4	-.11	-1326	4
5	-.04	-517	5
6	0	0	6
7	.04	219	7
8	.11	517	8
9	.22	687	9
10	.34	802	10
11	2.5	802	11
12			12
13			13
14			14
15			15
16			16

DATE
INITIALS
08/12/86DATE
INITIALS
6.1 $J = \frac{1}{1}$ $I = 1, \text{ NDUNLD}$

N D U N A D	VEL. (m/s)	FORCE LOAD (N)	NDUNLD (I,J)
1			1
2			
3			
4			
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			

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PROJECT ILTIS
 VEHICLE ID

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 INITIALS

6.2 - SUSPENSION DMC TABLES

Number of unique DMC - deflection tables for positive velocities

Number of unique DMC - deflection tables for negative velocities

Number of data points for positive velocities in Jth DMC table

Number of data points for negative velocities in Jth DMC table

DMC - DEFLECTION/POSITIVE VELOCITY J =

I = 1, NDMODP

N D M O D P	DEFL. (mm)	DMC	N D M O D P	DEFL. (mm)	DMC	CFCMDP (I,J)	CFCMDP (I,J)	DMC
1			9					
2			10					
3			11					
4			12					
5			13					
6			14					
7			15					
8			16					

DMC - DEFLECTION/NEGATIVE VELOCITY J =

I = 1, NDMODN

N D M O D N	DEFL. (mm)	DMC	N D M O D N	DEFL. (mm)	DMC
1			9		
2			10		
3			11		
4			12		
5			13		
6			14		
7			15		
8			16		

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PROJECT	ILTIS
VEHICLE ID	_____

DATE	08/12/86
INITIALS	_____

7.0

7.0 - GENERAL SUSPENSION CHARACTERISTICS AND UNSPRUNG SUSPENSION

Number of Unsprung suspensions	NU	0
Number of Independent suspensions	NI	2
Number of Walking Beam suspensions	NW	0
Number of Bogie suspensions	NB	0

Suspension Assembly number

Suspension Assembly number	I	1	2	3	4
Horizontal Coordinate of suspension with respect to hitch (mm)	ELL(I)	2772	753		
Tandem Axle? Yes (1) or No (0).	IT(I)	0	0		
Spacing between 1st and last nonsteered axle in multiple set (mm)	AXLSP(I)	2020	0		

Unsprung Suspension

Unsprung suspension number	I	IU(I)	ZWHL(IU(I))	LWHL(IU(I))
Wheel number				
Height of wheel center above ground (mm)				
Longitudinal length from CG to wheel center (mm)				

* SFLAG(I) to be determined VMS use only
--

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7.1

DATE	<u>08/12/86</u>
INITIALS	

7.1 - INDEPENDENT AND WALKING BEAM SUSPENSION

Independent Suspension

Wheel number

Number of the spring force deflection table to be used

Number of the damper force velocity table to be used

Number of the DMC table for positive velocities to be used

Number of the DMC table for negative velocities to be used INDMTN

Height of wheel center above ground (mm)

Longitudinal length from CG to wheel center (mm)

תְּנִינָה וְעַמְּדָה בְּבֵית הָרֶב מִזְרָחָה

Number of the spring season 2000-2001
marking year suspension number

NUMBER OF THE COMMUNES

Number 264 265 266 267 268 269 270 271 272 273

הנְּצָרָה כְּבָשָׂר וְלִשְׁאַלְמָנָה

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WBRDMP (K) - WBRDMP damping coefficient for resisting rotation

MBPHMN(K) to suspension/frame to beam and line from pivot

Slope of the resisting moment vs. min allowable angle seems

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A blank 4x10 grid for drawing.

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PROJECT ILTIS
VEHICLE ID

7.2 - WALKING BEAM SUSPENSION

Walking Beam (cont'd)

	DATE <u>08/12/86</u>	INITIALS <u>S</u>	7.2
Number of the damper force table to be used with fore outboard damper	IWODTB(1,K)		
Number of the damper force table to be used with aft outboard damper	IWODTB(2,K)		
Number of the DMC table for pos. velocities used with fore outboard damper	IWOMTP(1,K)		
Number of the DMC table for pos. velocities used with aft outboard damper	IWOMTP(2,K)		
Number of the DMC table for neg. velocities used with fore outboard damper	IWOMTN(1,K)		
Number of the DMC table for neg. velocities used with aft outboard damper	IWOMTN(2,K)		
Longitudinal distance from CG to connection point of fore outboard damper to frame	LWDF(1,K)		
Longitudinal distance from CG to connection point of aft outboard damper to frame	LWDF(2,K)		
Longitudinal distance from CG to connection point of fore outboard damper to beam	LWBD(1,K)		
Longitudinal distance from CG to connection point of aft outboard damper to beam	LWBD(2,K)		
Number of the fore wheel	IW(1,K)		
Number of the aft wheel	IW(2,K)		
Height of wheel center above ground (mm)	ZWHL(IW(1,K))		
Longitudinal length from CG to wheel center (mm)	LWHL(IW(1,K))		

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PROJECT	ILTIS
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DATE	08/12/86
INITIALS	_____

7.4 - BOGIE SUSPENSION

Bogie (cont'd)

Number of the DMC table for neg. velocities used with fore outboard damper	IBDMTN(1,J)
Number of the DMC table for neg. velocities used with aft outboard damper	IBDMTN(2,J)
Longitudinal distance from CG to connection point of fore outboard damper to beam	DLB(1,J)
Longitudinal distance from CG to connection point of aft outboard damper to beam	DLB(2,J)
Number of the fore wheel	IBB(1,J)
Number of the aft wheel	IBB(2,J)
Height of wheel center above ground (mm)	ZWHL(IBB(I,J))
Longitudinal length from CG to wheel center (mm)	LWHL(IBB(I,J))
Angular limit of travel front road wheel up	BALMU(I)
Angular limit of travel front road wheel down	BALMD(I)
Bogie swing arm width at suspension (mm)	BWIDTH(I)

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PROJECT ILTIS
VEHICLE ID _____

DATE 08/12/86
INITIALS 8.0

8.0 - POWER TRAIN DESCRIPTION

Data supplied for: tractive force - speed relationship

: power train characteristics

: both

Engine Description: _____

Number of engines

Number of cylinders/engine

Displacement/engine (L)

2-cycle diesel: YES

: NO

Maximum gross horsepower (kW)

Maximum gross torque (Nm)

Maximum net horsepower (kW)

Maximum net torque (Nm)

Torque converter present? YES

NO

If YES: description/identification _____

Lock-up capability? YES

NO

	IAPG = 2
✓	IAPG = 0
	IAPG = 1

	IDIESL = 2
✓	IDIESL = 1

	at RPM
	at RPM
	5000
	2800

	NENG
	NCYL
1.8	CID

1	
4	
1.8	
	IDIESL
55	HPNET
135	QMAX

Sheet 8.1 must be completed. Sheet 8.6 or sheets 8.2, 8.3, 8.4 and 8.5 must also be completed

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PROJECT ILTIS DATE 08/12/86
 VEHICLE ID INITIALS 8.1

8.1 - POWER TRAIN ENGINE CHARACTERISTICS

Number of pairs in engine torque relationship

Engine torque relationship - net as installed

J	RPM (I = 1)	TORQUE (I = 2)	J	RPM (I = 1)	TORQUE (I = 2)
1	1000	100	8	3000	132
2	1400	114	9	3200	130
3	1600	119	10	3400	129
4	2000	126	11	3600	126
5	2400	130	12	3800	123
6	2600	132	13	4000	121
7	2800	133	14	4400	115

ENGINE (I,J) J = 1, IENGIN

19	IENGIN
----	--------

J	RPM (I = 1)	TORQUE (I = 2)	J	RPM (I = 1)	TORQUE (I = 2)
15	4600	112	16	5000	105
17	5400	96	18	5600	92
19	6000	83	20		
21					

Engine to transmission transfer gears present? YES

ITCASE = 1

	✓
--	---

NO

ITCASE = 0

If YES: description/identification

Gear Ratio	: 1 TCASE (1)
Efficiency	% TCASE (2)

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PROJECT ILTIS
VEHICLE ID _____

DATE 08/12/86
INITIALS 8.2

8.2 - POWER TRAIN TRANSMISSION CHARACTERISTICS
AUTOMATIC TRANSMISSION DESCRIPTION

Number of pairs in input RPM vs. speed ratio relationship

Number of pairs in torque ratio vs. speed ratio relationship

Input torque for input RPM vs. speed ratio relationship (Nm)

CONV1 (I,J) Input RPM vs. Speed Ratio J = 1, ICONV1

J	RPM (I = 1)	SPEED RATIO (I = 2)	J	RPM (I = 1)	SPEED RATIO (I = 2)
1		10			
2		11			
3		12			
4		13			
5		14			
6		15			
7		16			
8		17			
9		18			

CONV2 (I,J) Torque Ratio vs. Speed Ratio J = 1, ICONV2

J	TORQUE (I = 1)	SPEED RATIO (I = 2)	J	TORQUE (I = 1)	SPEED RATIO (I = 2)
1				10	
2				11	
3				12	
4				13	
5				14	
6				15	
7				16	
8				17	
9				18	

STANDARD TRANSMISSION DESCRIPTION
Transmission description/identification

Number of gears 5

Gear number	1	2	3	4	5	6	7	8
Ratio	7.603	3.909	2.277	1.458	1.086			
Efficiency %	.95	.9	.9	.9	.9			

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PROJECT ILITIS
 VEHICLE ID _____

DATE 08/12/86
 INITIALS 8.3

8.3 - POWER TRAIN FINAL DRIVE AND TRANSFER GEARS

Transmission to final drive transfer gears present?

YES

NO

IF YES: identification/description _____

Number of gears

Can gears be shifted while in motion? YES

NO

Gear Number	1	2	3	4
Ratio				
Efficiency %				

Final drive description/identification _____

Locking differential? YES

NO

Number of gears

Can gear be shifted while in motion? YES

NO

Gear Number	1	2	3	4
Ratio	5.285			
Efficiency %	.95			

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PROJECT ILLTIS
VEHICLE ID _____

DATE 08/12/86
INITIALS 8.4

8.4 - POWER TRAIN OVERALL GEAR RATIO COMBINATION
Overall Gear Ratio Combinations

Number of gear ratio combinations

TRANS (I,J)

Gear Ratio Combination	J	1	2	3	4	5	6	7	8	9
Combined Gear Ratio (I = 1)		40.18	20.66	12.03	7.71	5.74				
Combined Efficiency % (I = 2)		.9	.9	.9	.9	.9				

Gear Ratio Combination	J	10	11	12	13	14	15	16	17	18
Combined Gear Ratio (I = 1)										
Combined Efficiency % (I = 2)										

Gear Ratio Combination	J	19	20	21	22	23	24	25	26	27
Combined Gear Ratio (I = 1)										
Combined Efficiency % (I = 2)										

Combined final drive ratio

27.94	FD(1)
0.9	FD(2)

Combined final drive efficiency

For final input to NRMN all gear ratio combinations should be assigned to the transmission with only a single final drive and transfer case ratio and efficiency. TRANS (I,J) may be used to show the combined overall gear ratios and efficiencies as input for NRMN.

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PROJECT ILTIS
 VEHICLE ID _____

DATE 08/12/86
 INITIALS 8.5

8.5 - POWER TRAIN TRACTIVE EFFORT VS. SPEED RELATION

Tractive Effort vs. Speed Relationship POWER (I,J)

Number of pairs in tractive effort vs. speed relationship

J	SPEED km/h (I = 1)	FORCE N (I = 2)	GEAR	J	SPEED km/h (I = 1)	FORCE N (I = 2)	GEAR
1				17			
2				18			
3				19			
4				20			
5				21			
6				22			
7				23			
8				24			
9				25			
10				26			
11				27			
12				28			
13				29			
14				30			
15				31			
16				32			

J	SPEED km/h (I = 1)	FORCE N (I = 2)	GEAR	J	SPEED km/h (I = 1)	FORCE N (I = 2)	GEAR
17				33			
18				34			
19				35			
20				36			
21				37			
22				38			
23				39			
24				40			
25				41			
26				42			
27				43			
28				44			
29				45			
30				46			
31				47			
32				48			

Supply at least 4 pairs for each gear - final drive combination

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PROJECT ILTIS
 VEHICLE ID

DATE 08/12/86
 INITIALS

9.0 - SPEED LIMITED BY OBSTACLE IMPACT

Number of height values used in the obstacle height vs. speed table
 Number of obstacle spacing values used in the obstacle spacing vs. speed table
 Uniform obstacle height used in the obstacle spacing vs. speed table

OBSTACLE HEIGHT VS. SPEED

N	Obstacle Height	Maximum Speed			
H	V	A	L	HVALS (I)	VOOB (I)
S	S	A	L	S	S
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					

NHVALS
 NSVALS

OBSTACLE SPACING VS. SPEED

N	Obstacle Spacing	Maximum Speed			
S	V	A	L	SVALS (I)	VOOBS (I)
S	S	A	L	S	S
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					

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9.1

PROJECT ILTIS
VEHICLE ID _____

DATE
08/12/86
INITIALS _____

9.1 - SPEED LIMITED BY ROUGHNESS

Number of RMS entries

Number of tolerance levels

MAXIPR
 MAXL

Number of tolerance levels

Tolerance level number			
	1	2	3
M	RMS (mm)	Speed (km/h)	Speed (km/h)
A			
X			
I			
P	RMS(I)	VRIDE(I,J)	VRIDE(I,2)
R			
1			
2			
3			
4			
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			

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PROJECT VEHICLE ID	ILTIS
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10.0 - EXTRAS AND DOUBLES

CGZ = CGH
ZCG = CGH
NUNITS = 1

NTRKS = 0
NUEH1 = 1
NUEH(I) = 1

DATE INITIALS	08/12/86
DATE	10.0

IFSEAT = 1

Axle Number	I	1	2	2	3	3	4
Load under wheel (N)	FUNDWL(I)	3715	4890				
Deflection of point from force-deflection rel.	DEFL(I)	12	16				
Force of point from force-deflection rel.	ZFORCE(I)	3715	4890				
Undeflected tire diameter (mm)	DIAW(I)	740	740				
Effective radius of tire (mm)	EFFRAD(I)	370	370				

Suspension Assembly Number	I	1	1	2	2	3	3	4
Powered (1) or unpowered (0) axle: wheel 1	IIP (I,1)	1	1					
wheel 2	IIP (I,2)	0	0					
Braked (1) or unbraked (0) axle: wheel 1	IIB (I,1)	1	1					
wheel 2	IIB (I,2)	0	0					
Suspension type: 0 - independent or 1 - bogie	SFLAG (I)	0	0					
Equilibrium load on suspension assembly (N)	EQUILF (I)	3550	3340					

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ANNEX C

SUMMARIES OF TERRAIN FEATURES OF FRG AND CFB PETAWAWA
OFF-ROAD TERRAIN TRANSECTS

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Characteristics of Off-Road Terrain Units

1. terrain unit number
2. soil type (fine grained, coarse grained, CH)
3. soil strength (RCI) - dry season
4. soil strength (RCI) - average season
5. soil strength (RCI) - wet season
6. topographic slope (percent)
7. obstacle approach angle (degrees)
8. obstacle height (inches)
9. obstacle width (inches)
10. obstacle length (feet)
11. obstacle spacing (feet)
12. obstacle spacing type (avoidable or non-avoidable)
13. surface roughness (rms inches)
14. spacing of vegetation in class size 1 (in feet)
15. spacing of vegetation in class size 2 (in feet)
16. spacing of vegetation in class size 3 (in feet)
17. spacing of vegetation in class size 4 (in feet)
18. spacing of vegetation in class size 5 (in feet)
19. spacing of vegetation in class size 6 (in feet)
20. spacing of vegetation in class size 7 (in feet)
21. spacing of vegetation in class size 8 (in feet)
22. recognition distance
23. area of terrain unit (square miles)

Characteristics of Road Segments

1. road segment number
2. road type (super highway, primary road, secondary road, trail)
3. soil type (fine grained, coarse grained, CH)
4. urban code
5. soil strength (RCI) - dry season
6. soil strength (RCI) - average season
7. soil strength (RCI) - wet season
8. soil strength (RCI) - wet, wet season
9. topographic slope (percent)
10. recognition distance (feet)
11. surface roughness (rms inches)
12. AASHO curvature speed limit (miles/hour)
13. length of road segment (miles)

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CFB Petawawa Transect

Number of Units 780 Total Area 459800.000

Type	Title	No. of Units	Surface Area	% of Total Area
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** SOIL TYPE **

Fine-Grained		0	.00	.0
Coarse-Grained		599	401950.00	87.4
Muskeg		181	57850.00	12.6
CH		0	.00	.0

** RMS ROUGHNESS (INCHES) **

1	0.0 - 0.5	269	96225.00	20.9
2	0.6 - 1.5	147	146050.00	31.8
3	1.6 - 2.5	364	217525.00	47.3
4	2.6 - 3.5	0	.00	.0
5	3.6 - 4.5	0	.00	.0
6	4.6 - 5.5	0	.00	.0
7	5.6 - 6.5	0	.00	.0
8	6.6 - 7.5	0	.00	.0
9	> 7.5	0	.00	.0

** SLOPE (PERCENT) **

1	0.0 - 2.0	555	415775.00	90.4
2	2.1 - 5.0	46	13300.00	2.9
3	5.1 - 10.0	50	6925.00	1.5
4	10.1 - 20.0	35	9325.00	2.0
5	20.1 - 40.0	61	10300.00	2.2
6	40.1 - 60.0	30	3825.00	.8
7	60.1 - 70.0	3	350.00	.1
8	> 70.	0	.00	.0

** SOIL STRENGTH (RCI) ** DRY SEASON

1	> 280	75	23950.00	5.2
2	221 - 280	93	24750.00	5.4
3	161 - 220	56	59950.00	13.0
4	101 - 160	1	25.00	.0
5	61 - 100	8	5450.00	1.2
6	41 - 60	192	197775.00	43.0
7	33 - 40	178	90725.00	19.7
8	26 - 32	17	1550.00	.3
9	17 - 25	94	32450.00	7.1
10	11 - 16	66	23175.00	5.0
11	0 - 10	0	.00	.0

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CFB Petawawa Transect

Type	Title	No. of Units	Surface Area	% of Total Area
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** SOIL STRENGTH (RCI) ** AVERAGE SEASON

1	> 280	0	.00	.0
2	221 - 280	75	23950.00	5.2
3	161 - 220	93	24750.00	5.4
4	101 - 160	56	59950.00	13.0
5	61 - 100	1	25.00	.0
6	41 - 60	8	5450.00	1.2
7	33 - 40	192	197775.00	43.0
8	26 - 32	178	90725.00	19.7
9	17 - 25	17	1550.002	.3
10	11 - 16	94	32450.00	7.1
11	0 - 10	66	23175.00	5.0

** SOIL STRENGTH (RCI) ** WET SEASON

1	> 280	0	.00	.0
2	221 - 280	0	.00	.0
3	161 - 220	75	23950.00	5.2
4	101 - 160	93	24750.00	5.4
5	61 - 100	56	59950.00	13.0
6	41 - 60	1	25.00	.0
7	33 - 40	8	5450.00	1.2
8	26 - 32	192	197775.00	43.0
9	17 - 25	178	90725.00	19.7
10	11 - 16	17	1550.00	.3
11	0 - 10	160	55625.00	12.1

** VISIBILITY (FEET) **

1	> 164.0	191	211600.00	46.0
2	79.1 - 164.0	212	43500.00	9.5
3	39.7 - 79.0	164	56100.00	12.2
4	29.9 - 39.8	213	148600.00	32.3
5	20.0 - 29.8	0	.00	.0
6	10.2 - 15.0	0	.00	.0
7	10.2 - 15.0	0	.00	.0
8	5.2 - 10.1	0	.00	.0
9	0.0 - 5.1	0	.00	.0

** OBSTACLE WIDTH (INCHES) **

1	> 47.2	48	30225.00	6.6
2	35.8 - 47.1	0	.00	.0
3	24.0 - 35.7	0	.00	.0
4	12.2 - 23.9	0	.00	.0
5	0.0 - 12.1	732	429575.00	93.4

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CFB Petawawa Transect

<u>Type</u>	<u>Title</u>	<u>No. of Units</u>	<u>Surface Area</u>	<u>% of Total Area</u>
** OBSTACLE SPACING TYPE **				
Avoidable		780	459800.00	100.0
Non-Avoidable		0	.00	.0
** OBSTABLE LENGTH (FEET) **				
1	0.0 - 1.	279	243025.00	52.9
2	1.1 - 3.	0	.00	.0
3	3.4 - 6.	0	.00	.0
4	6.7 - 9.	0	.00	.0
5	10.0 - 19.	501	216775.00	47.1
6	19.8 - 492.	0	.00	.0
7	> 492.0	0	.00	.0
** OBSTACLE SPACING (FEET) **				
1	Bare	279	243025.00	52.9
2	65.9 - 196.9	103	36550.00	7.9
3	36.4 - 65.8	398	180225.00	39.2
4	26.6 - 36.3	0	.00	.0
5	18.4 - 26.5	0	.00	.0
6	13.5 - 18.3	0	.00	.0
7	8.5 - 13.4	0	.00	.0
8	0.0 - 8.4	0	.00	.0
** APPROACH ANGLE **				
1	178.6 - 180.0	780	459800.00	100.0
2	180.0 - 181.5	0	.00	.0
3	175.6 - 178.5	0	.00	.0
4	181.5 - 184.5	0	.00	.0
5	170.1 - 175.5	0	.00	.0
6	184.5 - 190.0	0	.00	.0
7	158.1 - 170.0	0	.00	.0
8	190.1 - 202.0	0	.00	.0
9	149.1 - 158.0	0	.00	.0
10	202.1 - 211.0	0	.00	.0
11	135.1 - 149.0	0	.00	.0
12	211.1 - 225.0	0	.00	.0
13	90.0 - 135.0	0	.00	.0
14	> 225.0	0	.00	.0

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Germany Transect

Number of Units 481 Total Area 100.220

Type	Title	No. of Units	Surface Area	% of Total Area
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** SOIL TYPE **

Fine-Grained		481	100.22	100.0
Coarse-Grained		0	.00	.0
Muskeg		0	.00	.0
CH		0	.00	.0

** RMS ROUGHNESS (INCHES) **

1	0.0 - 0.5	1	.03	.0
2	0.6 - 1.5	335	77.40	77.2
3	1.6 - 2.5	70	16.85	16.8
4	2.6 - 3.5	74	5.94	5.9
5	3.6 - 4.5	0	.00	.0
6	4.6 - 5.5	0	.00	.0
7	5.6 - 6.5	0	.00	.0
8	6.6 - 7.5	1	.00	.0
9	> 7.5	0	.00	.0

** SLOPE (PERCENT) **

1	0.0 - 2.0	11	1.75	1.7
2	2.1 - 5.0	100	28.26	28.2
3	5.1 - 10.0	126	27.89	27.8
4	10.1 - 20.0	116	24.83	24.8
5	20.1 - 40.0	98	13.68	13.7
6	40.1 - 60.0	25	3.64	3.6
7	60.1 - 70.0	5	.17	.2
8	> 70.	0	.00	.0

** SOIL STRENGTH (RCI) ** DRY SEASON

1	> 280	454	96.71	96.5
2	221 - 280	2	.06	.1
3	161 - 220	25	3.45	3.4
4	101 - 160	0	.00	.0
5	61 - 100	0	.00	.0
6	41 - 60	0	.00	.0
7	33 - 40	0	.00	.0
8	26 - 32	0	.00	.0
9	17 - 25	0	.00	.0
10	11 - 16	0	.00	.0
11	0 - 10	0	.00	.0

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Germany Transect

<u>Type</u>	<u>Title</u>	<u>No. of Units</u>	<u>Surface Area</u>	<u>% of Total Area</u>
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** SOIL STRENGTH (RCI) ** AVERAGE SEASON

1	> 280	69	20.79	20.7
2	221 - 280	232	37.20	37.1
3	161 - 220	21	1.08	1.1
4	101 - 160	134	37.70	37.6
5	61 - 100	0	.00	.0
6	41 - 60	25	3.45	3.4
7	33 - 40	0	.00	.0
8	26 - 32	0	.00	.0
9	17 - 25	0	.00	.0
10	11 - 16	0	.00	.0
11	0 - 10	0	.00	.0

** SOIL STRENGTH (RCI) ** WET SEASON

1	> 280	0	.00	.0
2	221 - 280	0	.00	.0
3	161 - 220	0	.00	.0
4	101 - 160	301	57.99	57.9
5	61 - 100	21	1.08	1.1
6	41 - 60	134	37.70	37.6
7	33 - 40	25	3.45	3.4
8	26 - 32	0	.00	.0
9	17 - 25	0	.00	.0
10	11 - 16	0	.00	.0
11	0 - 10	0	.00	.0

** VISIBILITY (FEET) **

1	> 164.0	0	.00	.0
2	79.1 - 164.0	410	75.02	74.9
3	39.7 - 79.0	0	.00	.0
4	29.9 - 39.8	59	24.52	24.5
5	20.0 - 29.8	0	.00	.0
6	15.1 - 19.9	6	.29	.3
7	10.2 - 15.0	6	.39	.4
8	5.2 - 10.1	0	.00	.0
9	0.0 - 5.1	0	.00	.0

** OBSTACLE WIDTH (INCHES) **

1	> 47.2	71	25.69	25.6
2	35.8 - 47.1	2	.06	.1
3	24.0 - 35.7	63	3.91	3.9
4	12.2 - 23.9	146	54.83	54.7
5	0.0 - 12.1	199	15.73	15.7

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Germany Transect

<u>Type</u>	<u>Title</u>	<u>No. of Units</u>	<u>Surface Area</u>	<u>% of Total Area</u>
** OBSTACLE HEIGHT (INCHES) **				
1	0.0 - 5.9	174	16.03	16.0
2	6.0 - 9.8	182	56.15	56.0
3	9.9 - 13.8	97	26.64	26.6
4	13.9 - 14.2	15	.86	.9
5	14.3 - 23.6	4	.14	.1
6	23.7 - 33.5	1	.12	.1
7	> 33.5	8	.28	.3
** OBSTACLE SPACING TYPE **				
Avoidable		364	77.73	77.6
Non-Avoidable		117	22.49	22.4
** OBSTACLE LENGTH (FEET) **				
1	0.0 - 1.	31	4.75	4.7
2	1.1 - 3.	0	.00	.0
3	3.4 - 6.	0	.00	.0
4	6.7 - 9.	0	.00	.0
5	10.0 - 19.	80	26.02	26.0
6	19.8 - 492.	253	46.96	46.9
7	> 492.0	117	22.49	22.4
** OBSTACLE SPACING (FEET) **				
1	Bare	205	37.74	37.7
2	65.9 - 196.9	99	6.26	6.2
3	36.4 - 65.8	9	.42	.4
4	26.6 - 36.3	0	.00	.0
5	18.4 - 26.5	2	.06	.1
6	13.5 - 18.3	0	.00	.0
7	8.5 - 13.4	0	.00	.0
8	0.0 - 8.4	166	55.74	55.6

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Germany Transect

<u>Type</u>	<u>Title</u>	<u>No. of Units</u>	<u>Surface Area</u>	<u>% of Total Area</u>
** APPROACH ANGLE **				
1	178.6 - 180.0	5	.24	.2
2	180.0 - 181.5	0	.00	.0
3	175.6 - 178.5	68	5.75	5.7
4	181.5 - 184.5	0	.00	.0
5	170.1 - 175.5	135	9.31	9.3
6	184.5 - 190.0	0	.00	.0
7	158.1 - 170.0	70	25.13	25.1
8	190.1 - 202.0	0	.00	.0
9	149.1 - 158.0	142	53.92	53.8
10	202.1 - 211.0	0	.00	.0
11	135.1 - 149.0	18	.81	.8
12	211.1 - 225.0	0	.00	.0
13	90.0 - 135.0	3	.11	.1
14	> 225.0	40	4.95	4.9

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ANNEX D

MEASUREMENT OF WEIGHT SUPPORTED BY TIRES AT FORDING DEPTH

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The weight supported by the tires of an Iltis (laden), while fording through water 533 mm in depth, was determined by suspending the vehicle in a sling with a single cable and by performing the following:

1. Weight of Iltis and sling prior to immersion	2140 kg
2. Weight of Iltis and sling when vehicle immersed to fording depth	1492 kg
3. Buoyant force of water (#1 minus #2)	648 kg
4. Weight of Iltis without sling	1755 kg
5. Weight of Iltis when fording (#4 minus #3)	1107 kg
6. Percent of weight supported by front tires	43
7. Fording weight supported by front tires (#5 multiplied by #6)	757 kg
8. Fording weight supported by rear tires (#5 minus #7)	998 kg

Note: Items 7 and 8 assume the weight ratio among the axles is the same for an Iltis when fording as it is when not fording.

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ANNEX E

MEASUREMENTS OF AERODYNAMIC DRAG COEFFICIENT

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The aerodynamic drag coefficient was measured in the 30 foot wind tunnel at the National Research Council in Ottawa, Ontario. Experiments were performed at wind speeds of 30 km/hr to 140 km/hr. The aerodynamic drag coefficients appear in the table below. The variations in drag coefficient at different speeds are believed to have been caused by changes in the shape of the tarpaulin and upward pitching of the vehicle due to aerodynamic lift and drag.

The value of drag coefficient used in simulation runs is
CD = 0.537.

Wind Speed ±.5 km/hr	Aerodynamic Drag Coefficient (CD)
30	0.456
40	0.561
50	0.551
60	0.546
70	0.539
80	0.533
90	0.533
100	0.523
120	0.526
140	0.525

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ANNEX F

SUSPENSION AND POWER TRAIN CHARACTERISTICS RECEIVED FROM BOMBARDIER

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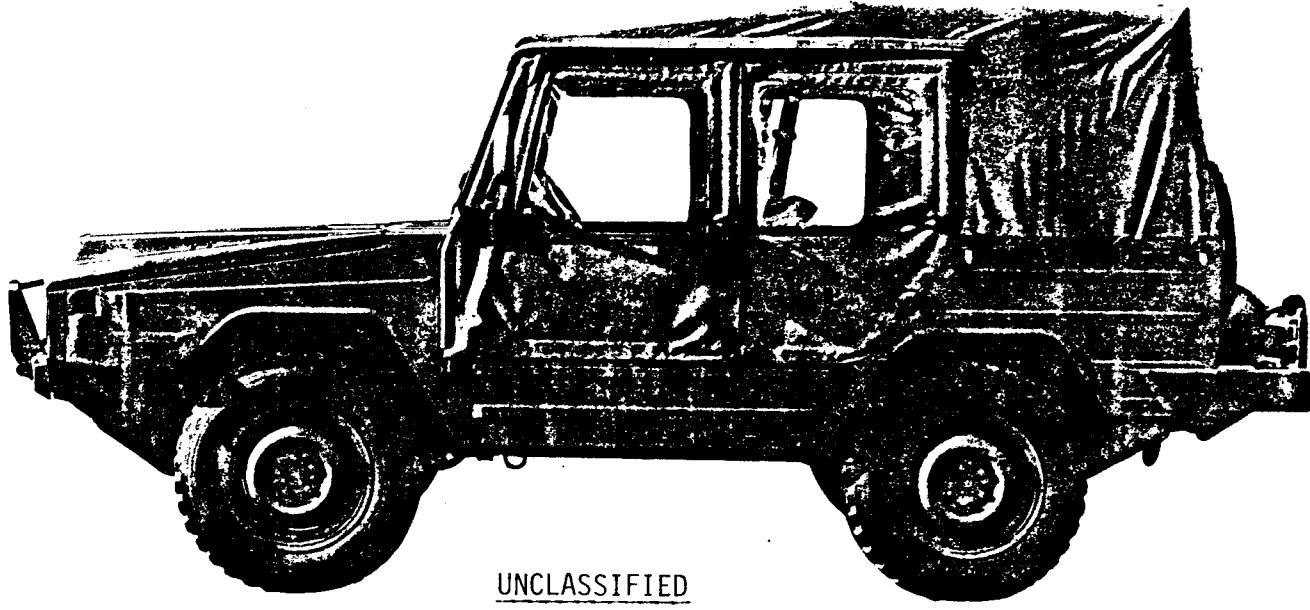
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F-2



Bombardier Iltis*

4x4 - 0.5 ton



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Bombardier Iltis – Technical Data

Engine:	METRIC	IMPERIAL
Model	VW 049	
Type	4 cylinder four stroke gasoline engine	
Displacement	1.7 litre • 1714 cm ³	105 in. ³
Bore and stroke	79.5 x 86.4 mm	3.13 x 3.40 in.
Compression ratio	8.2 : 1	
Fuel	gasoline low octane (regular)	
Fuel capacity	85 litres	18.7 imp. gal.
Horsepower maximum	55 kW @ 5,000 RPM (74 HP)	
Torque: maximum net	135 N·m @ 2800 RPM	100 lbs/ft.
Crankcase capacity	4.0 l w/o filter change 4.5 l w filter change	3.5 imp. qts. 4.0 imp. qts.
Cooling system capacity	7.5 litres	1.6 imp. gal.
Carburetor	Solex 1B1 with thermostarter	
Cooling fan	two thermostatically controlled electric fans: diameter 280 mm	11 in.

Transmission:

Type	manual gearbox with integrated differential, dry single plate clutch
Model	VW 005
Number of speeds: forward	5
reverse	1
Gear ratios:	
1st	3.909
2nd	2.277
3rd	1.458
4th	1.086
reverse	7.318 not synchronized
cross-country gear	7.603 not synchronized
Final drive ratio	37: 7 = 5.286
Lubricant capacity	3.6 litres
	3.2 imp. qts.

Axes and Differentials:

Front:	differential included in transmission
type	single reduction
ratio	5.285
– manually controlled from inside cab	
– differential lock optional - controlled manually from inside cab	
– wheels driven by 2 drive shafts with constant velocity joints	
Rear:	
type	single reduction
ratio	5.285
lubricant capacity	1.2 l w/o differential lock 1.6 l w differential lock
	1.0 imp. qt. 1.4 imp. qt.
– rear differential always in operation	
– differential lock optional - controlled manually from inside cab	
– wheels driven by 2 drive shafts with constant velocity joints	

Frame:

Type	ladder (side rails and crossmembers)
Side members	closed box section
Number of crossmembers	4 transverse bracings 2 spring carriers 1 bolt-on crossmember in front

Electrical system:

Waterproof	yes
Radio suppressed	yes
Voltage	24 V
Alternator rating	55 A
Number of batteries	2

Steering:

Type	rack and pinion (maintenance free)
Ratio	19.44

Brakes:

Type	hydraulic dual circuit diagonally split
Dimensions:	
front	drum 280 mm
rear	drum 280 mm
Total effective area per wheel:	
front	225.2 cm ²
rear	225.2 cm ²
Actuation	hydraulic with vacuum power unit
Parking brake type	mechanical acting on rear wheels

Suspension:

Type (front and rear)	independent wheel suspension on twin control arms
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Springs:

Type (front and rear)	multi-leaf semi-elliptic transversal springs and polyurethane supplementary spring on double action shock absorbers
Size (length x width)	97 cm x 7 cm approx. 38.18 in. x 2.75 in. approx
Number of leaves	4

Rate	73.8 kN/m	422 lbs/in
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Tires:

Size	6.50 R 16
------	-----------

Type	cross-country radial tires
------	----------------------------

	METRIC	IMPERIAL
Exterior		
• overall length	3954 mm	155.7 in.
• overall width w/o mirror	1520 mm	59.8 in.
• overall height - no load	1837 mm	72.3 in.
• wheelbase	2017 mm	79.4 in.
• tires - front/rear track	1230/1260 mm	42.4/49.6 in.
• turning radius	11 m	36.08 ft.
• road area	5.9 m ²	65.5 ft. ²
• ground clearance		
– under frame	330 mm	13 in
– under front axle	250 mm	9.8 in
– under rear axle	250 mm	9.8 in
– under front bumper	588 mm (no load)	23.1 in
– under rear bumper	590 mm (no load)	23.2 in
• fording depth	600 mm	23.6 in
• angle of approach/departure	41.5°/32.5°	
• ramp angle		32°
• rollover lateral resistance		37°
• Shipping dimensions:		
minimum reducible height	1370 mm	53.9 in

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• Shipping cubic at min reducible height	8.2 m ³	288 ft ³
• Shipping cubic at std. dimensions	11 m ³	388 ft. ³

Interior

• front		
– door to door (seat height)	1413 mm	55.6 in.
– door to door (shoulder height)	1450 mm	57.1 in.
• maximum height	1130 mm	44.5 in.
• headroom front/rear	1020/920 mm	40.2/36.2 in.
• seat width front/rear	1413/970 mm	55.6/38.2 in.
• shoulder height width front/rear	1450/1370 mm	57.0/53.9 in.
• seat height front/rear	363/363 mm	14.3/14.3 in.
• length of load area	400 mm	15.8 in.
• length of load area to frontseat backrest	1120 mm	44.1 in.
• width of load area	1370 mm	53.9 in.
• load area		
– rear seats up	0.55 m ²	5.9 ft ²
– rear seats folded	1.33 m ²	14.3 ft ²

Weights:

Unladen weight	1550 kg (depending on equipment)	3417 lbs
Payload	500 kg	1102 lbs
Total weight	2050 kg	4519 lbs
Permissible axle load:		
front	1000 kg	2200 lbs
rear	1250 kg	2756 lbs
Permissible trailer load:		
braked	2000 kg	4400 lbs
unbraked	750 kg	1653 lbs
Tongue weight (trailer)	75 kg	165 lbs

Performance:

Top speed	130 km/h	80 mi./h
Minimum speed	4 km/h	2.5 mi./h
Cruising range	700 km	435 mi.
Fuel consumption		
– in town cycle	14.6 l/100 km	19.3 mi./imp. gal.
– at constant 90 km/h	10.5 l/100 km	26.9 mi./imp. gal.
– at constant 120 km/h	15.0 l/100 km	18.8 mi./imp. gal.

Climbing ability fully laden:

1st gear	32.0%
2nd gear	16.8%
3rd gear	9.2%
4th gear	5.3%
Reverse gear	72.5%
Cross-country gear	77.0%

Climbing ability fully laden

(total vehicle weight) and 750 kg trailer weight:

1st gear	22%
Cross-country gear	48%

Climbing ability fully laden
and 2000 kg trailer weight:

1st gear	15%
Cross-country gear	32%

TOOLS and PUBLICATIONS

Each vehicle is equipped with one of each of the following items:

TOOLS

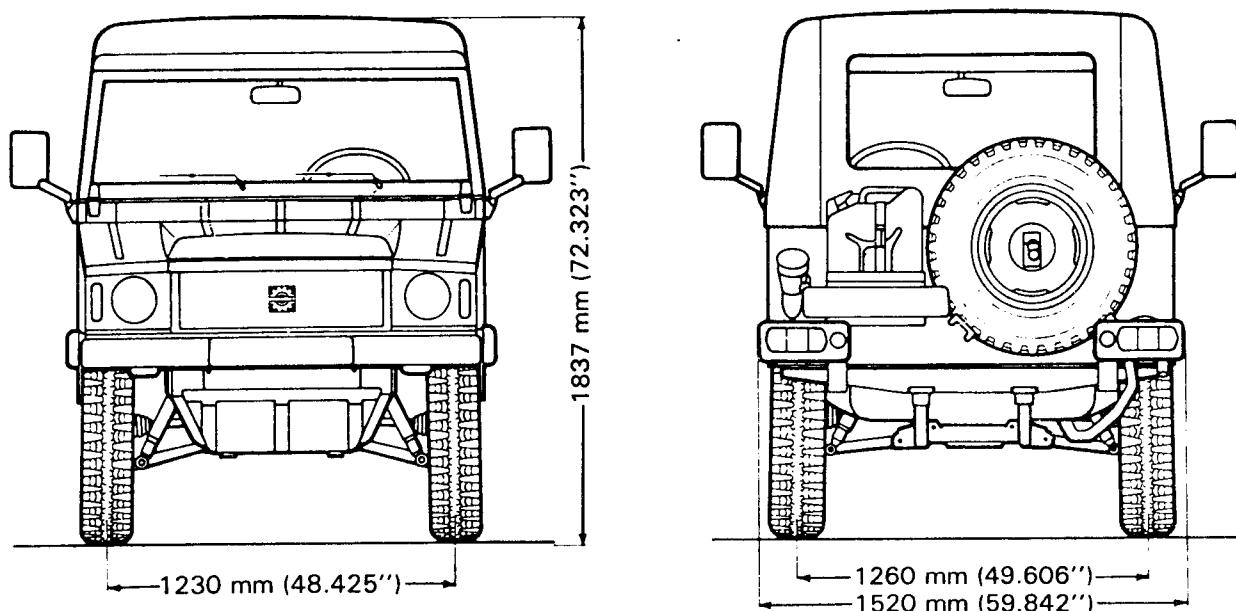
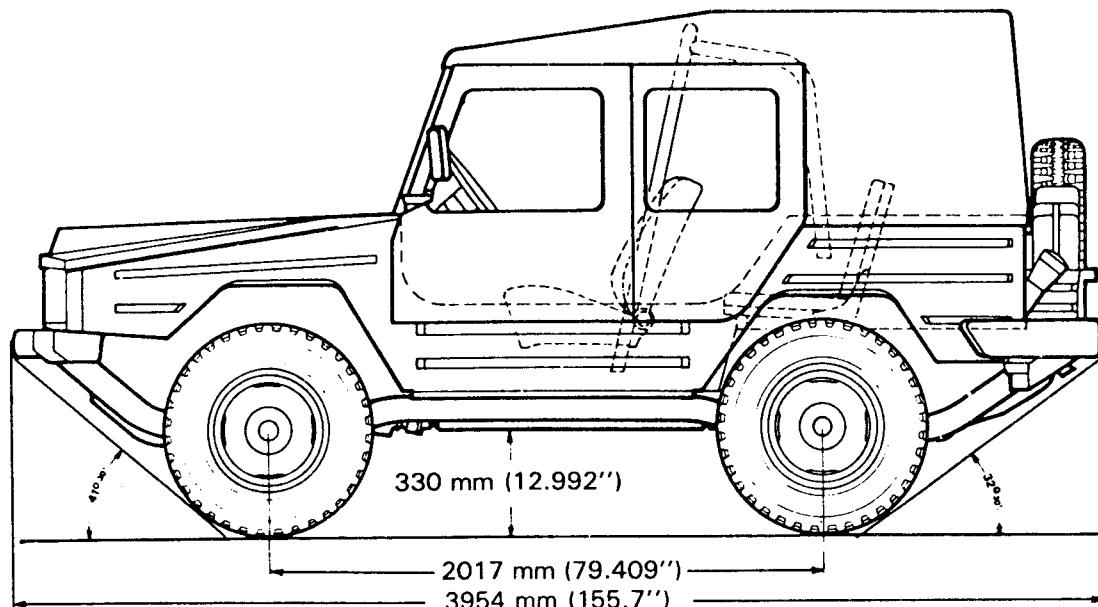
- Pliers slip joint
- Screwdriver flat tip
- Screwdriver Phillips #2
- Wrench drain plug for transmission and differential
- Wheel socket
- Bar wheel socket
- Guide pin wheel changing
- Tool bag
- Jack support
- Jack

PUBLICATIONS

- Operator's Manual
- Lubrication Chart

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BOMBARDIER ILTIS - DIMENSIONS



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SAMPLE COMPUTATION

SUSPENSION DATA - ILTIS

A. Springs

Reference : Drawing no.B183 411 103

On the diagram, the constant for fixed spring is : C=79.0 N/mm

Constant: $1 \text{ lb}_f = 4.448 \text{ N}$

$1 \text{ in} = 25.4 \text{ mm}$

Hence : $C = 451.1 \text{ lb}_f/\text{in}$

Remark: - $F = 0 \text{ N}$ is rest position ($+112 \text{ mm}$ displacement)

- $F = 3200 \text{ N}$ (719 lb_f) is the estimated weight on a front wheel *

- $F = 7600 \text{ N}$ (1709 lb_f) is the estimated weight on a rear wheel *

- The value of "C" is the same for front & rear, loaded or unloaded.

* based on a hypothetical distribution of the total weight for a German Iltis.

B. Shock Absorbers

Reference : Drawing No TAB 010 125

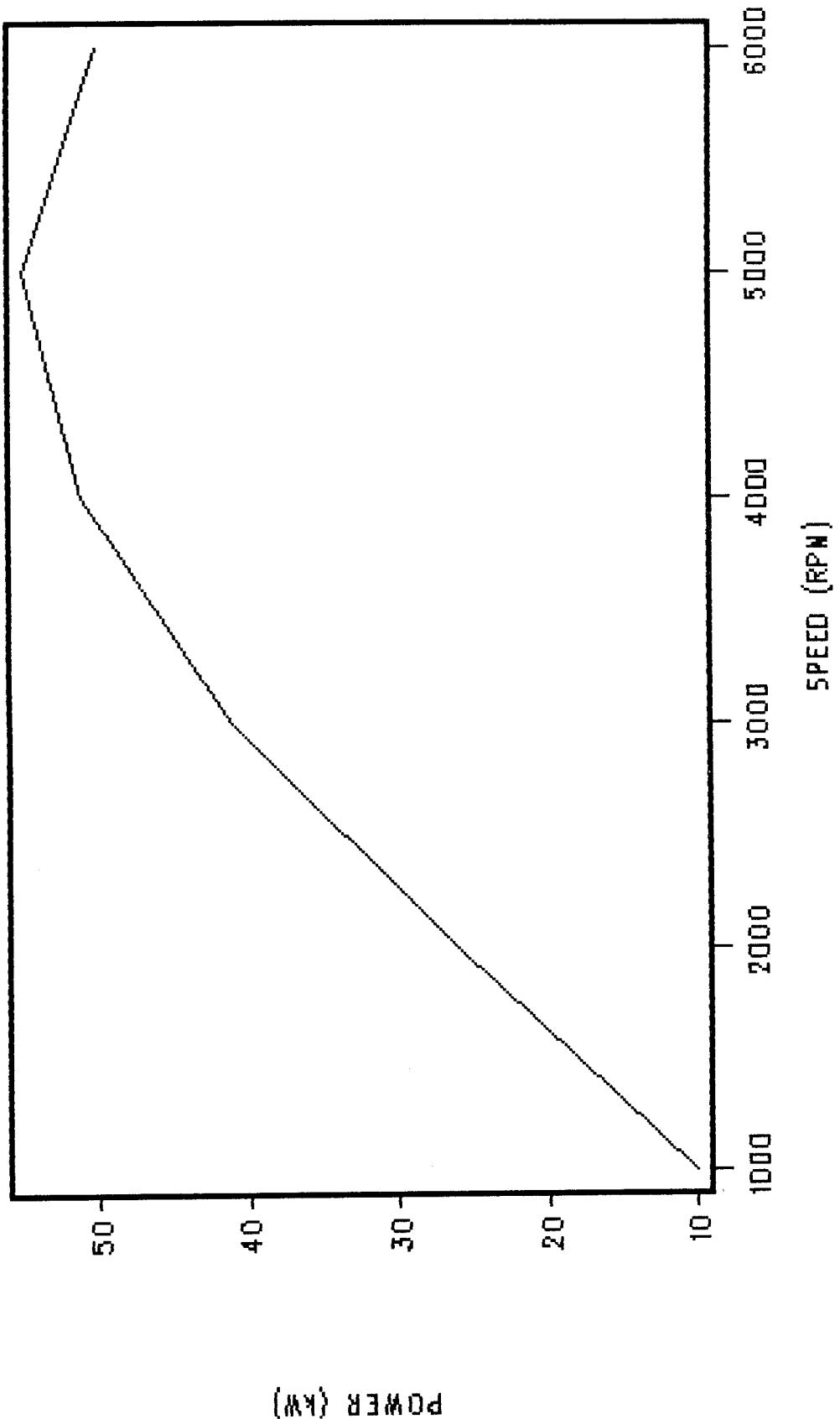
For shock absorber part no. B183 413 031 0Z

Conversion : Deflection rate (in/sec) where 1 cycle = 2 strokes

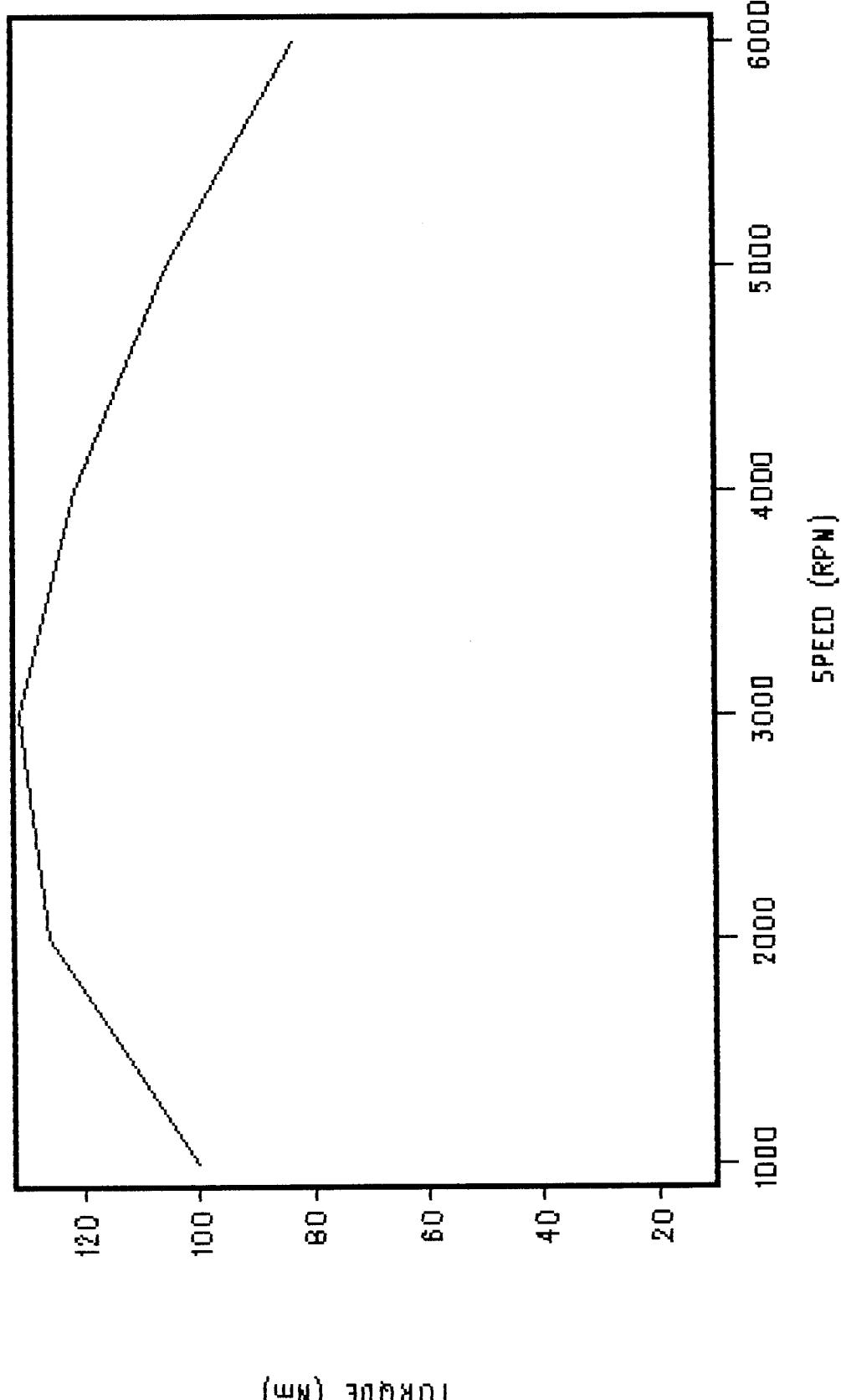
Then : $\frac{2 \times \text{stroke} (\text{mm}) \times 100 \text{ CPM} \times \frac{1 \text{ in}}{25.4 \text{ mm}} \times \frac{1 \text{ min}}{60 \text{ sec}}}{\text{Deflection rate}} = \frac{\text{in}}{\text{sec}}$

Interpretation: - Pull step = force unloading

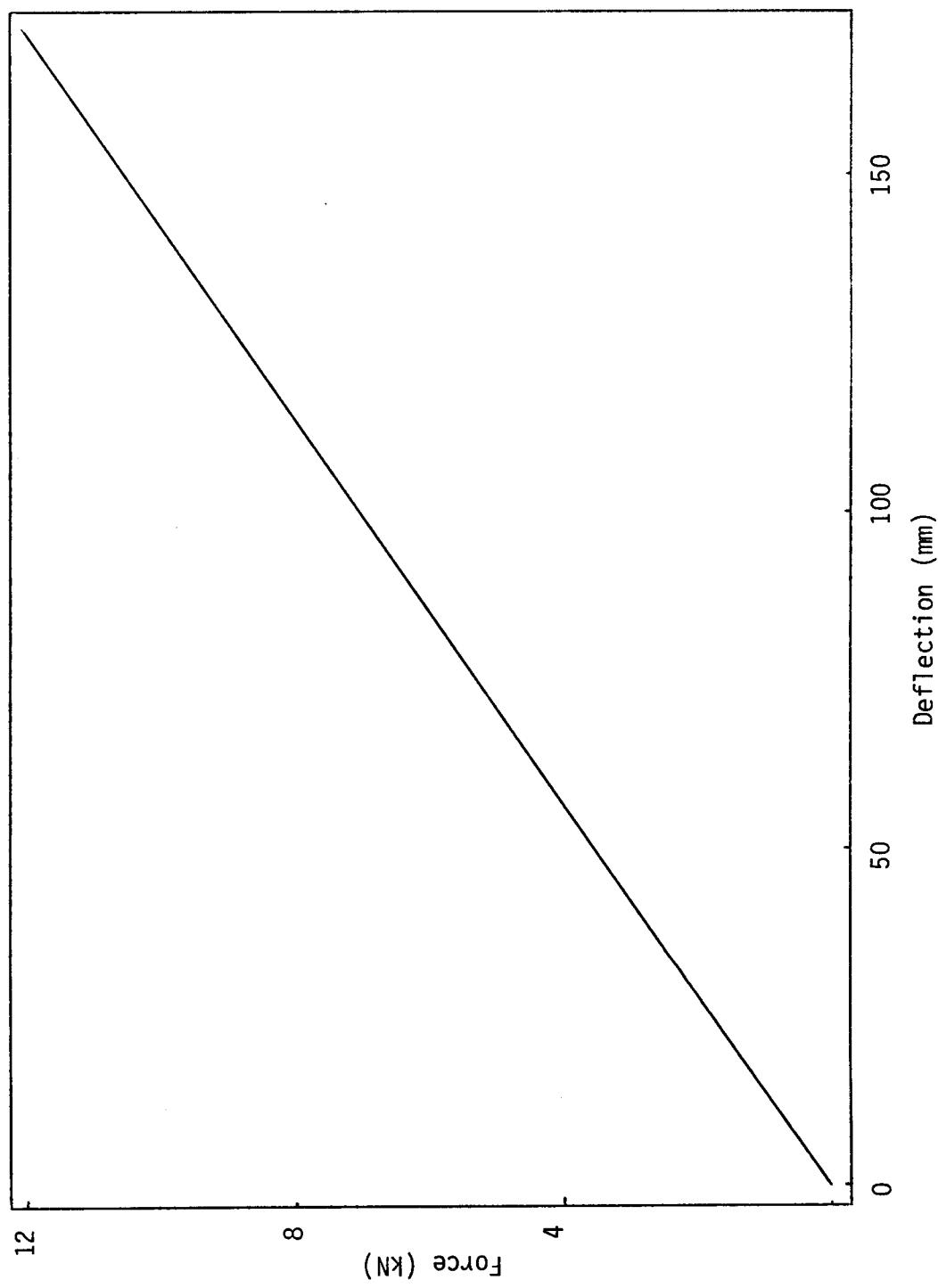
- Compression step = force loading



Power versus speed curve for VW - Iltis engine (displacement = 1.7l)



Torque versus speed curve for VW - Iltis engine (displacement = 1.78)



Force - deflection curve for Iltis leaf spring

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	Stroke (mm)	10	25	50	75
SHOCK ABSORBER IDENTIFICATION NUMBER	C.P.M. (min ⁻¹)	100	100	100	100
B183 400 021	extension force (N)	850	2180 ±200	2550 ±220	2780 ±250
	compression force (N)	360	850 ±110	1130 ±110	1320 ±140

Notes: 1. Damping tested at 20° ±2°C
2. Hydraulic stop, 3800 ±400N

Extension and compression forces for Iltis shock absorber when cycled
using various stroke lengths

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ANNEX G

NRMM TERRAIN UNIT SPEED PREDICTIONS

UNCLASSIFIED

The basic output of the NATO Reference Mobility Model for areal terrain units consists of the following (as it appears on the next 11 pages of this Annex):

- 1) Terrain unit number, NTU
- 2) Terrain type, ITUT
 - 1 - normally dry patch
 - 2 - marsh or other water covered patch
 - 11 - superhighway
 - 12 - primary road
 - 13 - secondary road
 - 14 - trail
- 3) The omnidirectional speed-made-good attainable by the vehicle in the terrain unit, VMAX (this is a harmonic average of 4, 5, and 6 below)
- 4) The attainable speed-made-good going with the topographic slope (up grade)
- 5) The attainable speed-made-good on the level across the grade)
- 6) The attainable speed-made-good going against the topographic slope (down grade)
- 7) The selected omnidirectional speed-made-good which considers both the vehicle capabilities and human factors, VSEL
- 8) The selected speed-made-good up grade
- 9) The selected speed-made-good across the grade
- 10) The selected speed-made-good down grade
- 11) Grade (topographic slope)
- 12) Area of the terrain unit.

Columns 13 through 20 present the same information given in columns 3 through 10 but in units of kilometers per hour rather than miles per hour. Column 21 is identical to column 1. It is repeated for ease of reading values in the table.

Note that the predicted speeds presented in columns 4, 5, and 6 as well as those in columns 8, 9, and 10 will be different only if slope is the speed limiting factor. Note also that the speed prediction listed as applying to operation on the level actually refers to operation across the slope. In other words, the vehicle is assumed to be operating on a side slope but not climbing or descending a grade.

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1	NTU	ITUT	VMAX	UP LEVEL	DOWN VSEL	UP LEVEL	DOWN VSEL	GRADE	AREA	VMAX	UP LEVEL	DOWN VSEL	UP LEVEL	DOWN VSEL	KM./HR.	LEVEL	DOWN NTU
4	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	.0100	23-01	23-01	.00	.00	4	.00
5	1	8-43	8-43	.00	.00	8-43	8-43	.00	.00	3-50	.0700	13-57	13-57	.00	.00	5	.00
10	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	.3300	23-01	23-01	.00	.00	10	.00
14	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	.9600	23-01	23-01	.00	.00	14	.00
19	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	.1100	23-01	23-01	.00	.00	19	.00
20	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	.0700	23-01	23-01	.00	.00	20	.00
23	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	.0100	23-01	23-01	.00	.00	23	.00
24	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	1.7300	23-01	23-01	.00	.00	24	.00
25	1	8-43	8-43	.00	.00	8-43	8-43	.00	.00	3-50	.1500	13-57	13-57	.00	.00	25	.00
26	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	3-50	.1200	23-01	23-01	.00	.00	26	.00
27	1	2-05	2-05	.00	.00	2-05	2-05	.00	.00	3-50	.0100	3-30	3-30	.00	.00	27	.00
32	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	7-50	.3400	11-99	11-99	.00	.00	32	.00
33	1	8-43	8-43	.00	.00	8-43	8-43	.00	.00	7-50	.0200	13-57	13-57	.00	.00	33	.00
37	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.1800	23-01	23-01	.00	.00	37	.00
38	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	7-50	.0900	11-99	11-99	.00	.00	38	.00
41	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.0000	23-01	23-01	.00	.00	41	.00
42	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.3600	23-01	23-01	.00	.00	42	.00
45	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.2200	23-01	23-01	.00	.00	45	.00
48	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	7-50	.0800	11-99	11-99	.00	.00	48	.00
52	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.1200	23-01	23-01	.00	.00	52	.00
53	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.2-4500	23-01	23-01	.00	.00	53	.00
55	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.6300	23-01	23-01	.00	.00	55	.00
58	1	2-05	2-05	.00	.00	2-05	2-05	.00	.00	7-50	.2200	3-30	3-30	.00	.00	58	.00
62	1	*00	*00	.00	.00	*00	*00	.00	.00	7-50	.0500	23-01	23-01	.00	.00	62	.00
63	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	7-50	.2500	23-01	23-01	.00	.00	63	.00
66	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	15-00	.2400	7-45	7-45	.00	.00	66	.00
71	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	15-00	.0800	7-45	7-45	.00	.00	71	.00
72	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	15-00	.1600	7-45	7-45	.00	.00	72	.00
75	1	14-30	14-30	.00	.00	14-30	14-30	.00	.00	15-00	.0500	23-01	23-01	.00	.00	75	.00
83	1	8-43	8-43	.00	.00	8-43	8-43	.00	.00	15-00	.0200	13-57	13-57	.00	.00	83	.00
86	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	15-00	.0900	11-99	11-99	.00	.00	86	.00
93	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	15-00	.0500	11-99	11-99	.00	.00	93	.00
98	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	15-00	.3-6700	11-99	11-99	.00	.00	98	.00
100	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	15-00	.1000	11-99	11-99	.00	.00	100	.00
103	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	15-00	.0200	7-45	7-45	.00	.00	103	.00
104	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	15-00	.7400	7-45	7-45	.00	.00	104	.00
113	1	3-51	3-51	.00	.00	3-51	3-51	.00	.00	15-00	.2800	5-65	5-65	.00	.00	113	.00
116	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	15-00	.0100	11-99	11-99	.00	.00	116	.00
117	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	30-00	.0400	7-45	7-45	.00	.00	117	.00
118	1	7-45	7-45	.00	.00	7-45	7-45	.00	.00	30-00	.0300	11-99	11-99	.00	.00	118	.00
126	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	30-00	-1000	7-45	7-45	.00	.00	126	.00
127	1	4-63	4-63	.00	.00	4-63	4-63	.00	.00	30-00	.1600	7-45	7-45	.00	.00	127	.00

1021	1	14-30	14-30	.00	.00	1021	.00	.00
1028	1	14-30	14-30	-00	-00	1028	.00	.00
1029	1	14-30	14-30	-00	-00	1029	.00	.00
1032	1	14-30	14-30	-00	-00	1032	.00	.00
1033	1	14-30	14-30	-00	-00	1033	.00	.00
1034	1	14-30	14-30	-00	-00	1034	.00	.00
1042	1	14-30	14-30	-00	-00	1042	.00	.00
1044	1	14-30	14-30	-00	-00	1044	.00	.00
1046	1	14-30	14-30	-00	-00	1046	.00	.00
1047	1	14-30	14-30	-00	-00	1047	.00	.00
1049	1	14-30	14-30	-00	-00	1049	.00	.00
1051	1	14-30	14-30	-00	-00	1051	.00	.00
1052	1	14-30	14-30	-00	-00	1052	.00	.00
1053	1	9-62	9-62	-00	-00	1053	.00	.00
1054	1	9-62	9-62	-00	-00	1054	.00	.00
1056	1	2-05	2-05	-00	-00	1056	.00	.00
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1058	1	2-05	2-05	-00	-00	1058	.00	.00
1061	1	2-05	2-05	-00	-00	1061	.00	.00
1063	1	14-30	14-30	-00	-00	1063	.00	.00
1065	1	00	00	-00	-00	1065	.00	.00
1066	1	3-80	3-80	-00	-00	1066	.00	.00
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1071	1	14-30	14-30	-00	-00	1071	.00	.00
1078	1	14-30	14-30	-00	-00	1078	.00	.00
1079	1	9-94	9-94	-00	-00	1079	.00	.00
1081	1	14-30	14-30	-00	-00	1081	.00	.00
1082	1	7-45	7-45	-00	-00	1082	.00	.00
1083	1	14-30	14-30	-00	-00	1083	.00	.00
1085	1	14-30	14-30	-00	-00	1085	.00	.00
1086	1	14-30	14-30	-00	-00	1086	.00	.00
1087	1	14-30	14-30	-00	-00	1087	.00	.00
1088	1	14-30	14-30	-00	-00	1088	.00	.00
1089	1	7-45	7-45	-00	-00	1089	.00	.00
1090	1	14-30	14-30	-00	-00	1090	.00	.00
1094	1	7-45	7-45	-00	-00	1094	.00	.00
1095	1	14-30	14-30	-00	-00	1095	.00	.00
1096	1	14-30	14-30	-00	-00	1096	.00	.00
1099	1	14-30	14-30	-00	-00	1099	.00	.00
1100	1	14-30	14-30	-00	-00	1100	.00	.00
1104	1	14-30	14-30	-00	-00	1104	.00	.00
1106	1	14-30	14-30	-00	-00	1106	.00	.00
1109	1	14-30	14-30	-00	-00	1109	.00	.00
1118	1	14-30	14-30	-00	-00	1118	.00	.00
1119	1	14-30	14-30	-00	-00	1119	.00	.00
1122	1	7-45	7-45	-00	-00	1122	.00	.00
1123	1	7-45	7-45	-00	-00	1123	.00	.00
1126	1	14-30	14-30	-00	-00	1126	.00	.00

1264	1	9.47	9.47	.00	9.47	9.47	.00	15.00	1100	15.24	.00	1264
1265	1	2.05	2.05	.00	2.05	2.05	.00	15.00	16600	3.30	.00	1265
1270	1	2.05	2.05	.00	2.05	2.05	.00	15.00	1400	3.30	.00	1270
1273	1	4.40	4.40	.00	4.40	4.40	.00	15.00	0000	3.30	.00	1273
1277	1	.00	.00	.00	.00	.00	.00	15.00	0700	7.07	.00	1277
1282	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0200	.00	.00	1277
1286	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0200	.00	.00	1282
1289	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0700	.00	.00	1286
1292	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0200	.00	.00	1289
1293	1	4.63	4.63	.00	4.63	4.63	.00	30.00	0600	.00	.00	1292
1294	1	7.45	7.45	.00	7.45	7.45	.00	30.00	0400	7.45	.00	1293
1295	1	7.45	7.45	.00	7.45	7.45	.00	30.00	0600	11.99	.00	1294
1298	1	14.30	14.30	.00	14.30	14.30	.00	30.00	0600	11.99	.00	1295
1299	1	14.30	14.30	.00	14.30	14.30	.00	30.00	0500	23.01	.00	1298
1308	1	14.30	14.30	.00	14.30	14.30	.00	30.00	1400	23.01	.00	1299
1311	1	4.63	4.63	.00	4.63	4.63	.00	30.00	2100	23.01	.00	1308
1317	1	14.30	14.30	.00	14.30	14.30	.00	30.00	0100	7.45	.00	1317
1318	1	12.65	12.65	.00	12.65	12.65	.00	30.00	0200	23.01	.00	1317
1320	1	14.30	14.30	.00	14.30	14.30	.00	30.00	0600	20.36	.00	1318
1321	1	14.30	14.30	.00	14.30	14.30	.00	30.00	0300	23.01	.00	1320
1326	1	14.30	14.30	.00	14.30	14.30	.00	30.00	0700	23.01	.00	1321
1330	1	2.05	2.05	.00	2.05	2.05	.00	30.00	2800	23.01	.00	1326
1333	1	14.30	14.30	.00	14.30	14.30	.00	30.00	4700	3.30	.00	1330
1337	1	4.63	4.63	.00	4.63	4.63	.00	30.00	0700	23.01	.00	1333
1338	1	.00	.00	.00	.00	.00	.00	30.00	0500	7.45	.00	1337
1354	1	4.63	4.63	.00	4.63	4.63	.00	30.00	0200	.00	.00	1338
1355	1	.00	.00	.00	.00	.00	.00	50.00	0100	7.45	.00	1354
1360	1	4.63	4.63	.00	4.63	4.63	.00	65.00	0700	.00	.00	1355
1361	1	4.63	4.63	.00	4.63	4.63	.00	15.00	0500	7.45	.00	1360
1364	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0100	7.45	.00	1361
1365	1	2.05	2.05	.00	2.05	2.05	.00	15.00	1200	23.01	.00	1364
1368	1	14.30	14.30	.00	14.30	14.30	.00	15.00	1400	3.30	.00	1365
1369	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0900	23.01	.00	1368
1370	1	14.30	14.30	.00	14.30	14.30	.00	15.00	1100	23.01	.00	1369
1372	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0200	23.01	.00	1370
1375	1	14.30	14.30	.00	14.30	14.30	.00	15.00	1200	23.01	.00	1372
1376	1	2.05	2.05	.00	2.05	2.05	.00	15.00	1600	23.01	.00	1375
1377	1	14.30	14.30	.00	14.30	14.30	.00	15.00	1000	3.30	.00	1376
1380	1	14.30	14.30	.00	14.30	14.30	.00	15.00	2500	23.01	.00	1380
1382	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0100	23.01	.00	1387
1384	1	14.30	14.30	.00	14.30	14.30	.00	15.00	1100	23.01	.00	1382
1386	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0000	23.01	.00	1384
1387	1	2.05	2.05	.00	2.05	2.05	.00	15.00	3300	23.01	.00	1386
1388	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0200	3.30	.00	1387
1392	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0300	23.01	.00	1388
1394	1	14.30	14.30	.00	14.30	14.30	.00	15.00	1100	23.01	.00	1392
1396	1	14.30	14.30	.00	14.30	14.30	.00	15.00	0200	23.01	.00	1395
1397	1	2.05	2.05	.00	2.05	2.05	.00	15.00	1600	23.01	.00	1396
								15.00	3.30	3.30	.00	1397

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785	00	1
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787	00	1
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795	00	1
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797	00	1
798	00	1
799	00	1
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13. ABSTRACT

The Directorate of Land Requirements (DLR), in an effort to assess the usefulness of the NATO Reference Mobility Model (NRMM) in vehicle procurement activities, initiated a study at the Defence Research Establishment Suffield with the following objectives: 1) to determine the difficulty and time required to provide all necessary NRMM input data for a typical wheeled vehicle; 2) to determine the time required to perform an NRMM evaluation; and 3) to establish a wheeled vehicle baseline. The vehicle chosen for this study was the Iltis 4X4 $\frac{1}{2}$ ton truck. All required vehicle characteristics were obtained within an acceptable time frame with the exception of the pitch-mass-moment of inertia of the sprung mass, which eventually was measured at an American laboratory. The NRMM simulation of the Iltis 4X4 required approximately one month to complete. The baseline performance is represented by curves of speed versus cumulative percent of area and by a mobility rating speed of 40 kilometers per hour over representative German terrain.

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